

Design, construction and test of thermally activated *ReBCO* switches



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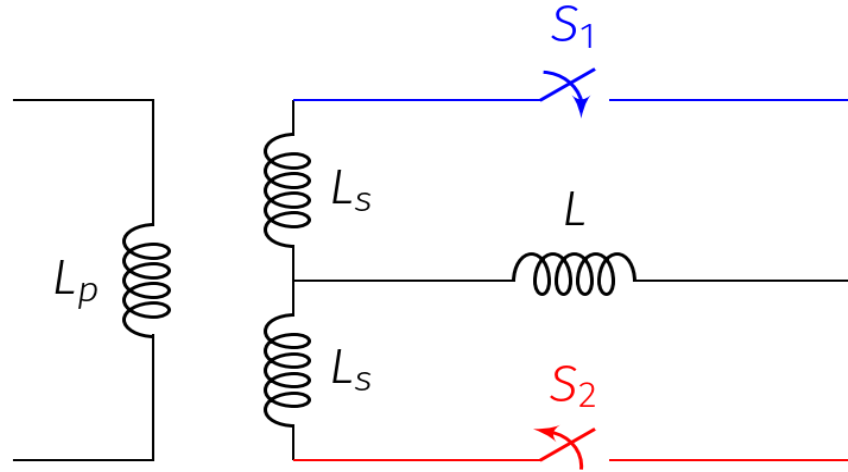
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Introduction: **superconducting rectifiers**



The feasibility of technology was demonstrated in late 70's using LTS switches and since that time it is in occasional use for detector magnets.

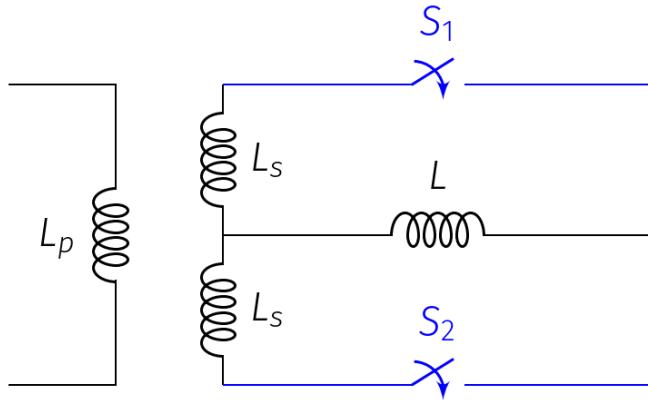
Pros:

- Minimized heats load at large current
- Compact size, even at very high currents, thus low impact of I_{op} on the overall cost
- Persistent mode when idle

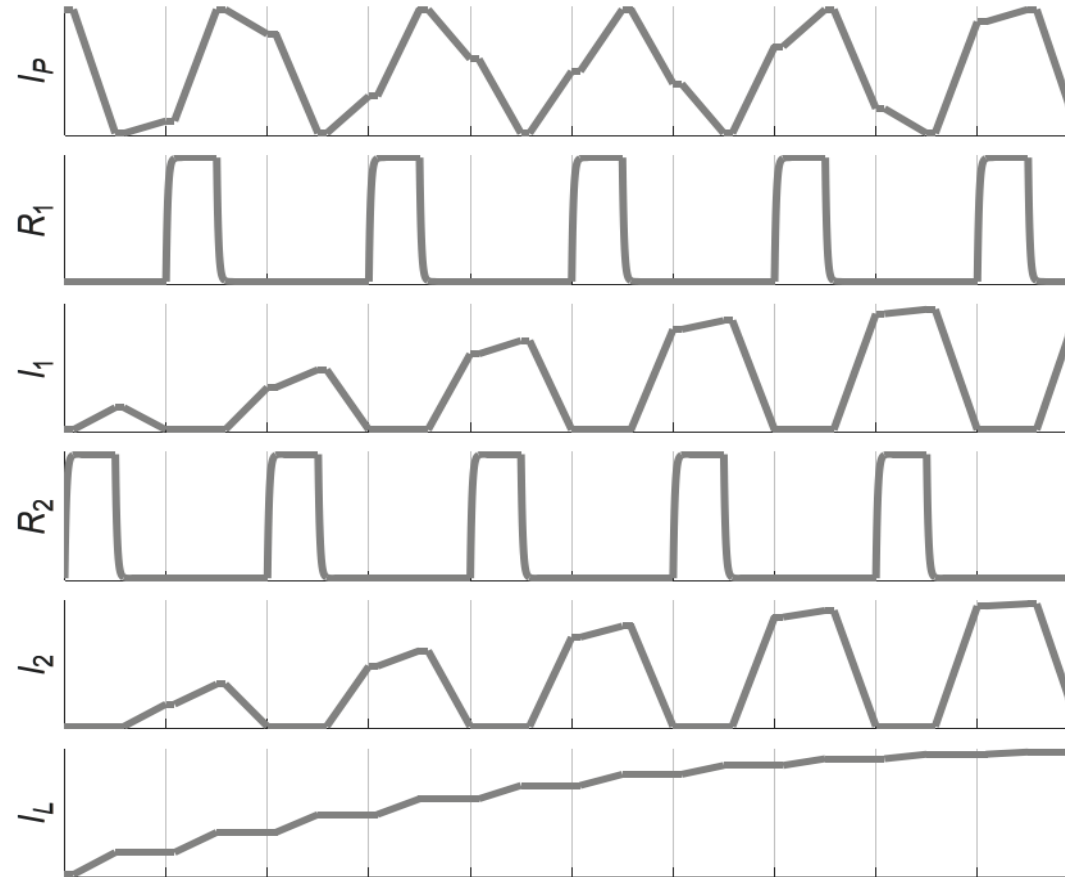
Cons:

- Relatively slow charging of magnet and troublesome control of switches
- Low stability of LTS switches

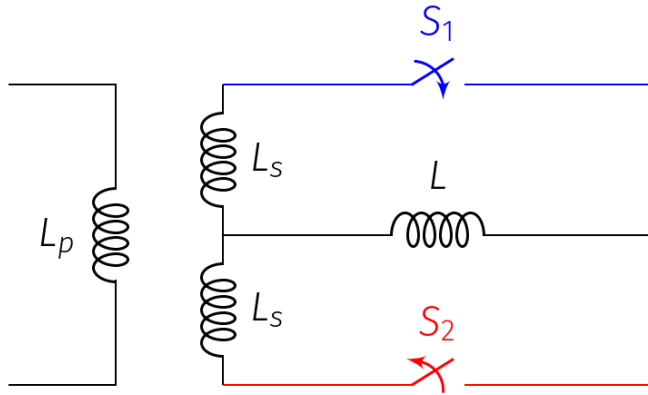
Introduction: diagram of operation



Every half-cycle consists of
4 stages:

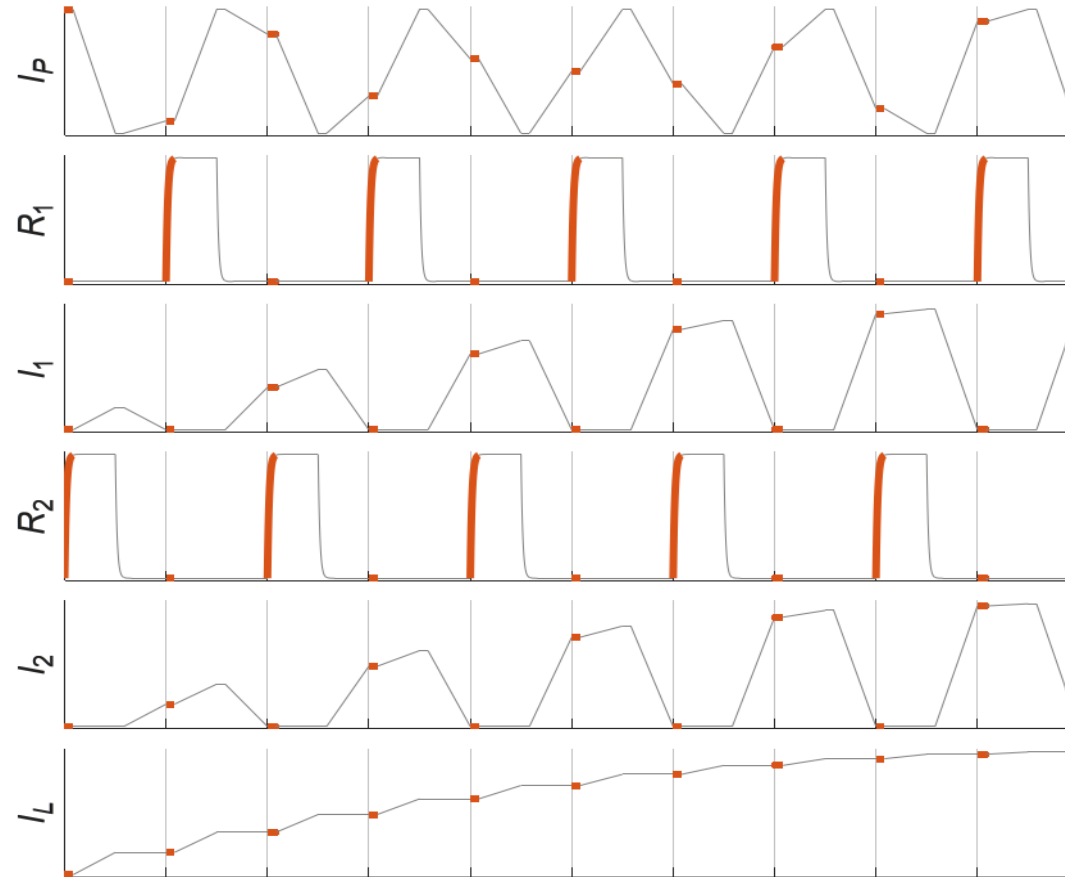


Introduction: diagram of operation

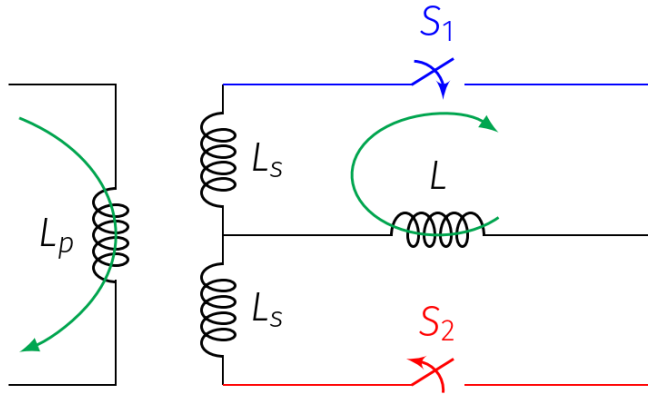


Every half-cycle consists of
4 stages:

1. opening a switch



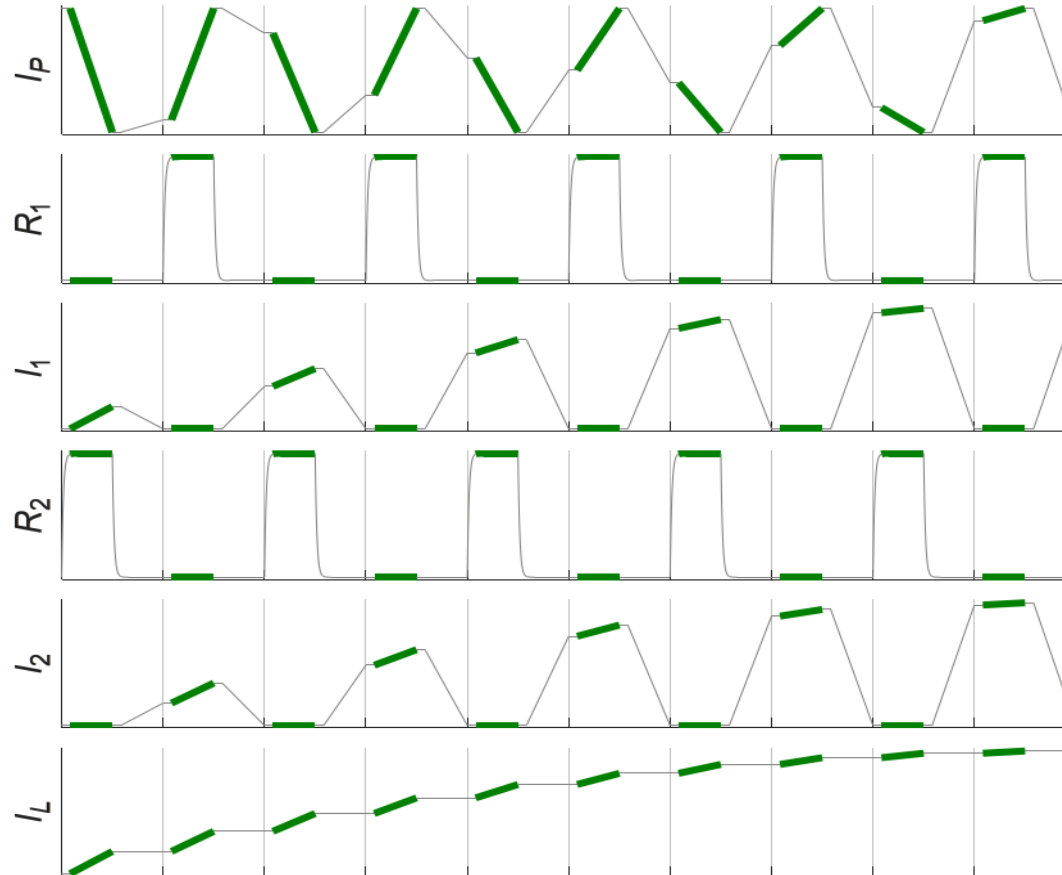
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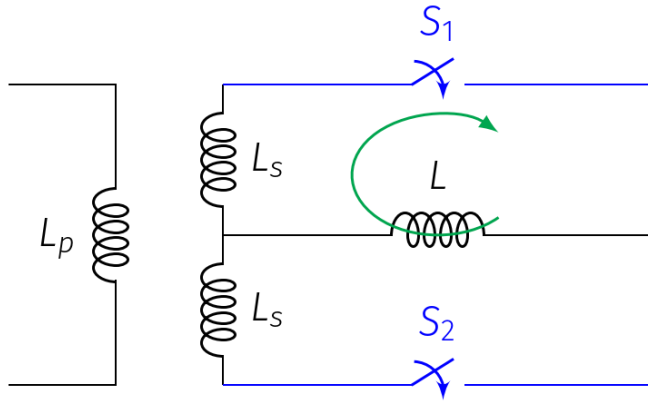
Every half-cycle consists of

4 stages:

1. opening a switch
2. pumping



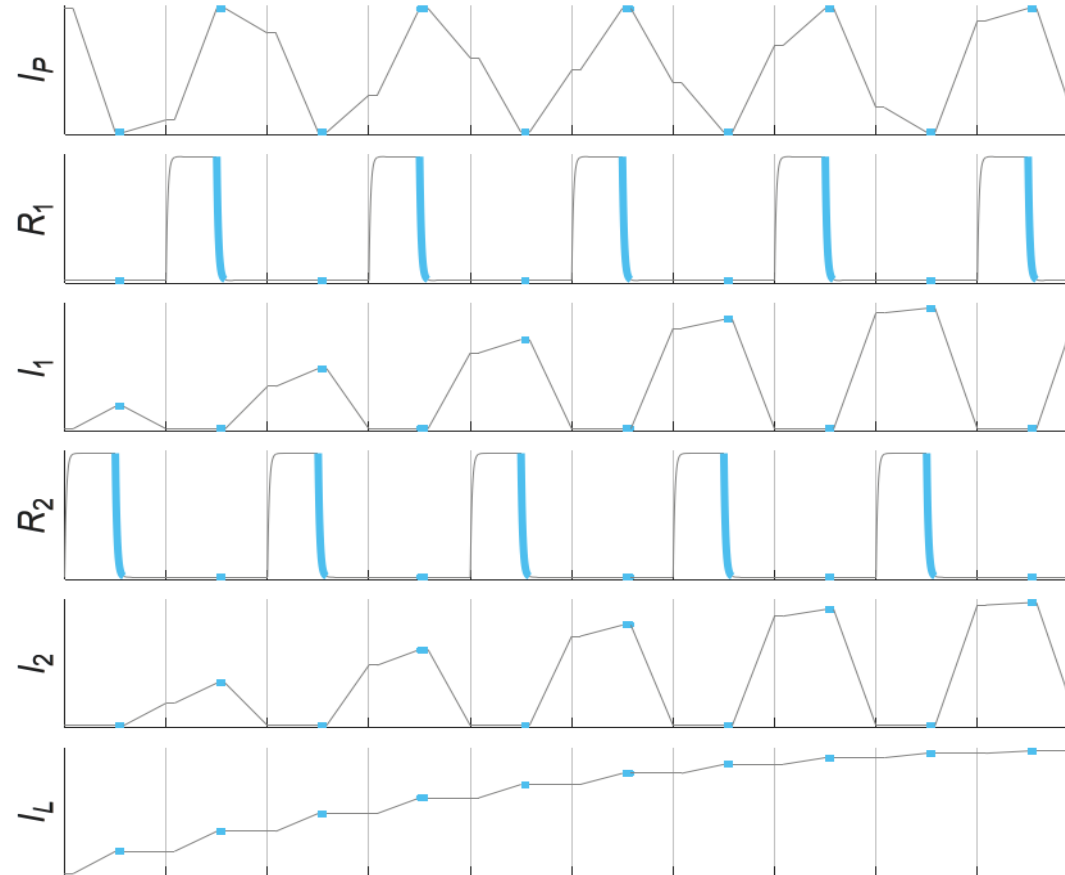
Introduction: diagram of operation



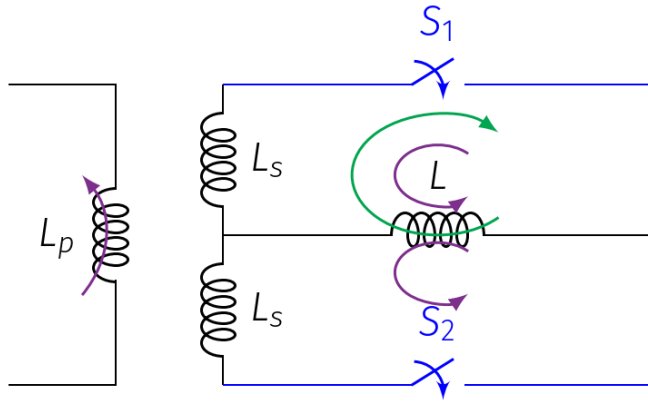
Every half-cycle consists of

4 stages:

1. opening a switch
2. pumping
3. closing a switch



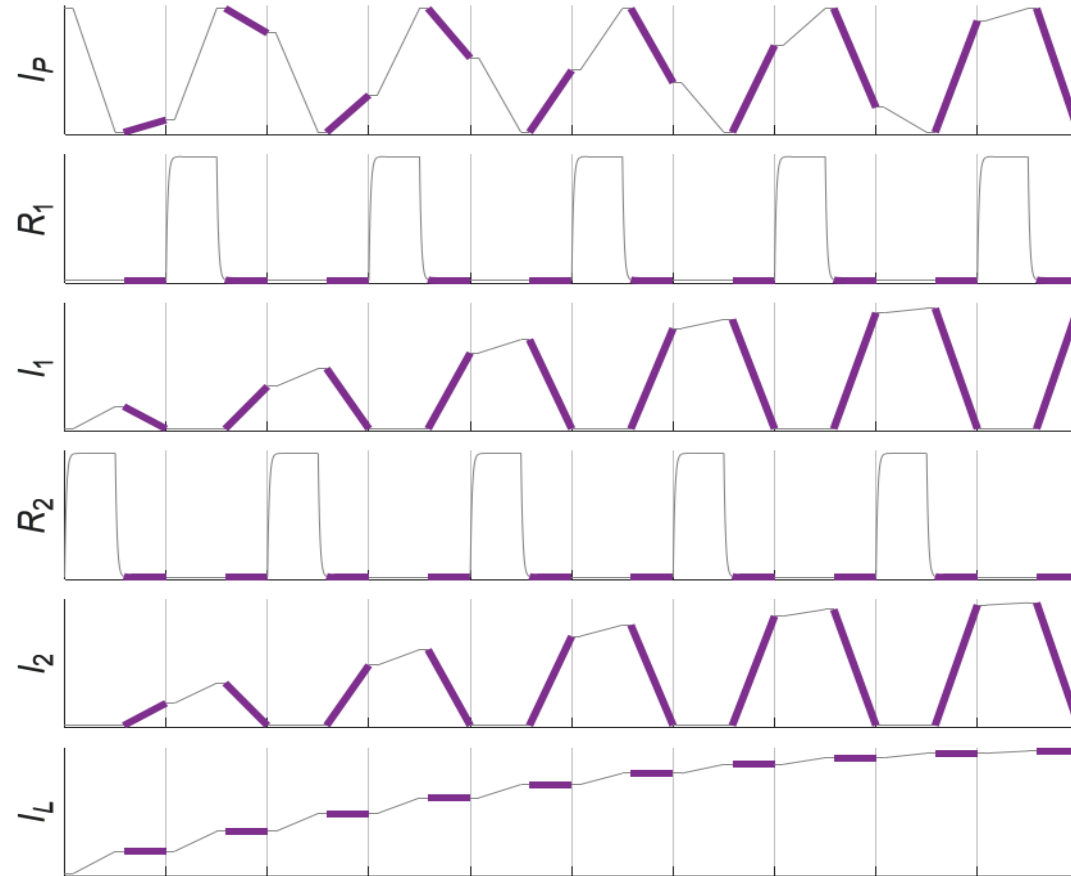
Introduction: diagram of operation



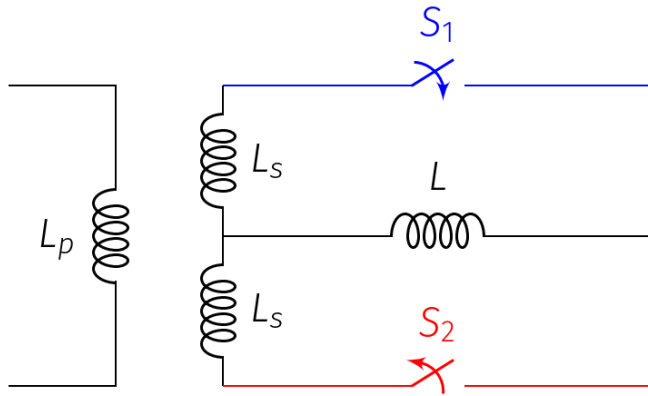
Every half-cycle consists of

4 stages:

1. opening a switch
2. pumping
3. closing a switch
4. commutation



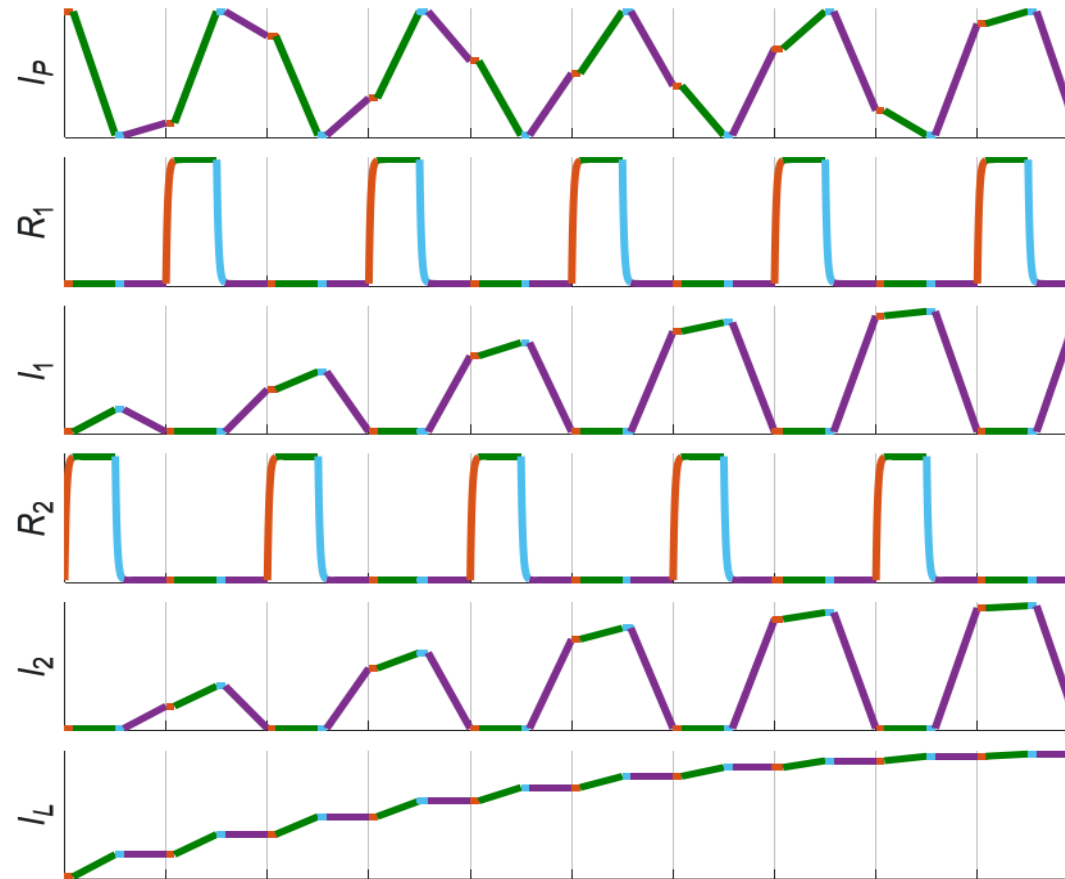
Introduction: diagram of operation



Every half-cycle consists of

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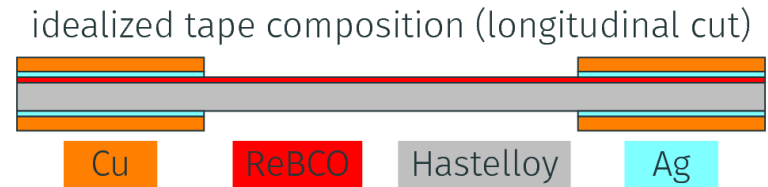
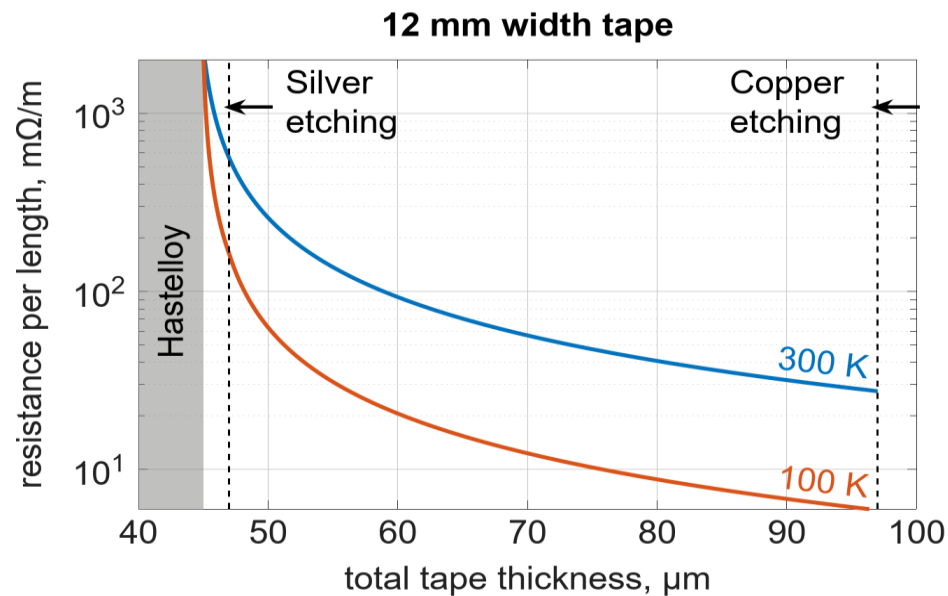


- $I_{max} \sim I_p \sqrt{L_p / L_s}$, not dependent on the load inductance L !
- Typically, I_{max} / I_p is order from hundreds to thousands
- Power loss in the open switch is proportional to $1/R$

Introduction: using ReBCO tapes for switches

Specific features of ReBCO switches:

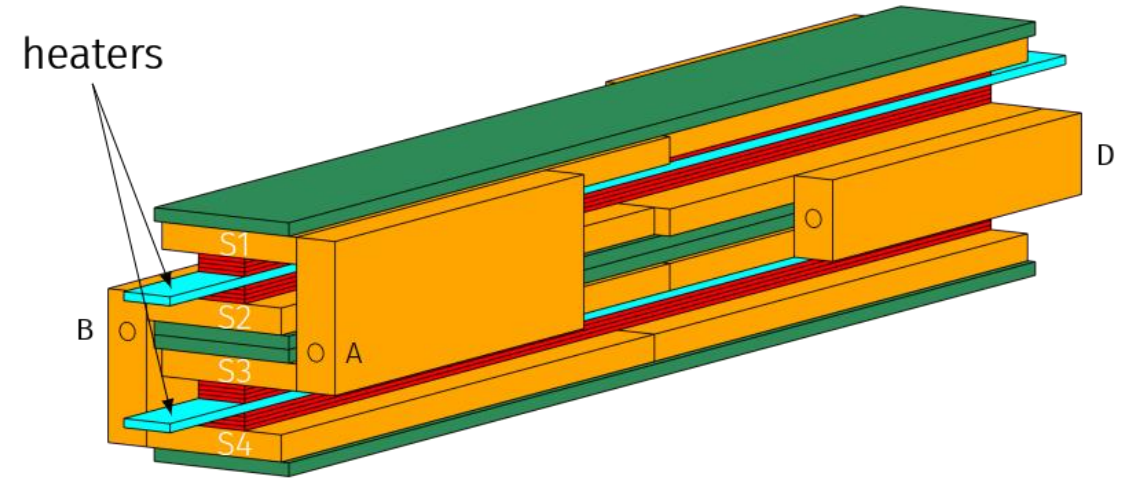
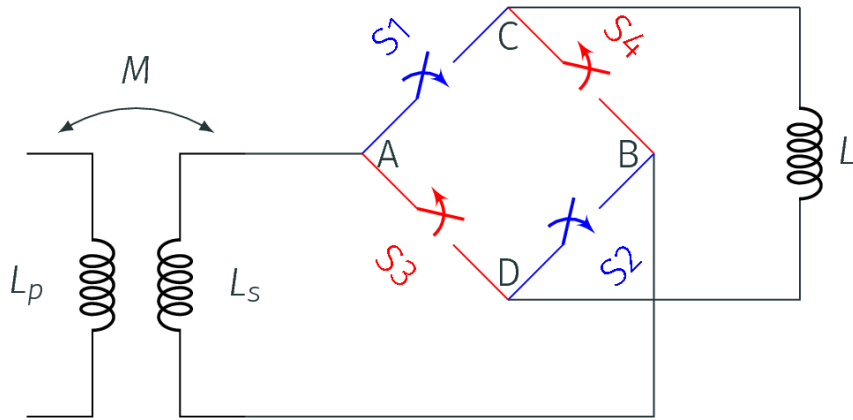
- **high stability** margin in a closed state
- possibility to operate at **elevated temperatures**, i.e. more efficient removal of heat loads
- resistance in the normal state is very promising for etched tapes:



Using 'in-house' etching method provides **both** the high 'off'-state and low joint resistances.

- ✓ Desired tape composition can be achieved ($0.1 \mu m$ Ag limit) by etching in $FeCl_3$, using tape **resistance as a feedback** and **magnetic stirrer** to get the process uniform.

Motivation: development of switch bridge



A full-wave bridge rectifier:

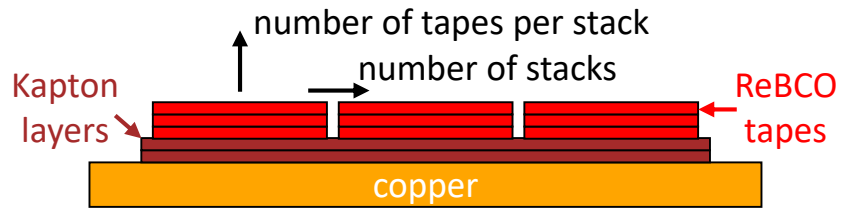
- modularity of the switch bridge, can be used with already existing sc transformers or be combined in parallel or in series
- simple design of the transformer secondary coil
- potential for faster charging, since the mutual inductance can be highest possible.

Features of the switch bridge layout:

- straightforward manufacturing and assembly of components
- use of 4 switches is simplified since only 2 heaters are required
- self-field effect on I_c is minimized due to anti-parallel current flow in the neighbouring stacks
- long length for connections with load coil and secondary winding and large surface to provide conduction cooling

Design study of switch bridge: **selected layout**

Schematic of tape arrangement:

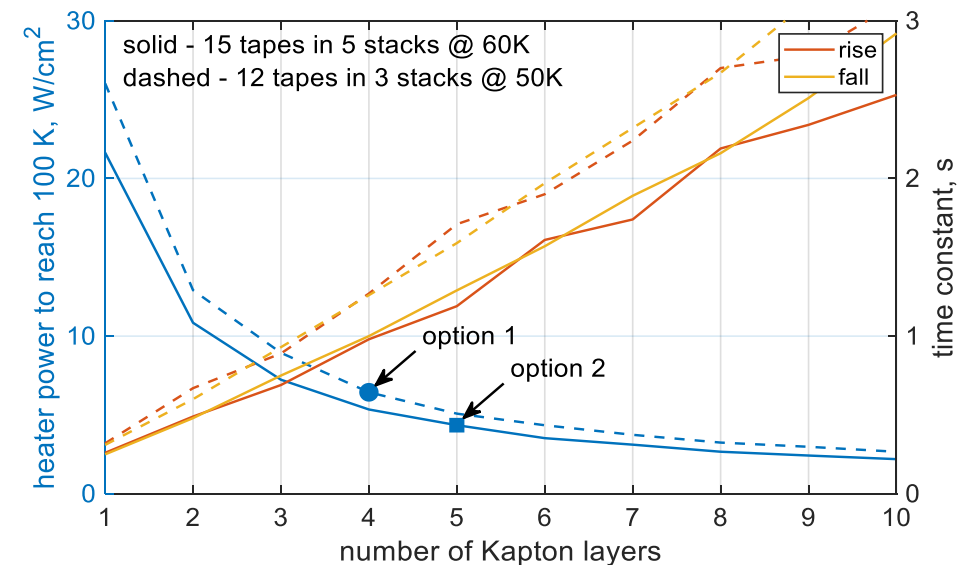
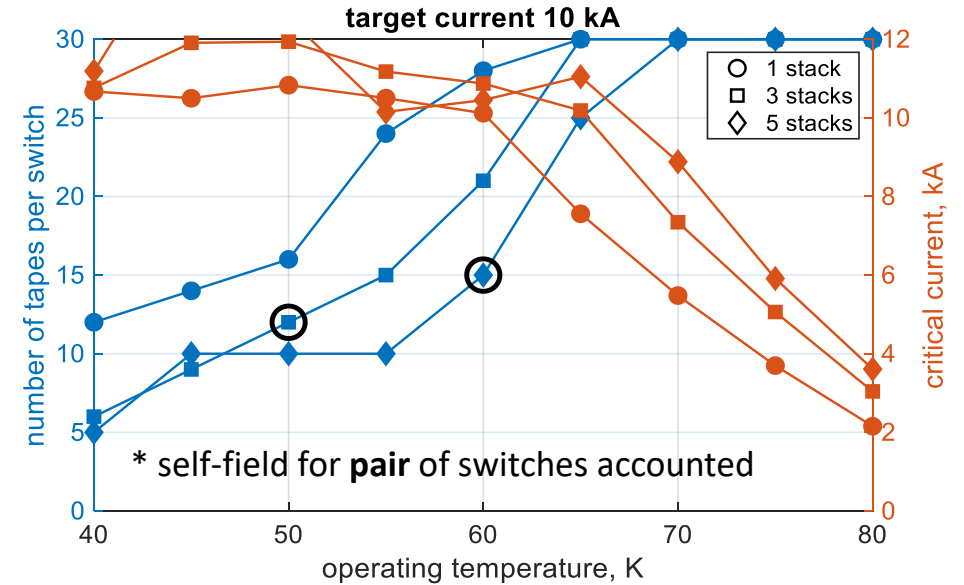


Requirements:

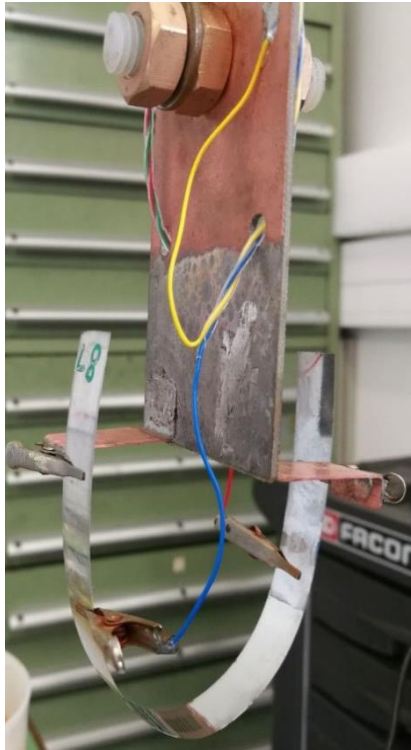
- **10 kA** current capacity @ 50-60 K
- Balancing **heat power** to reach 'off' state **vs** rise and fall **time constants** of transition **vs** 'off' state **resistance** of switch
- Low joint resistance

Selected switch layout (option 1):

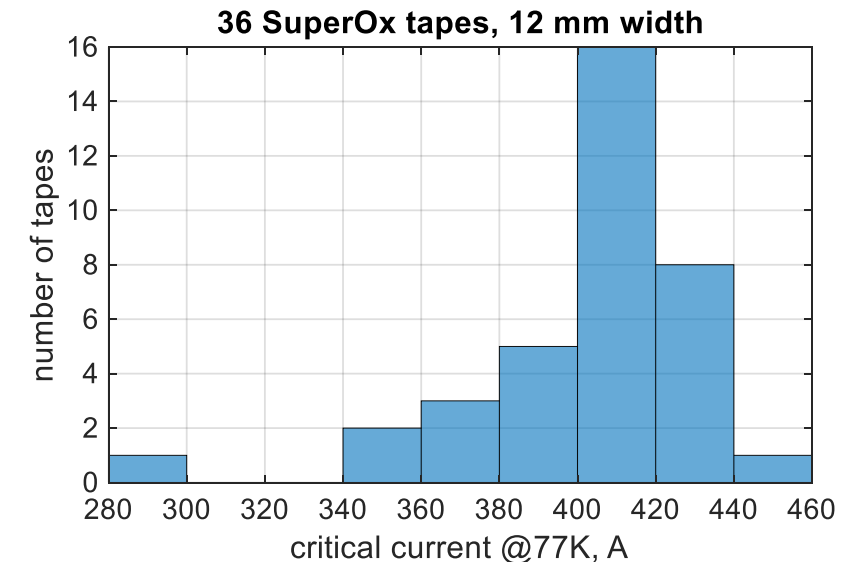
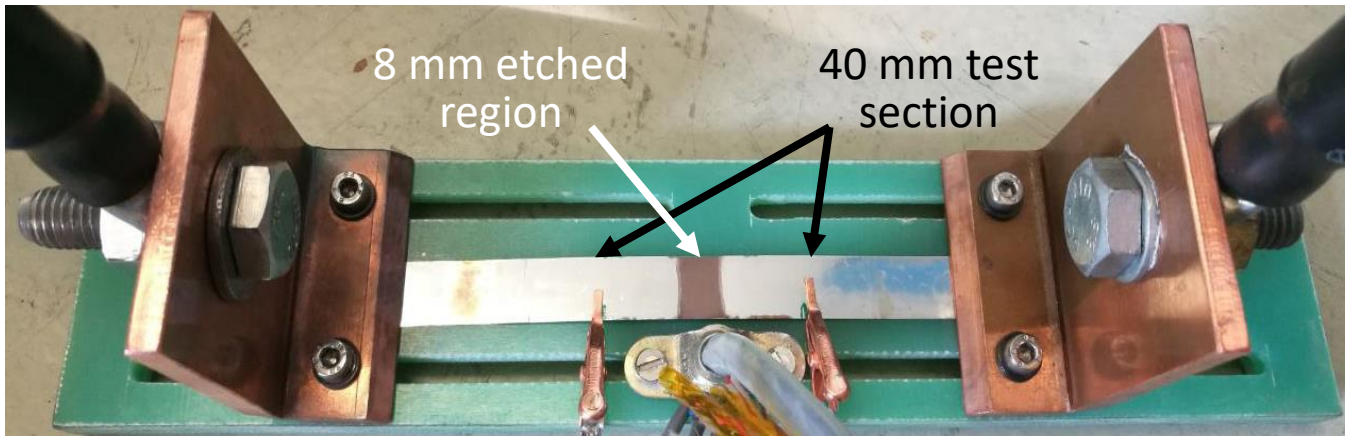
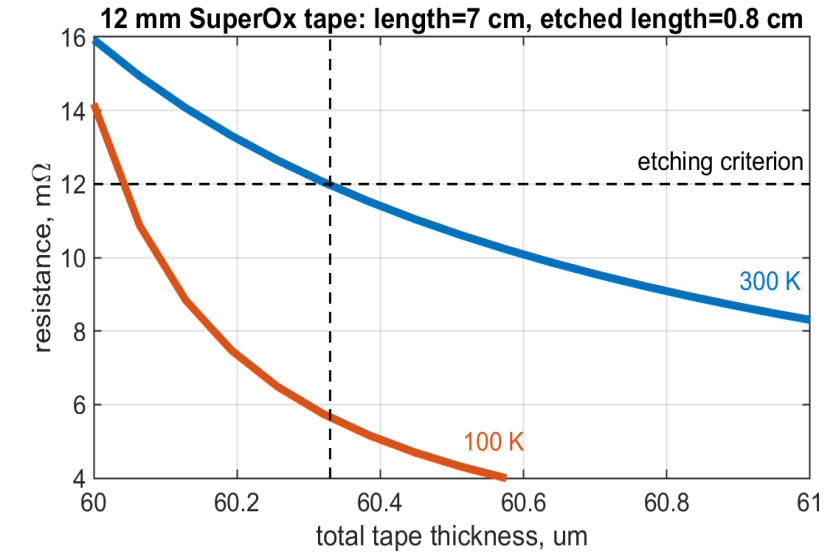
Number of tapes	12
Number of stacks	3
Number of Kapton layers	4
Heater power to reach 100 K	6.4 W/cm ²
'Off' state resistance per switch	1.2 mΩ/cm



Sample construction: **tape etching**

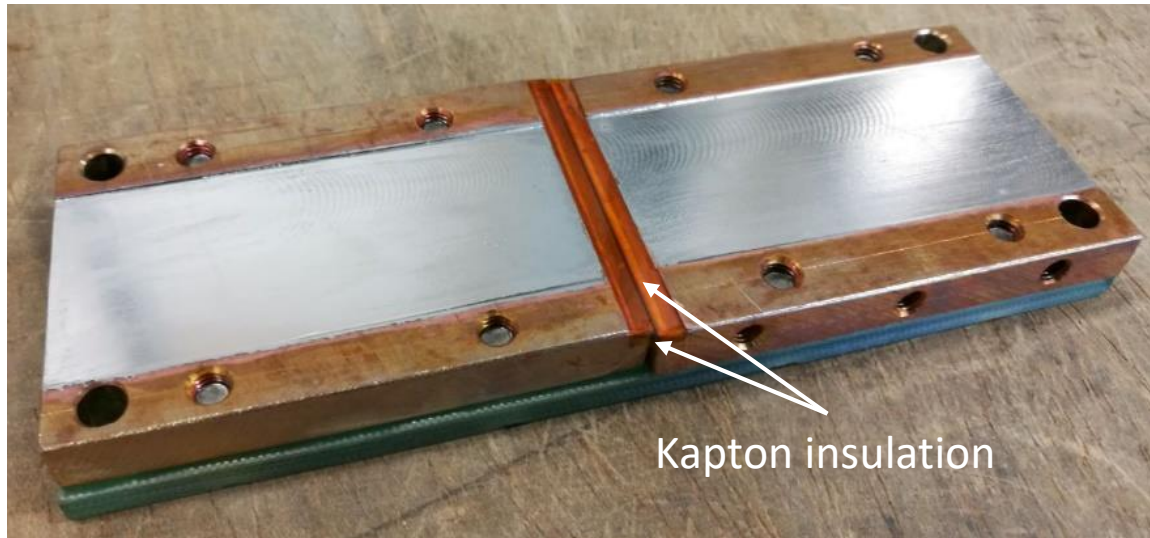


- Etching of **12 mm SuperOx pre-tinned tapes** in FeCl_3 using tape resistance as a feedback and magnetic stirrer for uniform process:
 - Varnish coating used to etch **8 mm section**, resistance measured over 70 mm section.
 - 12 m Ω etching threshold: SnPb and Cu layers removed, $\approx 0.3 \mu\text{m}$ thick Ag layer remained.
- I_c of tapes measured at 77 K after etching over 40 mm section, on average 400 A (**no reduction**).
- 36 tapes** prepared in total, 9 tapes per switch.

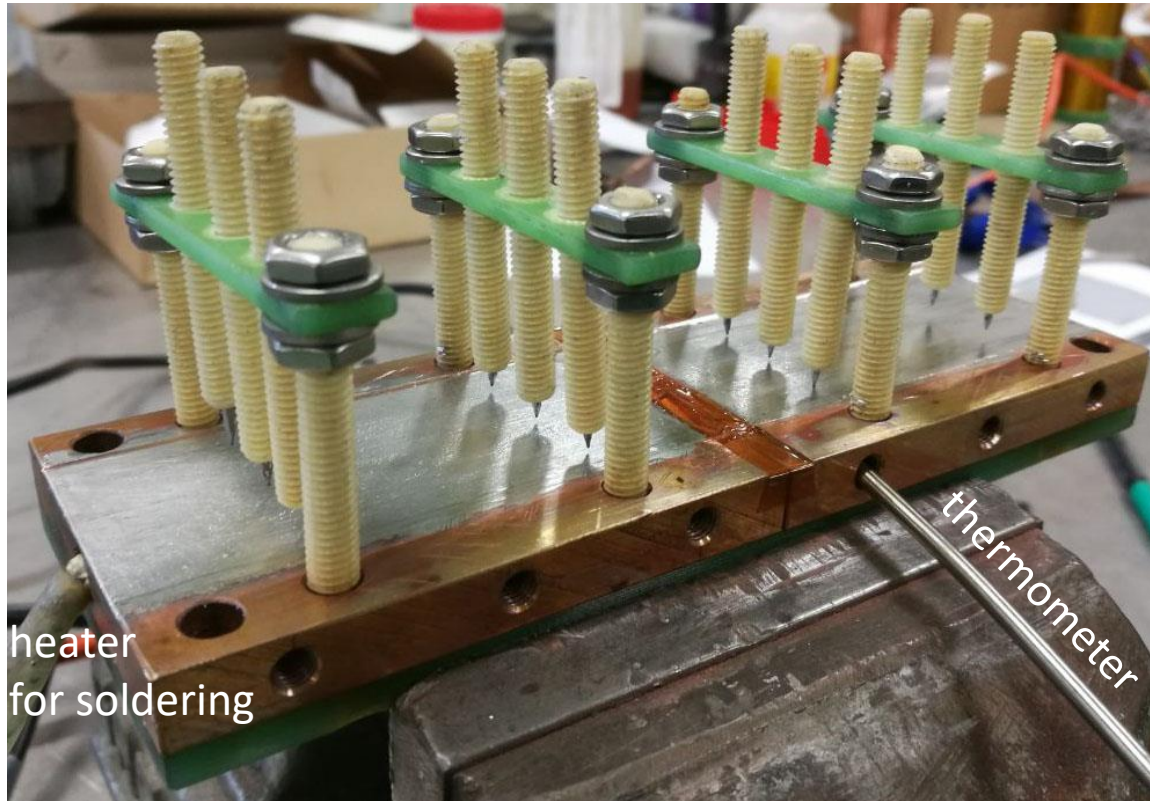


Sample construction: **soldering & assembly**

1. Copper plates pre-tinned



Sample construction: **soldering & assembly**



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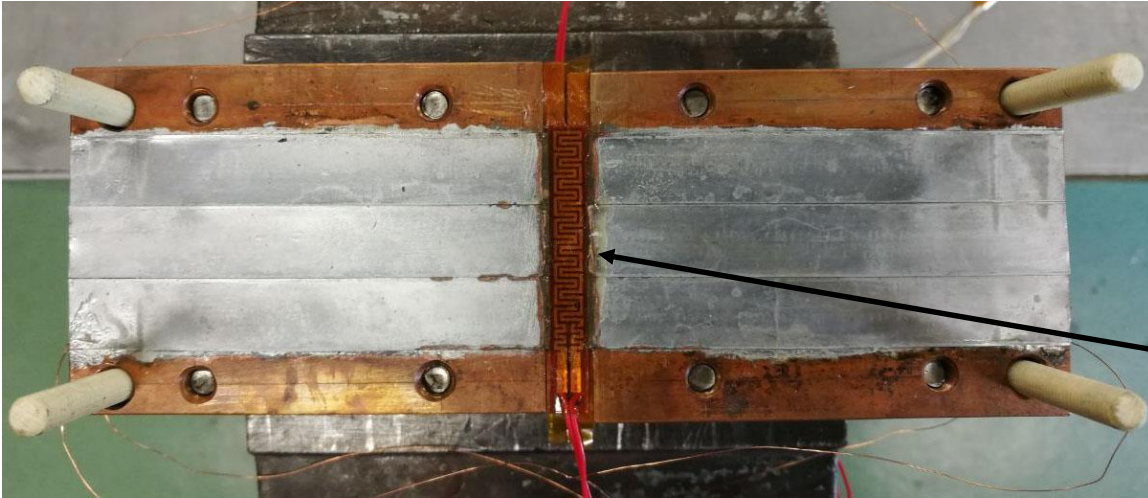
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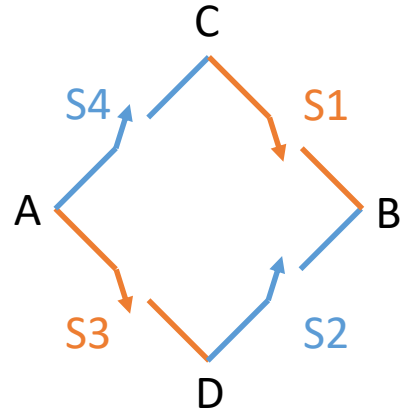
1. Copper plates pre-tinned
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 4. Packing and soldering
- * Ic tests in LN2 (next slide)

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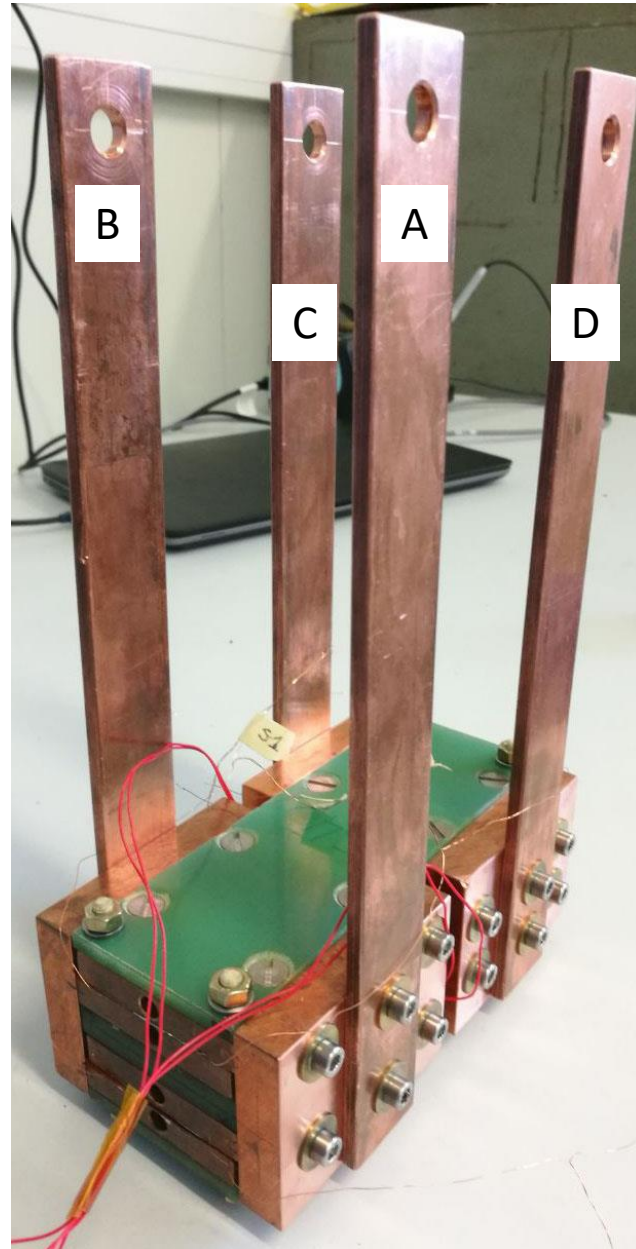


1. Copper plates pre-tinned
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5. Control heater attached

Sample construction: **soldering & assembly**

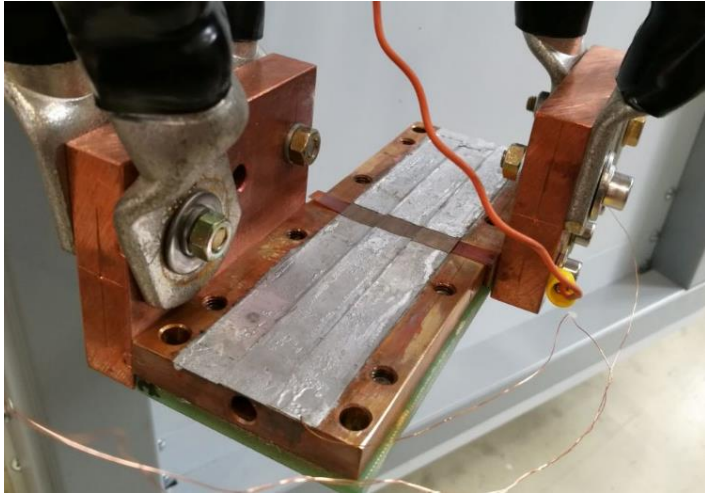


Standalone testing:
A-B: power supply
C-D: open

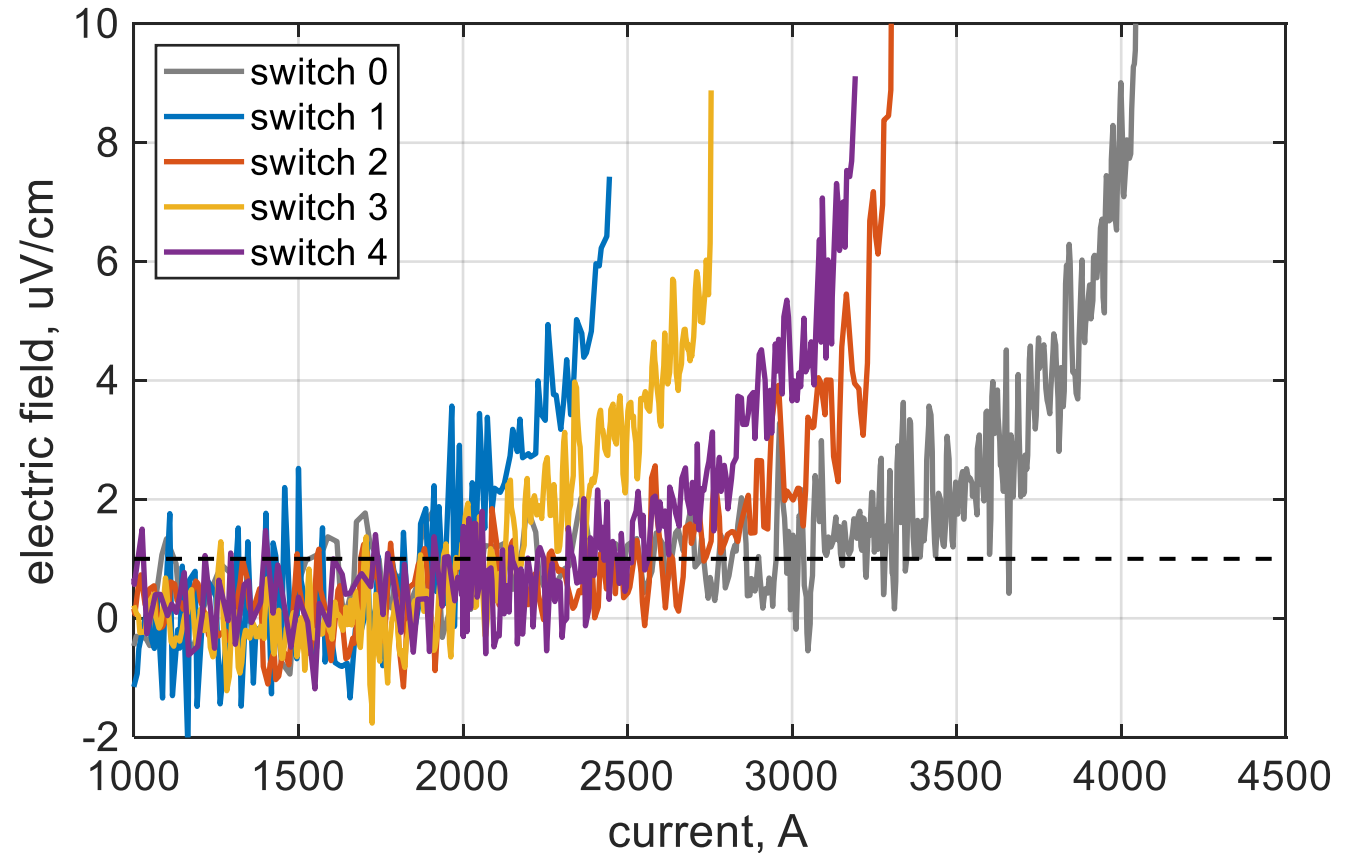


1. Copper plates pre-tinned
2. G10 fixators attached
3. Tapes arranged
4. Packing and soldering
 - * Ic tests in LN2 (next slide)
5. Control heater attached
6. Complete assembly
 - * testing in LN2, but rather conduction cooling conditions for ReBCO tapes

Sample construction: intermediate I_c tests

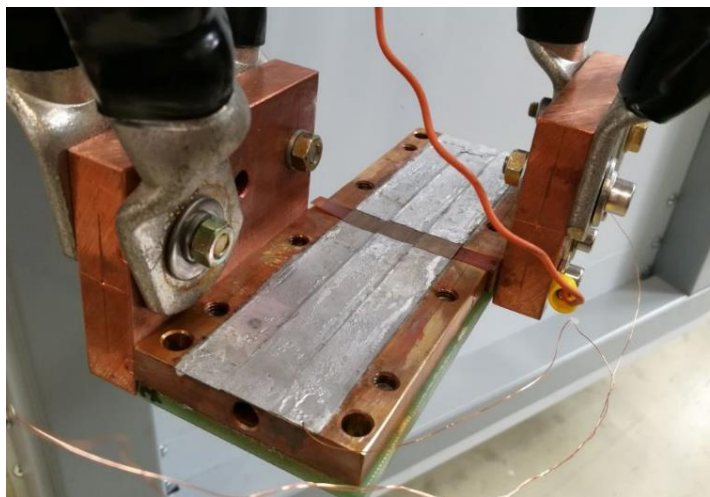


	S0	S1	S2	S3	S4
Sum tape I_c , kA	3.8	3.4	3.6	3.6	3.6
Expected I_c , kA	3.2	3.0	3.1	3.1	3.1
Measured I_c , kA	3.1	1.9	2.6	2.1	2.4
Retention	98 %	64 %	85 %	69 %	78 %

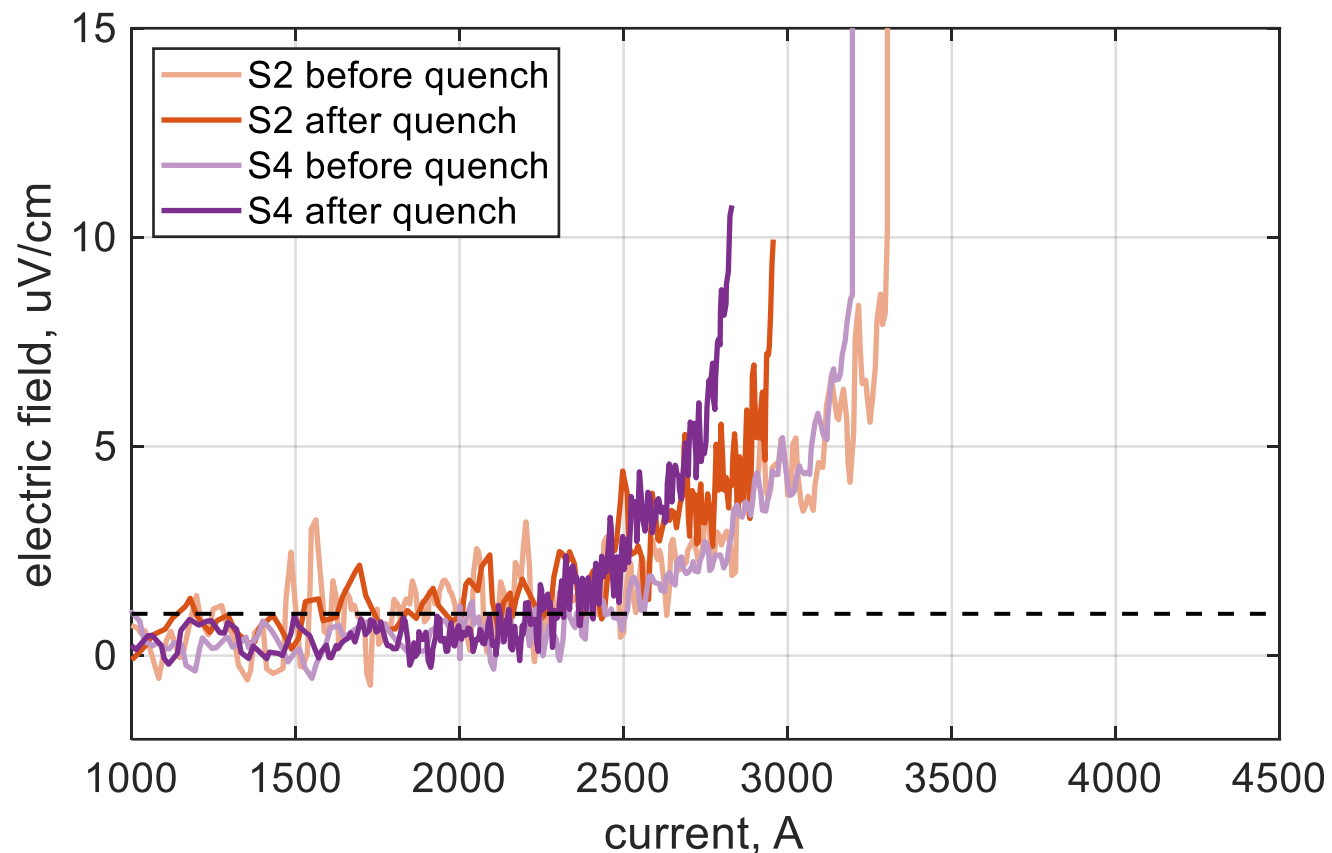


- S0 performed as expected, but noticeable reduction of I_c observed on S1-S4 (further discussed next)
- After quench of S2 and S4:
 I_c reduced negligibly at 1 $\mu\text{V}/\text{cm}$ criterion, but $\approx 10\%$ reduction at the higher threshold

Sample construction: intermediate I_c tests

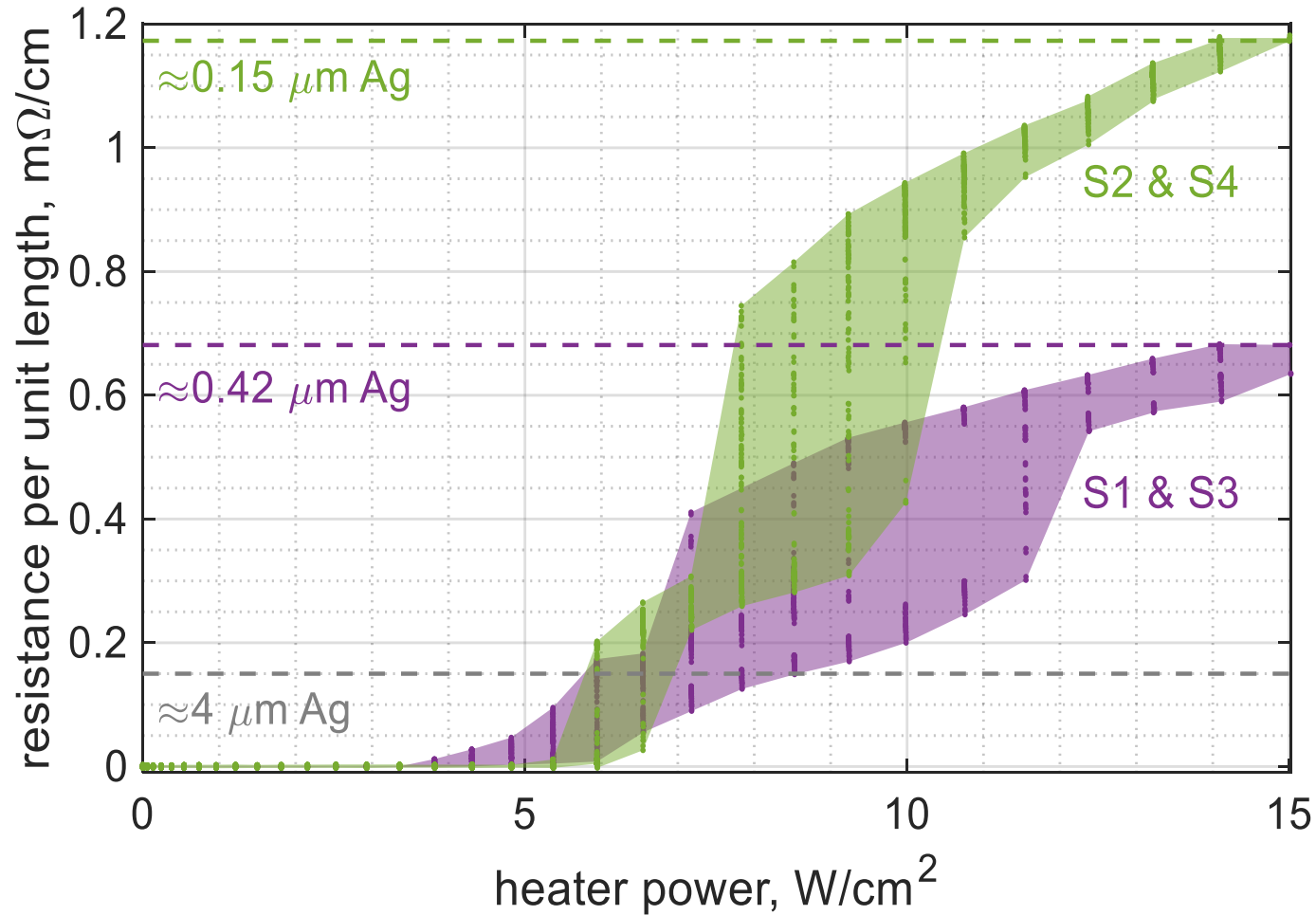


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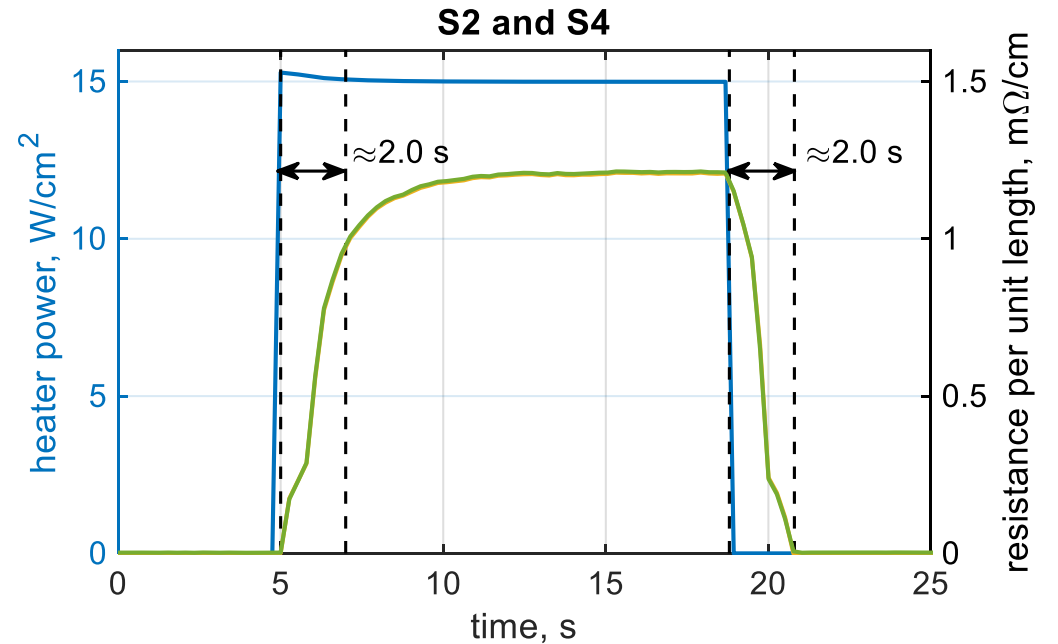
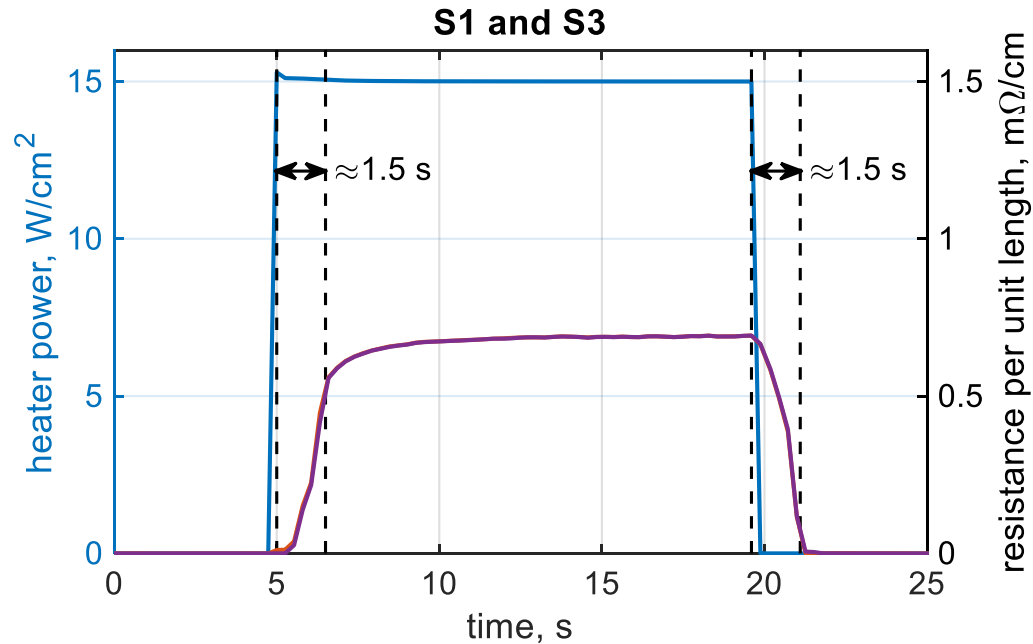
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Test in LN2: 'off'-state resistance



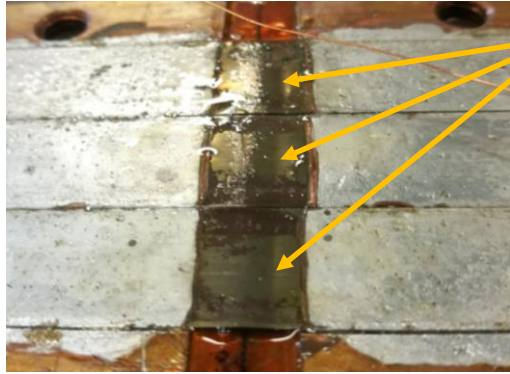
- Resistance of the open switch corresponds to $\approx 0.15 \mu\text{m}$ and $\approx 0.42 \mu\text{m}$ average remained thickness of Ag and 60 μm Hastelloy layers.
- Switches are activated starting from 5 W/cm^2 heater power and turned fully normal at $\approx 12 \text{ W/cm}^2$.
- High heater power required is due to **strong cooling** conditions in LN2 bath.

Test in LN2: transition metrics

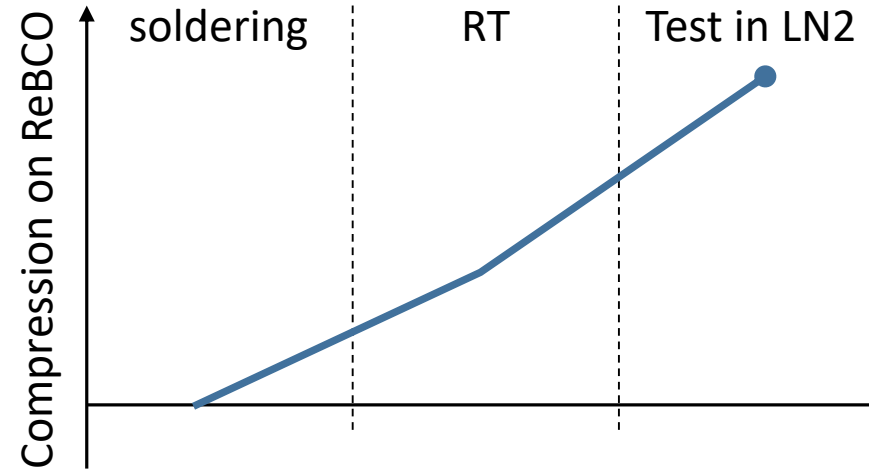


- Rise and fall times of the transitions are around **1.5 s** for S1 & S3 and **2.0 s** for S2 & S4, close to expected values from the thermal simulation model.
- Commutation of the switches can be applied right after these time delays.

Test in LN2: effect of thermal contraction



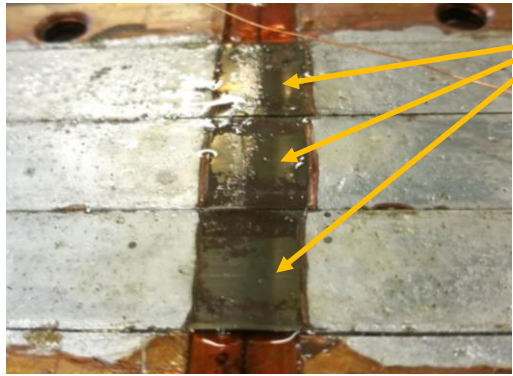
Damaged
after testing



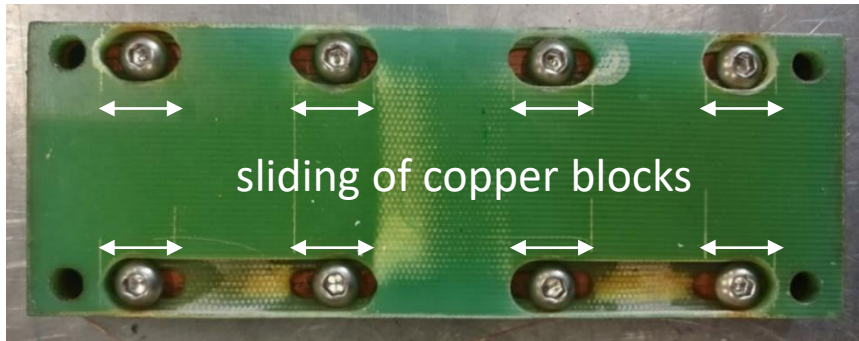
Material	Thermal expansion, %	
	@ 220 C	@ 77 K
Copper	0.34	-0.30
Hastelloy	0.23	-0.20
G10	//	-0.21
	⊥	-0.64

- Etched section more sensitive to mechanical strain and mismatch in **thermal shrinkage** of copper and Hastelloy might be at the origin of the damage.

Test in LN2: effect of thermal contraction



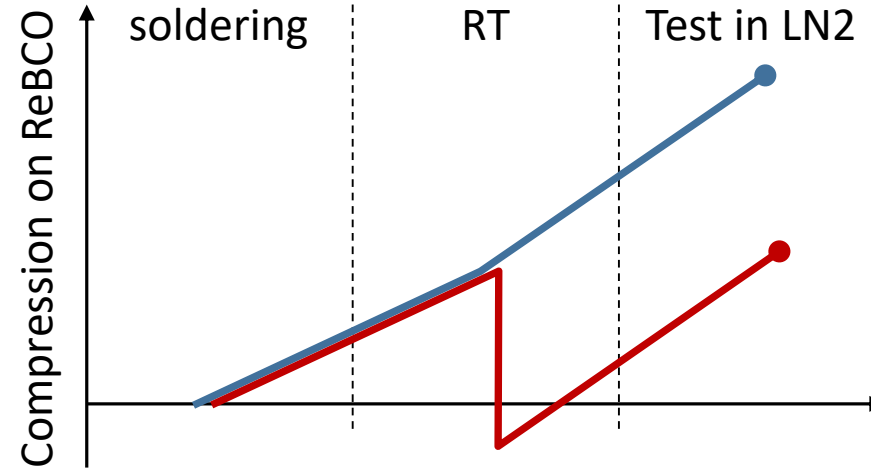
Damaged after testing



sliding of copper blocks



tension on tapes



Material	Thermal expansion, %	
	@ 220 C	@ 77 K
Copper	0.34	-0.30
Hastelloy	0.23	-0.20
G10	//	0.25
	⊥	0.82
		-0.21
		-0.64

- Etched section more sensitive to mechanical strain and mismatch in **thermal shrinkage** of copper and Hastelloy might be at the origin of the damage.
- Tapes can be tensioned after soldering to release exceeding compression on *ReBCO*.

Conclusion

- The bridge type switch layout based on etched *ReBCO* tapes is proposed for charging high current magnets using a superconducting rectifier type flux pump.
- The construction is performed using 12 mm wide, pre-tinned SuperOx tapes and components of a simple block geometry.
- OFF-state resistance and transition time delay measured at 77 K follow the values from the dedicated simulation model.
- Some loss of current capacity after full assembly to be addressed by pre-tensioning of tapes.
- Operation in 50 to 60 K temperature range using cryocoolers is foreseen for the next models.

