

Test Results of the First Two Full-Length Prototype Quadrupole Magnets for the LHC Hi-Lumi Upgrade

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Abstract— The future high luminosity (Hi-Lumi) upgrade of the Large Hadron Collider (LHC) at CERN will include eight (plus two spares) 8.4 m-long cryostatted cold masses which will be components of the triplets for two LHC insertion regions. Each cold mass will consist of two 4.2 m-long Nb₃Sn high gradient quadrupole magnets, designated MQXFA, with aperture 150 mm and operating gradient 132.6 T/m, for a total of twenty magnets. Before assembling and testing the final cold masses at Fermilab, the twenty component quadrupoles will be tested first at the vertical superconducting magnet test facility of the Superconducting Magnet Division (SMD) at Brookhaven National Laboratory (BNL), in superfluid He at 1.9 K and to 18.0 kA, in accordance with operational requirements of the LHC. Following a test of the first long single coil (in a mirror configuration) of the MQXFA design, the first two full-length prototype quadrupole magnets, MQXFAP1 and MQXFAP2, have been tested at BNL. This paper reports on the quench test and training results of these two magnets, and also the retest of the first prototype, rebuilt and designated as MQXFAP1b. The test results of these magnets will be important for validating the MQXFA design.

Index Terms— LARP, AUP, Hi-Lumi, LHC, Nb₃Sn, superconducting magnets

I. INTRODUCTION

The future high luminosity (Hi-Lumi) upgrade of the Large Hadron Collider (LHC) at CERN will include eight 8.4 m-long cryostatted cold masses (plus two spares) which will be components of the Q1 and Q3 elements of the triplets at two LHC insertion regions. Each cold mass will consist of two 4.2 m-long (magnetic length) high gradient quadrupole magnets, designated MQXF_{axx}, with aperture 150 mm and nominal operating gradient 132.6 T/m, for a total of twenty magnets. The fabrication and testing of these magnets are the combined effort of three US DOE laboratories: Brookhaven National Laboratory (BNL), Fermilab, and Lawrence Berkeley National Laboratory (LBNL), which together comprise the Accelerator Upgrade Project (AUP). In order to achieve the high field gradient necessary, the magnet coils are wound with Nb₃Sn superconductor cable, because of the high current densities possible, especially at 1.9 K. These coils must go through extensive heat treatment to create the superconductor, then vacuum impregnation to harden the coils against motion of the cables during cooldowns, warmups, and powering. Because of the strain-sensitive behavior of Nb₃Sn superconductor

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and the necessity to limit the thickness of ground insulation to accommodate required quench protection heaters, these magnets are challenging to fabricate and test, and both mechanical and electrical issues are possible, and have occurred. For this reason, before assembling and testing the final cold masses at Fermilab, the component quadrupoles will be tested individually at the vertical superconducting magnet test facility of the Superconducting Magnet Division (SMD) at BNL, in superfluid He at 1.9 K and 1 bar pressure, and to 18.0 kA, in accordance with operational requirements of the LHC. Data from extensive cold testing of short models at Fermilab and CERN have shown successful, though slow, quench training and excellent training memory over thermal cycles. The first two long prototypes MQXFAP1 (and a rebuilt version MQXFAP1b) and MQXFAP2 have been tested at BNL in a 6 m deep vertical test cryostat, and the results of the quench training for these three tests are discussed here.

II. MAGNET DESCRIPTION

Fig. 1 shows the cross-section of the MQXFA design, with four 2-layer coils in the preloading structure. For vertical tests of the individual magnets, only the aluminum shell, consisting of 8 segments, is included. The stainless steel He containment vessel shown in the drawing will be installed at Fermilab when assembling the cold mass containing two quadrupoles.

The main parameters of the full-length MQXFA quadrupoles are listed in Table I and these are the values of most concern for testing. It should be noted that the magnetic length of MQXFAP1/MQXFAP1b is 4.0 m, and not the final design length of 4.2 m. The actual length of both prototype structures,

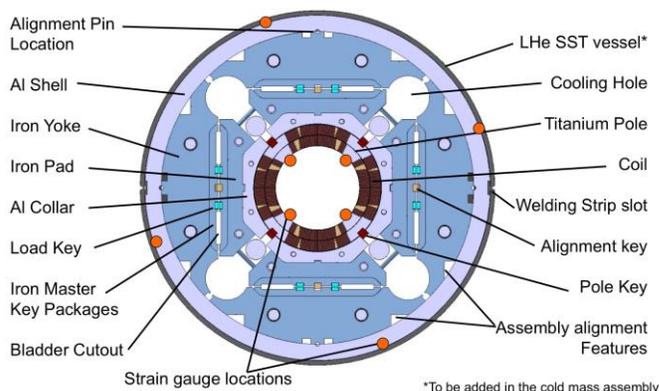


Fig. 1. MQXFA high gradient quadrupole cross-section.

TABLE I
MQXFQA DESIGN AND TEST PARAMETERS

Parameter	Value
Coil inner aperture:	150 mm
Coil magnetic length:	4.2 m (4.0 m MQXFAP1)
Total length with end plates:	5 m (nom)
Operational temperature and pressure:	1.9 K and 1 bar
LHC nominal operating current (1.9 K):	16.470 kA
LHC ultimate operating current (1.9 K):	17.890 kA
Conductor limit at 1.9 K:	21.600 kA
Conductor limit at 4.5 K:	19.550 kA
Nominal ramp rate:	20 A/s
Magnet inductance (1.9 K, 1 kA):	43.0 mH
Magnet inductance (1.9 K, $I_{nom}=16.5$ kA):	34.4 mH
Nominal stored energy (at B_{nom} , I_{nom}):	4.67 MJ
Ultimate stored energy (at B_{ult} , I_{ult}):	5.50 MJ
Maximum allowed temperature at quench:	250 K (27-32 MIIts)
Maximum allowed voltage across magnet:	1000 V
Dump resistor (energy extraction) options:	30, 37.5, 50, 75, 150 m Ω
Data sampling rate:	10 – 100 MHz

and all production magnets (with endplates), is 5 m, for which the He vessel of the test cryostat at BNL was upgraded to accommodate, among other upgrades for testing the MQXFQA quadrupoles. As shown in Table I, the nominal operating current of MQXFQA quadrupoles is 16.470 A, and the so-called ultimate current is 17.890 A, for a future energy upgrade of the LHC. These were the target currents to be reached during testing. It should also be noted that the maximum quench hot spot temperature is given as 250 K, but the corresponding quench integral ($\int I^2 dt$) values can be in the range 28 – 32 MIIts, depending on the conductor used in each magnet. A higher temperature of 350 K was allowed only for the prototypes after training was completed and only during quench protection studies. Also important to note is the high stored energy released during a quench. This resulted in several burst disc rupture events and subsequent loss of He at the start of training the first prototype MQXFAP1. This necessitated several unplanned thermal cycles in order to modify the pressure relief system for He recovery after a quench.

III. EXPERIMENTAL INSTRUMENTATION AND PROCEDURES

Test procedures for the prototypes derive from an AUP specifications document [1], which is based on operational conditions of the magnets in the LHC triplets. Test parameters that must be met by the test facility are detailed in [2]; these include 1.9 K superfluid He at 1 bar vapor pressure, powering up to 24 kA, 20 A/s ramp rate for training, up to 160 A/s for special tests, and the capability of He gas recovery at high and swiftly increasing pressures due to the large storage energy at high quench currents. Upgrades to the facility were necessary to meet these requirements [3],[4].

The MQXFQA prototypes were instrumented with the following devices:

- 1) Voltage taps – main (fixed) taps for quench detection and auxiliary (configurable) taps for quench location.
- 2) Quench antenna with 16 elements each having two sets of windings.

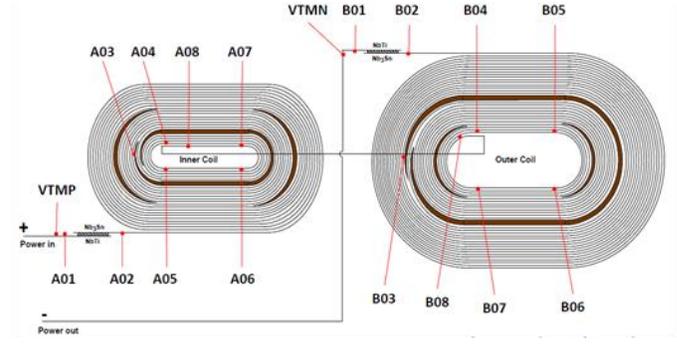


Fig. 2. MQXFQA voltage tap configuration.

- 3) Strain gauges – two independent systems (Vishay and HBM) installed on coil poles, shells, and axial rods.
- 4) Rotating coil magnetic field measuring probe with 220 mm, 110 mm length windings.
- 5) Temperature, LHe level, and pressure measurement systems.

This paper is concerned with the quench test results only; other testing operations are reported in additional papers at this conference [5]-[7]. Therefore, the instrumentation most relevant to this discussion are the voltage taps and the signals produced during quenches. Fig. 2 shows the voltage tap schematic, a configuration used by all the AUP collaborating laboratories and CERN. Each layer of each coil has 8 taps which are located mainly on the pole turns, as can be seen. Additional taps are located at splices between coils and on the leads.

Data acquisition was done with a fast data logger, sampling at 10 kHz – 100 kHz, depending on requirements, and a slow data logger which sampled at 1 Hz during quench and other ramp tests. Two FPGA-based digital quench detector systems were inputted with the half magnet voltage difference, total magnet voltage minus $L(dI/dt)$, and voltages of special tap sections, such as splices and superconducting leads [4].

Quench protection during testing of the prototypes was provided by the following systems and settings:

- 1) energy extraction using 37.5 m Ω dump resistance;
- 2) quench protection heaters at 465 V, 190 A, and 12.4 mF to achieve the necessary power density;
- 3) Coupling Loss Induced Quench (CLIQ) system [8], set to 500 V and 40 mF.

Cooldown of a magnet under test consisted of three stages:

- 1) cooldown to 100 K with liquid N₂ heat exchanger;
- 2) cooldown to 4.5 K with liquid He bath; electrical checks and validation of the quench protection heaters may be done at this stage;
- 3) cooldown to 1.9 K using a liquid He heat exchanger in a magnet cooling hole and pumping on it with a 150 W, 2.7 g/s vacuum pump to 16 mbar vapor pressure.

After cooldown and initial cold electrical checkout, including voltage withstand tests and validation of the quench protection heater operation, the quench training program at 1.9 K started using 20 A/s ramp rate and typically 100 kHz fast logger sampling rate. Quench tests were to be repeated until a stable quench current level was achieved, quench currents

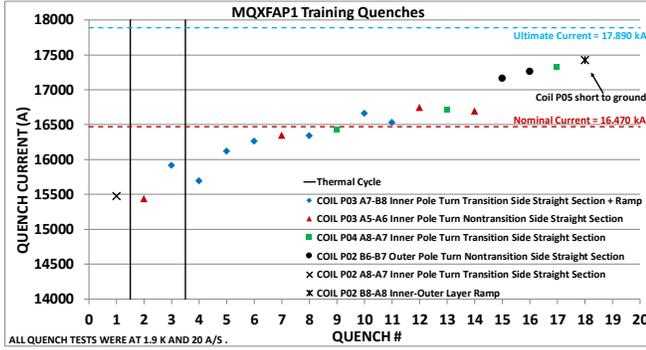


Fig. 3. MQXFAP1 quench performance plot. Testing was terminated when Coil P05 developed a short to ground.

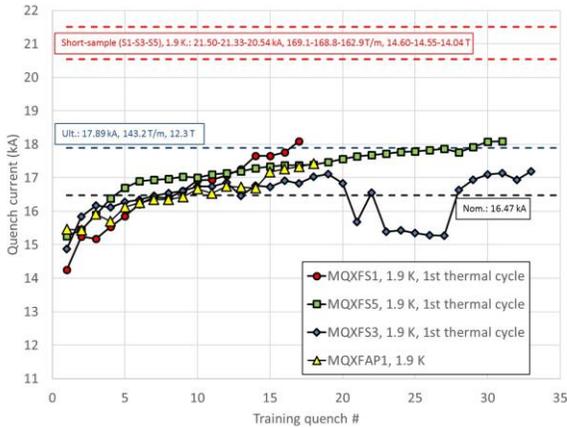


Fig. 4. Comparison of short and long MQXFAs training performance. MQXFAP1 training was similar to the short prototypes.

reached above the ultimate current and could be held in stable operation, or the quench currents were erratic and there was no training. Quench voltage tap signals and other signals were analyzed to look for artifacts, to verify a quench event was not a spurious QD trip, to determine the quench start location, and to calculate the quench integral to estimate the hot spot temperature to determine if it was below allowed maximum value.

IV. QUENCH TRAINING RESULTS

For the first long prototype MQXFAP1, the training history is plotted in Fig. 3, and it shows that the training did follow a mostly upward trend and in fact, if compared to the short models, as seen in Fig. 4, very similar training. Most quenches were in the inner layer pole turns, which is expected for a nominally training magnet. The first two quenches, each with stored energy of 3.8 MJ, resulted in the relief system burst disc rupturing and caused the escape of the He from the test cryostat. In each case, a thermal cycle was done, and changes were made to the relief system; after the second thermal cycle when an upgraded relief valve and burst disc assembly was installed, burst disc ruptures were eliminated, though some He was still being lost due to opening of the reliefs. Since energies up to about 6 MJ were possible for these tests, further upgrades were needed. Since this magnet test, further upgrades to the He recovery system were made which so far has eliminated the opening of the relief valves.

As can be seen, in addition to a typical training curve, there was also exhibited memory of the training after each thermal cycle. This test also provided several milestones. The last 5 quenches were done with the CLIQ system added, the first such application on a long MQXFAs magnet. Quench integral values decreased from ~ 29 (270 K) to ~ 25 MIIt (220 K), as expected. In addition, the last 4 quenches were done without the inner layer protection heaters, and MIIt values were not affected. This was an important result, as inner layer heaters are no longer to be used in MQXF magnets.

Unfortunately, MQXFAP1 testing ended with Quench 18, when Coil P05 developed a short to ground. Hipot tests in-

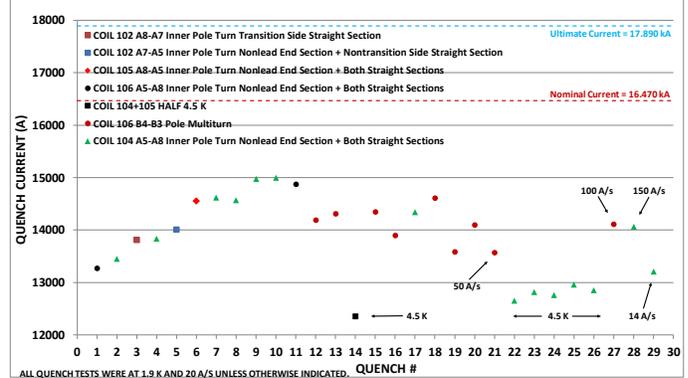


Fig. 5. MQXFAP2 quench performance plot. Quench current were low and became erratic, though temperature dependence was exhibited.

volving this coil had been problematic starting with the first cooldown, and later at the first warmup, where the Coil P05 outer layer - low field heater started exhibiting a short to the coil. The Coil P05 issue is attributed to a combination of the following causes: 1) non-conforming impregnation of Coil P05, and 2) hipots that were done at room temperature after the testing at 1.9 K, so there was the possibility of trapped He gas in the coils. After testing was finished, Coil P05 was subsequently replaced with a new 4.0 m coil (P06) for re-test of the magnet later as MQXFAP1b.

The quench current plot for MQXFAP2 is shown in Fig. 5, and it is seen that the magnet did not demonstrate training, starting at an atypically low first quench and remaining at currents lower than usual, not even reaching the nominal operating current of 16.470 kA, and quench currents eventually becoming erratic in nature. Quenches occurred in all four coils, but starting with Quench 7, all quenches were in Coil 104 or Coil 106. There were only a few early quenches in Coils 102 (#3,5) and 105 (#6).

For all coils, most of the taps A6, A7 and B5, B6, which bracket the nonlead end sections in the inner and outer layer pole turns, respectively (see Fig. 2), opened during quenches. For quenches that were in pole turns, the quenching sections included both nonlead end and one or both straight sections due to the lost nonlead end taps, so quench localization was compromised in these cases. Quenches in the outer layer multiturn could not be localized by the taps. However, quench antenna data analysis [9] showed that most inner layer quenches originated in or near the nonlead end.



Fig. 6. MQXFAP2 nonlead end shell cracks, which all originated at corners of the alignment cut-outs. Photo is courtesy of D. Cheng, LBNL.

For many quenches, voltage signals exhibited precursor spikes 0-8 ms prior to the quench start. The presence of precursor spikes and the erratic nature of the quench currents imply mechanical motion, but it can also be seen in the quench plot that quench currents were affected by changes in temperature, which implies conductor damage. Quench integral values ranged from 25 – 28 MIIts (~ 170 – ~ 200 K), which were well within the target of 250 K maximum for training quenches.

Testing was finally ended due to the lack of training. After warmup, it was seen that the nonlead end Al shell had developed a large crack along the axial direction, along with other smaller cracks starting to propagate. (See Fig. 6.) This observation agrees with the nonlead end quench locations and the loss of taps at that end. All cracks originated at corners of the alignment cut-outs; these corners are locations of concentrated stress. It was later shown that the radius of curvature of the end shell corners was too small.

After the ground short of Coil P05 which ended the training program of MQXFAP1, Coil P05 was replaced by a newly wound 4.0 m-long coil, denoted P06, and the magnet, now designated MQXFAP1b, was retested. Fig. 7 shows the quench current history, and as can be seen, the first 3 quenches were in the new, untested P06, and it trained normally to nominal operating current; locations were in the inner layer pole turn, as expected. Other than one more quench in Coil P06, which continued its training, the rest of the quenches were in Coil P03 inner layer, somewhere in the two multitrans blocks; unfortunately, tap A3 in P03 was open so the resulting section comprised all the turns other than the pole turn. Quench antenna data showed that quench locations varied axially, ranging from lead end to nonlead end and in between [9].

Quench currents 8-18 were highly erratic, implying mechanical motion. Starting with Quench 19, quench currents were stable but low, and were affected by both ramp rate and temperature, implying conductor damage. These results suggest that motion of the coil during earlier quenches might have caused damage to the conductor, as seen in the behavior of the later quenches. Since Coil P03 was now limiting the performance of the magnet, testing was stopped so that the issue could be investigated. MQXFAP1b will be disassembled and Coil P03 will be inspected. Epoxy failure due to impregnation issues is suspected.

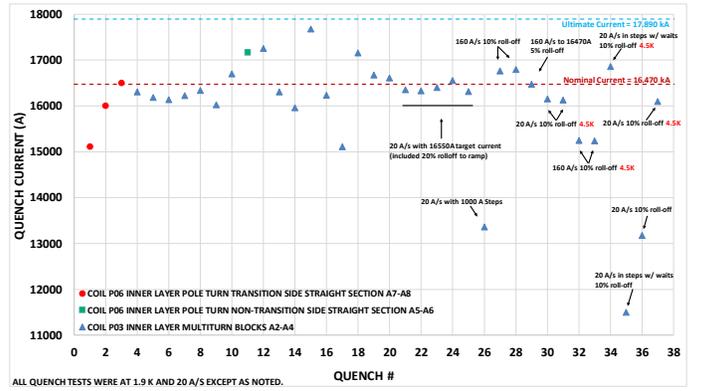


Fig. 7. MQXFAP1b quench performance plot.

V. LESSONS LEARNED AND MITIGATIONS

- 1) MQXFAP1 Coil P05 failure:
 - a. The supplier of the insulation between heaters and coil has been changed.
 - b. The coil impregnation process has been upgraded and is still being investigated.
 - c. After initial cold hipots and exposure to He, warm hipot voltages are now reduced to safer levels, a factor of 5 less than initial cold [10].
- 2) MQXFAP2 End Shell failure:
 - a. Heat treatment of the aluminum used in the failed shell will no longer be used.
 - b. Pole key gap is increased to reduce shell stresses [5].
 - b. Shell alignment cut-outs are now to have 10 - 15 mm fillet radius at the corners to minimize stress at those locations [5], [11].
- 3) MQXFAP1b Coil P03 failure:
 - a. Coil P03 has not yet been removed from the structure and so is still under investigation.
 - b. Epoxy failure is suspected.
 - c. Pre-load sequence has been changed [5].

VI. CONCLUSIONS

Two MQXFA long prototypes have been tested in three tests: MQXFAP1, MQXFAP2, and MQXFAP1b. In each case, there was a specific failure which pointed to an issue which has been addressed or is under investigation. MQXFAP1 training and early MQXFAP1b training does validate the long magnet structural design, but some specific issues were uncovered by the testing and these are being addressed before the test of MQXFA03, the first pre-series MQXFA magnet.

Also, during the testing, various modifications to the test facility were implemented to increase the efficiency of the test procedures, to accommodate the high quench energies for the He recovery system, and to help meet the testing requirements of the Hi-Lumi program.

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