

# Test and commissioning of the NHMFL 32 T superconducting magnet



**MT 26**  
**International Conference  
on Magnet Technology**  
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## Introduction

- Specifications

## First test

- Performance versus specifications

## Commissioning

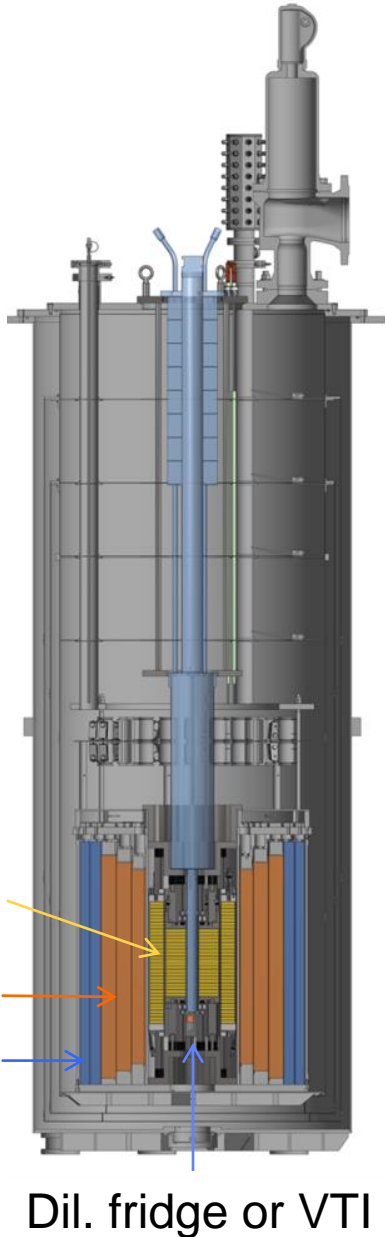
- Inspection
- MilliKelvin facilities
- Field-Current Non-linearities

## Lessons learned

## Summary



# The 32 T magnet



## Specifications:

Center field	32 T
Clear bore	34 mm
Ramp time	1 hour
Uniformity 1 cm DSV	<500 ppm
Operating temperature	4.2 K
Helium refill interval	> 20 h
Quench	Robust
Expected cycles/20 years	50,000

## Features:

Stored energy	8.3 MJ
System weight	2.6 ton

15 T / 250 mm bore LTS magnet

17 T / 34 mm bore REBCO coils

Separately powered, simultaneously ramped

HTS & LTS Quench detection and *active protection with quench heaters*



4 Just before the union of HTS and LTS coils





# The 32 T system during first test



Top of cryostat

Data Acquisition





# The 32 T system during first test

Crowbar resistor  
(protects supply,  
not magnet)



Switch Box 1 & 2

Interlock

HTS Quench  
management

LTS Quench  
management

LTS  
magnet  
PS

HTS  
magnet  
PS

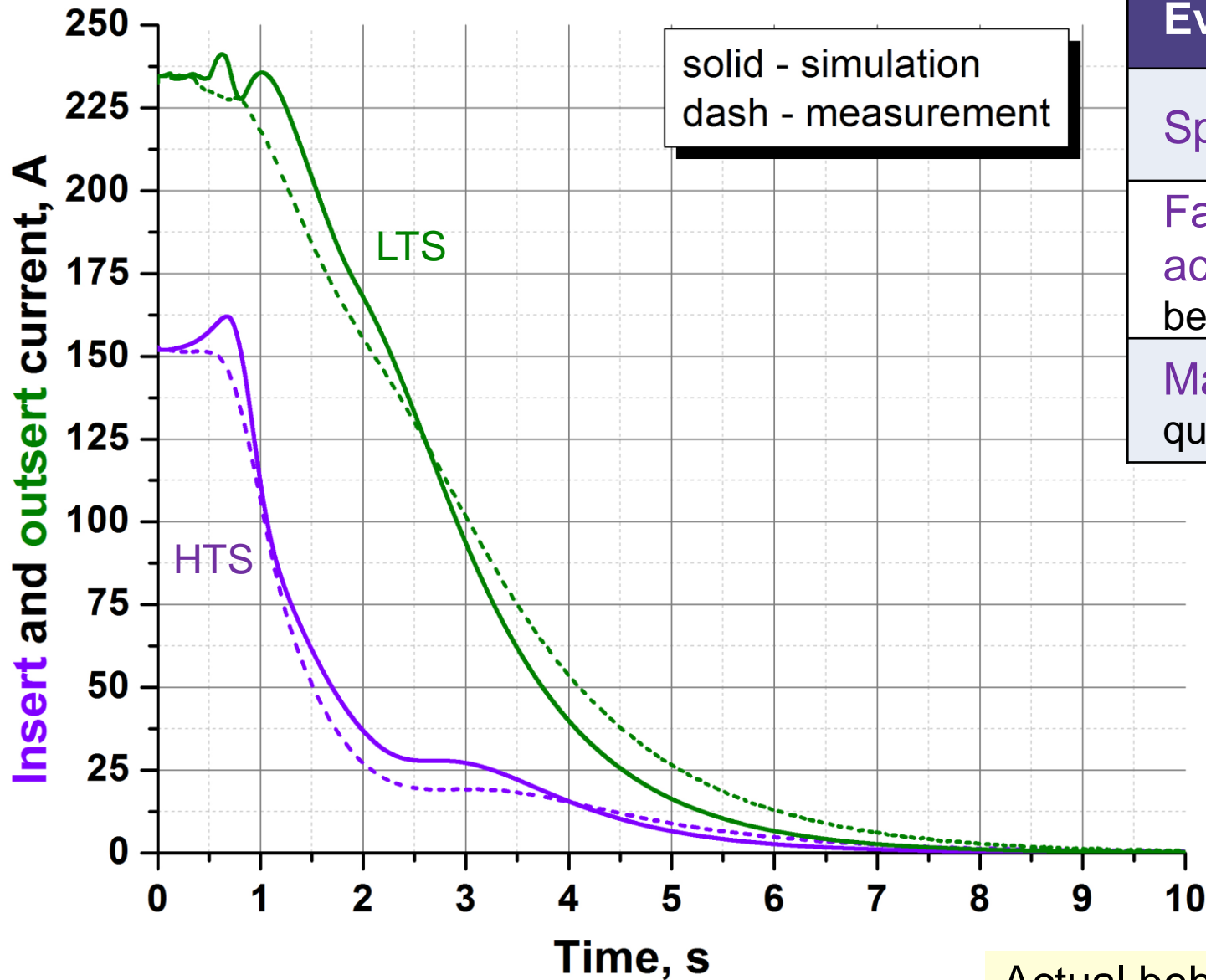
Battery  
bank



# Actual performance versus specifications: quench

28 T deliberate quench

43 runs  $\geq 16$  T, 9 to 32 T



Event	#
Spontaneous quenches	zero
False positive in quench detection, activating quench (protection) heaters before sensitivity adjustment	11
Manually induced quenches quarter, half and $\frac{3}{4}$ energy: 16, 22.5, 28 T	3

This is unique data:

- High-value high-field HTS coils
- The HTS and LTS coils survived
- Quench Robust ✓

Actual behavior slightly more favorable than simulation <sup>7</sup>



## Specifications:

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Project started with 32 mm bore specification  
Delivering 34.0 mm clear bore



4.28 K in bath-cooled areas  
≤ 4.4 K in “helium bubble” zone\*

\* In parts of the windings and bore:  $-B_z \cdot dB_z/dz > 2100 \text{ T}^2/\text{m}$   
so downward force on helium gas bubbles exceeds buoyancy → gas is trapped → heat exchange (cooling) reduced





# Actual performance versus specifications: peak field, ramp time and helium use

## Specifications:

Center field

Clear bore

Ramp time

Uniformity 1 cm DSV

Operating temperature

Helium refill interval

Quench

Expected cycles/20 years

32 T ✓

34 mm ✓

1 hour ✓

<500 ppm

4.2 K ✓

> 20 h ✓

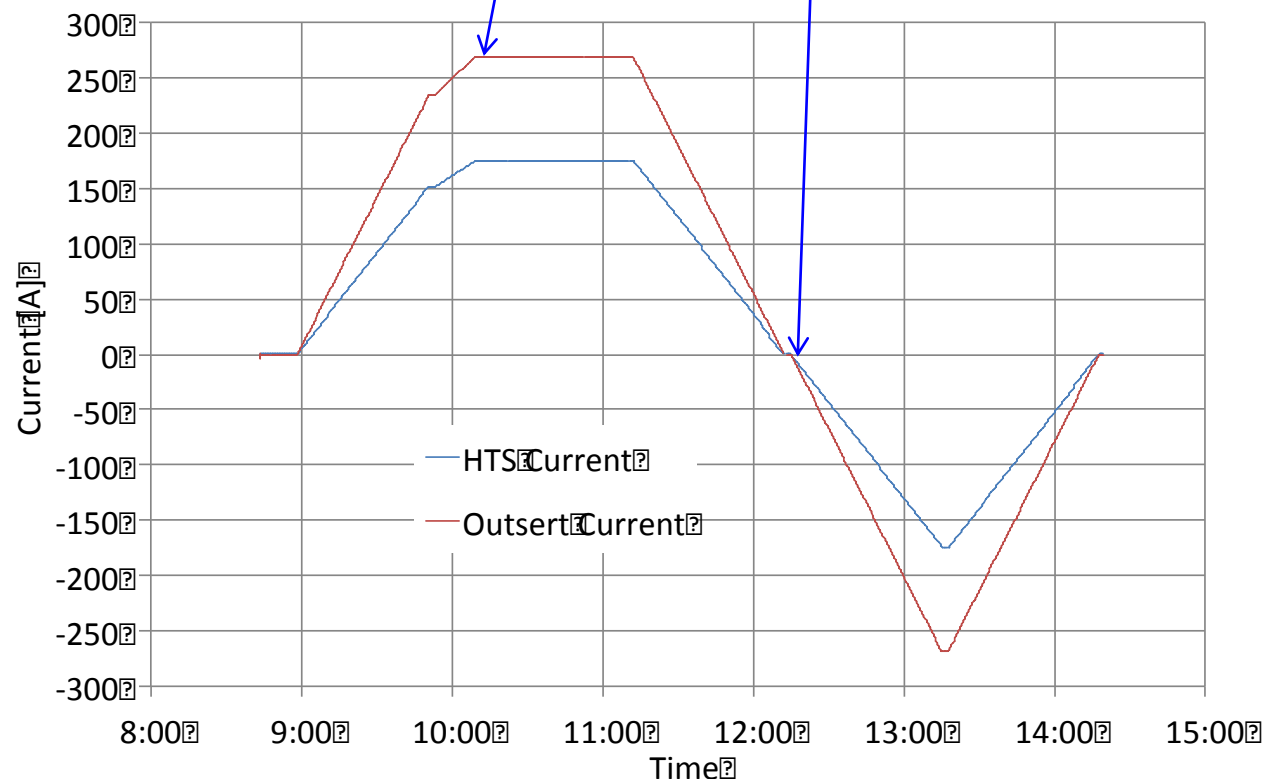
Robust ✓

50,000

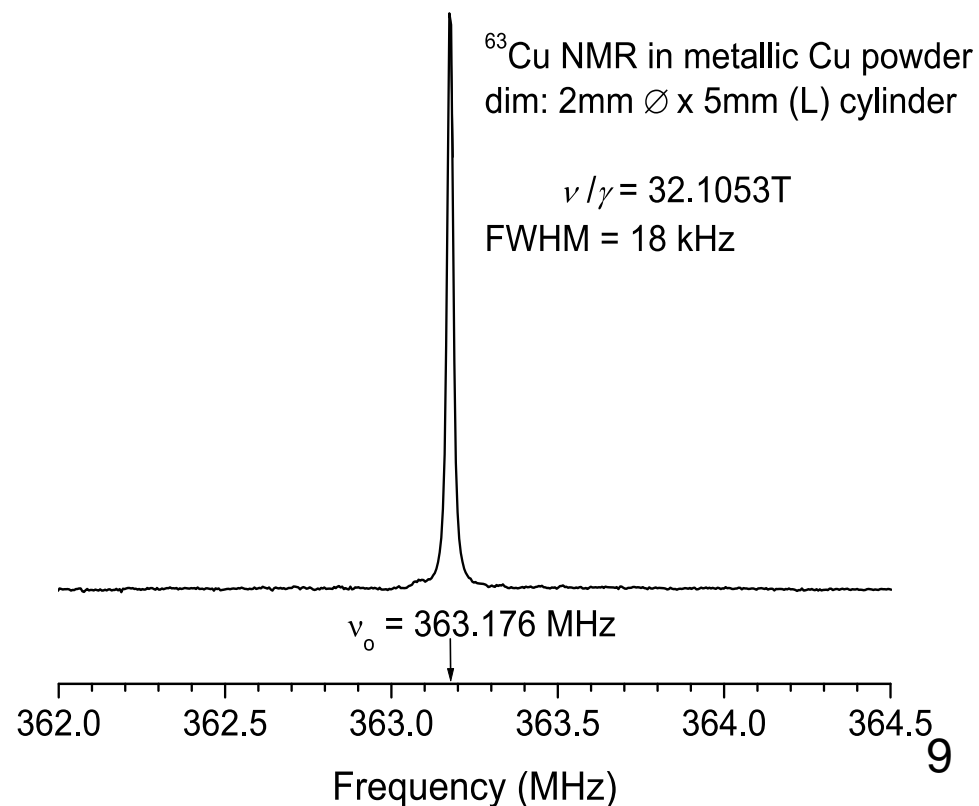
Used 32 liters helium for this run

- ~ 6 liter/hour versus 11.3 liter/hour max in heat load budget
- → 130 liter/day with 24/7 ramping operation
- ~ 60 l/day steady state at 32 T
- With 300 l useable helium → 2 to ~5 days between refill

Dec 8, 2017



Peak field (32.1 T) later confirmed with <sup>63</sup>Cu NMR measurement





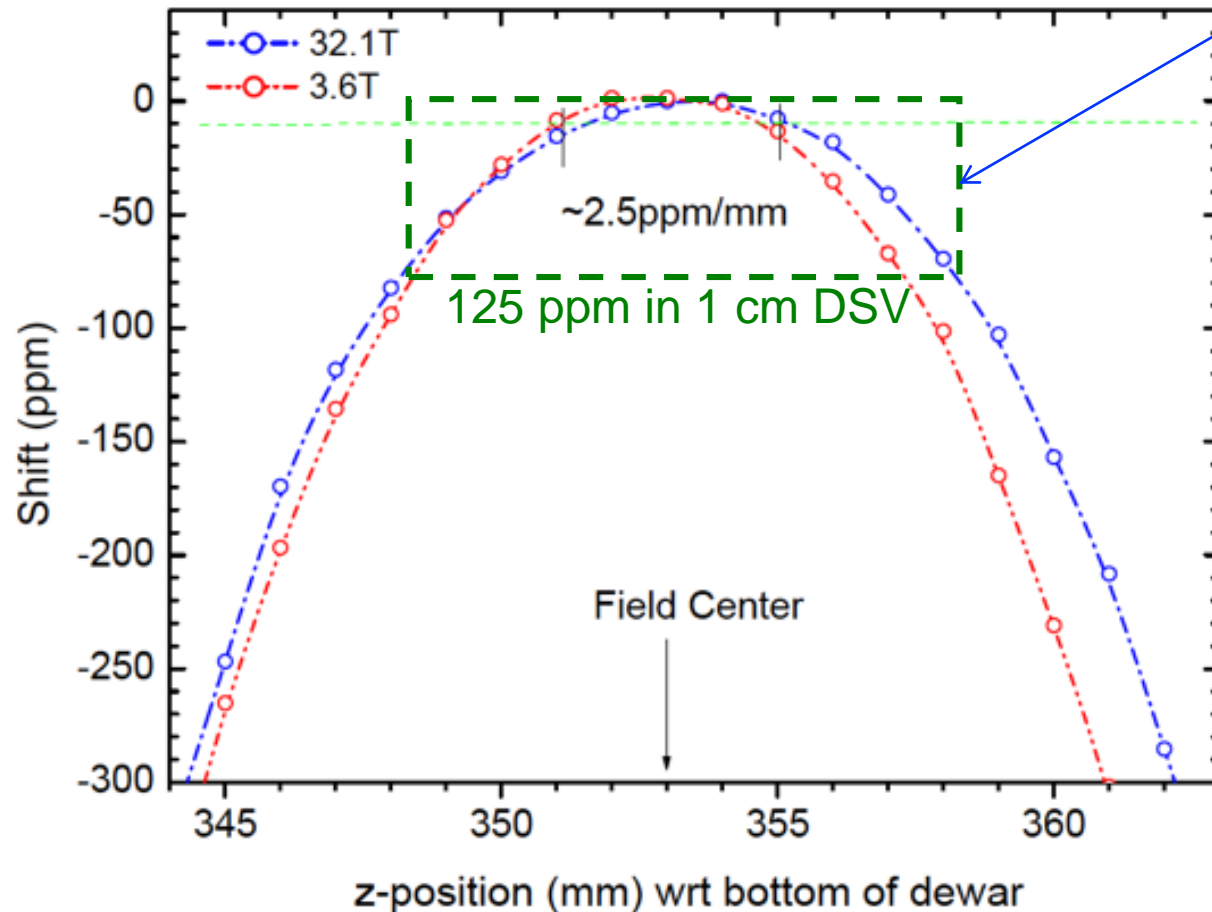
# Observed behavior: Uniformity

Uniformity is ~ 125 ppm in 1 cm DSV ~independent of  $B$

- Well within spec of 500 PPM

## Specifications:

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Clear bore	34 mm ✓
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Operating temperature	4.2 K ✓
Helium refill interval	> 20 h ✓
Quench	Robust ✓
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All specifications met

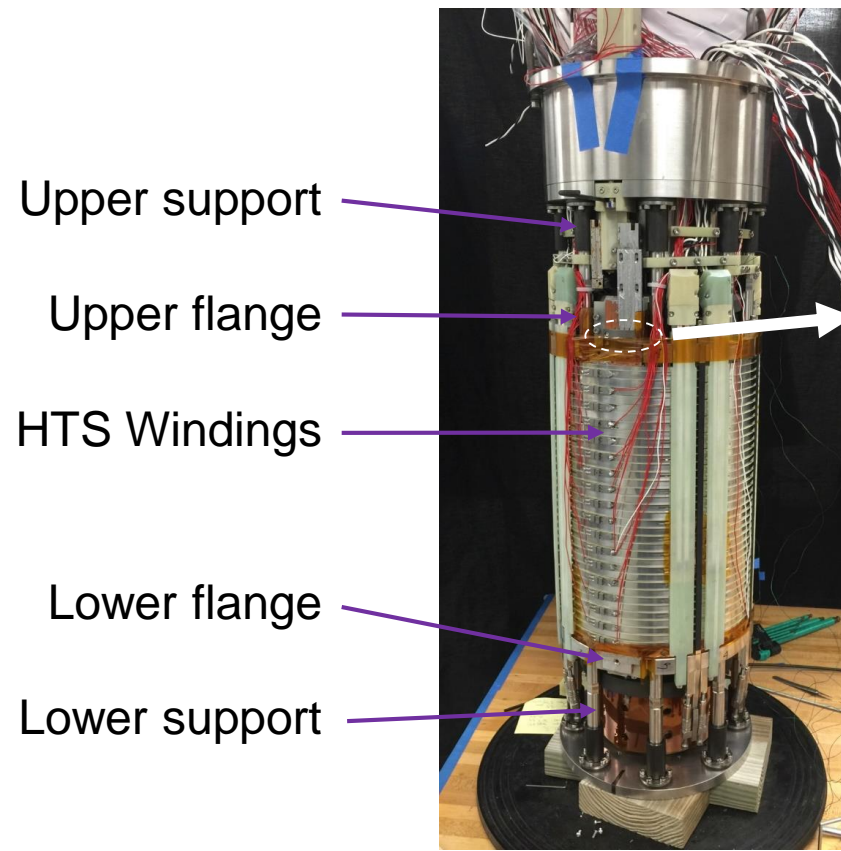
- Except lifetime cycles

- Inspection of magnet
- Upgrade Interlock functionality for safe operation with users
  - Data recording upgrades
- New building, new layout
  - Rewire all electronics
  - Facilitate routine maintenance
- User magnet infrastructure
  - Dilution refrigerator,
  - Variable Temperature Insert
  - Low noise environment
- Safety as user facility



Data suggests: Coil flanges do not move freely, separate from windings

- HTS outer coil terminals affected, redundancy and terminal lifetime expectation reduced
- Modified flange suspension while maintaining pre-compression
  - Avoid disassembly to double pancake level
- Redesigned terminals, stand-alone fatigue testing to 200,000 cycles, re-assembled magnet
- Added optical displacement sensors to monitor relative motion of support, flanges, windings, terminals



Original terminals:  
Two out of four parallel tapes compromised,  
still functional, but longevity unclear

New terminals have added axial flexibility



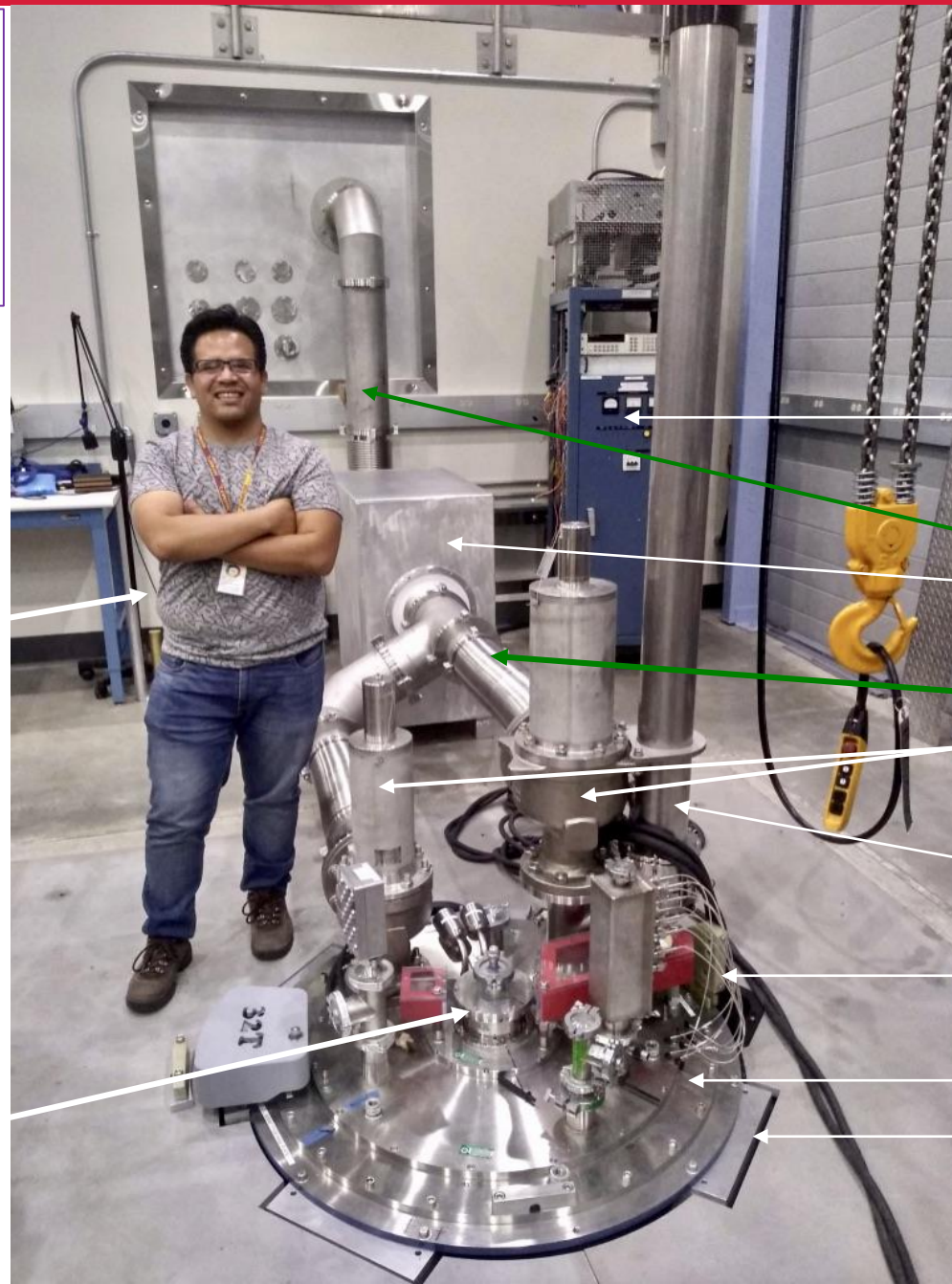
# The MilliKelvin facility: home of the 32 T magnet

MilliKelvin facility houses three  $\leq 20$  T superconducting magnets

Extension with two pits: 32 T and future 40 T

Edgar Berrospe-Juarez of UNAM visiting the NHMFL (MT26-Fri-Mo-Or27-07)

Port for VTI and Dilution Refrigerator



One (of 2) magnet power supplies

Quench valve plumbing  
Vibration isolation sand box

Quench valve plumbing  
Quench valves

Burst disk vent

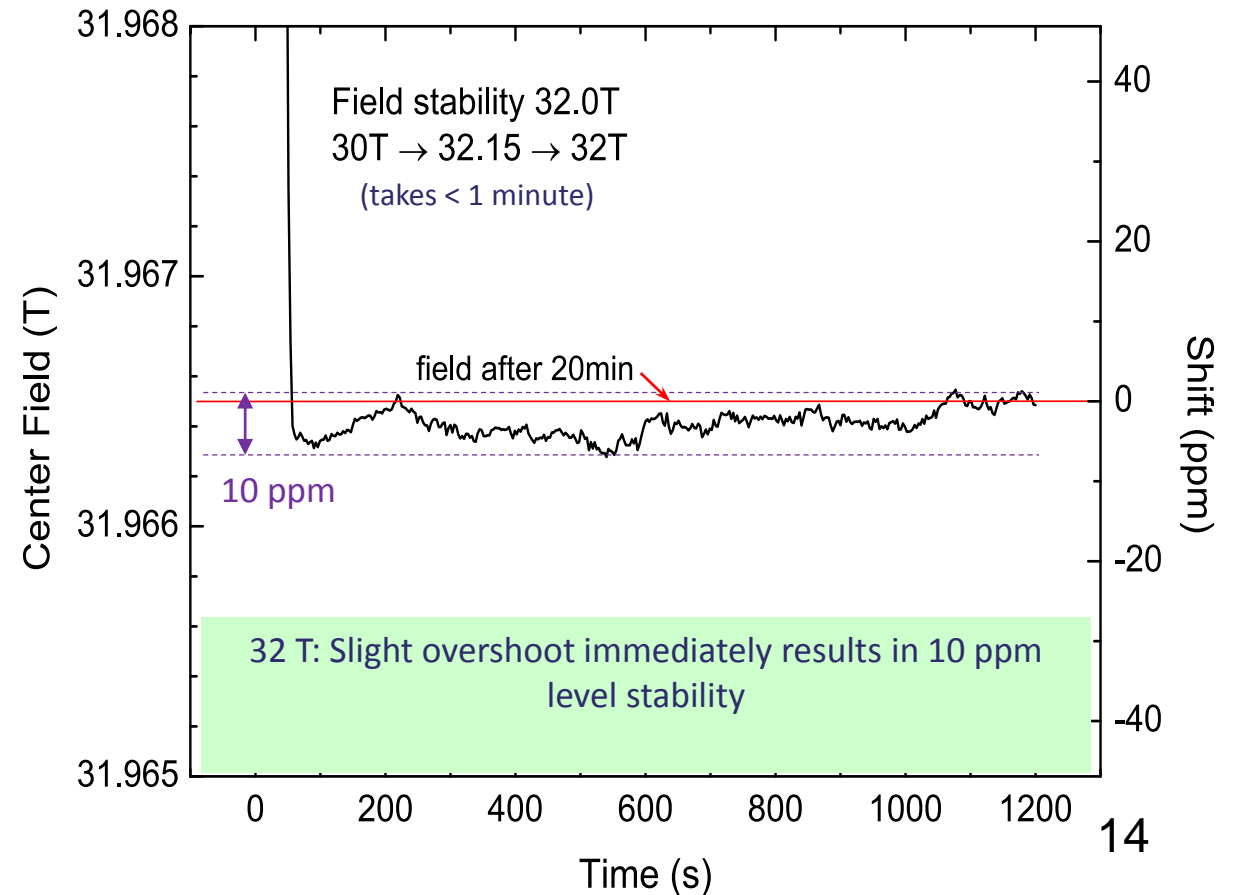
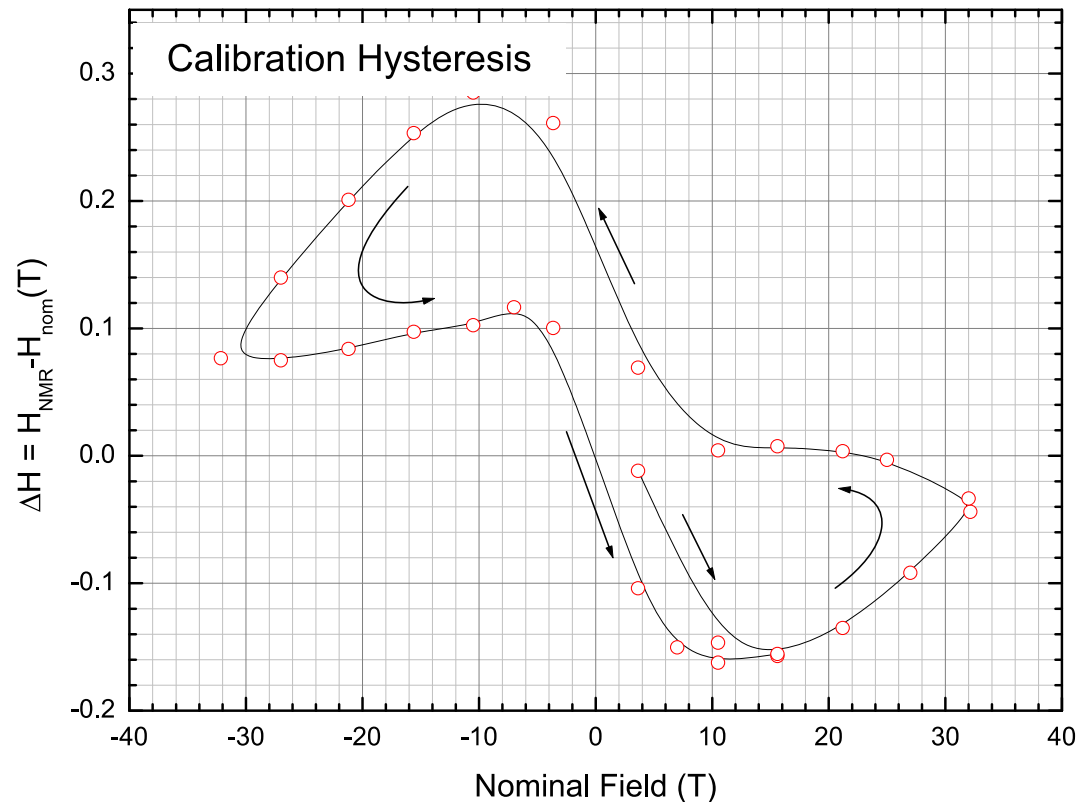
Optical fibers (displacement sensors)

Cryostat top flange  
Air-suspended supports



# Commissioning: Dealing with non-linearity

- Slight overshoot in current mitigates field drift/relaxation to power supply level
- Screening currents cause non-linearity in field-current ratio (<1% field deviation)
  - Available data suggest this is reproducible
  - Plan to measure this further on 32 T to develop prediction algorithm based on  $I$ ,  $dI/dt$  and history
    - Screening current simulations now run faster than real time
    - Augment with field measurement if needed





## Quench protection

- High field REBCO coils do not self-protect against quench (incl. NI)
  - Either energy extraction or distribution is needed
- Distribution means creating normal zones by heating  $\rightarrow T_{CS}$ : Order(kJ/kg)
  - Available time determined by  $J_{ave}$  in windings and quench dynamics
- High  $I_c$  margin  $\rightarrow$  high power density
  - Manageable in 32 T with Battery bank energy source
  - Prefer going to capacitor based Pulse Forming Network

## Screening currents\*

- Cause hysteresis in  $B$  (SCIF) and additional strain (torque)
- High  $I_c$  margin  $\rightarrow$  more screening currents
- 9 cycles (32 T) or  $> 100$  cycles (prototypes) to  $\geq$  design stress/strain: OK
  - Ability to reach 50,000 cycles unproven

## Going forward

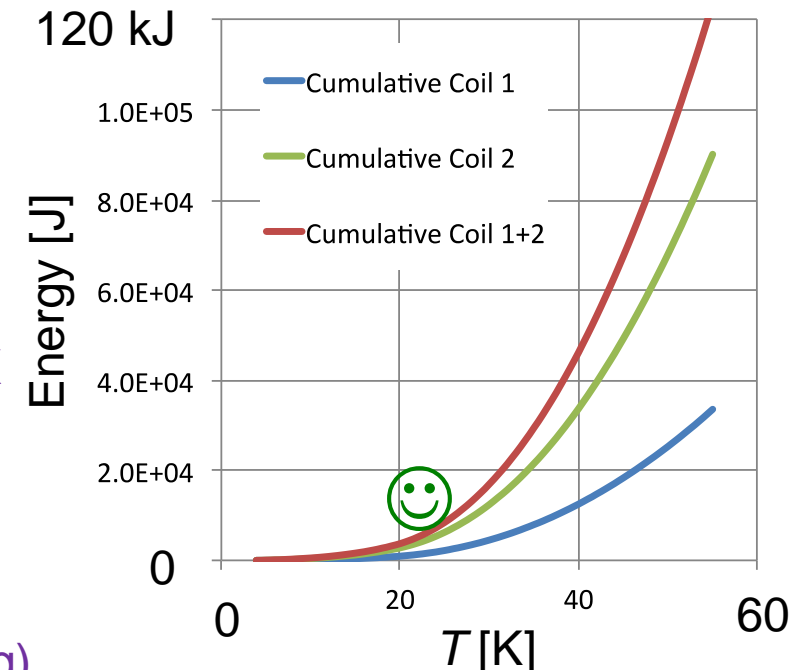
- Magnet designs with specified range and distribution of temperature margin
- Conductor specification with multiple minimums and maximums on  $I_c$  (grading)
- Re-use prototype coil conductor for new fatigue test coil, benchmark simulations

\*: MT26-Fri-Mo-Or27-07 (Edgar Berrospe), also SuST 32 (2019) 065003  
 MT26-Mon-Af-Po1.11-05 (Dylan Kolb-Bond)

Conductor is at 10-33% of  $I_c$  at 32 T  
 $\rightarrow$  margin is 25 to 40<sup>+</sup> K  
 Higher at lower field  $\rightarrow$  ☹️

32T

180 kJ



Energy needed to heat the  
 32 T HTS windings (~80 kg)

32 T magnet tested: reached field repeatedly and met all specifications

- In transition to be the first HTS-LTS superconducting **user magnet** > 30 T
- High-power quench heaters for quench protection
- Magnet is very stable: large  $I_c$  margin, no spontaneous quenches

Key design comments

- **Quench management demonstrated effective**
- **Desirable to engineer  $I_c$  and temperature margins** across coil via conductor grading

Commissioning as user magnet underway in new MilliKelvin facility expansion

Thank you

Questions?