

A Design Study on No-Insulation HTS 385 MeV/u Isochronous Cyclotron Magnet for Carbon Ion Therapy

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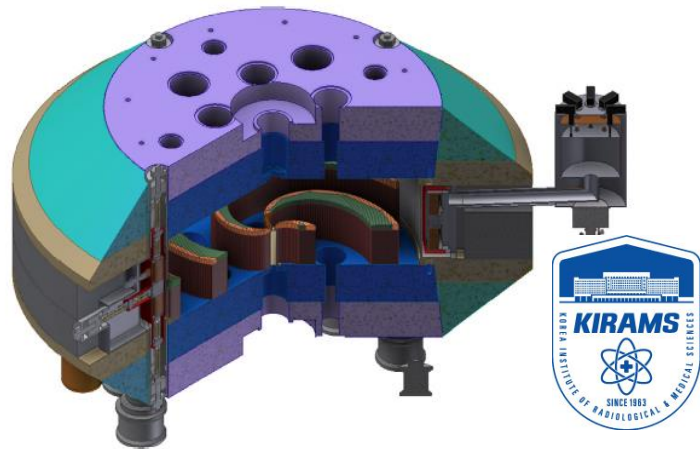
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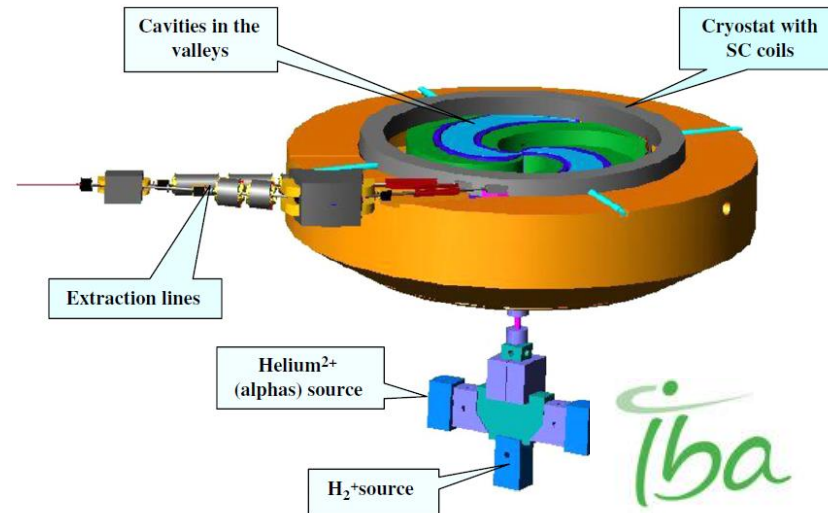
1.1 Former Studies on Carbon Ion Accelerator for Cancer Treatment

■ Cyclotron

- Carbon cyclotron has not been built yet. (C400, KIRAMS430 designs are presented)
- (1) Small space
- (2) DC operation: simple control
- (3) Continuous beam



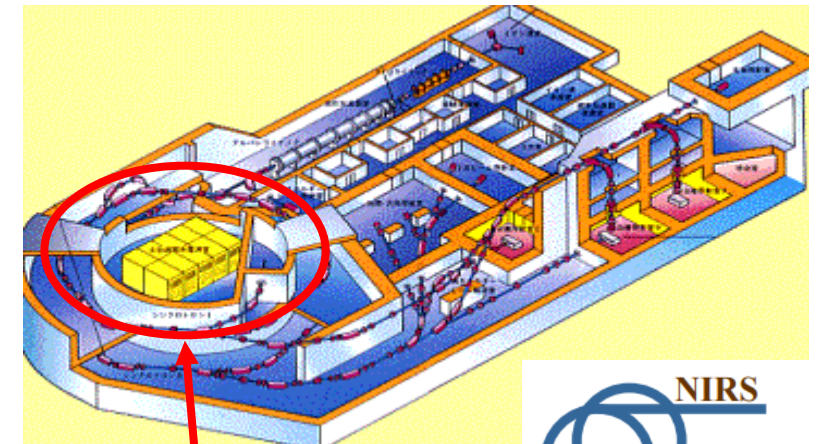
Ref: H. W. kim *et al.*, "Design study of the KIRAMS-430 superconducting cyclotron magnet," *Nucl. Inst. Methods Pys. Res.*, A 823 (2016), 26-31



Ref: Y. Jongen *et al.*, "Compact superconducting cyclotron C 400 for hadron therapy," *Nucl. Inst. Methods Pys. Res.*, A 823 (2010), 47-53

■ Synchrotron

- Several systems are available (HIMAC, HIT...)
- (1) Large space
- (2) AC operation: complex control
- (3) Discontinuous beam



Synchrotron system

Ref: https://www.nirs.qst.go.jp/ENG/rd/1ban/himac_inf.html

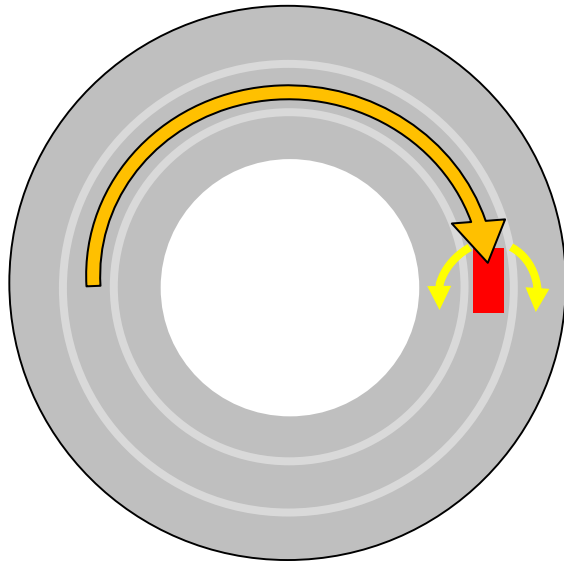
Current systems are constructed (or designed) with Cu (or LTS) technology

1.2 Key Concepts: No Insulation (NI) / Multi-Width (MW) / Cryocooling

■ No-Insulation (NI)

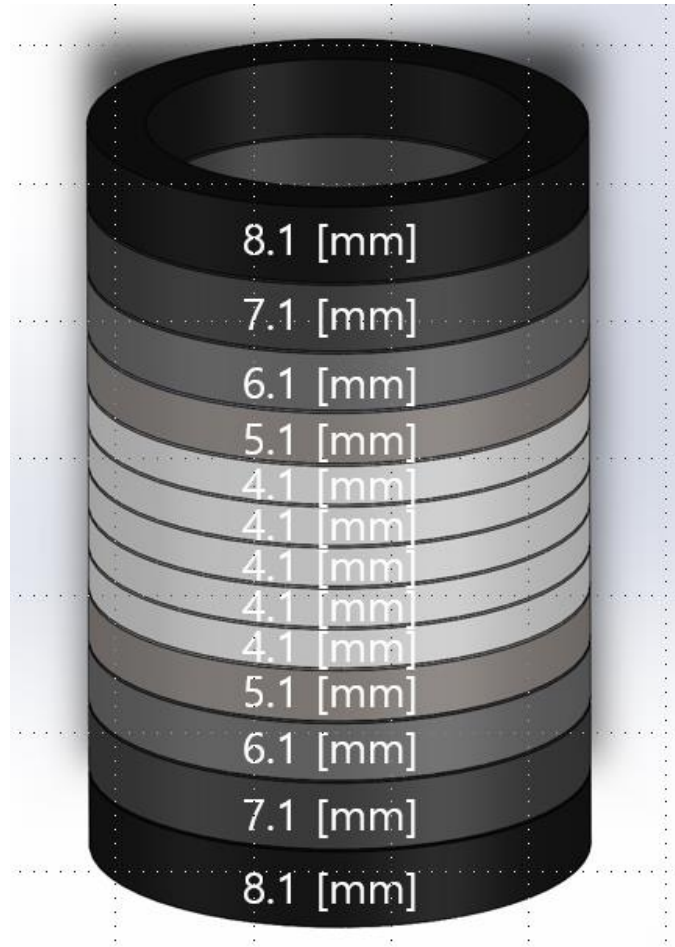
- 1. Excellent protection
- 2. High mechanical intensity
- 3. High current density

NI: "Quench Current Bypass"



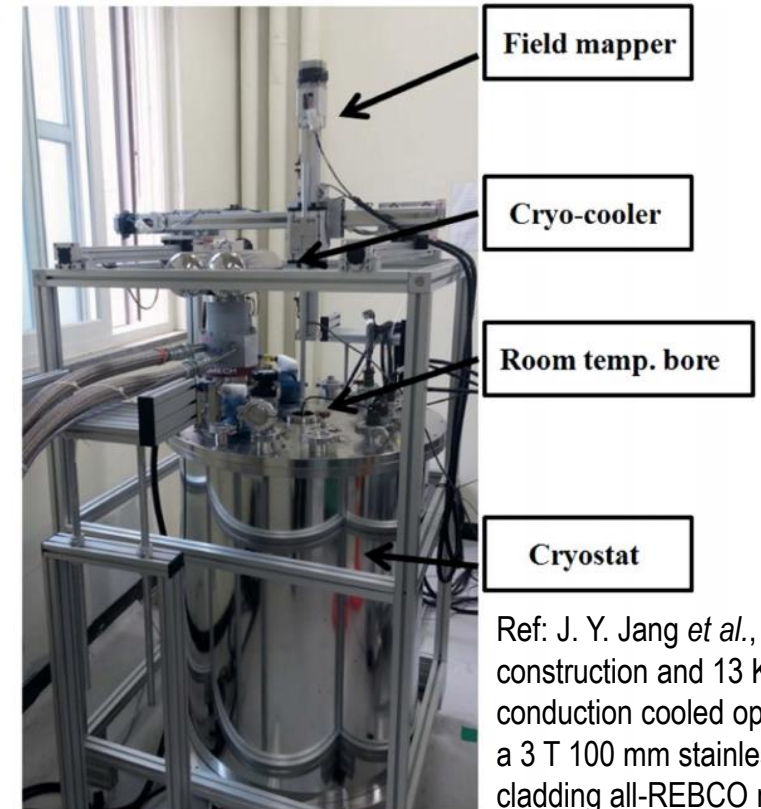
■ Multi-Width (MW)

Minimization of conductor usage



■ Cryocooling: 20 K operation

- 1. Helium free cryogenic system
- 2. >100 stability margin than LTS



Ref: J. Y. Jang *et al.*, "Design, construction and 13 K conduction cooled operation of a 3 T 100 mm stainless steel cladding all-REBCO magnet," *Supercond. Sci. Technol.*, 30, (2017), 105012

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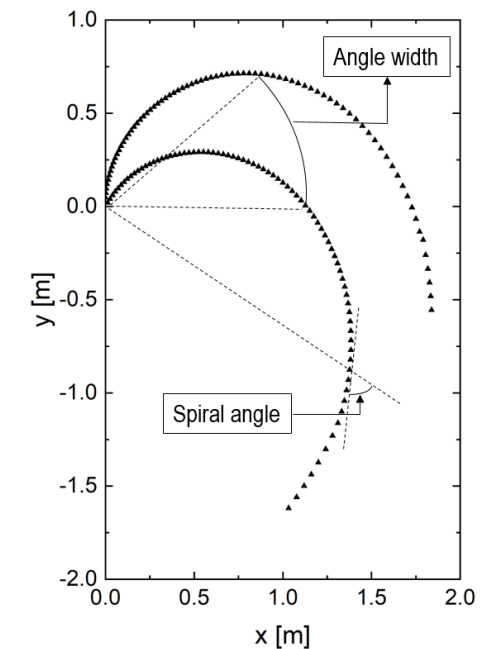
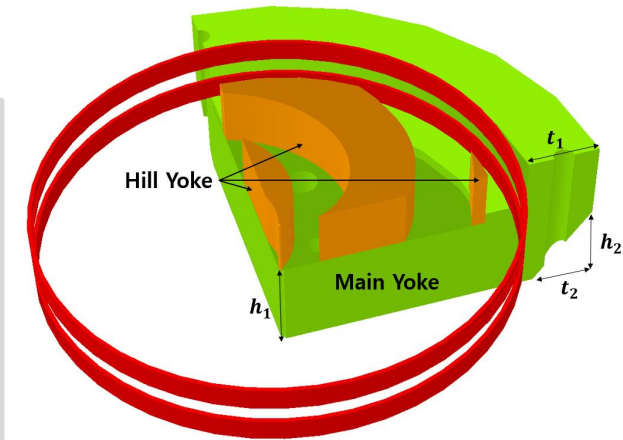
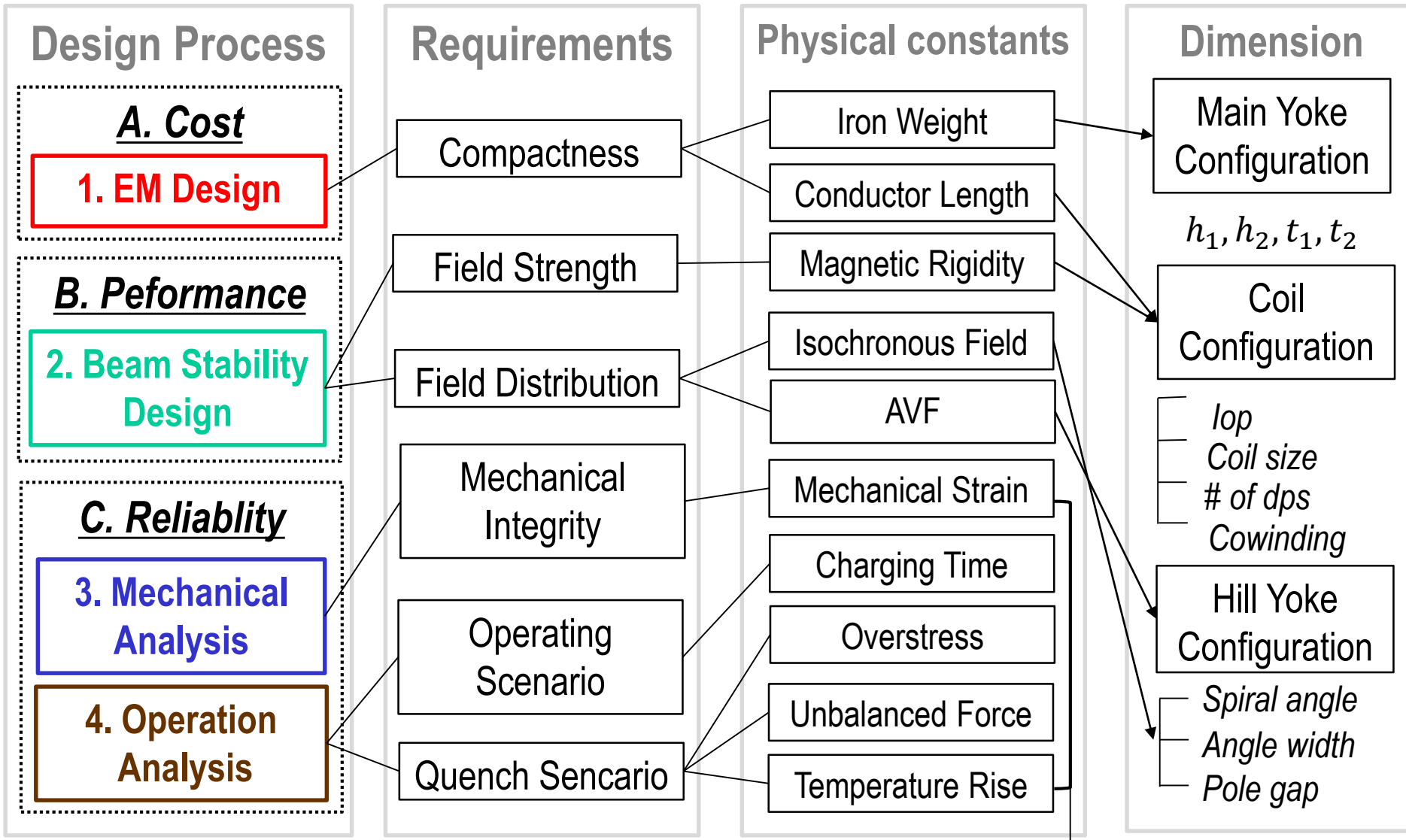
3.3 Operation Analysis: Charging Scenario with NI Characteristic Considered

3.4 Quench Analysis: Temperature Rise & Unbalanced Force

4. Summary: 385 MeV/u NI-HTS Magnet (6.2 m OD; 540 tons; 20 K)

2.1 Overview Table: Requirements & Physical Constants & Dimension

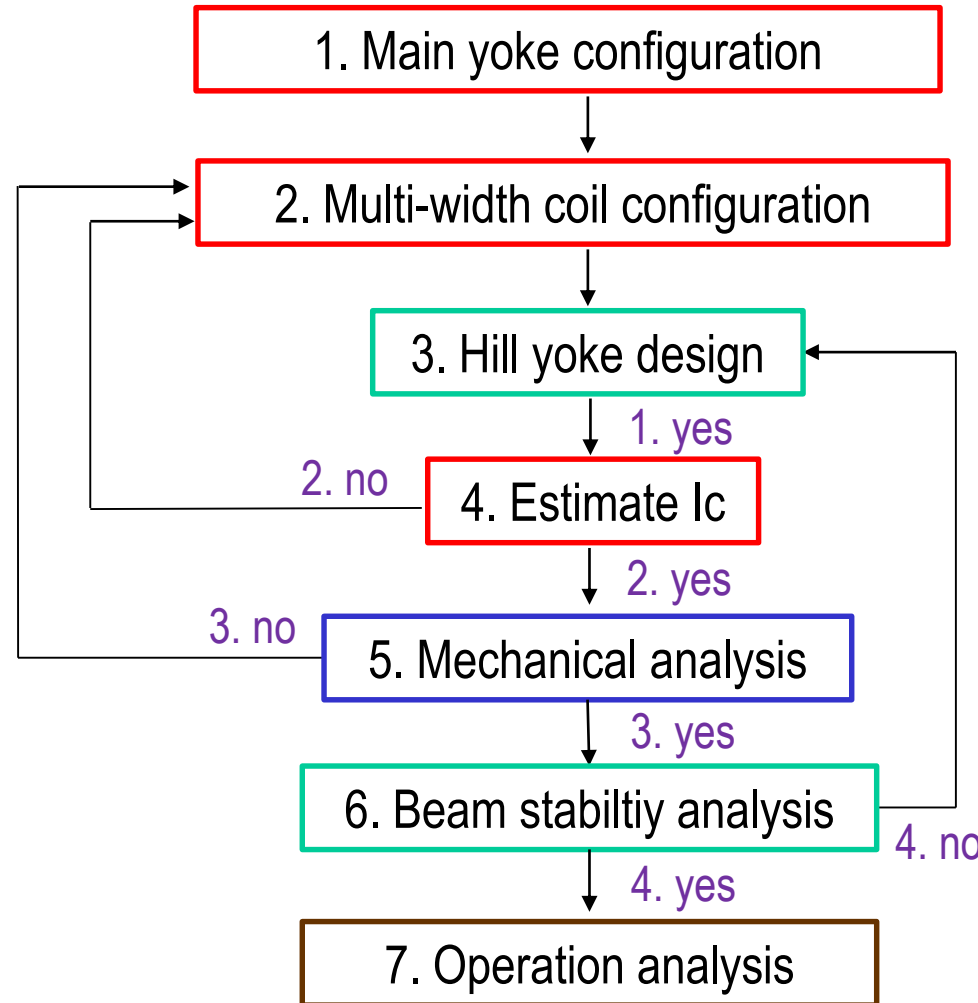
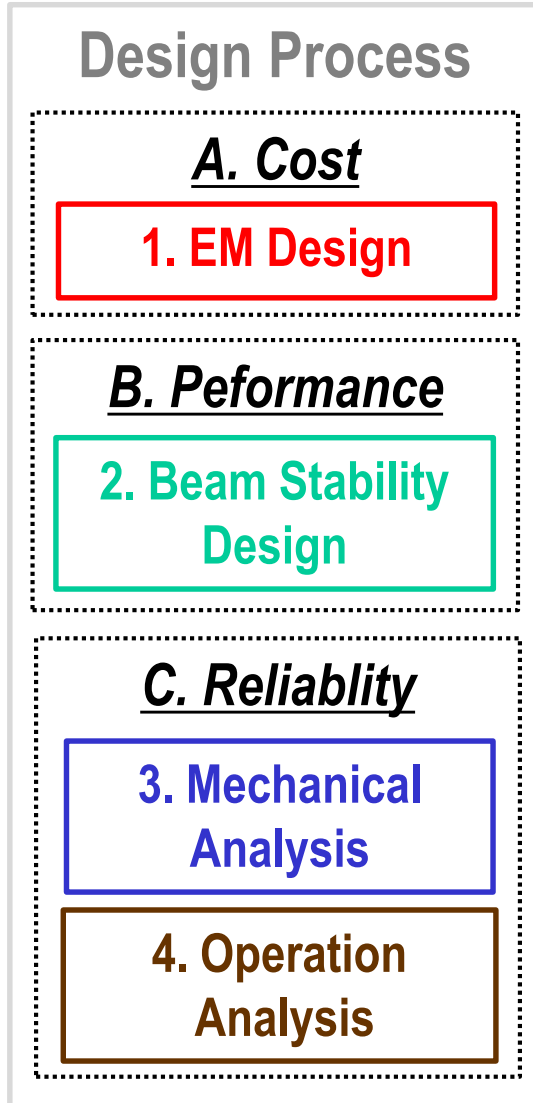
- 3 Considerations: (A) Cost (B) Performance (C) Reliability



Analysis from field distribution & coil parameters

2.2 Design Process: Design Flowchart

7 Steps for Specified Design Process



Constraints

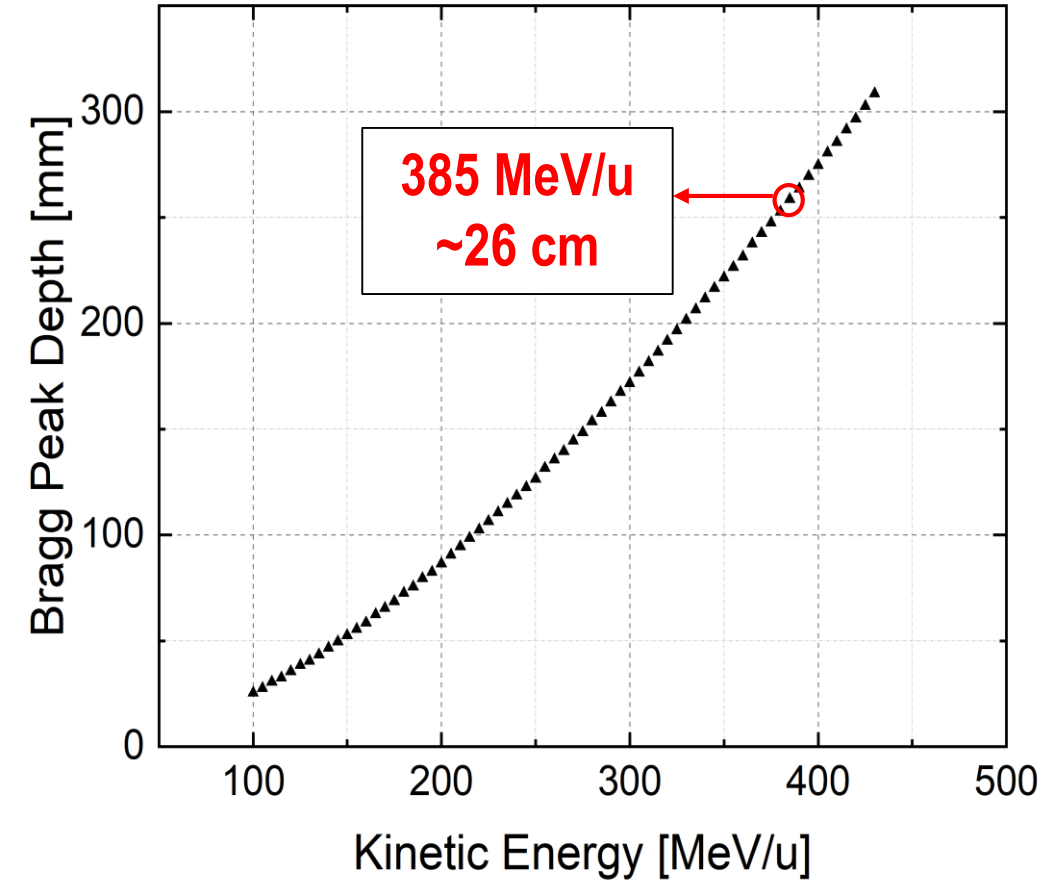
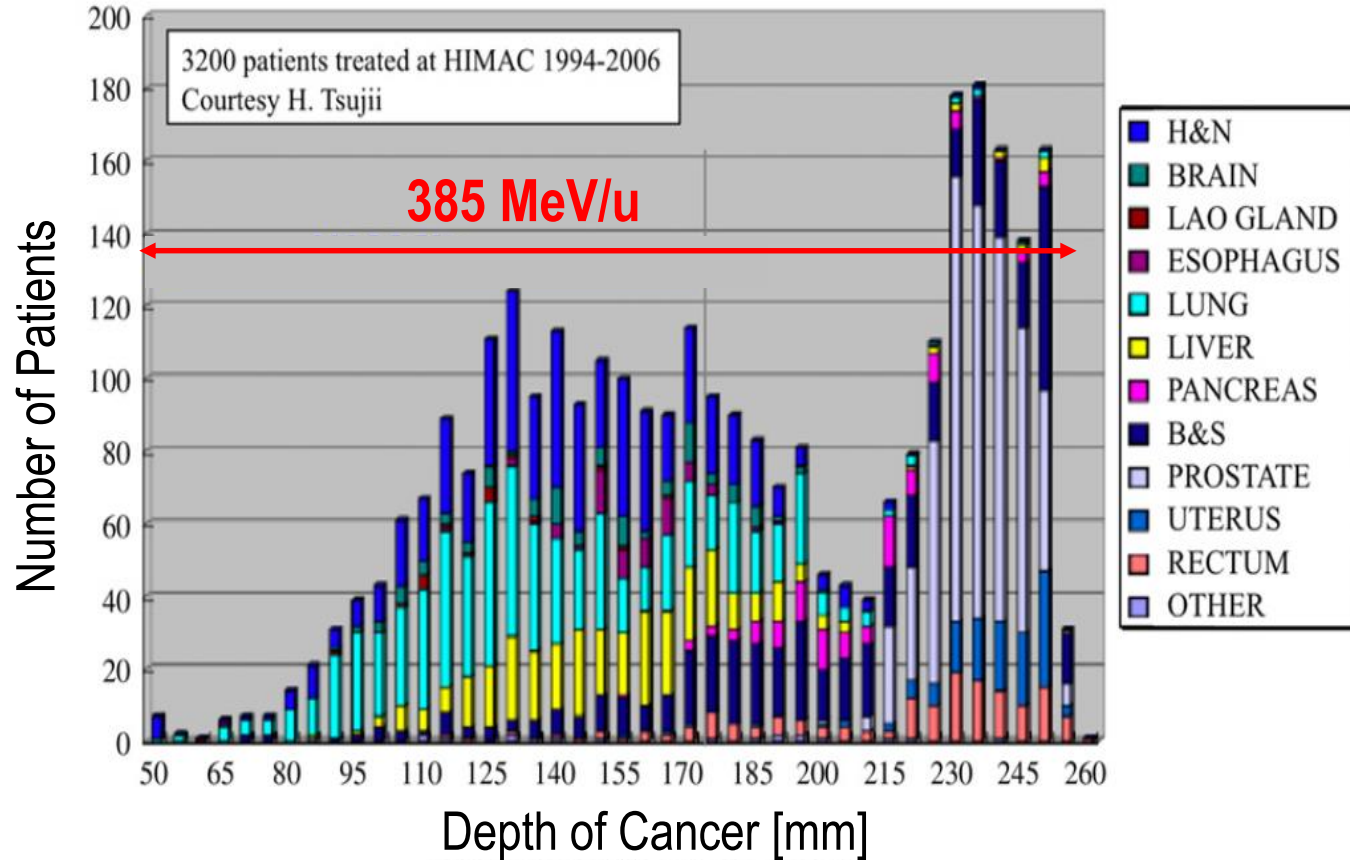
1. $|B_{cal}-B_{iso}| < 10 \text{ gauss}$
2. $(I_{op} < 0.8 I_c)$
3. $Strain < 0.4\%$
4. *Stable beam dynamics*

Keywords for each design steps

- 1: Parameter sweep method
- 2: Gauss-Newton method
- 3: Isochronous field
- 4 : $I_c(|B, \theta, 20 \text{ K}|)$
- 5 : Strain
- 6 : Tune diagram
- 7 : Charging delay & quench analysis

2.3 Design Target: Extraction Energy of 385 MeV/u

- Why 385 MeV/u? : To treat cancer deep in ~26 cm
- Depth Distribution of Cancer for Patients at HIMAC
- GEANT4 Simulation Results



Ref) U. Amaldi *et al.*, "Accelerators for hadrontherapy: from Lawrence cyclotrons to linacs," *Nucl. Inst. Methods Phys. Res., A* 620 (2010), 563-577

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3.1.1 Electromagnetic Design: Parameter Sweep for Main Yoke

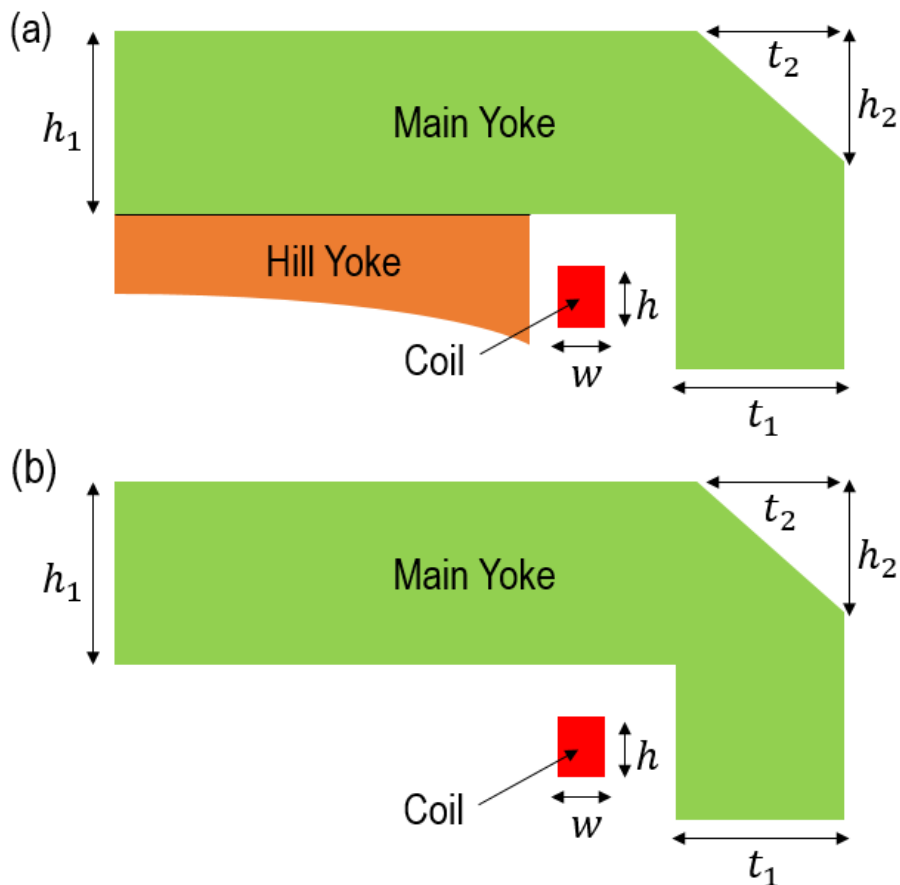
■ Main yoke Configuration: Ampere Turn vs. Main Yoke Weight

□ Simplified 2D Axisymmetric Model

□ Gauss-Newton Method

$$B_{app}^{3D}(r) = \alpha(r)B_h(r) + (1 - \alpha(r))B_v(r)$$

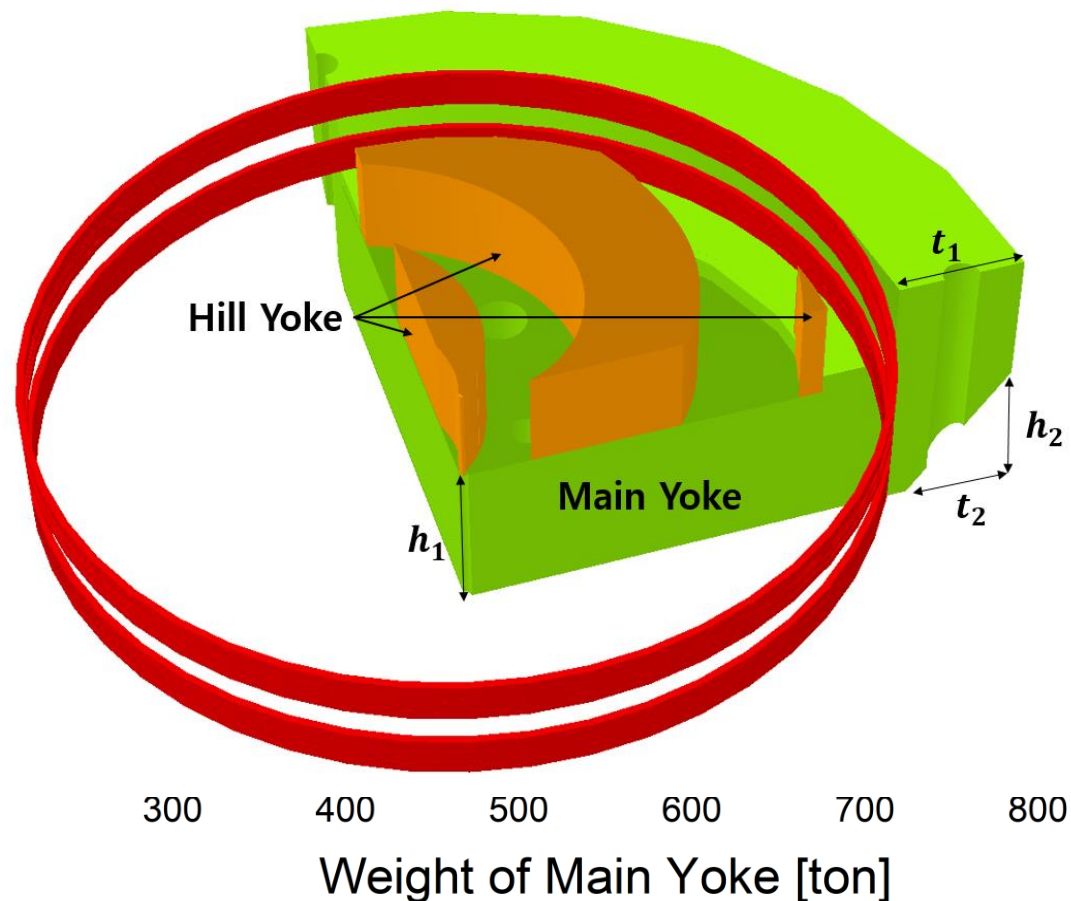
$B_h(r), B_v(r)$: field at (a) and (b) / α : arbitrary hill ratio



Sweeping Parameters
$h_1 : [0.6 \ 0.05 \ 1.2]$
$t_1 : [0.6 \ 0.05 \ 1.0]$
$r : [0.6 \ 0.1 \ 1]$
$(= t_2/t_1 = h_2/h_1)$
Gauss-Newton Parameters
h, w

$$f = \sum_{i=1}^n |B_{app}^{3D}(r_i) - B_{iso}(r_i, h, w)|^2$$

where $B_{iso}(r_i, h, w) = \frac{m_0 c}{4\pi r_i^2}$



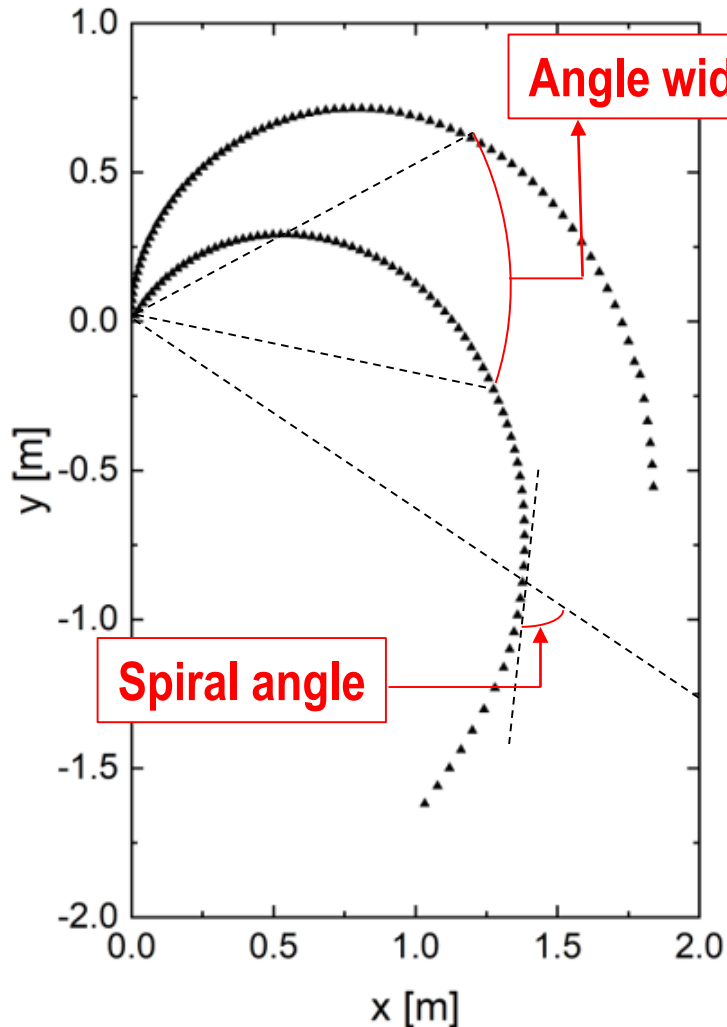
3.1.2 Electromagnetic Design: Hill Yoke Design toward Isochronous Field

■ Hill yoke Configuration: Shaped by Controlling Angle Width & Spiral Angle

□ Mapping Points on xy Plane

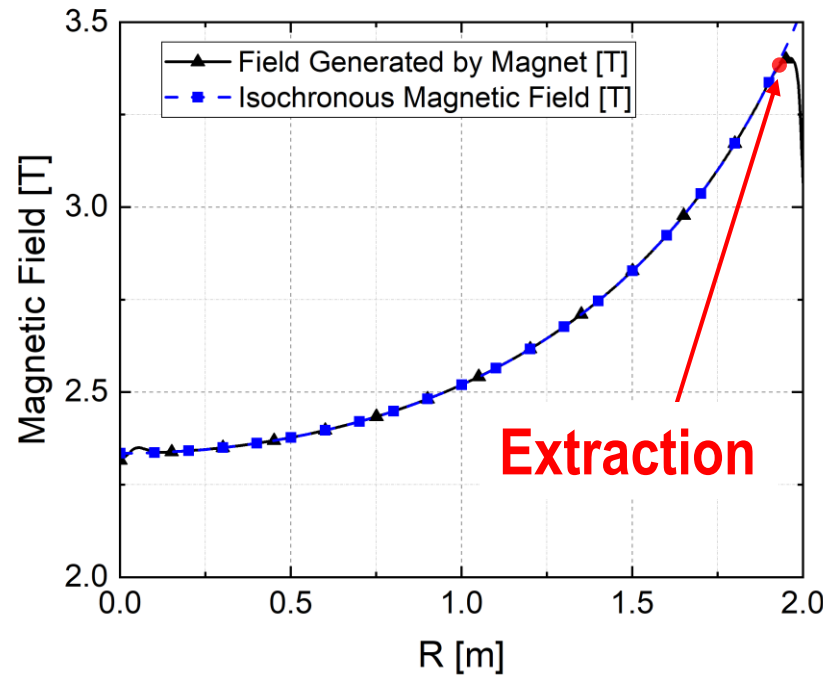
□ Field Distribution

□ Tune Diagram: using "Cyclone" code

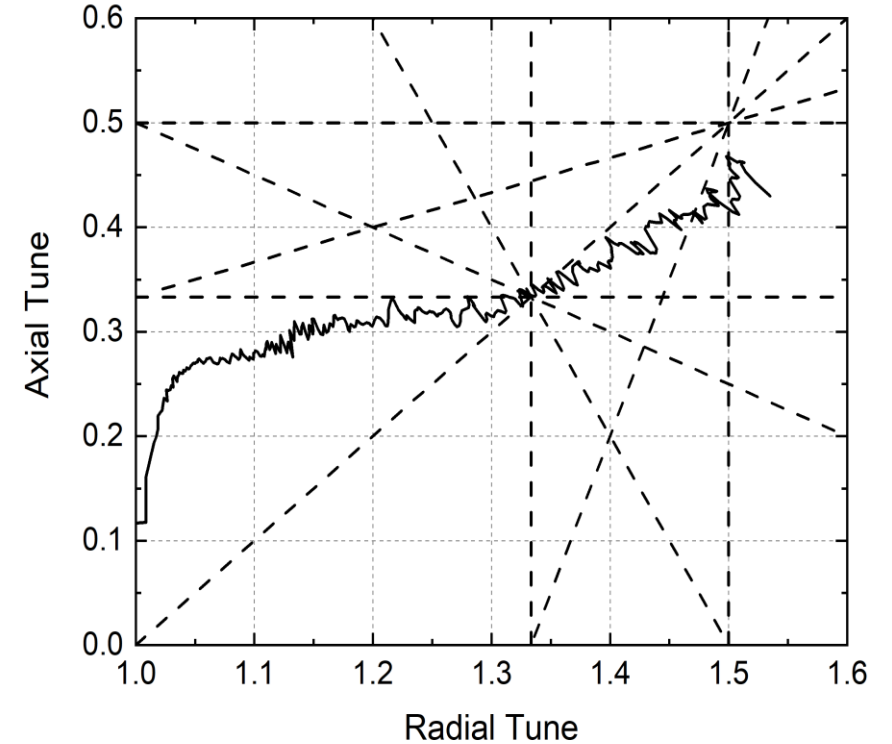


Automatic iteration process

$$\Delta(\text{Angle width ratio}) = (B_{iso} - B_{cal}) / (B_{hill} - B_{valley})$$



10 MeV to 4620 MeV with 10 MeV interval



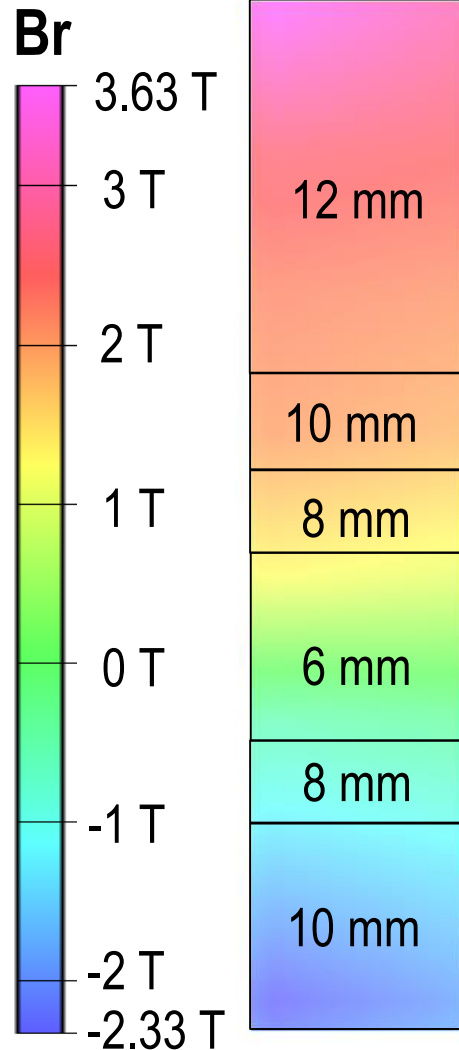
Missing Parameters in This Draft Design

- RF field simulation
- Reference field shaping
- Injection / Extraction

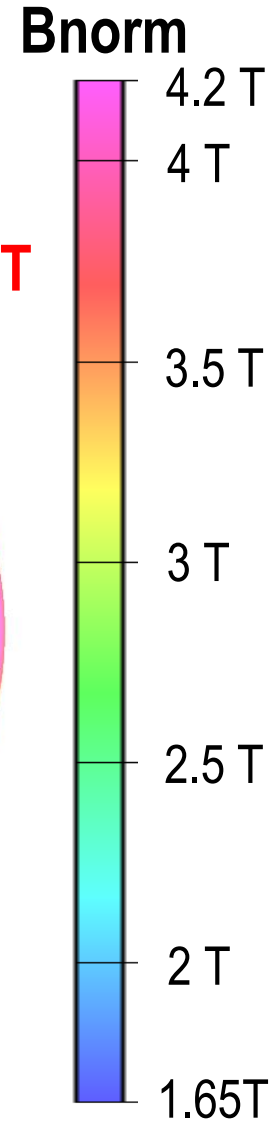
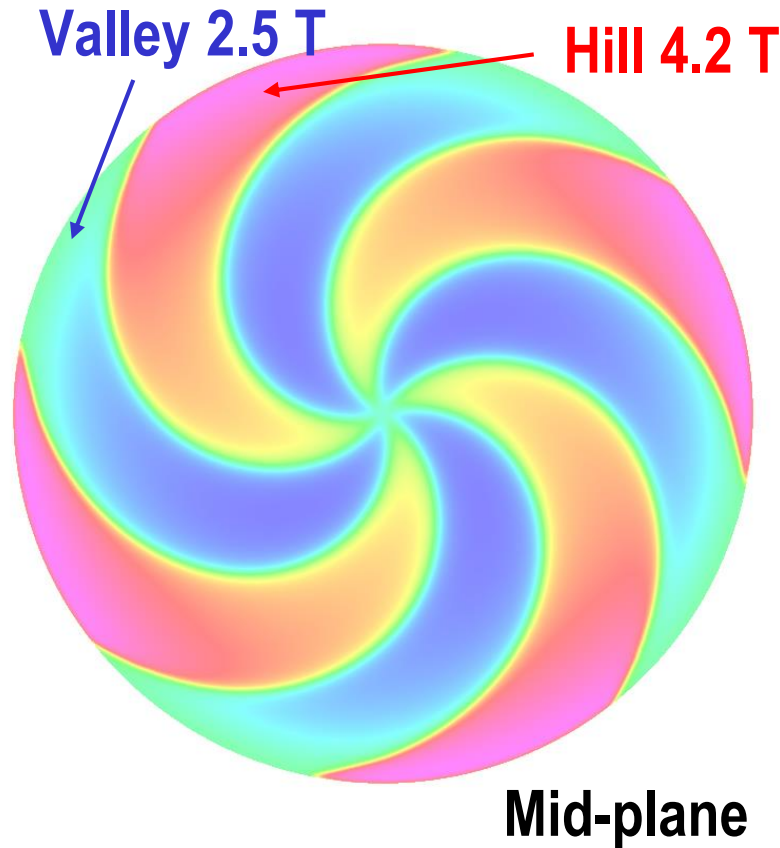
3.1.3 Electromagnetic Design: Coil Configuration with 20 % I_c Margin

Finalized Magnet Configuration: Corresponding Parameters & Field Distribution

Asymmetric Multi-Width Configuration



Magnetic Field Distribution



Key Parameters

Parameters	Value
Bending Limit, K [MeV]	1540
Magnet Dimension [m]	6.2 (D) 3 (H)
Weight [ton]	540
Conductor Usage [km]	112

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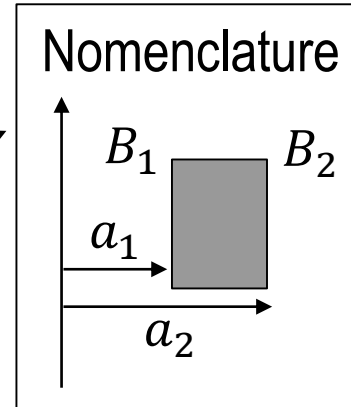
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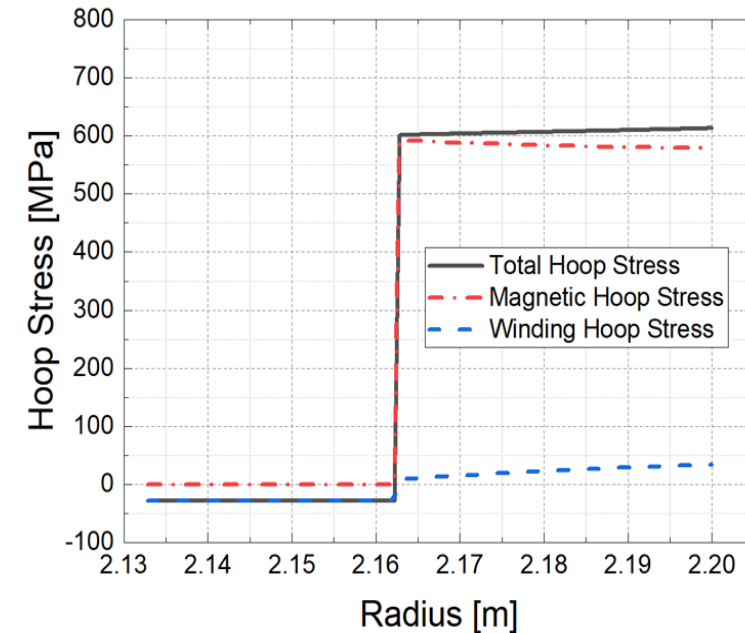
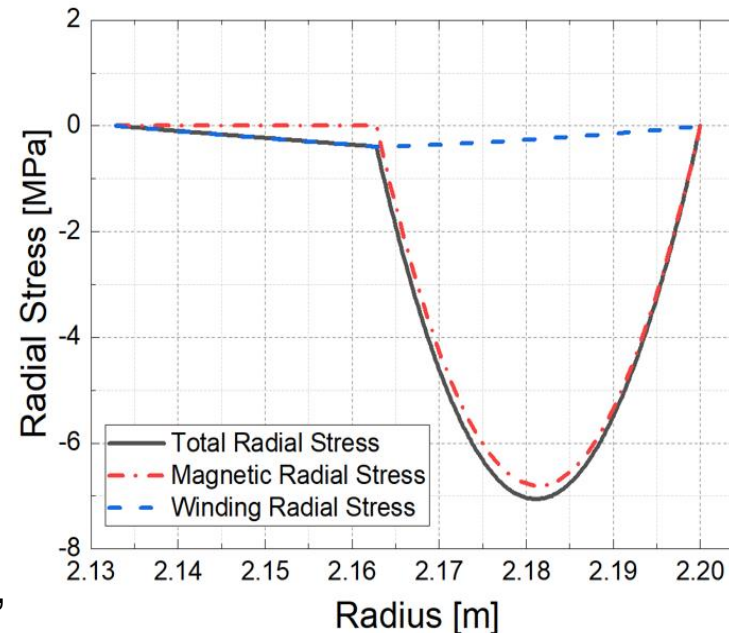
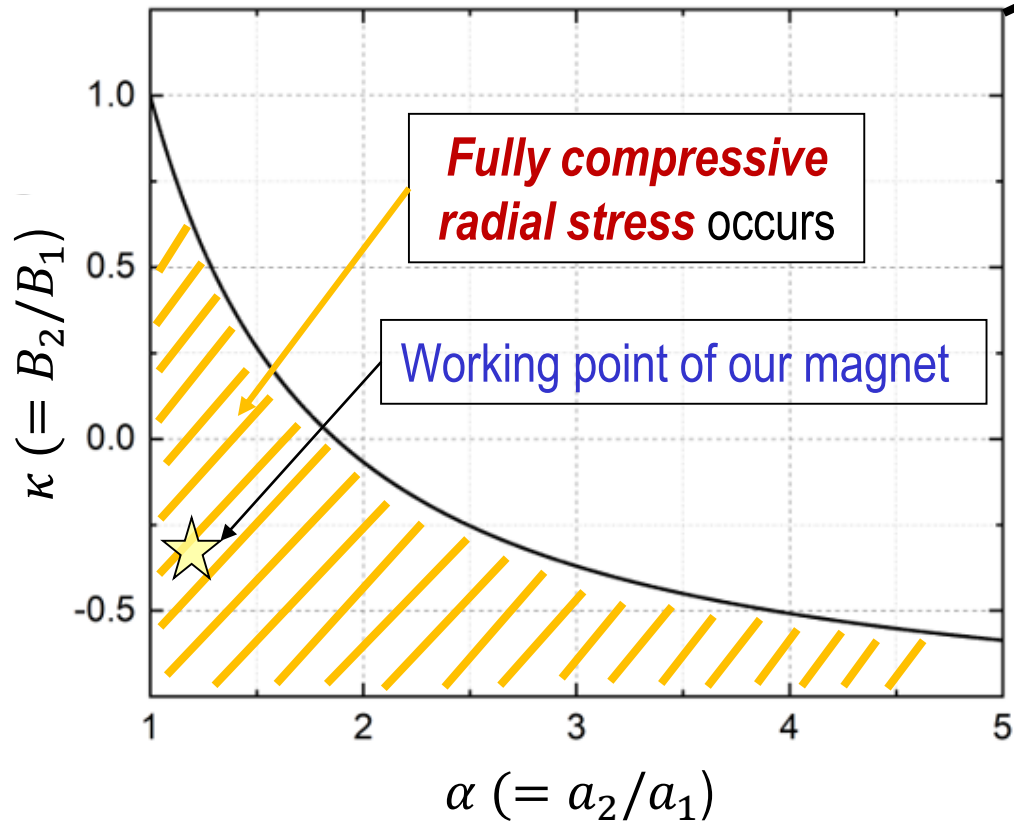
■ Governing Equation (Force Balance Equation) : $\sigma_r - \sigma_h + B Jr + r \frac{\partial \sigma_r}{\partial r} = 0$

□ “Analytic Condition” for Fully Compressive Radial Stress



□ Peak Hoop Stress in “6-mm” Coils

- 3-kg winding tension
- Bending and thermal stress neglected
- Maximum hoop stress: 612 MPa
- Maximum hoop strain: **0.33 %**

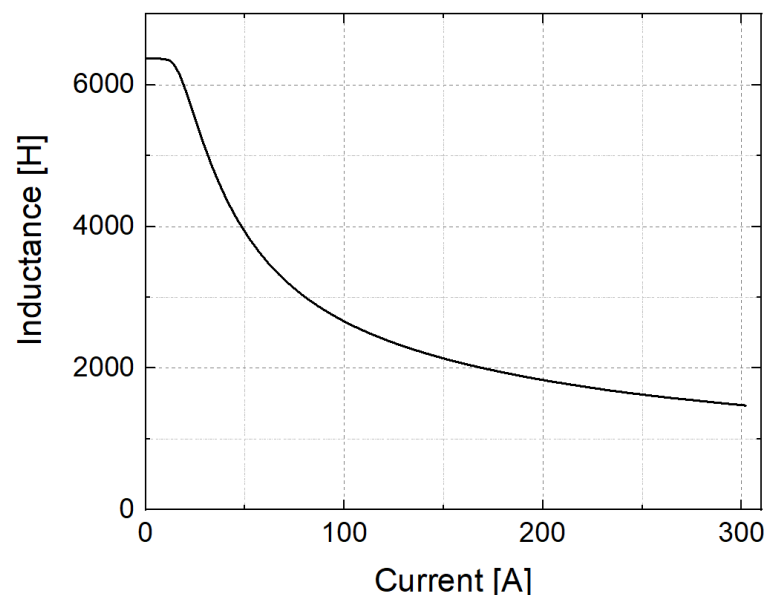
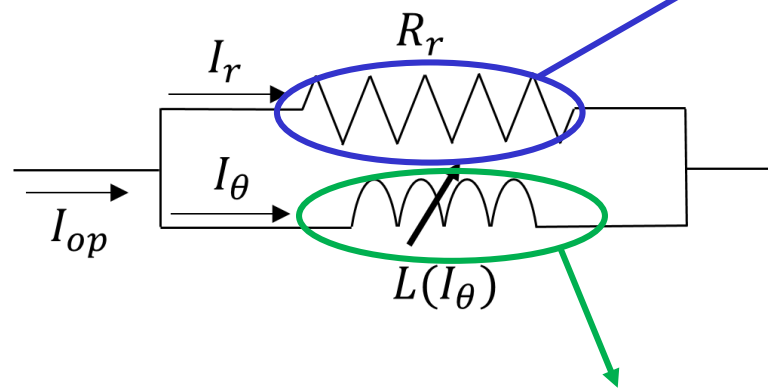


presented by Jeonghwan Park at “Tue-Mo-Po2.05-04 [27]”

3.3 Operation Analysis: NI Characteristics Considered Charging Analysis

■ Charging Scenario with “Active Control System” + “Overshoot Technique”

□ Analysis Circuit Model



□ Contact Resistance

10 T metal insulation HTS insert in Grenoble 32T

Ref) Xavier CHAUD *et al.*, “A 10 T HTS insert made of MI Pancakes Tested in a Magnetic Field up to 20 T,” presented at EUCAS 2019, Glasgow, UK, 2019.



$R_{ct} > 1,000 \mu\Omega \cdot \text{cm}^2$ in previous studies

Ref) T. Lecomte *et al.*, “A (RE)BCO Pancake Winding With Metal-as-Insulation,” *IEEE Trans. Appl. Supercond.*, vol.26, no. 3, 2016

□ Strategy for Reducing Charging Delay

(1) Use of bundle tape

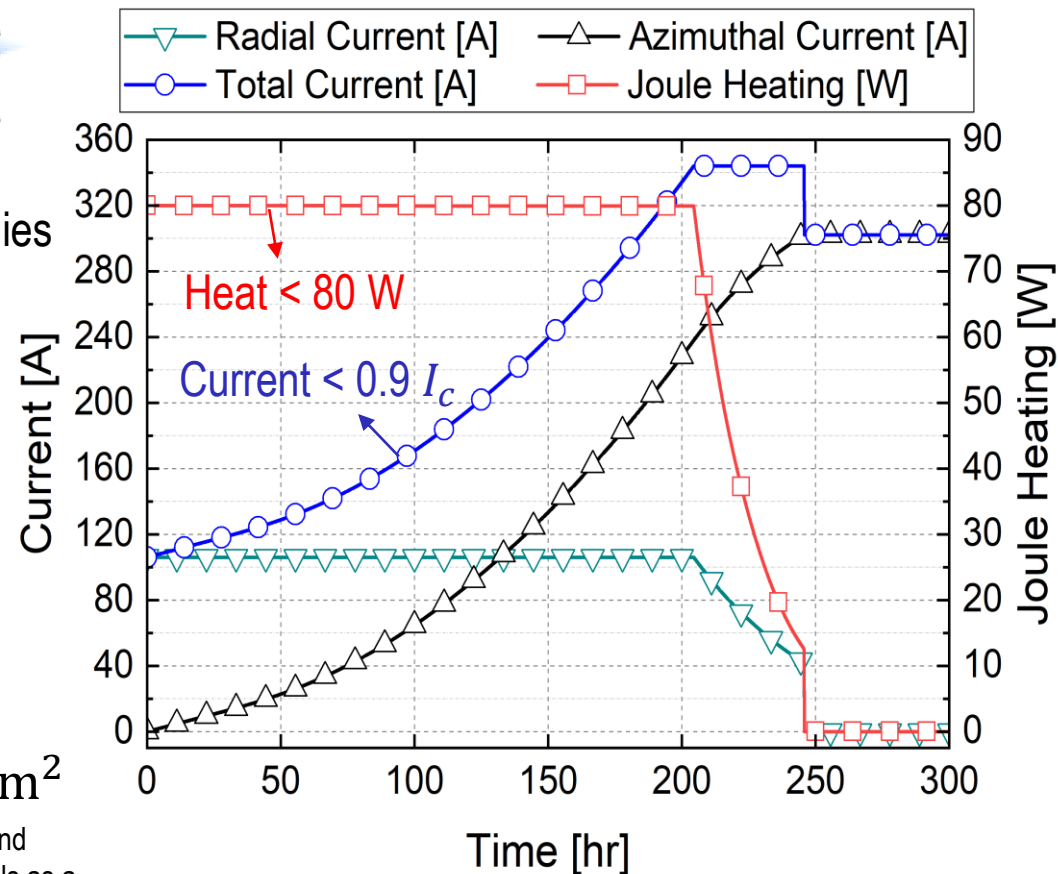
Ref) T. Watanabe *et al.*, “HTS Coils Wound by Bundle Conductor Composed of No-insulated REBCO Tapes,” presented at EUCAS 2019, Glasgow, UK, 2019.

(2) Increase $R_{ct} > 20,000 \mu\Omega \cdot \text{cm}^2$

Ref) WD Markiewicz *et al.*, “Quench transient current and quench propagation limit in pancake wound REBCO coils as a function of contact resistance, critical current, and coil size,” *Supercond. Sci. Technol.*, 32, 2019, 105010

□ Charging Analysis Results

Total Radial Resistance: **7.1 mΩ**



It takes 250 hrs to charge the magnet

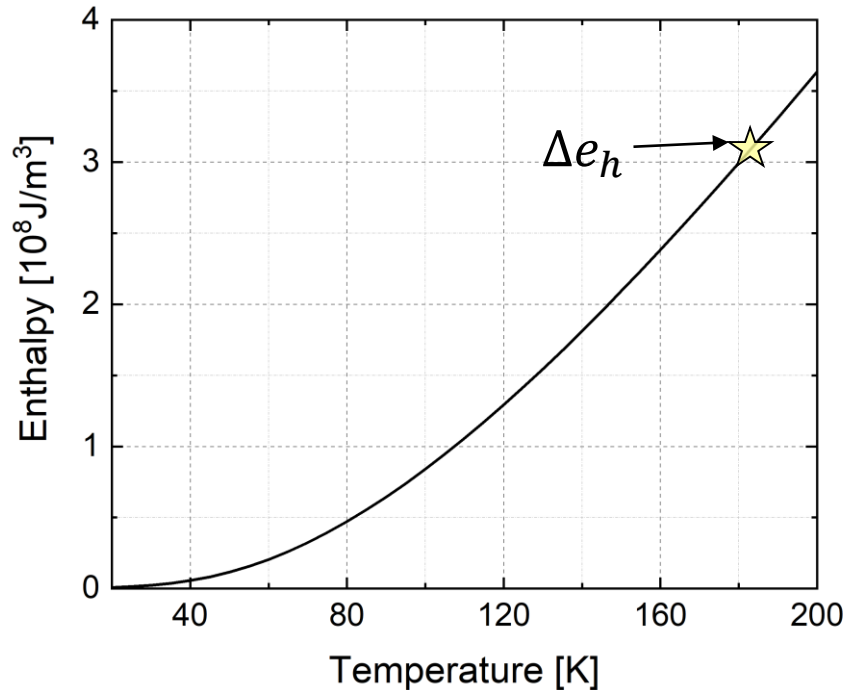
3.4 Preliminary Quench Analysis: 168 K Rise, 4.3 MN Unbalanced Force

- Temperature Rise

- Enthalpy Analysis: **~170 K** rise.

Total energy: 67 MJ
Winding volume: 0.21 m³

$$\Delta e_h = 3.2 \times 10^8 \text{ J/m}^3$$

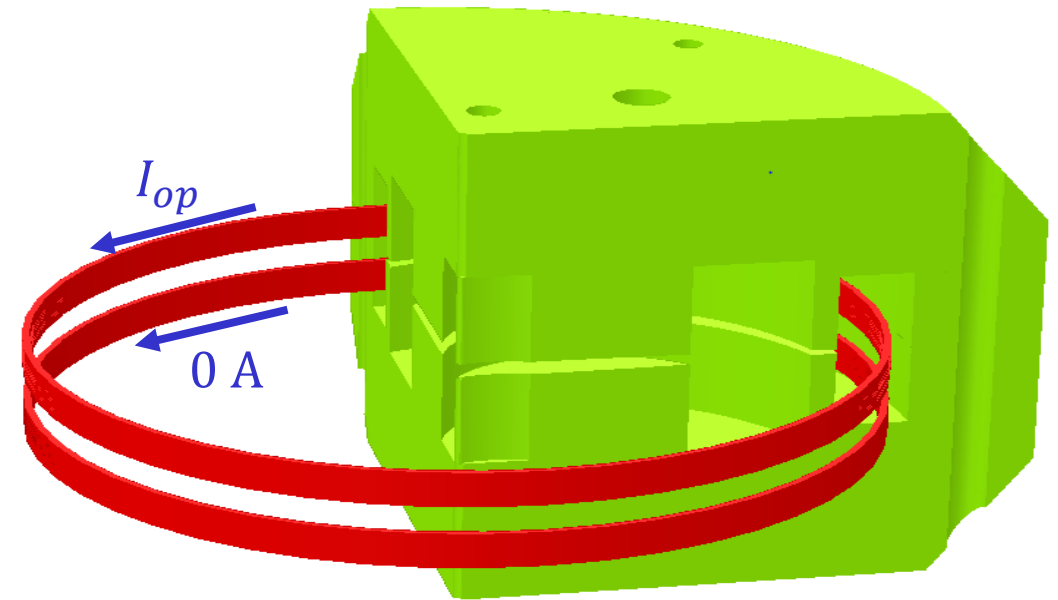


- Unbalanced Force (Worst Scenario)

- Total Axial Lorentz Force: 4.4 MN

A situation that one split coil is fully discharged

Fig. Quarter model for magnetic simulation



Other issues (maybe critical) on quench scenario

- (1) Overstress in NI magnet;
- (2) Screening-current induced stress

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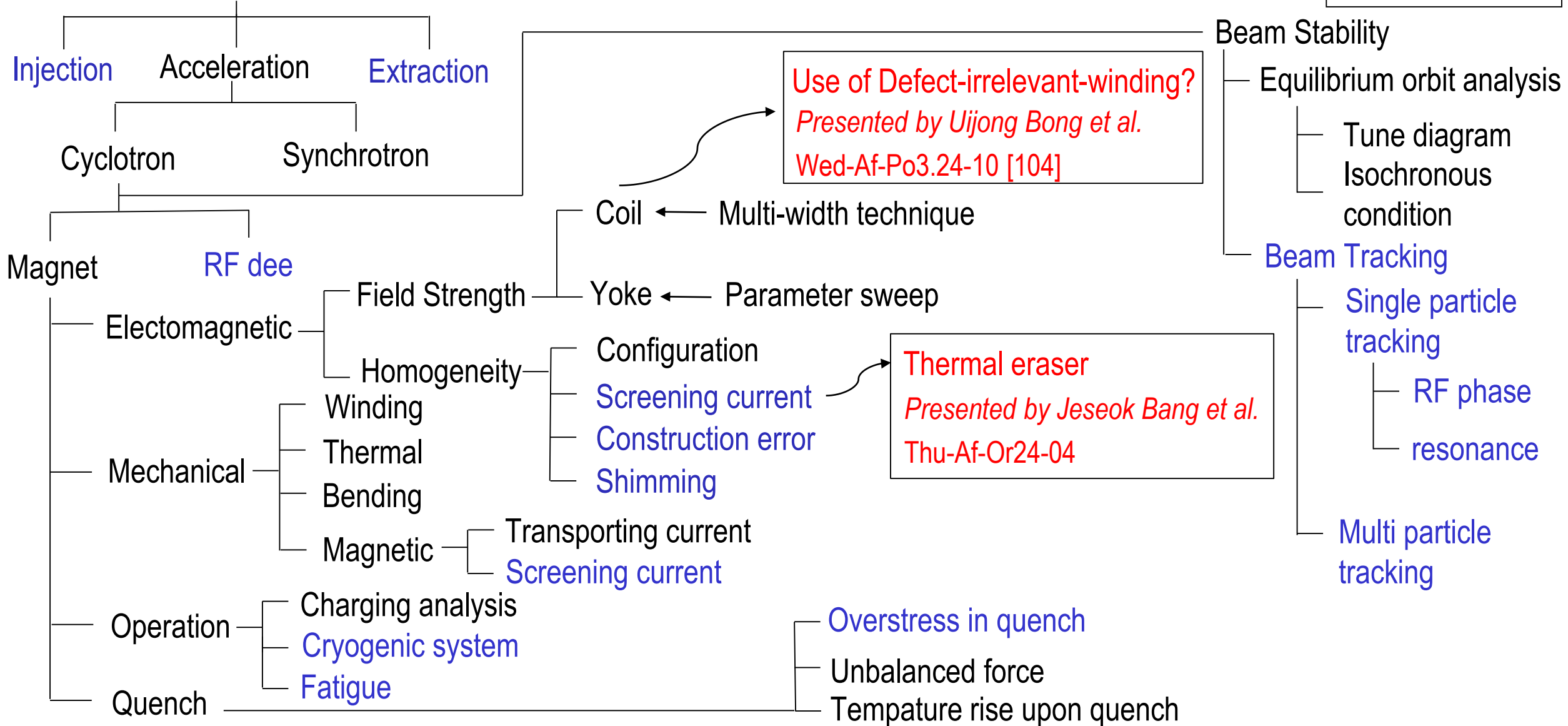
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■ Carbon Ion Accelerator

Future Works



Thanks for your attention

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