

Progress in the Construction of the HFML 45 T Hybrid Magnet

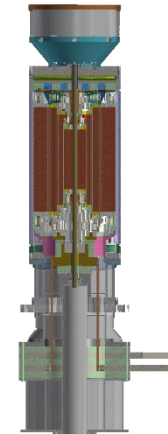
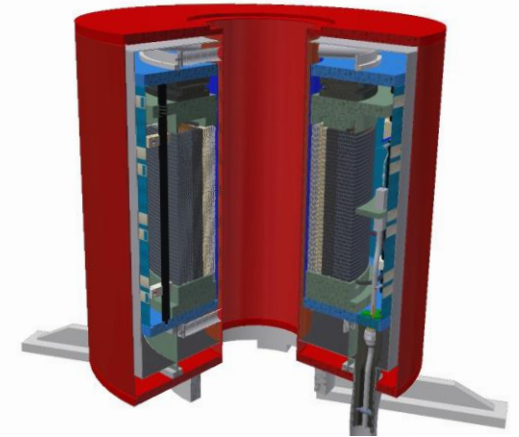
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HFML 45 T Hybrid Magnet program

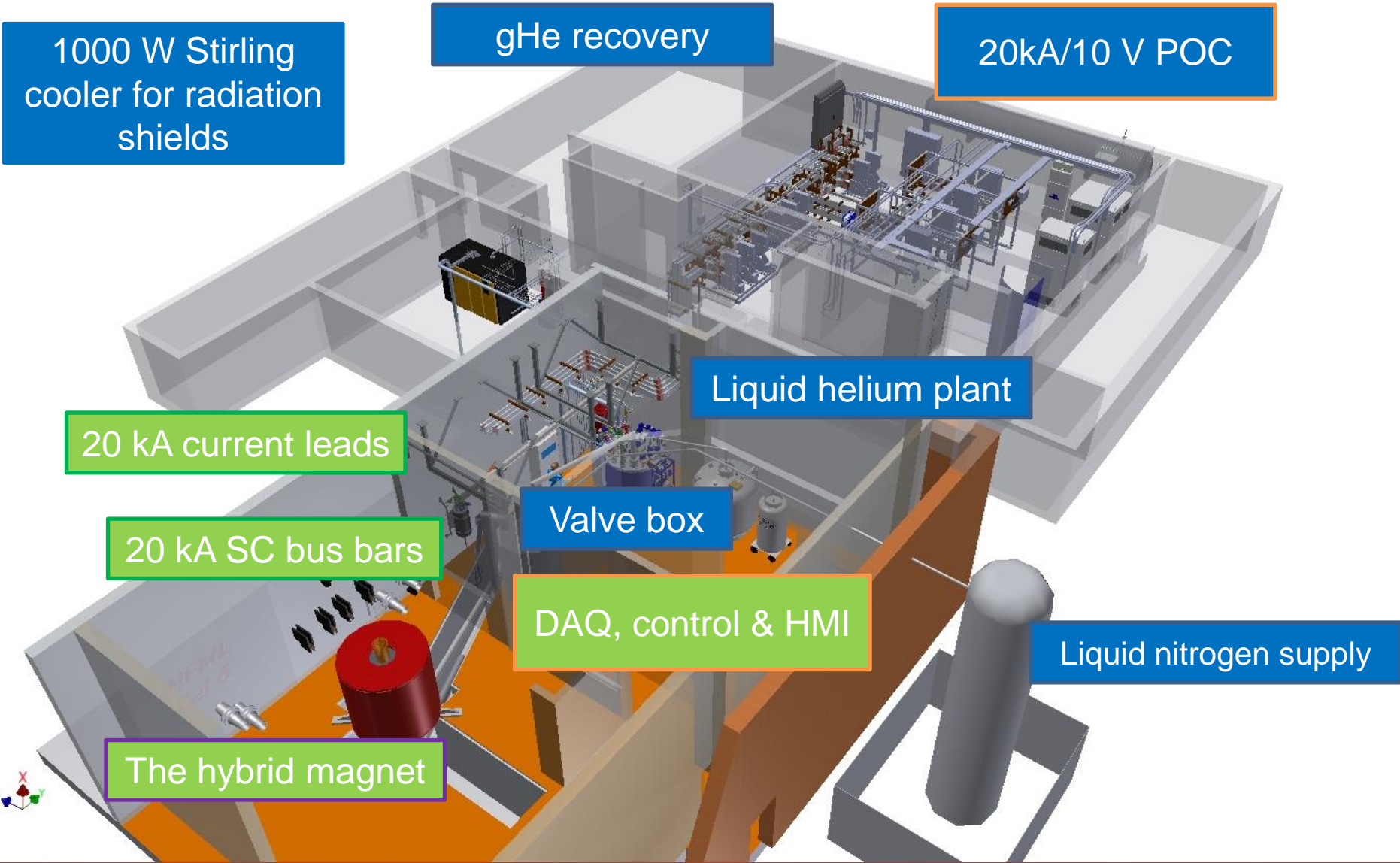
- Combined on-axis field 45 T
- Resistive Florida-Bitter type **insert** magnet generates **33 T** at 40 kA, 22 MW
- Superconducting Nb₃Sn-CICC based **outsert** magnet delivers **12.3 T** at 20 kA
- Insert bore 32 mm, outsert RT bore 620 mm



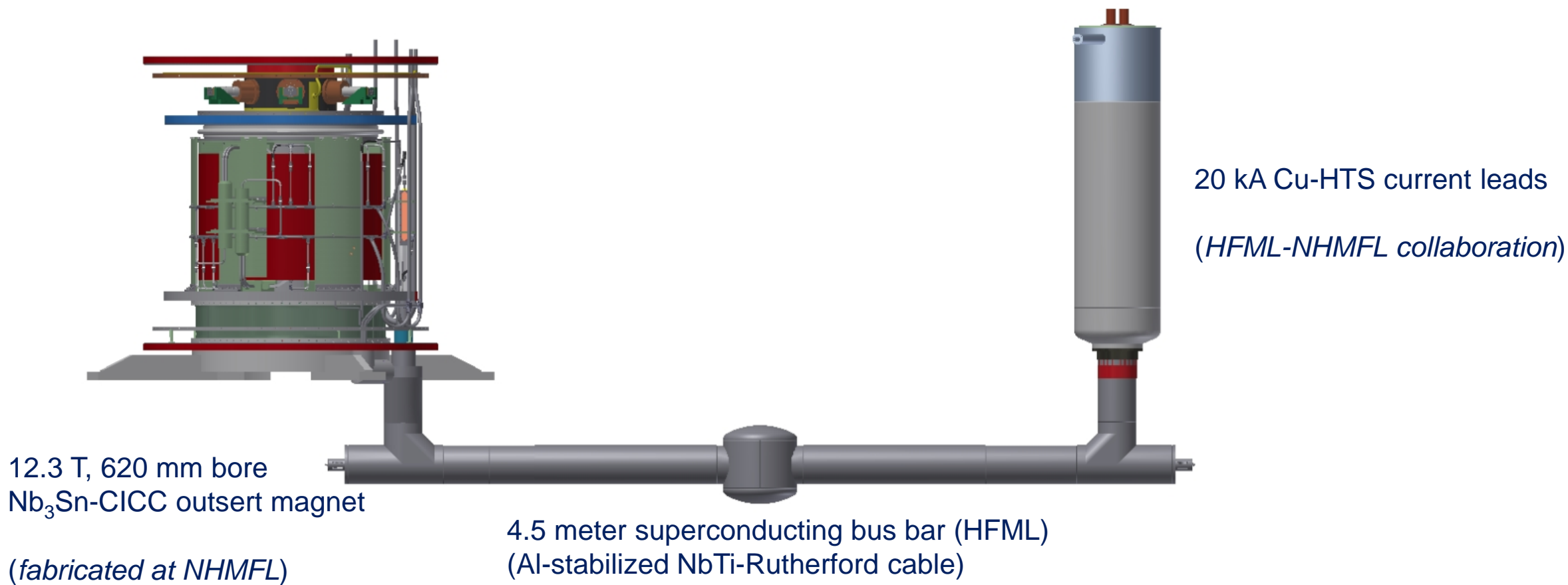
Collaboration with US-NHMFL (SCH program)

- common CICC design, outsert coil design & fabrication
- Cu-HTS current lead development

Hybrid Magnet SYSTEM



Superconducting outsert circuit HFML 45 T hybrid magnet



Outsert 20kA power converter

(protection breakers, dump resistors and bus bars to magnet cell)

(manufactured by Ampulz B.V., The Netherlands)

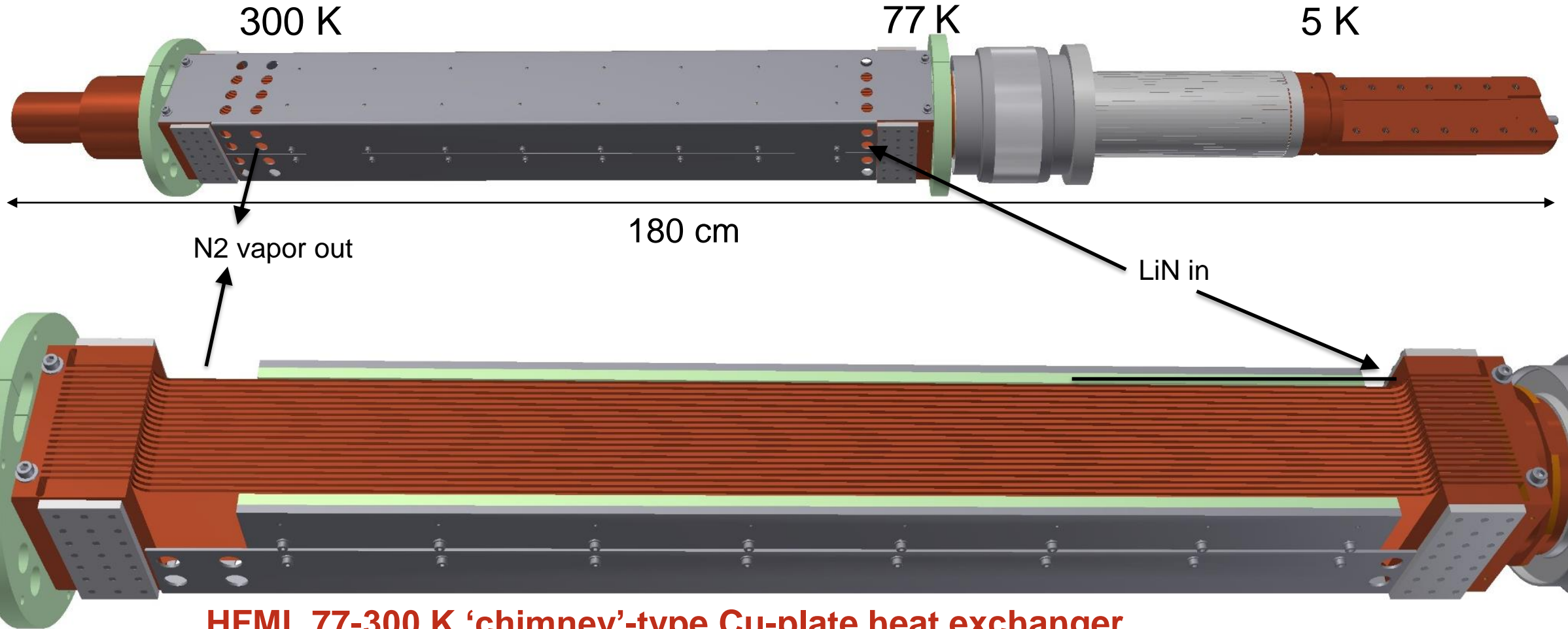


Installation, test and commissioning
July 2015



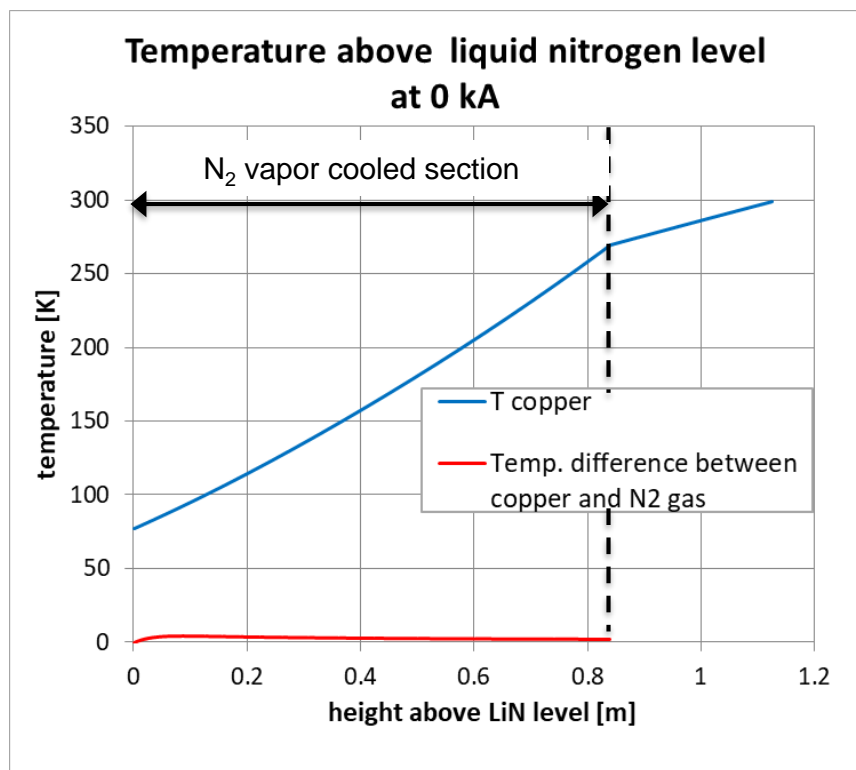
20kA, binary Cu-HTS (Bi2223), LiN cooled current leads

(in collaboration with NHMFL, USA)

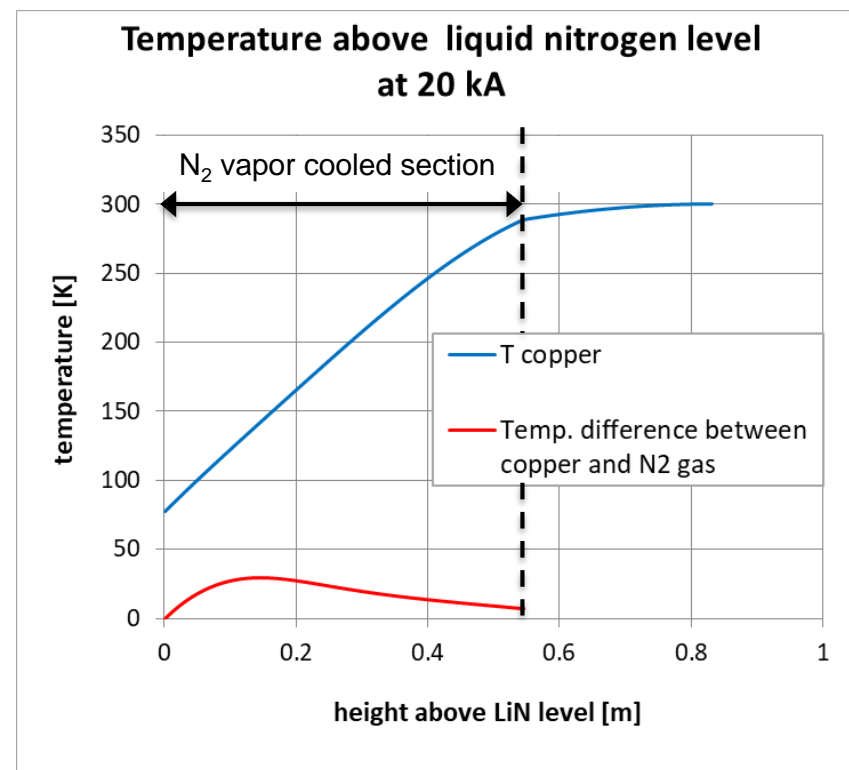


HFML 77-300 K 'chimney'-type Cu-plate heat exchanger

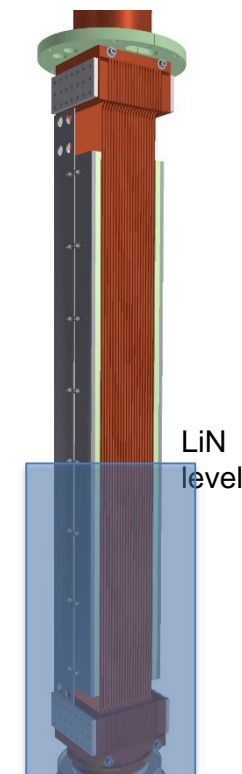
Calculated temperature profiles resistive section (RRR ~ 5, $T_{\text{warm}} = 300$ K)



$I = 0$ kA
 $P_{\text{cold}} = 167$ W/lead
 $P_{\text{warm}} = 335$ W/lead



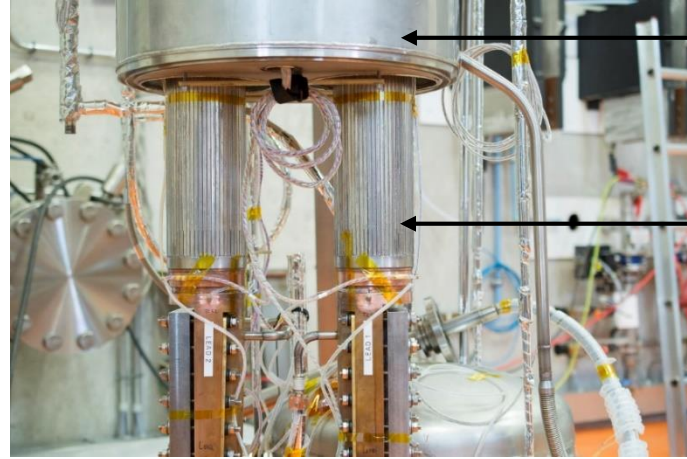
$I = 20$ kA
 $V_{\text{resistive}} = 47$ mV
 $P_{\text{cold}} = 620$ W/lead (14 litre LiN/h)
 $P_{\text{warm}} = 2$ W/lead



20kA Cu-HTS, LiN cooled current leads

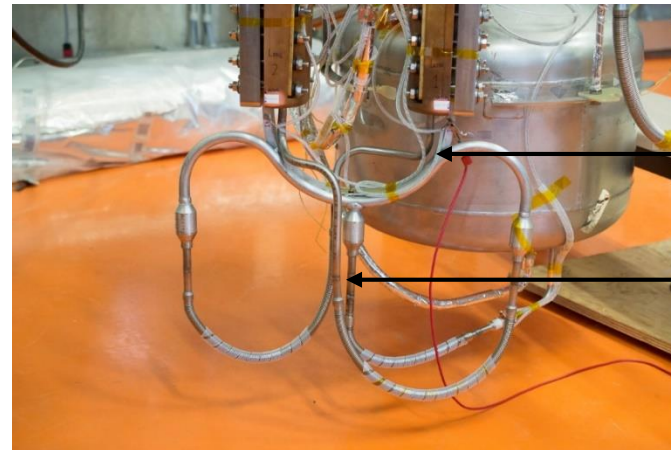


Test and commissioning 2018
Ready for integration into CL
cryostat



LiN vessel Cu-HEX

BiSrCaCuO(2223) section



Al stabilized NbTi jumper

Supercritical helium cooling
channel @ 6 bar, 5 K

Cryogenic components



Aluminium 20 kA bus bars

Cryo-line to Stirling cryo-cooler

Current leads location

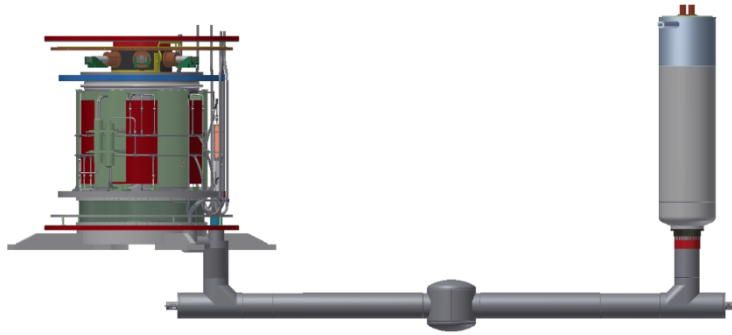
Cryo-line valve box -
magnet cryostat

Valve & distribution box

Helium refrigerator/
liquefier in operation

All components ready for
testing and integration

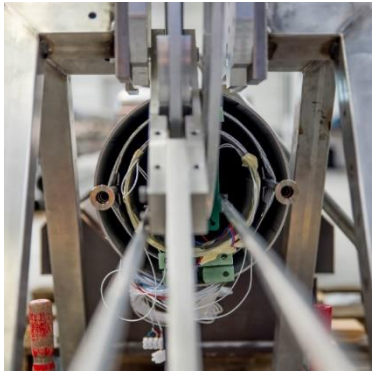
Superconducting bus bars between current leads and cryostat (in collaboration with Cryoworld B.V., the Netherlands)



Actively cooled Al-stabilized NbTi Rutherford cable
(CERN-ATLAS ECT grade, 5T, 4.2 K, 60 kA)

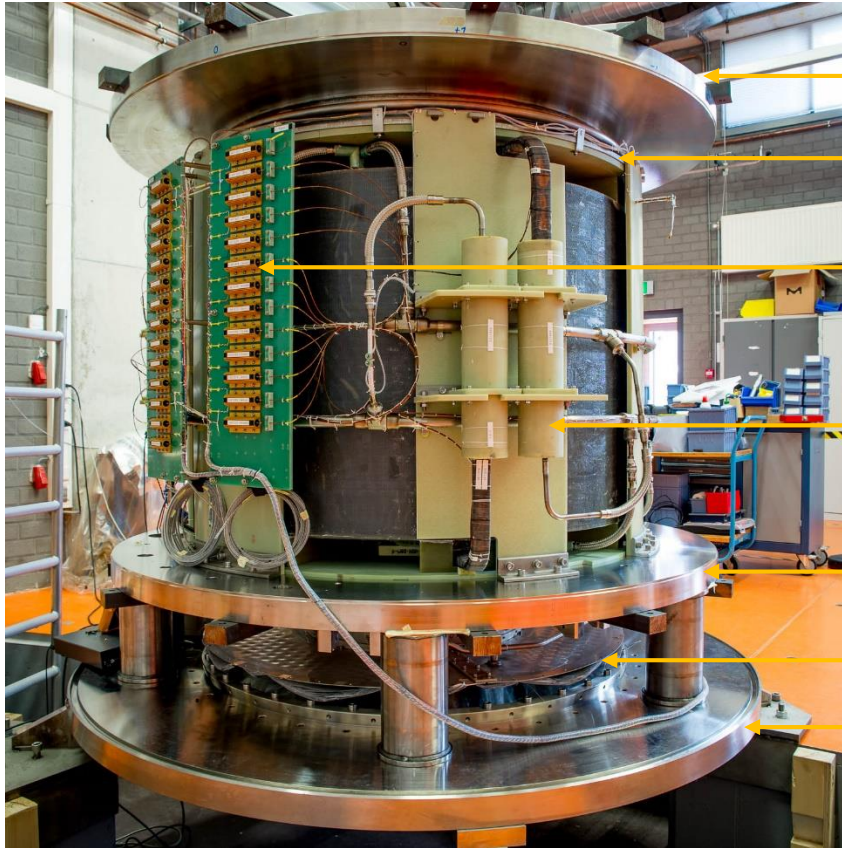


Thermal strain relief



Superconducting Quench
Detector (developed at CERN)

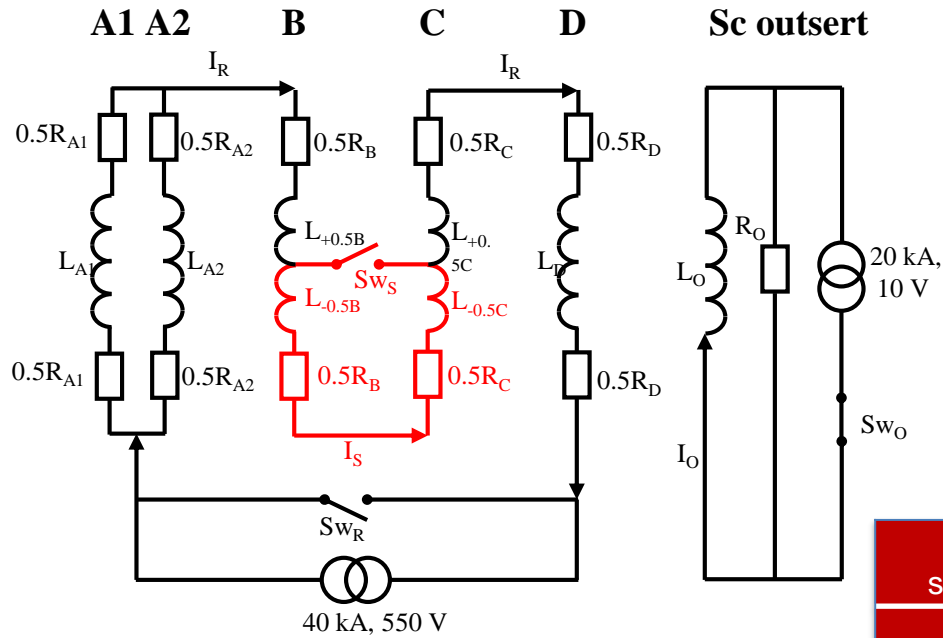
12.3 T Nb₃Sn-CICC superconducting outsert magnet



- Top plate magnet vessel (1 bar He gas @ 4.5 K)
- 4.5K and 18 bar helium filled pre-compression bellow
- current limiting resistors (13 k Ω) voltage tap wiring
- Section joint box
- Bottom plate magnet vessel
- Pillow plate bottom radiation shield
- Bottom plate vacuum vessel

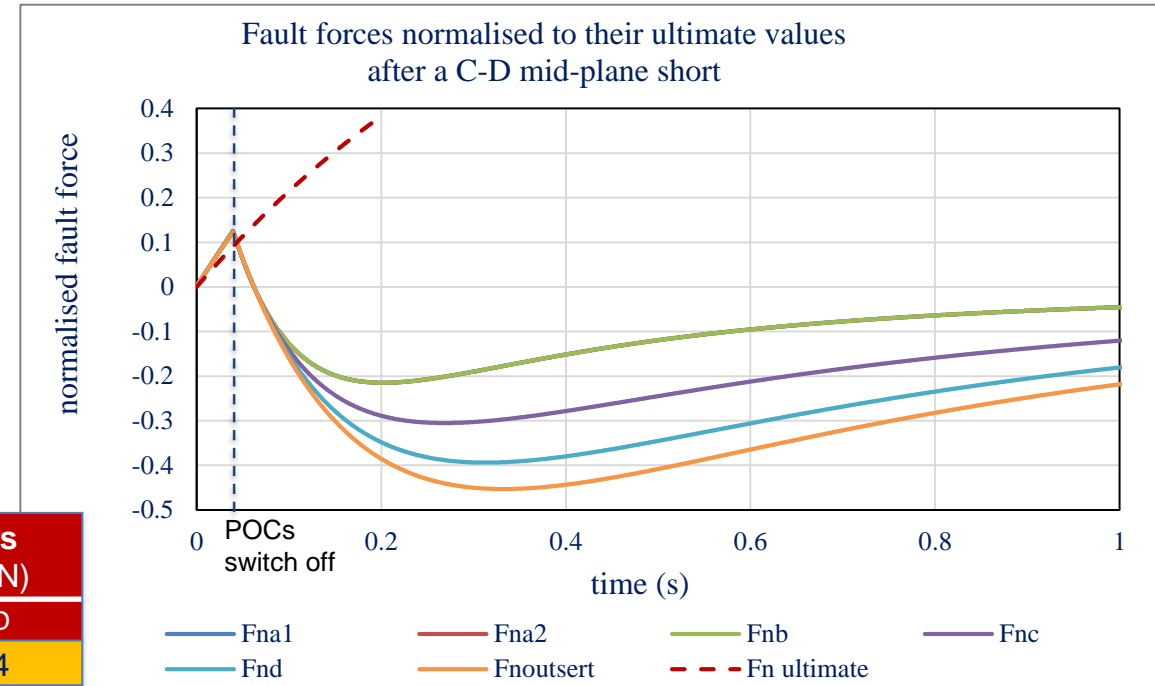
Coil manufacturing by NHMFL completed in 2018
Integration in cryostat well underway
All parts of cryostat have been manufactured

Axial fault forces after insert coil failure (Presented Tue-Po2.15-03)



PROPERTIES INSERT COILS					
	A1	A2	B	C	D
operating current (kA)	13	27	40	40	40
current density (A/mm ²)	603	345	214	111	95
power density (W/mm ³)	9.9	3.1	1.2	0.23	0.17
uncooled heating rate (K/s)	2868	900	338	67	50
voltage drop (V/winding)	2.0	2.0	2.7	1.6	2.1

Ultimate static fault forces shorted coils at mid-plane (kN)		
	B-C	C-D
A1	83	-54
A2	600	-389
B	-1032	-1383
C	-1829	1694
D	1274	2988
Outsert	903	-2856



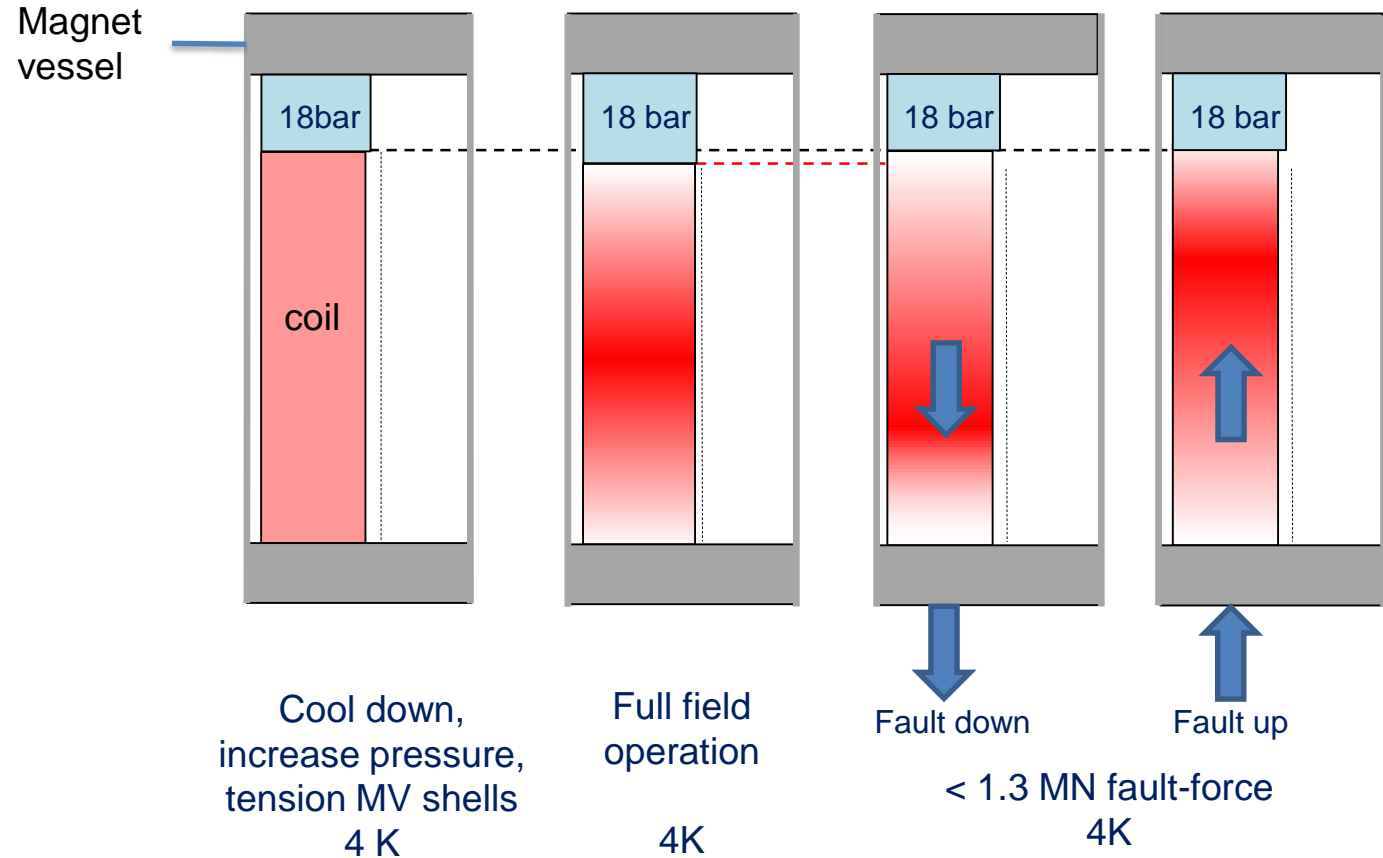
- If coil protection systems work properly:
- Fault forces stay well within 50% of ultimate
 - Fault forces change sign = direction

Axial support handling fault forces outsert: HFML approach

During an insert fault a constant stress in inner & outer shell of Magnet Vessel at 4.5 K is maintained with a pressurised helium gas bellow ($p_{op} < 30$ bar)

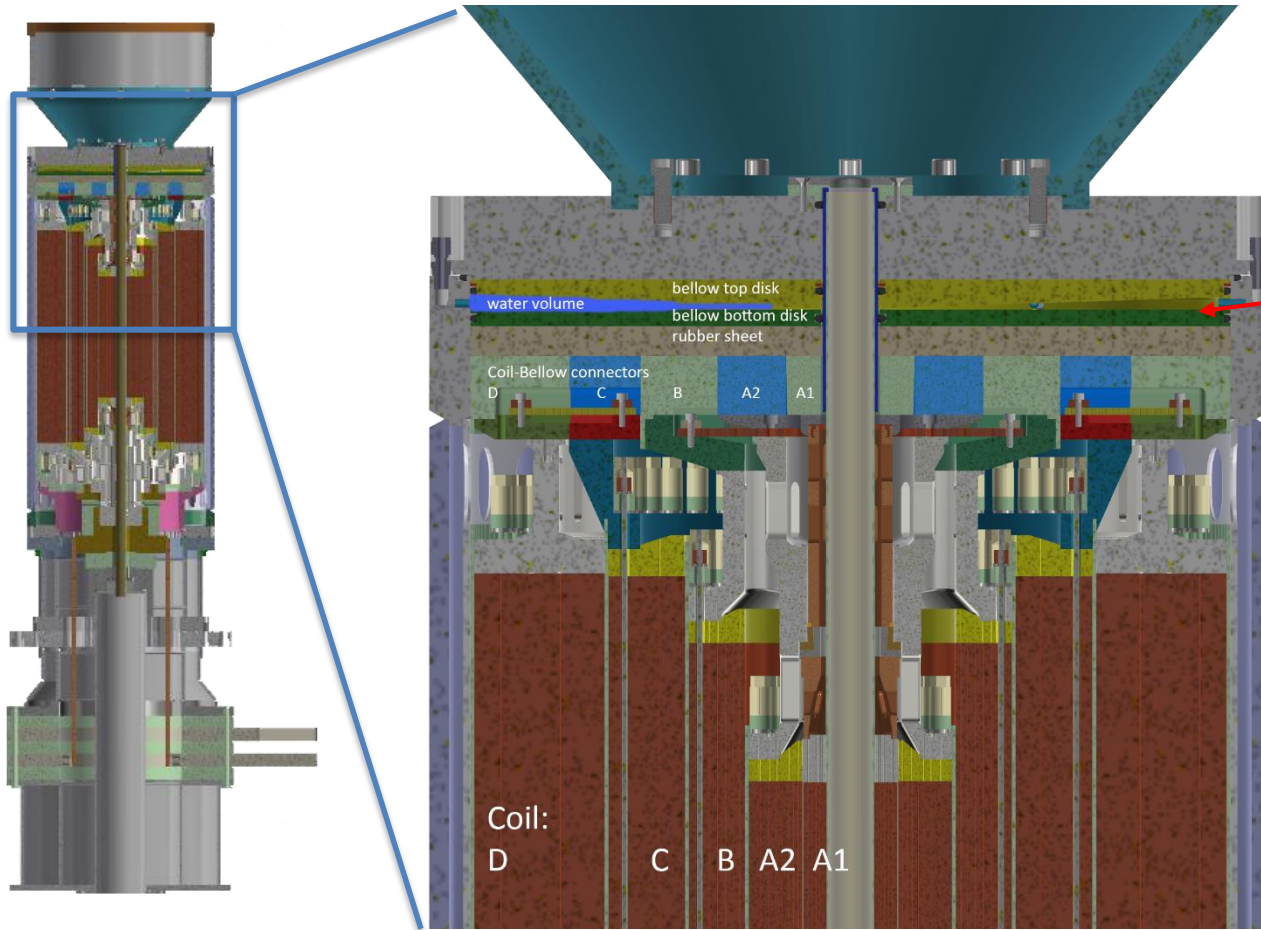


Force constant: 73 kN/bar
Axial stiffness: 17 kN/mm
Lateral stiffness: 1.2 MN/mm
Minimum gas volume: 7 dm³



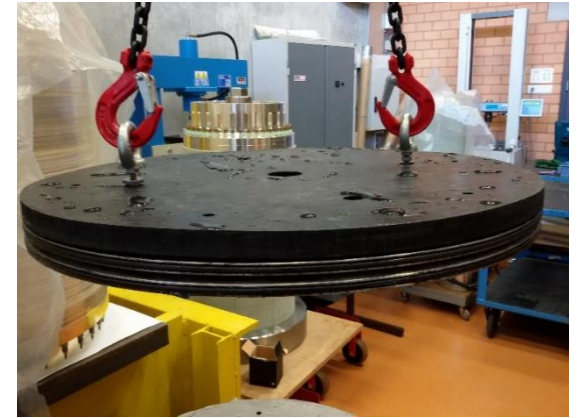
33 T Florida-Bitter insert magnet (40 kA, 22 MW)

(presented Tue-Po2.15-02)



100 bar hydraulic pre-compression 'bellow'

- Mitigates end-turn issues
- Sustains axial fault forces



Mock-up test hydraulic bellow

All insert coil components being purchased

Summary

Key components for the outsert magnet nearly ready for integration

Insert components are being purchased or manufactured

Control & monitoring systems in production
(quench detection, cryogenics, magnet operation)

Commissioning expected to start mid 2020

Acknowledgements

This work is supported in part by the NWO-BIG program of the Netherlands Foundation for Scientific Research NWO

HFML

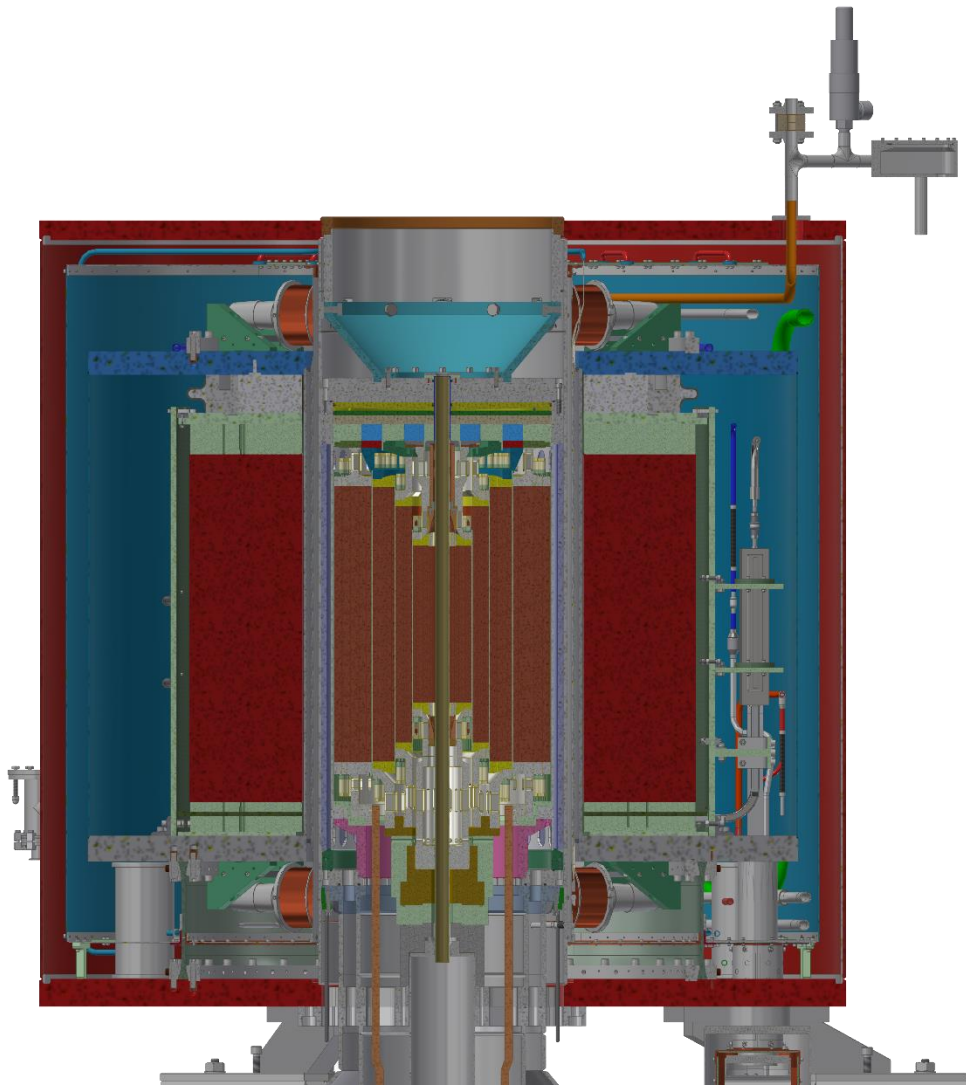
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S. Bole and technical staff

Technical Advisory Committee

H. ten Kate (UT-CERN), A. Bonito-Oliva (F4E),
P. Bruzzone (EPFL/CRPP) and U. Wagner (CERN)



	Insert	Outsert
operating current I_i, I_o (A)	40,000	20,000
contribution to central field (T)	32.7	12.3
free RT bore diameter (mm)	32	600
expected # powering cycles	30,000	3,000
cooling medium	forced flow water (~ 140 l/s)	forced flow supercritical helium (~ 11 g/s@5 bar)
operating temperature T_{op} (K)	< 360	4.6
self inductance (mH)	5	266
mutual inductance (mH)	11	11
(dump) resistance R_i, R_o (m Ω)	15	130/2.5
decay time constant (L/R) (s)	0.3	2.0/106
required power (MW)	21.5	0.2
stored energy (MJ)	5	55