

Standard results and Code based results or how the ubiquitous codes set a hierarchy of methods

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December 2017

Outline

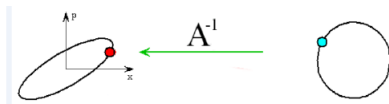
- 1 Foreword
- 2 One-degree-of-freedom Courant-Snyder theory
- 3 One-degree-of-freedom Courant-Snyder in a Code
- 4 Generality of the Twiss Loop
- 5 Why is the code so general?

What is the purpose of this lecture

- Courant-Snyder theory, if presented in a correct framework, is a very general theory
 - linear motion
 - coupled motion
 - nonlinear motion
 - magnet modulation
 - linear/nonlinear phase slip
 - one-resonance theory
 - system with radiation
 - all the above with spin
 - etc. . .
- This theory elevates the tracking code on a pedestal because it is closest to the real machine
- it uses only things available to the code
- It assumes that the tracking code can produce approximate Taylor maps
- It is a primarily geometrical theory based on the orbits produced by the code
- It is a highly hierarchical theory well suited to modern computers and thus easily understandable
- It can make the connection with the world of analytical perturbation theory shown in text books
 - Formulae based on delta-function expansion perturbations of the ring, for example, $d\nu = \frac{1}{4\pi} \beta k ds$
 - Formulae based on a Fourier-expansion of a perturbation around the ring such as Guignard's theory

Why a Courant-Snyder theory?

From geometry



From equation of motion

$$x(s) = \sqrt{2\beta_s J} \cos\left(\int_0^s \frac{1}{\beta_s} ds + \phi_0\right)$$

For example we can answer the question: what is $\langle x^2 \rangle$ for a distribution of particles or a single particle (time average).

The advantage of the geometrical description will be its enormous generality. If we know A^{-1} , say from a tracking code, we are done.

Textbook results of Courant-Snyder Theory

What is really behind it?

The following results are derived using ODE theory in many textbooks: S.Y. Lee, H. Wiedemann, etc... They are really a parameterization.

- Equation of motion in the simplest case

$$\ddot{x} + k(s)x = 0 \quad (1)$$

- Assuming $k(s + C) = k(s)$ and periodicity
- The Courant-Snyder “solution” emerges

$$x(s) = \sqrt{2\beta_s J} \cos \left(\int_0^s \frac{1}{\beta_s} ds + \phi_0 \right) \quad (2)$$

β_s is a periodic function ($\beta_{s+C} = \beta_s$) and J is a constant.

Why it is not a “solution”

It is a parameterization

The standard result is really a parameterization

- a parametrisation assuming stability

$$|x(s)| \leq \sqrt{2\beta_{max}J} \quad (3)$$

- Indeed if $k = 0$, it is not stable. The solution has a different form

$$x(s) = x_0 + sx'_0 \quad (4)$$

- And if $k < 0$ and constant, it is exponentially unstable, and it has also a different form

$$x(s) = A \cosh ks + B \sinh ks \quad (5)$$

- Therefore Eq. (2) can represent **only** the stable linear motion of an accelerator in 1-d-f.

Problems with generalisation

- This analytical parametrisation assumes a simple analytical form : $\ddot{x} + k(s)x = 0$
- Can we use that easily in a code?
- Can it be **easily** generalised to coupled systems, to non-linear systems or to spin for example?

The answer to these questions is “**no**”.

Most importantly, it is not easy to implement generally in a code. But there exists an approach which is easy to put in a code **no matter how complicated and discontinuous** the equations of motion are!

Goal of the slides that will follow

Sorry for the crowded transparency

Basic goal is to derive Eq. (2): $x(s) = \sqrt{2\beta_s J} \cos\left(\int_0^s \frac{1}{\beta_s} ds + \phi_0\right)$

- 1 Parameterize the motion using finite maps (matrices in this case)
- 2 Introduce the assumption of stability and area preservation (Hamiltonian flow)
- 3 “normalise the map”, i.e., exploit stability
- 4 Consider the existence of two points of observation in a ring
- 5 Use an infinite number of points, i.e., Eq. (1): $\ddot{x} + k(s)x = 0$
- 6 Then using item 5, derive Eq. (2)

Finally we must convince ourselves that this is the only reasonable starting point for the more general theory (coupling, non-linear, spin, etc....) which is faithful to a code. That takes a bit of thought and work.

Examine first the one-turn map

Symplectic=Hamiltonian

One-turn map at $s = 0$ computed from the code:

$$\begin{pmatrix} x(C) \\ p(C) \end{pmatrix} = \underbrace{\begin{pmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{pmatrix}}_M \begin{pmatrix} x(0) \\ p(0) \end{pmatrix} \quad \text{where } p = x' \quad (6)$$

The Hamiltonian nature of the flow implies, in the linear 1-d-f case, that

$$\det \begin{pmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{pmatrix} = |M| = M_{11}M_{22} - M_{12}M_{21} = 1 \quad (7)$$

Go back to stability

Examine first the one-turn map

$$\det(M - \lambda I) = 0 \quad , \quad \det(M) = 1 \quad \text{and stability} \quad \Rightarrow \quad \left| \frac{1}{2} \text{Tr}(M) \right| < 1$$

\Downarrow

$$\lambda = \exp(\pm i\mu) = \cos(\mu) \pm i \sin(\mu) \quad \text{where} \quad \cos(\mu) = \frac{1}{2} \text{Tr}(M)$$

Normalisation

We look for

$$M = \begin{pmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{pmatrix} \begin{pmatrix} \cos(\mu) & \sin(\mu) \\ -\sin(\mu) & \cos(\mu) \end{pmatrix} \begin{pmatrix} A_{22} & -A_{12} \\ -A_{21} & A_{11} \end{pmatrix}$$

where $\det(A) = 1$.

This insures, in 1-d-f, that the map A is Hamiltonian and the invariant J is indeed invariant. $2\pi J$ is the area circumscribed by the trajectory and it is preserved if A is area preserving.

The preservation of J is also true for nonlinear multidimensional maps if the map A is a nonlinear symplectic transformation

Choice for A

Notice that if

$$M = ARA^{-1}$$



$$M = ArRr^{-1}A^{-1}$$

The rotation r commutes with R and can be chosen such that

$$Ar \implies \begin{pmatrix} A_{11} & 0 \\ A_{21} & A_{11}^{-1} \end{pmatrix}$$

Result for A

Invariant

$$A_{11} = \left| \frac{M_{12}}{\sin(\mu)} \right|^{1/2} \quad A_{21} = \frac{(M_{21}A_{11} + \sin(\mu)A_{11}^{-1})}{\cos(\mu) - M_{22}}$$

We can compute an invariant using A^{-1} :

$$\varepsilon = 2J = \underbrace{(A_{11}^{-2} + A_{21}^2)}_{\gamma} x^2 + 2 \underbrace{(-A_{21}A_{11})}_{\alpha} xp + \underbrace{A_{11}^2}_{\beta} p^2 \quad (8)$$

We will see that ε is indeed $2J$ of Eq. (2)

Writing M in terms of A

Invariant

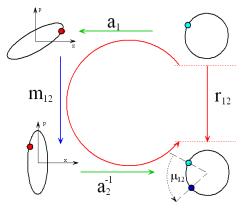
$$\begin{aligned}
 M &= \begin{pmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{pmatrix} \begin{pmatrix} \cos(\mu) & \sin(\mu) \\ -\sin(\mu) & \cos(\mu) \end{pmatrix} \begin{pmatrix} A_{22} & -A_{12} \\ -A_{21} & A_{11} \end{pmatrix} \\
 &= \begin{pmatrix} \cos(\mu) - (A_{11}A_{21} + A_{12}A_{22}) \sin(\mu) & (A_{11}^2 + A_{12}^2) \sin(\mu) \\ - (A_{22}^2 + A_{21}^2) \sin(\mu) & \cos(\mu) + (A_{11}A_{21} + A_{12}A_{22}) \sin(\mu) \end{pmatrix} \\
 &= \begin{pmatrix} \cos(\mu) + \alpha \sin(\mu) & \beta \sin(\mu) \\ -\gamma \sin(\mu) & \cos(\mu) - \alpha \sin(\mu) \end{pmatrix} \tag{9}
 \end{aligned}$$

Notice that $1 + \alpha^2 = \beta\gamma$ because $\det(A) = 1$

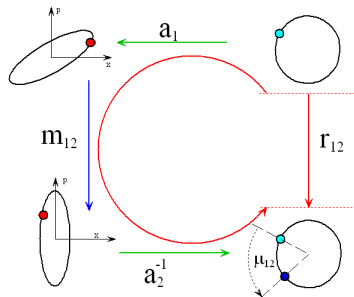
More than one point of observation in the ring

- Eq. (2), i.e., $x(s) = \sqrt{2\beta_s J} \cos\left(\int_0^s \frac{1}{\beta_s} ds + \phi_0\right)$, assumes more than one location
- in fact an infinite number since s is a continuous variable: **It cannot be compatible with a tracking code**
- So we first derive Eq. (2) for two locations: 1 location is a trivial degenerate case

We reduce Eq. (2) to a diagram



Phase advance diagram



- 1 Assume m_{12} , a_1 and a_2 are area preserving
- 2 a_1 and a_2 turn the one-turn maps m_1 and m_2 into rotations
- 3 Then r_{12} must be a rotation if a_1 and a_2 are area preserving (symplectic in general)
- 4 In what follows we assume that they are linear maps

Here we go....

$$M_1 = A_1 R A_1^{-1} \quad M_2 = A_2 R A_2^{-1}$$

$$\Downarrow$$

$$M_{12} = A_2 R_{12} A_1^{-1} \quad \leftarrow \text{Using phase advance figure}$$

$$A_k = \begin{pmatrix} \sqrt{\beta_k} & 0 \\ -\alpha_k/\sqrt{\beta_k} & 1/\sqrt{\beta_k} \end{pmatrix} \quad k = 1, 2$$

$$M_{12} = \begin{pmatrix} \cos(\mu_{12}) & \sin(\mu_{12}) \\ -\sin(\mu_{12}) & \cos(\mu_{12}) \end{pmatrix}$$

- Notice that μ_{12} depends on the choice for A_k and also depends on M_{12} .
- In a code, we cannot say much more.
- But to compare to Eq. (2), we compute x_2 in terms of x_1 .

x_2 in terms of x_1

$$x_2 = \underbrace{\sqrt{\beta_2} \left\{ \frac{1}{\sqrt{\beta_1}} x_1 \right\}}_E \cos(\mu_{12}) + \underbrace{\sqrt{\beta_2} \left\{ \frac{\alpha_1}{\sqrt{\beta_1}} x_1 + \sqrt{\beta_1} p_1 \right\}}_F \sin(\mu_{12})$$

$$x_2 = \sqrt{\beta_2 (E^2 + F^2)} \cos(\mu_{12} + \phi_1) \quad (10)$$

Bonus result p_2 :

$$p_2 = -\frac{1}{\sqrt{\beta_2}} \sqrt{(E^2 + F^2)} \{ \alpha_2 \cos(\mu_{12} + \phi_1) + \sin(\mu_{12} + \phi_1) \}$$

$$\varepsilon_1 = E^2 + F^2 = 2J_1 = \gamma_1 x_1^2 + 2\alpha_1 x_1 p_1 + \beta_1 p_1^2 \quad (11)$$

$$\text{where } \cos(\phi_1) = \frac{E}{\sqrt{E^2 + F^2}} \quad \text{and} \quad \sin(\phi_1) = -\frac{F}{\sqrt{E^2 + F^2}}$$

What if $\ddot{x} + k(s)x = 0$?

Continuous case

- Eqs. (10) and (11) are correct for any 1-d-f system and therefore applicable to any code
- μ_{12} in a code depends on details unavailable to the usual user: fringe fields, misalignments, bizarre magnets, etc. . .
- Therefore $\mu_{12} = \int_{s_1}^{s_2} \frac{ds}{\beta(s)}$ is valid for our choice of A_s for the underlying equation $\ddot{x} + k(s)x = 0$

Let us derive $\mu_{12} = \int_{s_1}^{s_2} \frac{ds}{\beta(s)}$ by assuming that position 1 and 2 are separated by an infinitesimal length of ds

Phase advance using maps

Continuous case

$$M_{12} = A_2 R_{12} A_1^{-1} \implies M_{12} A_1 R_{12}^{-1} = A_2$$

$$\Downarrow$$

$$M_{12} = \begin{pmatrix} 1 & ds \\ -kds & 1 \end{pmatrix} \quad A_1 = \begin{pmatrix} \sqrt{\beta_s} & 0 \\ -\alpha_s/\sqrt{\beta_s} & 1/\sqrt{\beta_s} \end{pmatrix} \quad R_{12}^{-1} = \begin{pmatrix} 1 & -d\mu \\ d\mu & 1 \end{pmatrix}$$

$$\Downarrow$$

$$A_2 = \begin{pmatrix} \sqrt{\beta_s} - ds \alpha_s/\sqrt{\beta_s} & -d\mu\sqrt{\beta_s} + ds/\sqrt{\beta_s} \\ -\alpha_s/\sqrt{\beta_s} + ds/\beta_s^{3/2} - k\sqrt{\beta_s}ds & 1/\sqrt{\beta_s} + ds \alpha_s/\beta_s^{3/2} \end{pmatrix} + O(ds, d\mu)^2$$

Our choice for A_2 requires that the $A_{2;12}$ be zero:

$$-d\mu\sqrt{\beta_s} + ds/\sqrt{\beta_s} = 0 \implies \frac{d\mu}{ds} = \frac{1}{\beta_s} \implies \mu_{12} = \int_{s_1}^{s_2} \frac{ds}{\beta_s}$$

Q.E.D.

Time evolution of lattice functions

Corollary

- $A_{11} = \sqrt{\beta_s} - ds \alpha_s / \sqrt{\beta_s}$

$$\implies \frac{d\beta_s}{ds} = -2\alpha_s$$

- $A_{21} = -\alpha_s / \sqrt{\beta_s} + ds / \beta_s^{3/2} - k\sqrt{\beta_s} ds$

$$\implies \frac{d\alpha_s}{ds} = \frac{1}{2} \frac{\alpha_s}{\beta_s} \frac{d\beta_s}{ds} + k\beta_s - \frac{1}{\beta_s} = k\beta_s - \gamma_s$$

- Finally,

$$\frac{d\gamma_s}{ds} = 2\alpha_s k$$

Hamiltonian in our example code

The following Hamiltonian is implemented in our small code and in PTC:

$$H = \frac{p^2}{2(1+\delta)} (1 + e_1 k_q) + b_0 \left(x + h \frac{x^2}{2} \right) - hx(1+\delta) + \frac{k_q}{2} x^2 + \frac{k_o}{4} x^4 \quad (12)$$

- 1 e_1 is added to show later that a code based theory is impervious to “false” physics
- 2 δ is the momentum deviation from the design momentum k_q and k_o are the quadrupole and octupole strength respectively
- 3 The Hamiltonian of Eq. (12) with $e_1 = 0$ represents motion in the small angle approximation in the presence of a quadrupole-octupole system.

The Courant-Snyder small angle Hamiltonian

$$H = \frac{p^2}{2(1+\delta)} (1 + e_1 k_q) + b_0 \left(x + h \frac{x^2}{2} \right) - hx(1+\delta) + \frac{k_q}{2} x^2 + \frac{k_o}{4} x^4 \quad (13)$$

$$\frac{dx}{ds} = \frac{(1 + e_1 k_q)}{(1 + \delta)} p \quad (14)$$

$$\frac{dp}{ds} = -b_0(1 + hx) + h(1 + \delta) - k_q x - k_o x^3 \quad (15)$$

↓

$$\ddot{x} + \frac{(1 + e_1 k_q) k_q}{1 + \delta} x = \frac{(1 + e_1 k_q) k_o}{1 + \delta} \left(-b_0(1 + hx) + h(1 + \delta) - k_o x^3 \right)$$

We now switch from our small code to PTC

Using the polymorph `real_8`

Code for the Taylor series in PTC

Using the polymorph real_8

Second order Symplectic Integrator Drift-Kick-Drift type

```

CASE (2)
  DH=EL%L/2.0_dp/EL%P%NST
  D=EL%L/EL%P%NST
  DD=EL%P%LD/2.0_dp/EL%P%NST

  CALL DRIFT (DH,DD,EL%P%beta0,k%TOTALPATH,EL%P%EXACT,k%TIME,X)
  if (e1_cas/=0.and.el%p%nmul>1) then
    X(1)=X(1)+DH*X(2)/SQRT(1.0_dp+2.0_dp*X(5)/EL%P%beta0+x(5)**2)*e1_cas*el%bn(2)
  endif
  CALL KICK (EL,D,X,k)
  CALL DRIFT (DH,DD,EL%P%beta0,k%TOTALPATH,EL%P%EXACT,k%TIME,X)
  if (e1_cas/=0.and.el%p%nmul>1) then
    X(1)=X(1)+DH*X(2)/SQRT(1.0_dp+2.0_dp*X(5)/EL%P%beta0+x(5)**2)*e1_cas*el%bn(2)
  endif

```

real(dp) —> real_8 where **dp=8**

What can the code do?

- 1 You can view the code as a black box function giving you a propagator from point i to $i + 1$
- 2 i can denote any “Poincaré” surface of section in the lattice including the integration steps
- 3 The propagator propagates phase space (x, p_x, \dots) , spin, etc. . .
- 4 Through the magic of polymorphism, that code can propagate Taylor series
- 5 If you can propagate Taylor series, then you can propagate approximates maps such as linear maps, i.e., matrices

How to treat a library analysing Taylor maps

Normal form library

- 1 It will have normal formal form procedures
 - 1 *For linear maps*
 - 2 *nonlinear maps*
 - 3 *radiative maps*
 - 4 *spin motion*
 - 5 *etc. . .*
- 2 It will manipulate maps into different forms
 - 1 *Taylor series representations (so-called matrices)*
 - 2 *Lie representation*
 - 3 *Generating functions for Hamiltonian maps*
 - 4 *Various useful factored representations*
 - 5 *etc. . .*
- 3 Maps, computed by the code, manipulated into a normal form, are reinserted in the code: the Twiss algorithm
 - 1 *Propagates lattice functions, i.e., the results of the normal form*
 - 2 *Computes the phase advance if wanted*
 - 3 *The above things for linear, nonlinear, spin, etc. . .*

The Phase Advance Diagram

Complete loop

```

r=a_cs+r0
f->ring%start
do i=1,ring%n
call propagate(ring,r,state,fibre1=i,fibre2=i+1)

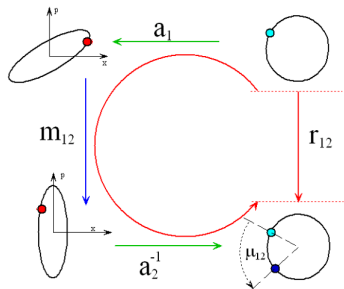
a_cs=r
call c_full_canonise(a_cs,a_cs,a_spin, &
disp,A_L,A_NL,phase=phase,nu_spin=phase_spin)

r0=r
r=a_cs+r0

!!!!!!!!!!!!!! Do something !!!!!!!!!!!!!!!

!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!

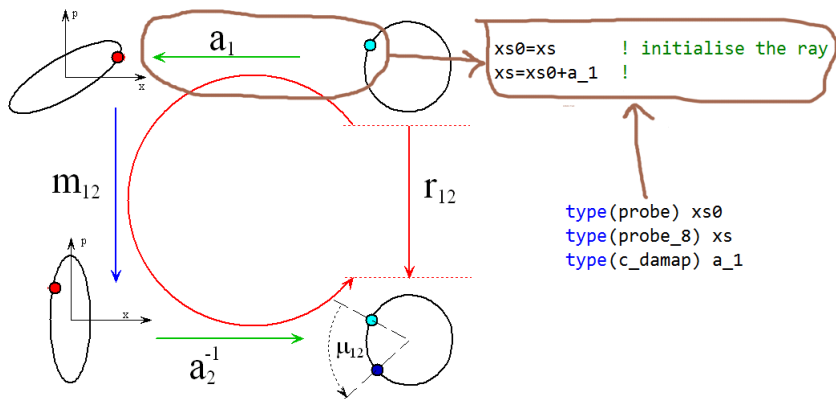
```



`c_full_canonise` can be replaced by `c_fast_canonise` in a linear calculation without system parameters.

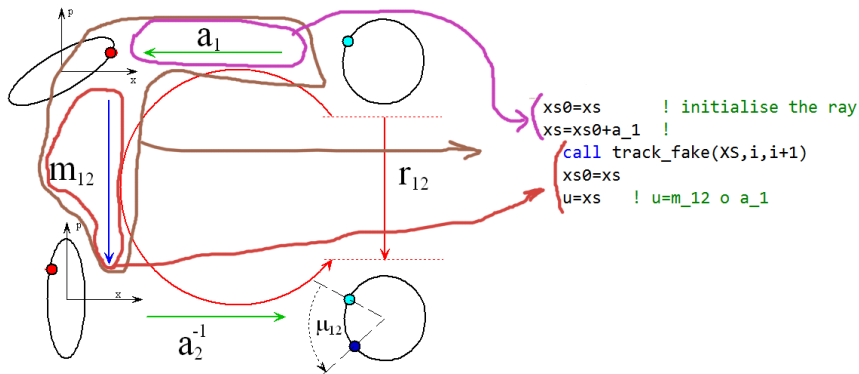
From the Advance Diagram

Initializing with a_1



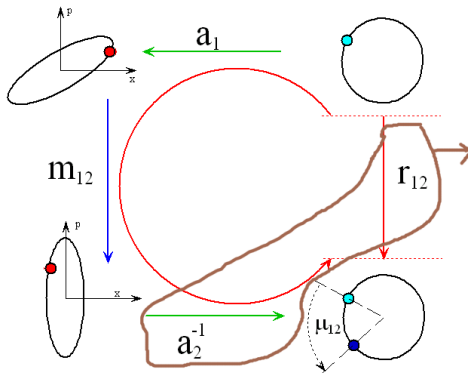
From to the Advance Diagram

Tracking : computing m_{12}



From to the Advance Diagram

Finding a_2 and r_{12}



```

u=xs      ! u=m_12 o a_1
! u = a_2 o r_12(phase)
call c_full_canonise(u,a_2,phase=phase)

```

$$a_2 = \begin{pmatrix} \sqrt{\beta_2} & 0 \\ -\frac{\alpha_2}{\sqrt{\beta_2}} & \frac{1}{\sqrt{\beta_2}} \end{pmatrix}$$

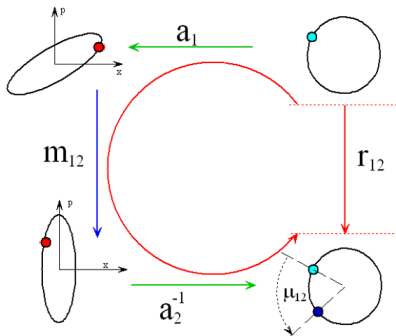
The Phase Advance Diagram

Complete loop

```

r=a_cs+rθ
f=>ring%start
do i=1,ring%n
call propagate(ring,r,state,fibre1=i,fibre2=i+1)
a_cs=r
call c_full_canonise(a_cs,a_cs,a_spin, &
disp,A_L,A_NL,phase=phase,nu_spin=phase_spin)
rθ=r
r=a_cs+rθ
!!!!!!!!!!!!!! Do something !!!!!!!!!!!!!!!
!!!!!!!!!!!!!!

```



Same Twiss Loop from the Code “PTC”

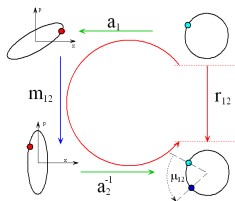
A basic Twiss loop

$$xs = xs0 + a_{-1} \quad \leftarrow A_1 = \begin{pmatrix} \sqrt{\beta_{x;1}} & 0 \\ -\alpha_{x;1}/\sqrt{\beta_{x;1}} & 1/\sqrt{\beta_{x;1}} \end{pmatrix} \quad k = 1, 2$$

```
do i=1,ring%n
```

```
call propagate(ring,xs,state,fibre1=i,fibre2=i+1)  $\leftarrow$  This is the  $m_{12} \circ a_1$  of the figure
```

```
!!!!!!!!!!!!!!!!!!!! doing something !!!!!!!!!!!!!!!!!!!!!
```



```
!!!!!!!!!!!!!!!!!!!! end of doing something !!!!!!!!!!!!!!!!!!!!!
```

```
enddo
```

What am I trying to convey?

- The difference between my approach and the standard approach is epistemological in nature
- It is about conceptual knowledge and its organisation
- What does it mean to “understand” something?
- Understand entails a hierarchical organisation of physics concepts
- The more the knowledge is hierarchical, the greater our comprehension
- This makes it easier to perform traditional calculations as well:
 - Analytic formulae such

$$\frac{\partial \langle \tilde{x} \rangle}{\partial J} = \frac{\beta_s^{1/2}}{2(1 - \cos(\mu))} \oint_0^C (-\sin(\mu_{S\sigma}) + \sin(\mu_{S\sigma} - \mu)) \beta_\sigma^{3/2} k_S(\sigma) d\sigma$$

- Guignard-Deprit calculation using a mode decomposition in the variable around the ring (s or $\theta(s)$)

We can choose the appropriate methods not on the basis of our taste but on the basis of real understanding

(taste = wimpy euphemism for our incompetence or ignorance)

Example of non-hierarchical knowledge

- 1 Newton laws seem to predict accurately the motion of planets (Concept)
- 2 Mercury's orbit cannot be accounted
- 3 We conclude the following
 - 1 Some invisible planet must be present in the inner solar system (Newton Laws unchanged)
 - 2 Some other force must exist which acts on Mercury (Newton Laws complemented)
 - 3 Newton's Laws are not completely correct (Newton Laws superseded by a better set)

In the absence of evidence, Mercury's orbit is a perception of reality which is not derivable from Newton's Laws. It stands alone and it is not part of any hierarchy.

Therefore I say : we do not understand why Mercury's orbit precesses

Here comes Einstein!

Knowledge is now hierarchical

- 1 Einstein's laws seem to predict accurately the motion of planets (Concept)
- 2 Mercury's orbit can be accounted from Einstein's General Relativity
- 3 So the motion of Mercury is not part of a new concept which must be learnt separately

Now we have a hierarchy. Newton's Law is a consequence of Einstein GR which accounts for Mercury's orbit. We now understand.

Now, I go back to the Twiss loop accessible to the code.

Same Twiss Loop from the Code “PTC”

Apparently unrelated things computed in a basic Twiss loop

```
xs=xs0+a_1
```

```
do i=1,ring%n
```

```
call propagate(ring,xs,state,fibre1=i,fibre2=i+1)
```

```
!!!!!!!!!!!!!!!!!!!! doing something !!!!!!!!!!!!!!!!!!!!!
```

```
!!!!!!!!!!!!!!!!!!!! end of doing something !!!!!!!!!!!!!!!!!!!!!
```

Same Twiss Loop from the Code “PTC”

Apparently unrelated things computed in a basic Twiss loop

$$xs = xs_0 + a_1 \quad \leftarrow A_1 = \begin{pmatrix} \sqrt{\beta_{x;1}} & 0 \\ -\alpha_{x;1}/\sqrt{\beta_{x;1}} & 1/\sqrt{\beta_{x;1}} \end{pmatrix} \quad k = 1, 2$$

```
do i=1,ring%n
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call propagate(ring,xs,state,fibre1=i,fibre2=i+1)
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```
do i=1,ring%n
```

```
call propagate(ring,xs,state,fibre1=i,fibre2=i+1)
```

```
!!!!!!!!!!!!!!!!!!!!!! doing something !!!!!!!!!!!!!!!!!!!!!!!
```

```
! Computation of beta function defined as  $\partial \langle x^2 \rangle / \partial J \Rightarrow A_{11}^2 + A_{12}^2$ 
```

```
!!!!!!!!!!!!!!!!!!!!!! end of doing something !!!!!!!!!!!!!!!!!!!!!!!
```

Same Twiss Loop from the Code “PTC”

Apparently unrelated things computed in a basic Twiss loop

$$xs = xs_0 + a_1 \quad \leftarrow A_1 = \begin{pmatrix} \sqrt{\beta_{x;1}} & 0 \\ -\alpha_{x;1}/\sqrt{\beta_{x;1}} & 1/\sqrt{\beta_{x;1}} \end{pmatrix} \quad k = 1, 2$$

```
do i=1,ring%n
```

```
call propagate(ring,xs,state,fibre1=i,fibre2=i+1)
```

```
!!!!!!!!!!!!!!!!!!!!!! doing something !!!!!!!!!!!!!!!!!!!!!!!
```

```
! Computation of beta function defined as  $\partial \langle x^2 \rangle / \partial J \Rightarrow A_{11}^2 + A_{12}^2$ 
```

```
  a_1=xs
```

```
  betax_1=(a_1%v(1).index.1)**2+(a_1%v(1).index.2)**2
```

```
!!!!!!!!!!!!!!!!!!!!!! end of doing something !!!!!!!!!!!!!!!!!!!!!!!
```


Same Twiss Loop from the Code “PTC”

Apparently unrelated things computed in a basic Twiss loop

$$xs = xs_0 + a_1 \quad \leftarrow A_1 = \begin{pmatrix} \sqrt{\beta_{x;1}} & 0 \\ -\alpha_{x;1}/\sqrt{\beta_{x;1}} & 1/\sqrt{\beta_{x;1}} \end{pmatrix} \quad k = 1, 2$$

```
do i=1,ring%n
```

```
call propagate(ring,xs,state,fibre1=i,fibre2=i+1)
```

```
!!!!!!!!!!!!!!!!!!!!!! doing something !!!!!!!!!!!!!!!!!!!!!!!
```

```
! Computation of beta function defined as  $\partial \langle x^2 \rangle / \partial J \Rightarrow A_{11}^2 + A_{12}^2$ 
```

```
  a_1=xs
```

```
  betax_1=(a_1%v(1).index.1)**2+(a_1%v(1).index.2)**2
```

```
! Modulating the strength of magnet (a bend here) : useful in spin experiments I am told by the experts
```

```
 $\partial \langle x^2 \rangle / \partial J_m \Rightarrow A_{15}^2 + A_{16}^2$ 
```

```
!!!!!!!!!!!!!!!!!!!!!! end of doing something !!!!!!!!!!!!!!!!!!!!!!!
```

Same Twiss Loop from the Code “PTC”

Apparently unrelated things computed in a basic Twiss loop

$$xs = xs0 + a_1 \quad \leftarrow A_1 = \begin{pmatrix} \sqrt{\beta_{x;1}} & 0 \\ -\alpha_{x;1}/\sqrt{\beta_{x;1}} & 1/\sqrt{\beta_{x;1}} \end{pmatrix} \quad k = 1, 2$$

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 $\partial \langle x^2 \rangle / \partial J_m \Rightarrow A_{15}^2 + A_{16}^2$ 
```

```
  betax_m=(a_1%v(1).index.5)**2+(a_1%v(1).index.6)**2
```

```
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  betax_m=(a_1%v(1).index.5)**2+(a_1%v(1).index.6)**2
```

```
! Computation of invariant spin field  $\vec{n}$  and  $\partial n / \partial p_y$ 
```

```
! Stuff needed in lattice design with spin and in the Derbenev-Kondratenko formula
```

```
!!!!!!!!!!!!!!!!!!!!!! end of doing something !!!!!!!!!!!!!!!!!!!!!!!
```

Same Twiss Loop from the Code “PTC”

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$$xs=xs0+a_1 \quad \leftarrow A_1 = \begin{pmatrix} \sqrt{\beta_{x;1}} & 0 \\ -\alpha_{x;1}/\sqrt{\beta_{x;1}} & 1/\sqrt{\beta_{x;1}} \end{pmatrix} \quad k = 1, 2$$

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```
! Computation of invariant spin field  $\vec{n}$  and  $\partial n / \partial p_y$ 
```

```
! Stuff needed in lattice design with spin and in the Derbenev-Kondratenko formula
```

```
  a_1%S=a_1%S*a_1**(-1)
```

```
  isf=a_1%S*e_y
```

```
  dnx_dpy=isf%v(1).index.4
```

```
!!!!!!!!!!!!!!!!!!!!!! end of doing something !!!!!!!!!!!!!!!!!!!!!!!
```

Same Twiss Loop from the Code “PTC”

Apparently unrelated things computed in a basic Twiss loop

$$xs = xs0 + a_1 \quad \leftarrow A_1 = \begin{pmatrix} \sqrt{\beta_{x;1}} & 0 \\ -\alpha_{x;1}/\sqrt{\beta_{x;1}} & 1/\sqrt{\beta_{x;1}} \end{pmatrix} \quad k = 1, 2$$

```
do i=1,ring%n
```

```
call propagate ring xs state file rel i like 2 r1 1
```

What about MAD?

```
!!!!!!!!!!!!!!!!!!!!!! doing something !!!!!!!!!!!!!!!!!!!!!!!
```

! Computation of beta function defined as $\partial \langle x^2 \rangle / \partial J \Rightarrow A_{11}^2 + A_{12}^2$

```
a_1=xs
```

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betax_1=(a_1%v(1).index.1)**2+(a_1%v(1).index.2)**2
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$\partial \langle x^2 \rangle / \partial J_m \Rightarrow A_{15}^2 + A_{16}^2$

```
betax_m=(a_1%v(1).index.5)**2+(a_1%v(1).index.6)**2
```

! Computation of invariant spin field \vec{n} and $\partial n / \partial p_y$

! Stuff needed in lattice design with spin and in the Derbenev-Kondratenko formula

```
a_1%s=a_1%s*a_1**(-1)
```

```
isf=a_1%s*e_y
```

```
dnx_dpy=isf%v(1).index.4
```

```
!!!!!!!!!!!!!!!!!!!!!! end of doing something !!!!!!!!!!!!!!!!!!!!!!!
```

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$$xs = xs0 + a_1 \quad \leftarrow A_1 = \begin{pmatrix} \sqrt{\beta_{x;1}} & 0 \\ -\alpha_{x;1}/\sqrt{\beta_{x;1}} & 1/\sqrt{\beta_{x;1}} \end{pmatrix} \quad k = 1, 2$$

```
do i=1,ring%n
```

```
call propagate(my_ring,A_script_probe,default,node1=nodePtr%pos,node2=nodePtr%pos+1)
```

What about MAD?

```
!!!!!!!!!!!!!!!!!!!!!! doing something !!!!!!!!!!!!!!!!!!!!!!!
```

! Computation of beta function defined as $\partial \langle x^2 \rangle / \partial J \Rightarrow A_{11}^2 + A_{12}^2$

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$\partial \langle x^2 \rangle / \partial J_m \Rightarrow A_{15}^2 + A_{16}^2$

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betax_m=(a_1%v(1).index.5)**2+(a_1%v(1).index.6)**2
```

! Computation of invariant spin field \vec{n} and $\partial n / \partial p_y$

! Stuff needed in lattice design with spin and in the Derbenev-Kondratenko formula

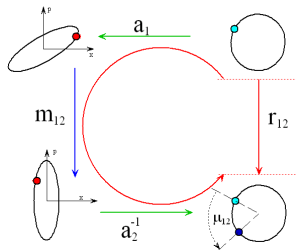
```
a_1%S=a_1%S*a_1**(-1)
```

```
isf=a_1%S*e_y
```

```
dnx_dpy=isf%v(1).index.4
```

```
!!!!!!!!!!!!!!!!!!!!!! end of doing something !!!!!!!!!!!!!!!!!!!!!!!
```

The linear 1-d-f case



What can we notice from the above graph?

- The phase space plots are turned into circles
- The circles have the same size (a_i 's are area preserving in 1-d-f)
- Allegedly this can be extended to nonlinear maps

Now we make a bold claim

What if everything turns into circles?

$$M = a \circ n \circ a^{-1}$$

$$n = r_x \circ r_y \circ \cdots \circ r_{mod} \circ r_{spin}$$

- All the r_i 's are rotations in the plane
- Their angles are the fractional tunes
- All these angles can depend on the radii of the other planes
- r_{mod} is a rotation describing the modulation frequency of a magnet family
- r_{spin} is a rotation of the spin. Its angle depends on all the other radii
- the transformation “ a ” acts on the orbital motion and on the spin. It transforms the spin differently at every point in phase space

This implies a **unique and universal** C-S theory

$$M = a \circ n \circ a^{-1}$$

$$n = r_x \circ r_y \circ \cdots \circ r_{mod} \circ r_{spin}$$

- All the r_i 's are rotations in the plane
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The **do-loop** presented before is universal.

- One simply tracks the canonical transformation a_s from $s = 0$ to some s of interest
- All imaginable and unimaginable lattice functions are gotten by manipulating s
- The phase advance is defined as the difference between the tracked a_s and a special form for a_s chosen by the physicist— Courant-Snyder form for example.

Other kind of normal form? Only circles?

- Circles + drift
 - Only circles (presented already)
 - Circles and a drift in the longitudinal plane: relevant in the absence of RF-cavities
- One-resonance normal form : a discrete rotational symmetry
 - Ordinary orbital resonance in a single plane:
 $3\nu_x = k, 4\nu_x = k \dots$
 - Coupled resonances: orbital and spin
 - ▶ Orbital: $2\nu_x + \nu_y = k$, etc ...
 - ▶ Spin : $\nu_x + \nu_s = k$, etc ... (always linear in spin)
- Spiraling sinks in the case of radiation:
 - Orbital (+ spin)
 - Orbital + stochastic moments: Synchrotron integral theory