

Winding and 77K Testing of Non-Insulated Coils for the IBS 25T, 100 mm bore HTS Solenoid

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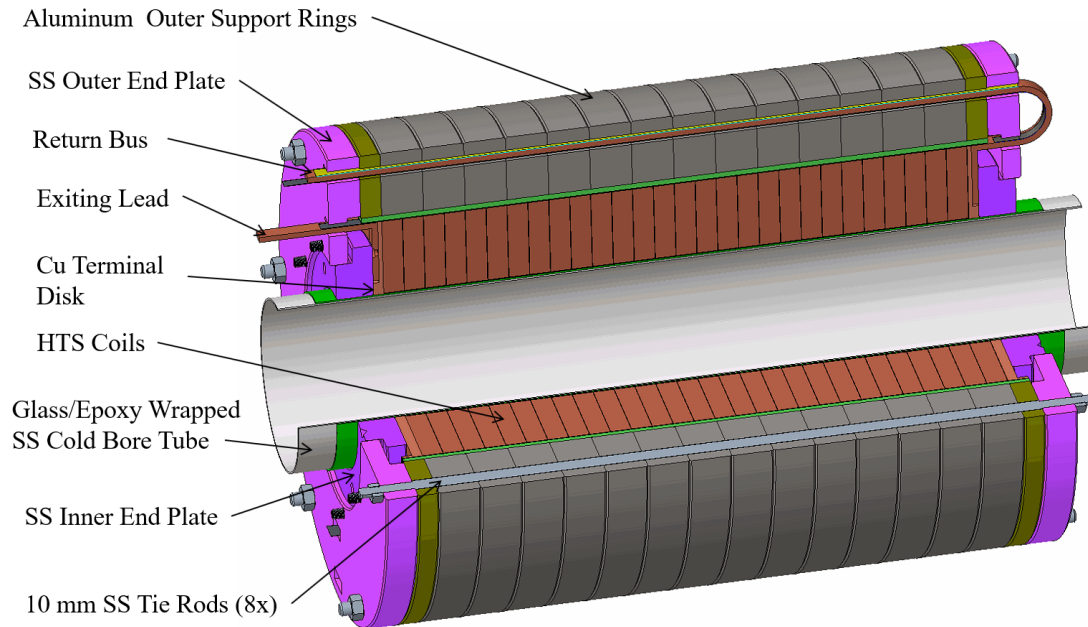
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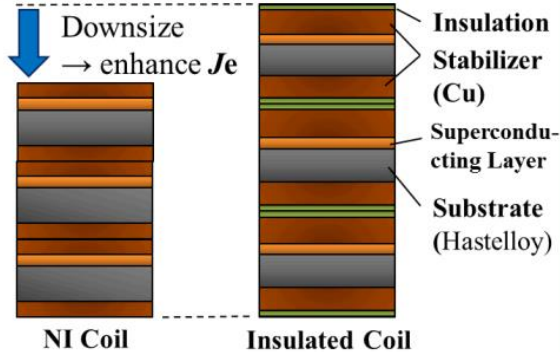
INTRODUCTION



- The Institute of Basic Science (IBS) in South Korea requires a **25 Tesla, 100 mm bore solenoid for experiments searching for dark matter axions search.**
- The Superconducting Magnet Division at Brookhaven National Laboratory received a contract to design and build this magnet.
- The **design is based on no-insulation approach using second generation HTS.**
- **BNL has built 16 of the 28 coils needed; tested 12 (@ 77 K) of the 16 built.**
- This presentation summarizes the construction and 77 K test results.

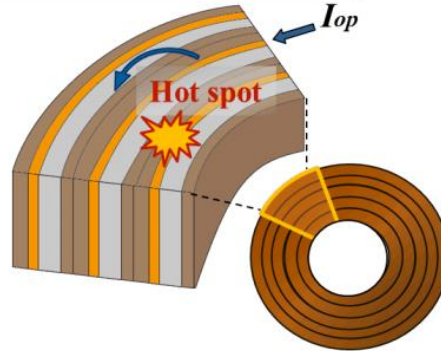
NO-INSULATION

High Current Density



1. Stabilizer thickness can be reduced by no-insulation between turns in winding.
2. Overall current density can be increased.
3. Downsizing of pancake coils can be realized.

High Thermal Stability



1. Current can bypass the local hotspot.
2. Local temperature rise can be avoided.
3. Thermal stability can be enhanced due to the low temperature rise under high current density

Non-Insulated (HTS) Magnet coils offer:

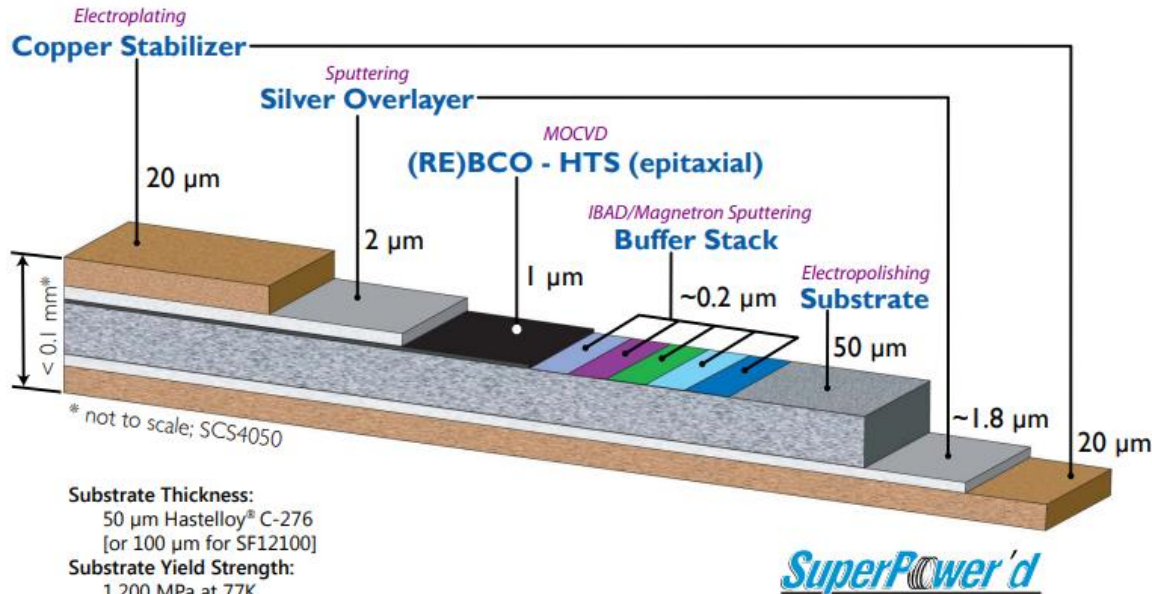
- **reliable intrinsic quench protection**
- **the ability to tolerate local defects in the conductor or sudden changes in operation**

as compared to HTS coils made with metallic or non-metallic insulation.

Reference:

Wang, T., Noguchi, S., Wang, X., Arakawa, I., Minami, K., Monma, K., ... Iwasa, Y. (2015). Analyses of transient behaviors of no-insulation REBCO pancake coils during sudden discharging and overcurrent. *IEEE Transactions on Applied Superconductivity*.
<https://doi.org/10.1109/TASC.2015.2393058>

CONDUCTOR



Substrate Thickness:

50 μm Hastelloy® C-276
[or 100 μm for SF12100]

Substrate Yield Strength:

1,200 MPa at 77K

Substrate Resistivity:

125 $\mu\Omega\text{-cm}$ – higher resistivity leads to lower eddy current ac loss

Magnetic Properties:

non-magnetic, leads to lower ferromagnetic ac loss

Reference:

http://www.superpower-inc.com/system/files/SP_2G+Wire+Spec+Sheet_2014_web_v1_0.pdf

- Width of the tape : 2 mm to 12 mm
 - 12 mm gives larger current, smaller impact of local defect and fewer coils
- Choice of substrate: Hastelloy, SS, Ni and others
 - Hastelloy for the best mechanical properties
- Amount of copper : 20 micron to 100 micron
 - 20 micron gives the best mechanical properties

DESIGN SPECIFICATIONS

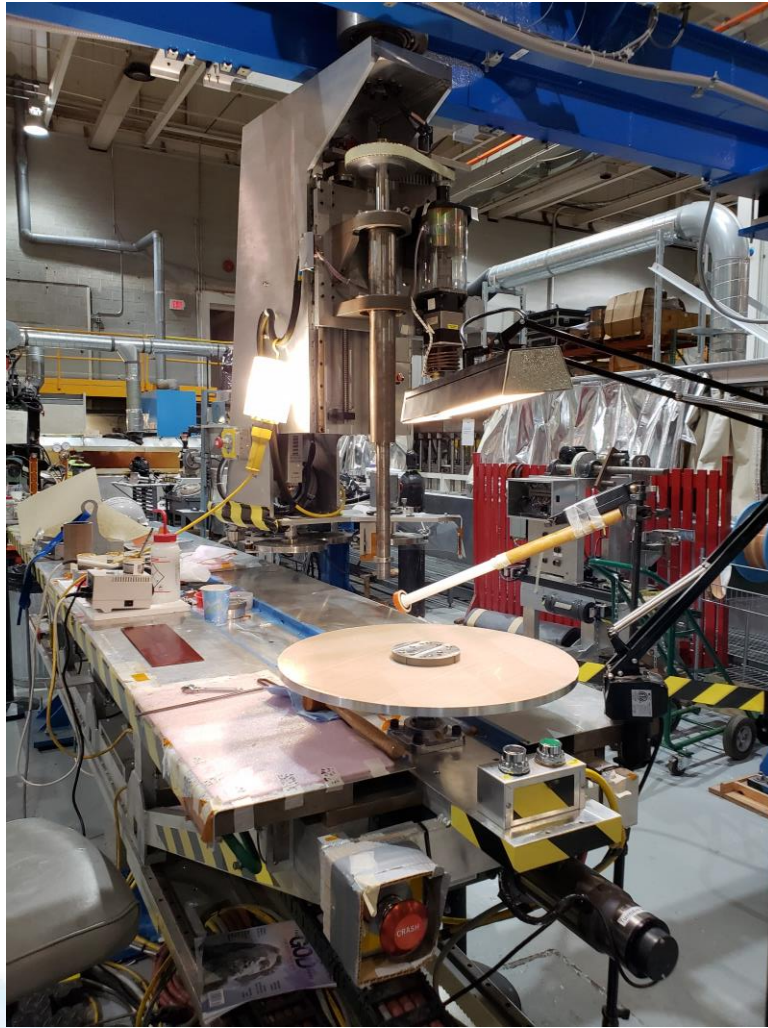
Conductor Information

Manufacturer	SuperPower Inc. ¹⁰
HTS	REBCO
Stabilizer	Copper
Stabilizer thickness (each side)	10 μm
Substrate	Hastelloy
Substrate thickness	$\sim 50 \mu\text{m}$
Nominal tape width	12 mm
Nominal tape thickness	0.075 mm
Critical bend radius	11 mm

Coil Specifications

Maximum center-axis field	25 T
Operating temperature	4.2 K
Number pancake coils	28
Inner diameter (ID)	105 mm
Outer diameter (OD)	200 mm
Insulation	None
Winding tension	9 lbs (40 N)
Total turns	~ 630
Total length of conductor	$\sim 300 \text{ m}$

COIL WINDING



Above, left to right: Multi-Axis Coil winding Machine, Designed and Built at BNL; LabView based coil winding machine control program; Coil winding tension control

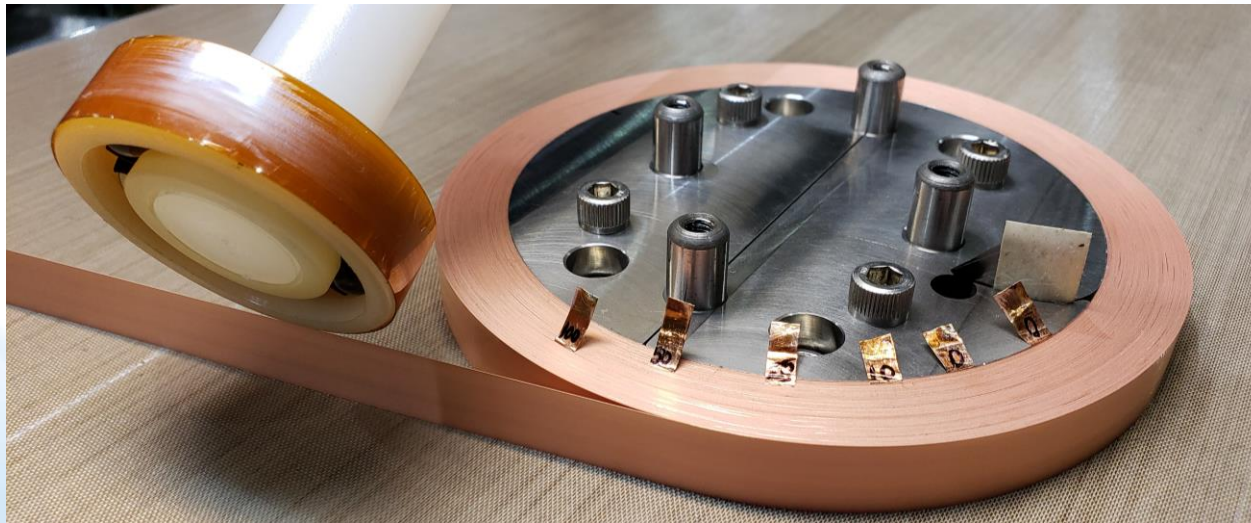
COIL WINDING



Above: Tin first turn for future leads and or coil inter-connections – **HTS side FACING bobbin**



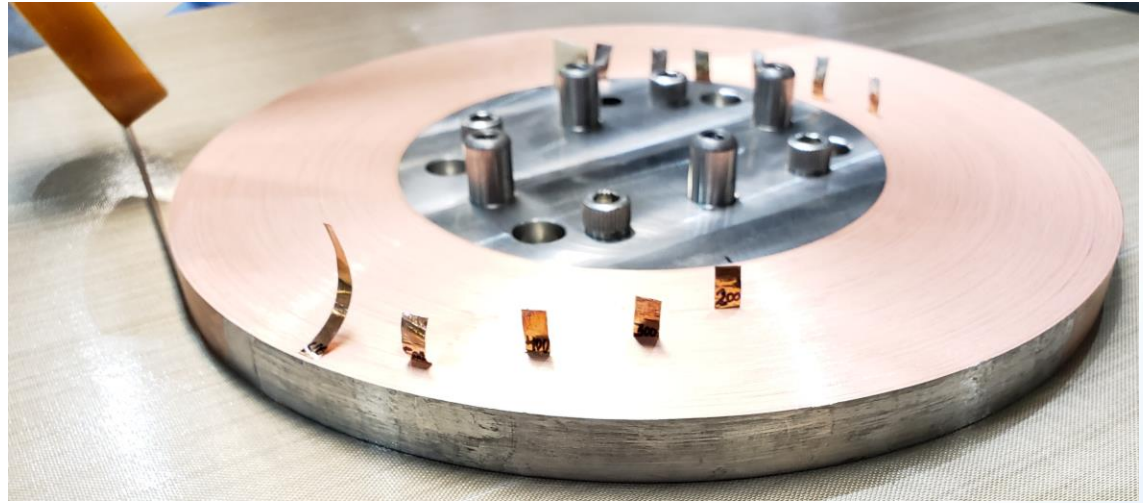
Above: Solder first turn to itself to secure inner part of coil for **reusable bobbin** removal



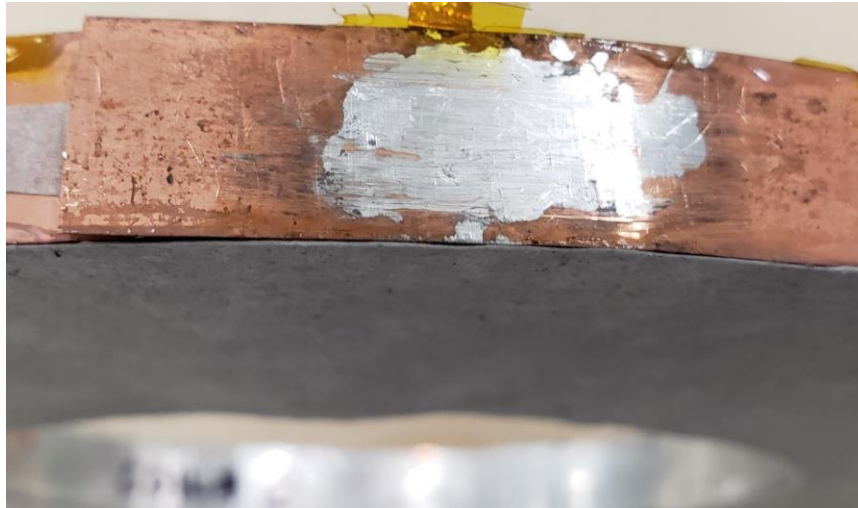
Left: Continue winding, with conductor under **9 lbs of tension**, until conductor runs out or splice needs to be made to reverse HTS orientation (**conductor HTS side has to be FACING AWAY from bobbin on the final turn** for future leads and or coil inter-connections)

COIL WINDING

Left: Line up conductors together using splicing tool. Splice (~23 cm in length) conductors using Indium solder and scrape away access Indium – minimize the thickness of the splice



Above: Spliced joint being wound into the coil



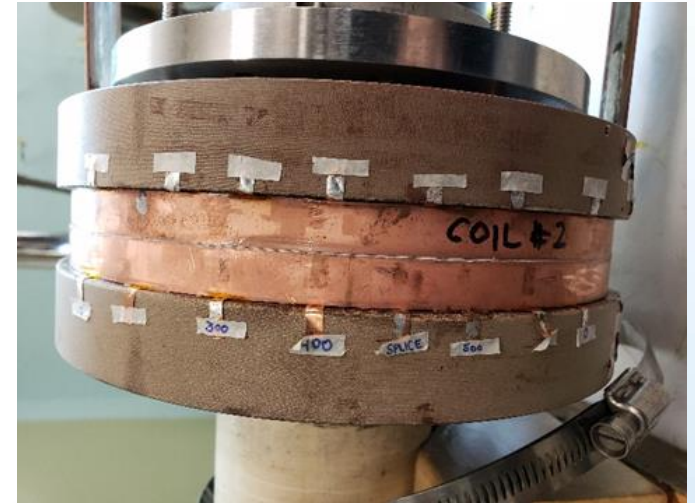
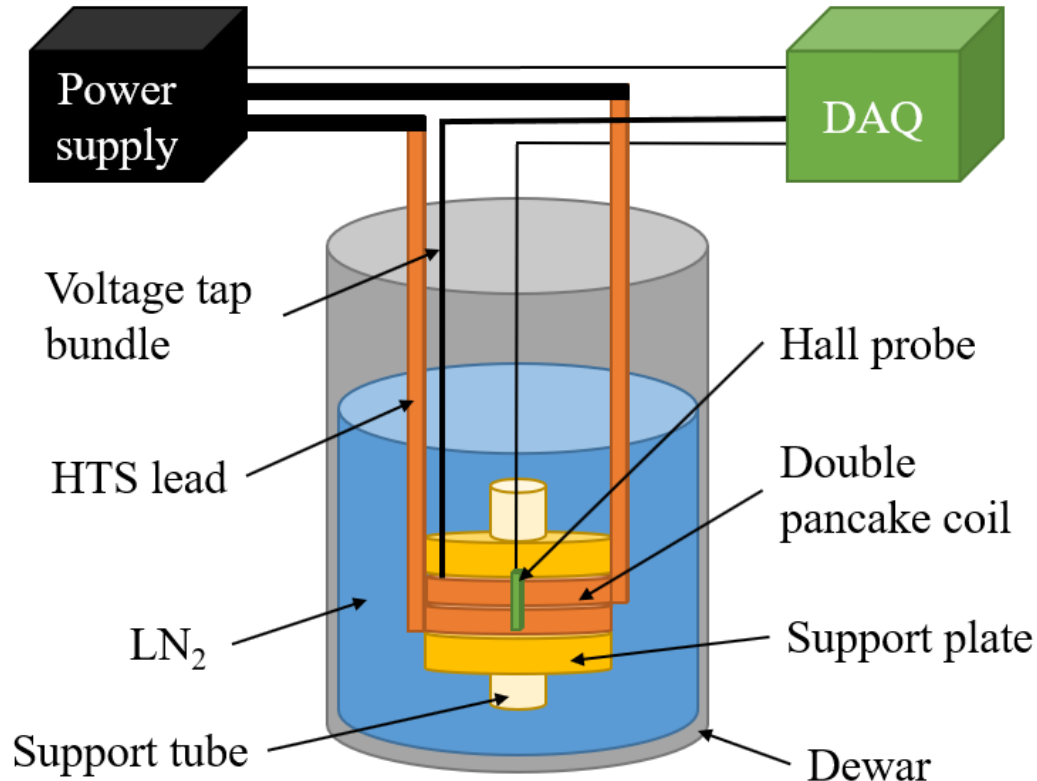
Left: Continue winding coil until coil O.D equals 200mm (~625-630 turns of 20 μ m Cu HTS tape). Solder last turn to itself to hold outer part of coil together once conductor is disconnected from spool.

CONTACT RESISTANCE AND TIME CONSTANT

TURN	COIL #1			at 1 A		at R.T.							TURN	COIL #2			at 1 A		at R.T.								
	mV	mV	mV	mV	mV	mV	mV	mV	mV	mV	mV	mV		mV	mV	mV	mV	mV	mV	mV	mV	mV	mV	mV	mV		
10	0.452	-	-	-	-	-	-	-	-	-	-	-	6/6/18	10	0.409	-	-	-	-	-	-	-	-	-	-	6/14/18	
25	0.275	0.727	-	-	-	-	-	-	-	-	-	-	6/6/18	25	0.276	0.675	-	-	-	-	-	-	-	-	-	6/14/18	
50	0.252	0.539	1.145	-	-	-	-	-	-	-	-	-	6/6/18	50	0.25	0.499	1.113	-	-	-	-	-	-	-	-	6/14/18	
100	0.242	0.52	0.993	2	-	-	-	-	-	-	-	-	6/6/18	50 O.N	0.241	0.485	1.088	-	-	-	-	-	-	-	-	6/15/18	
150*	0.238	0.512	0.974	1.873	-	-	-	-	-	-	-	-	6/6/18	100	0.241	0.482	0.87	1.862	-	-	-	-	-	-	-	6/15/18	
150*O.N	0.231	0.5	0.951	1.827	-	-	-	-	-	-	-	-	6/7/18	200	0.235	0.474	0.857	1.598	2.883	-	-	-	-	-	-	6/15/18	
200	0.231	0.499	0.95	1.821	3.344	-	-	-	-	-	-	-	6/7/18	300	0.234	0.474	0.855	1.593	2.921	4.111	-	-	-	-	-	6/15/18	
300	0.23	0.496	0.94	1.793	3.333	4.692	-	-	-	-	-	-	6/8/18	400	0.234	0.474	0.856	1.594	2.916	4.136	5.199	-	-	-	-	6/15/18	
400	0.228	0.494	0.937	1.785	3.298	4.62	5.79	-	-	-	-	-	6/8/18	400 O.N	0.228	0.464	0.839	1.553	2.874	4.074	5.107	-	-	-	-	6/18/18	
500	0.231	0.497	0.94	1.788	3.298	4.595	5.794	6.789	-	-	-	-	6/8/18	500	0.228	0.466	0.844	1.576	2.881	4.08	5.184	6.16	-	-	-	6/18/18	
600	0.231	0.499	0.945	1.795	3.307	4.604	5.788	6.824	7.705	-	-	-	6/8/18	600	0.229	0.468	0.847	1.581	2.888	4.089	5.186	6.216	7.117	-	-	6/18/18	
630 N.T	0.229	0.496	0.942	1.795	3.312	4.61	5.793	6.82	7.77	8.29	-	-	6/8/18	629 ON/NT	0.228	0.466	0.844	1.575	2.879	4.074	5.165	6.183	7.148	7.535	-	-	6/19/18
630 NT.ON	0.228	0.492	0.932	1.774	3.27	4.544	5.701	6.7	7.619	7.914	-	-	6/11/18														
630 (in coil fixture)	0.199	0.487	0.959	1.83	3.36	4.672	5.854	6.878	7.826	-	8.431	-	6/20/18														

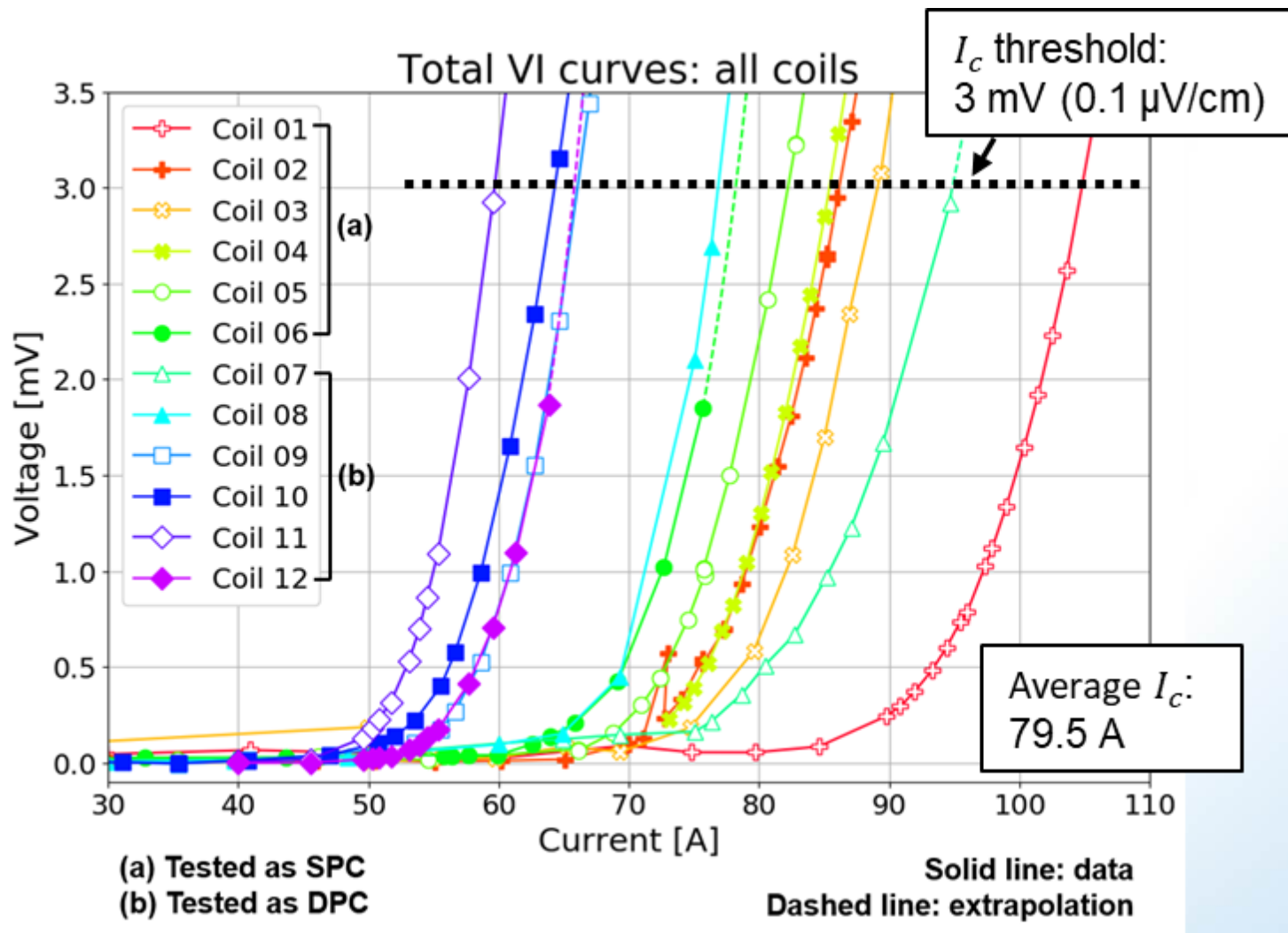
- **Resistance measurements were taken while Coils 1 and 2 were being wound at intervals of 10, 25, 50, 100, 200, 300, 400, 500, 600, and finished coil.**
- **The resistance of the inner turns decreased, due to compression, as more turns were wound. This signifies better conductor to conductor contact between the turns.**

COIL TESTING - SETUP



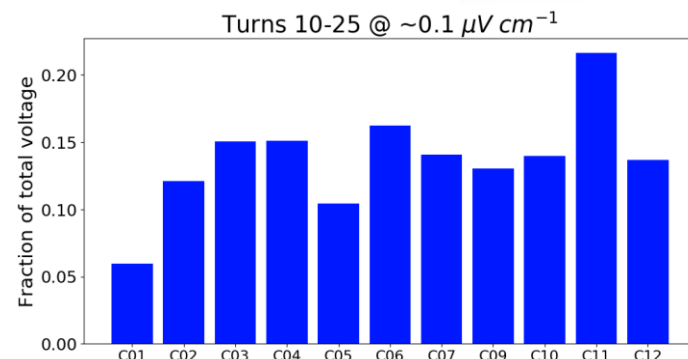
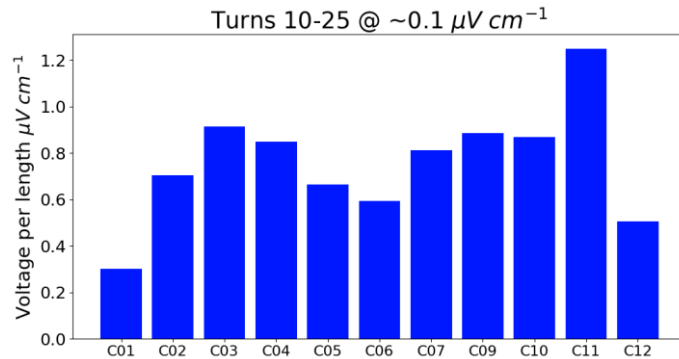
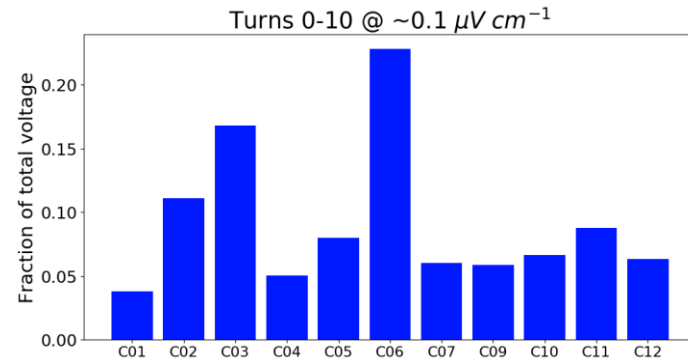
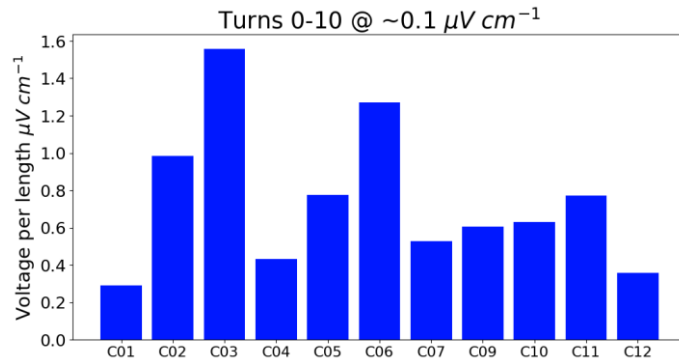
- Coils 1-6 were tested in a Single Pancake configuration;
- Coils 7-12 were tested in a Double Pancake configuration.

OVERALL LN2 TEST RESULTS FOR TESTED COILS



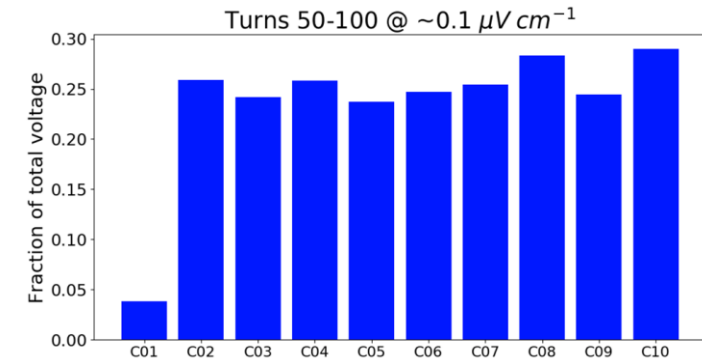
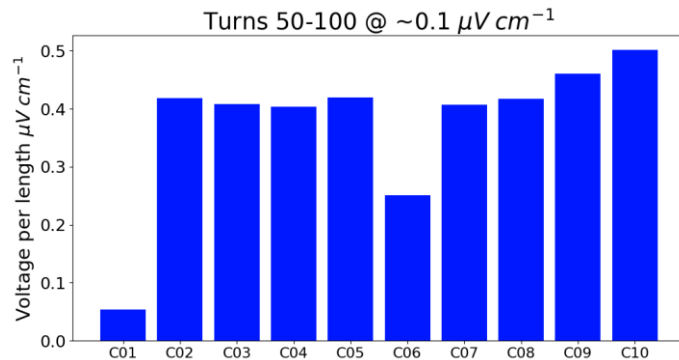
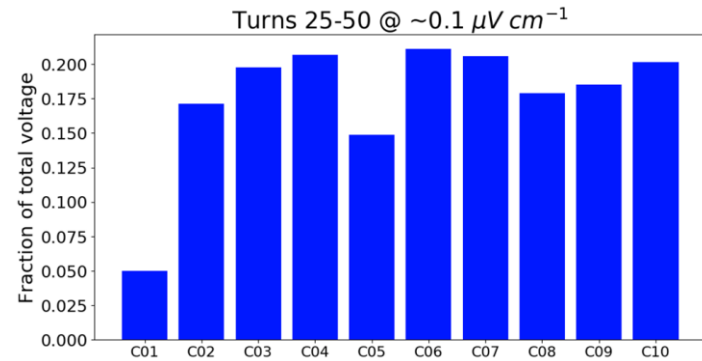
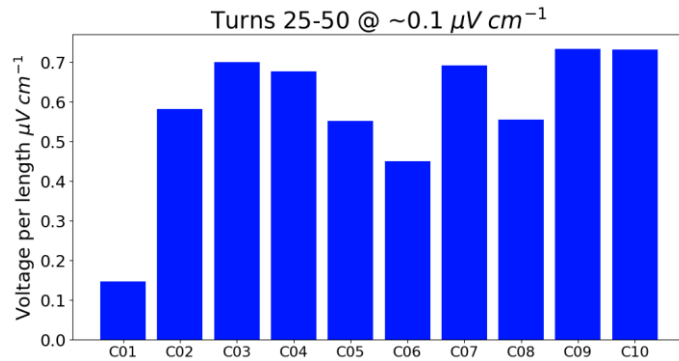
SIGNIFICANT VARIATION IN COIL I_c FROM COIL TO COIL

LN2 TEST RESULTS COMPARISON



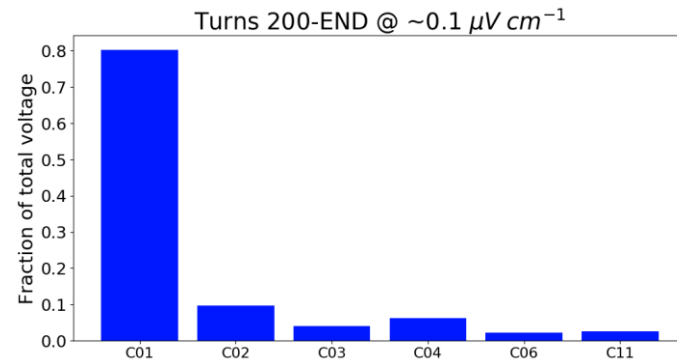
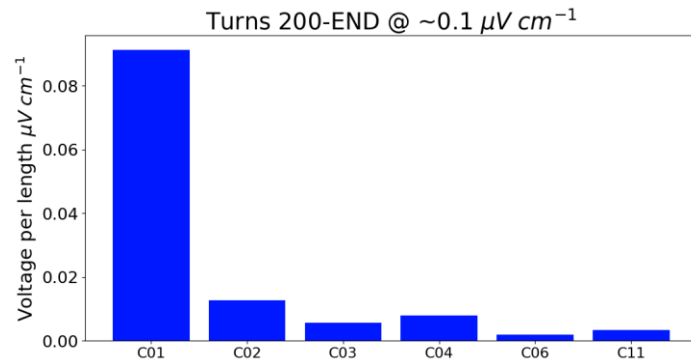
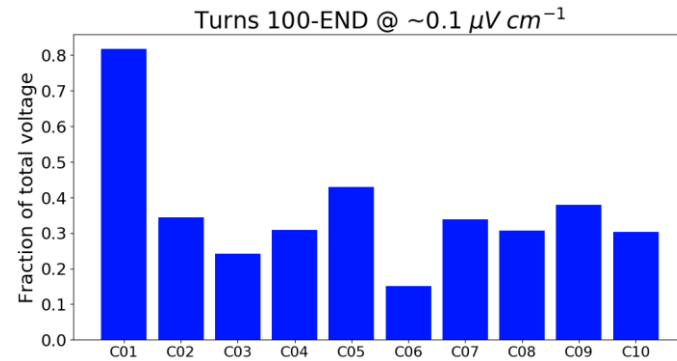
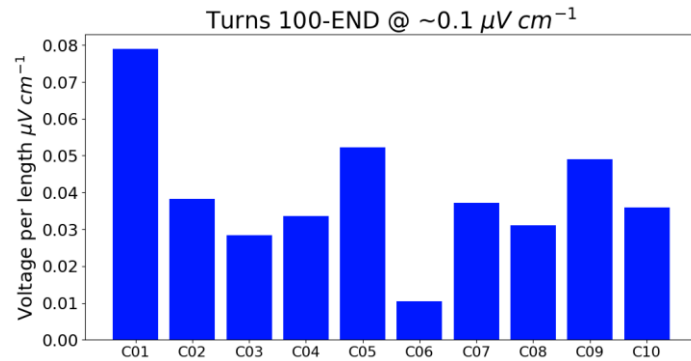
- **Variation in voltage distribution observed throughout all coils.**
- $\sim 10\%$ of the total coil voltage, on the average, was developing the first 10 turns
- $\sim 15\%$ of the total coil voltage, on the average, was developing between turns 10 and 25

LN2 TEST RESULTS COMPARISON (continued)



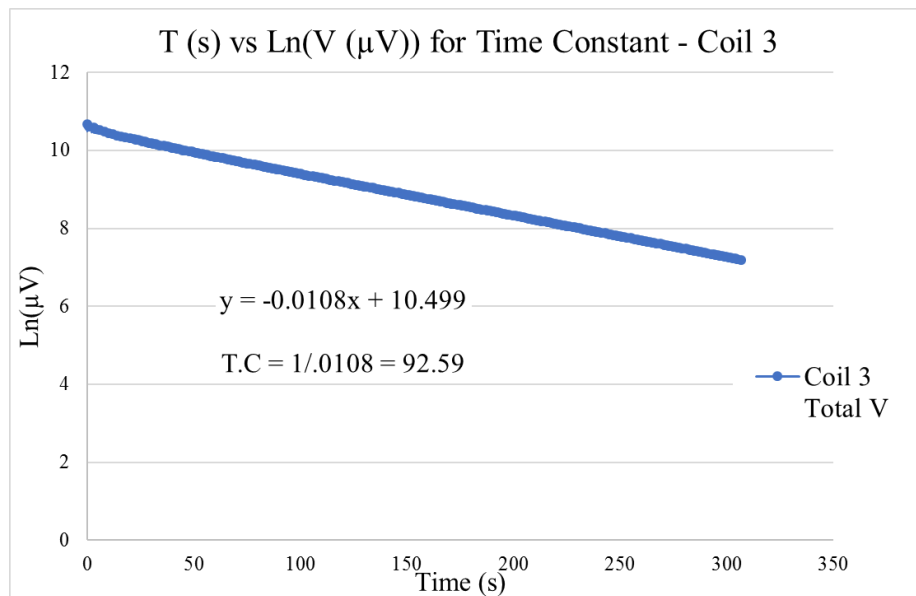
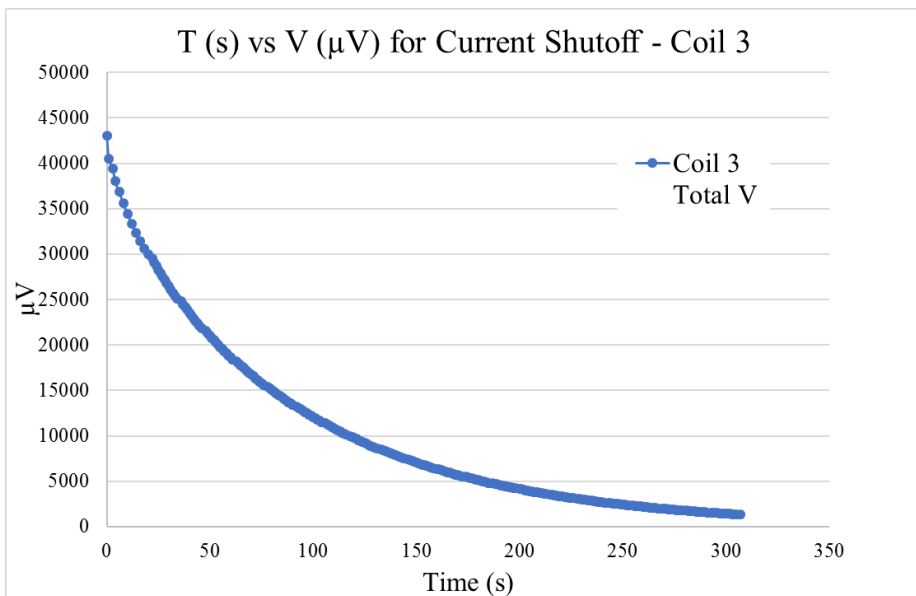
- Variation in voltage distribution observed throughout all coils.
- $\sim 18\%$ of the total coil voltage, on the average, was developing between turns 25 and 50
- $\sim 25\%$ of the total coil voltage, on the average, was developing between turns 50 and 100

LN2 TEST RESULTS COMPARISON (continued)



- Variation in voltage distribution observed throughout all coils.
- $\sim 30\%$ of the total coil voltage, on the average, was developing between turns 100 and the remaining ~ 520 turns of the coil
- Less than 10% of the total coil voltage, on the average, was developing between turns 200 and the remaining ~ 420 turns of the coil

CONTACT RESISTANCE AND TIME CONSTANT

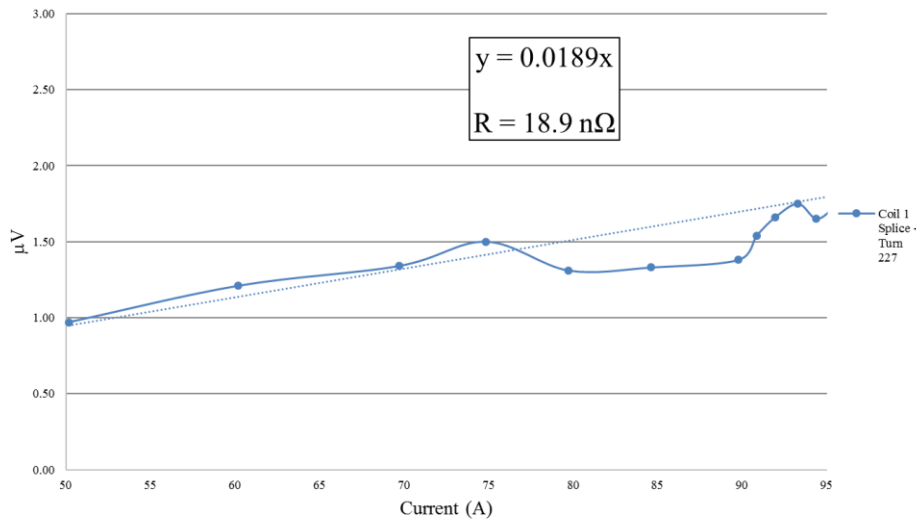


After Coil 3 was **ramped up and stabilized at 50 A (@ 77 K)**, the **power supply was shut off**. The time constant of Coil 3 was calculated to be 92.59 seconds. **Generally, higher contact resistance results in a smaller time constant.**

Coil #	Contact Resistance @ ~1 A (mV)	Time Constant (s)
1	9.1	78.4
2	8.3	97.1
3	8.4	92.6
4	8.5	95.2

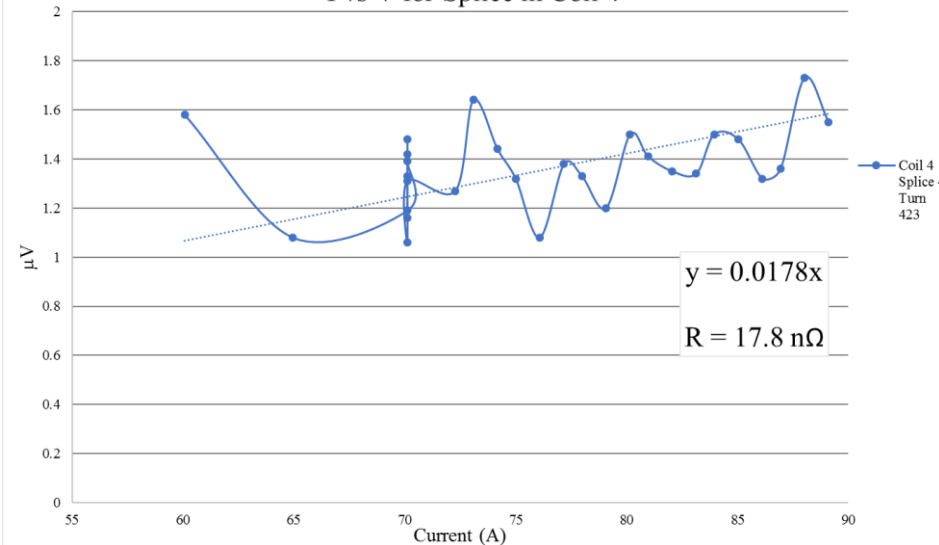
INNER-COIL SPLICE

I vs V for Splice in Coil 1



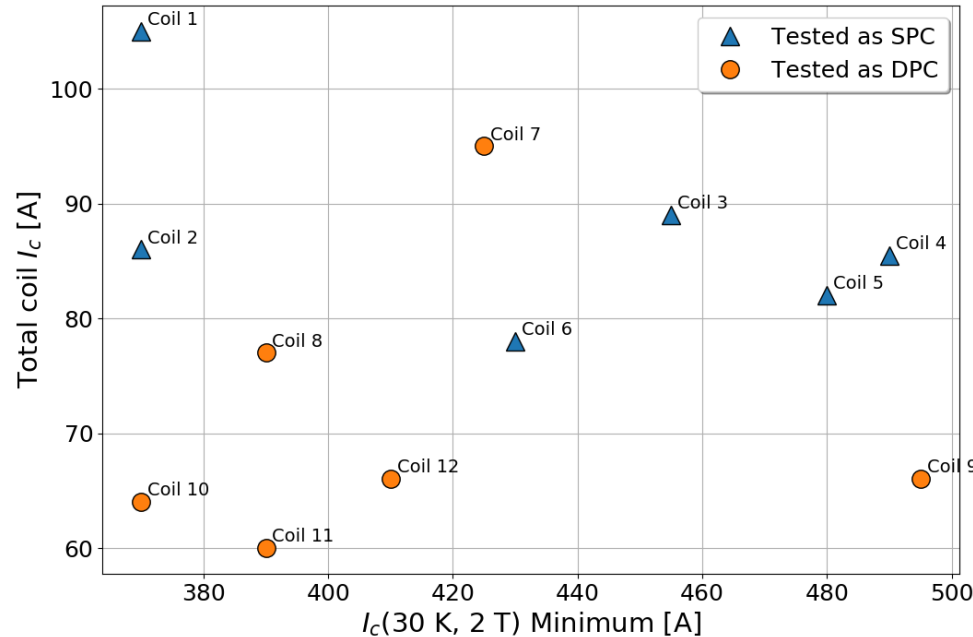
Above: I vs V curve for the splice in coil 1 @ turn 227. The resistance from the splice averages out to **18.9 nΩ**.

I vs V for Splice in Coil 4



Above: I vs V curve for the splice in coil 4 @ turn 423. The resistance from the splice averages out to **17.8 nΩ**.

CORRELATION BETWEEN CONDUCTOR I_c AND COIL I_c AT 77 K



Coil I.D	Coil I_c (A) (@3000 μ V)	Conductor Used	Amount Used (estimate)	Turns	Transfer Current	TapeStar I_c (77K)	30K, 2T I_c
Coil 1	105	20180509-2b "M3-1311-5"	90	0-227	570	578	450/560
		20180509-1a "M4-430-5"	215	227-630	383	390.7	400/370
Coil 2	86	20180509-1a "M4-430-5"	300	0-611	383	390.7	400/370
		20180509-1a "M4-430-5"		611-629	383	390.7	400/370
Coil 3	89	20180625-1a "M4-462-5"	143	0-346	405	407	475/525
		20180625-1d "M3-1309-6"	158	346-629	424	-	455
Coil 4	85.5	20180625-1b "M3-1309-6"	183	0-423	410	407	490
		20180625-1c "M3-1309-6"	117	423-624	399	-	-
Coil 5	82	20180509-1b "M4-430-5"	186	0-429	348	368.2	480/395
		20180625-1c "M3-1309-6"	116	429-627	399	-	-
Coil 6	78	20180730-4b "M4-465-5"	147	0-354	349	358.4	430
		20180911-1a "M4-478-2"	154	354-624	416.2	415.1	550/495
Coil 7	95	20180730-3a "M4-424-5"	113	0-283	385	369	425
		20180911-1a "M4-478-2"	187	283-626	416.2	415.1	550/495
Coil 8	77	20180730-1a "M3-1320-2"	175	0-406	589	594.6	390/430
		20180911-1a "M4-478-2"	125	406-627	416.2	415.1	550/495
Coil 9	66	20180911-1a "M4-478-2"	194	0-444	416.2	415.1	550/494
		20180911-2a "M3-1330-3"	106	444-623	382	363.7	-
Coil 10	64	20180730-1b "M4-424-5"	100	0-255	367	346	460
		20180730-2b "M3-1320-3"	106	255-466	599	599	410
		20180509-1a "M4-430-5"	56	466-557	383	390.7	400/370
		20180911-2b "M3-1330-3"	38	557-626	410.9	403.6	390
Coil 11	60	20180911-2b "M3-1330-3"	100	0-249	410.9	403.6	390
		20181116-2 "M4-470-55"	200	249-622	430	449.2	430/390
Coil 12	66	20180911-1b "M3-1326-3"	100	0-255	370.6	354.3	410/490
		20181116-1 "M3-1324-A"	200	255-630	391	373.5	500/485

There was **no obvious or significant correlation** between quality of the conductor (defined though Transport, TapeStar, and In-Field (@30K, 2T I_c measurements conducted by the manufacturer) and the quality of the coil performance at 77 K (defined by its $I_c - I_c$ threshold being 3mV as per .1 μ V/cm industry standard) after winding.

SUMMARY

- Winding Techniques, Procedures, and Instrumentations have been optimized for consistency in coil quality.
- 16 coils have been wound; 12 coils have been tested in LN2.
- The 12 tested coils show an average I_c of 79.5A @ 77K.
- **Coil performance varies from coil to coil.**
- **Inner-Coil splices show ~18 - 19 n Ω of resistance at 77K.**
- **Generally, higher contact resistance results in a smaller time constant**
- **Approximately 70% of the coils voltage was developed within the first 100 turns – where the magnetic field is the highest**
- No significant correlations was found between quality of the conductor (defined though Transport, TapeStar, and In-Field (@30K, 2T I_c measurements conducted by the manufacturer) and quality of the coil (defined by its I_c) after winding.