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# Analysis of AC Power System for JT-60SA Superconducting Magnets

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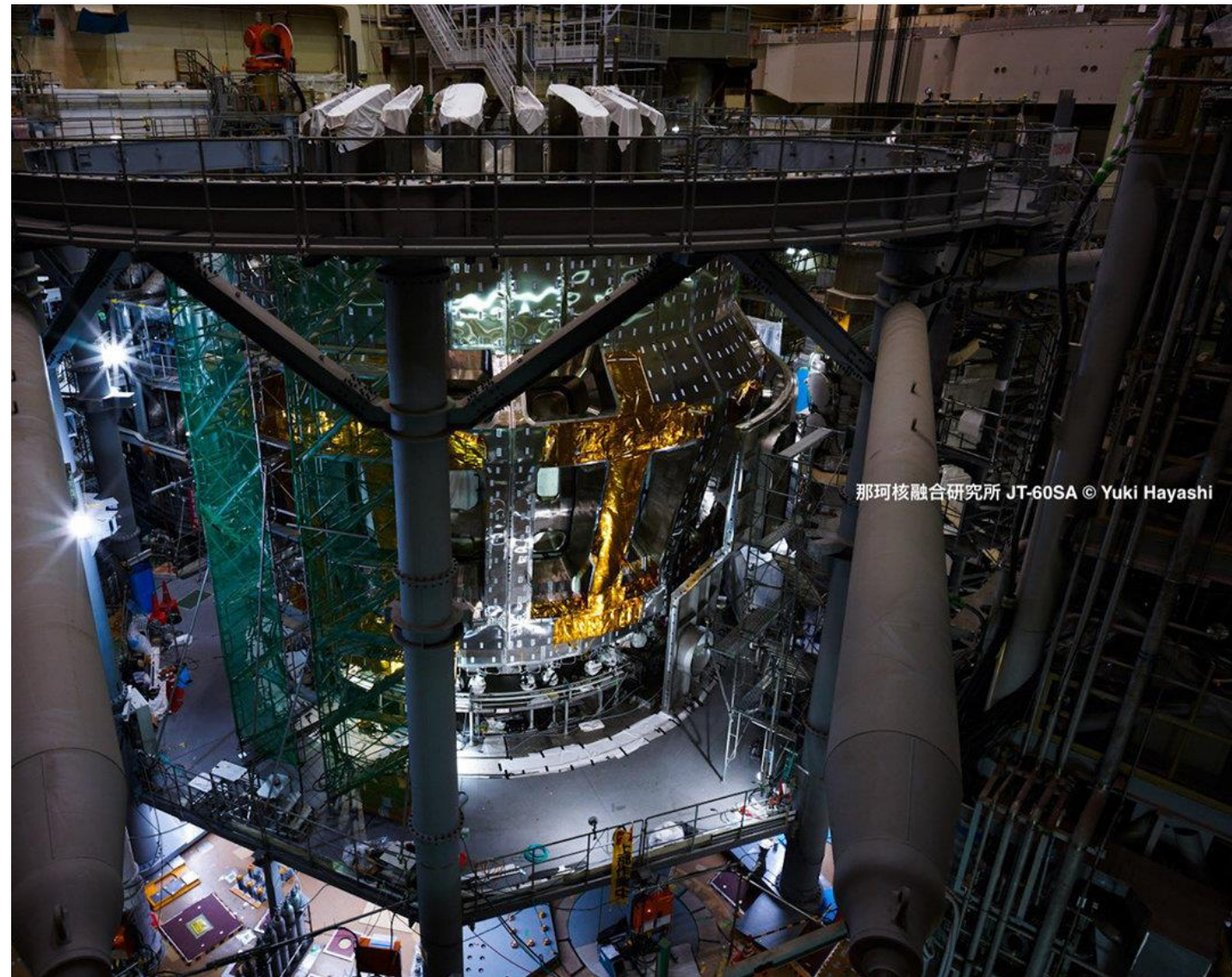
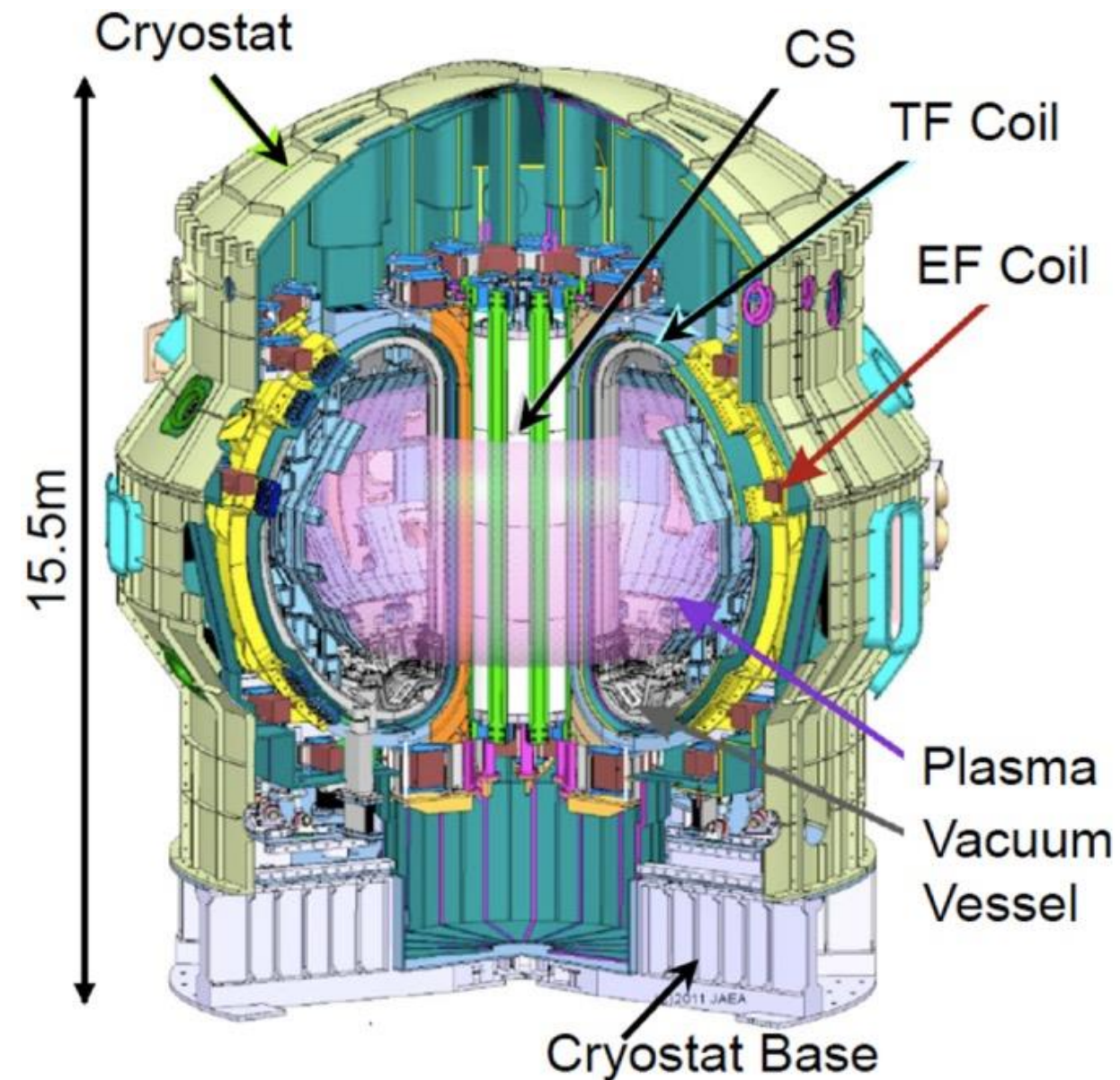


National Institute for Quantum and Radiological Science and Technology



# One of the largest tokamak JT-60SA

Assembly and commissioning ongoing aiming operation in Sep. 2020.



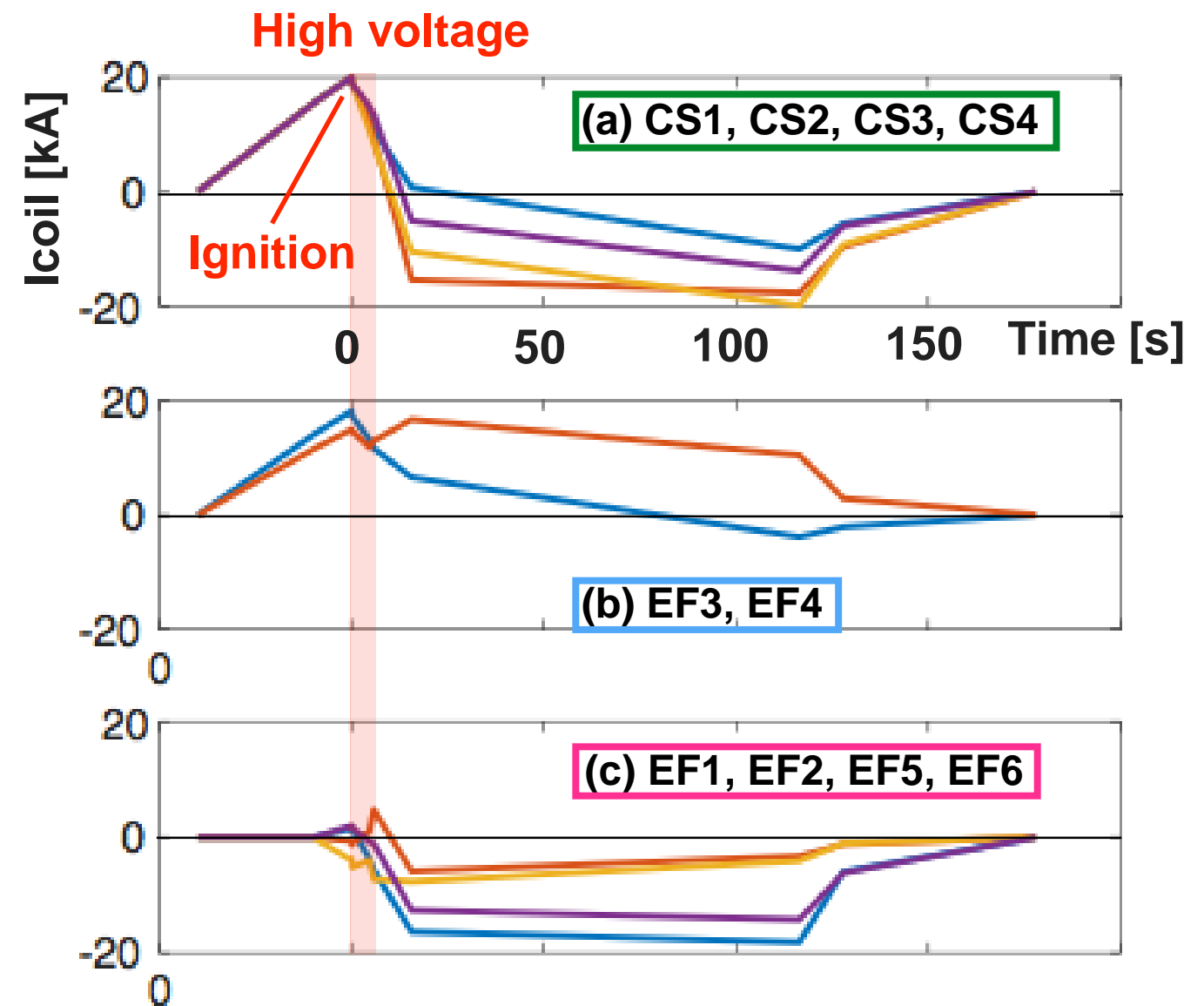
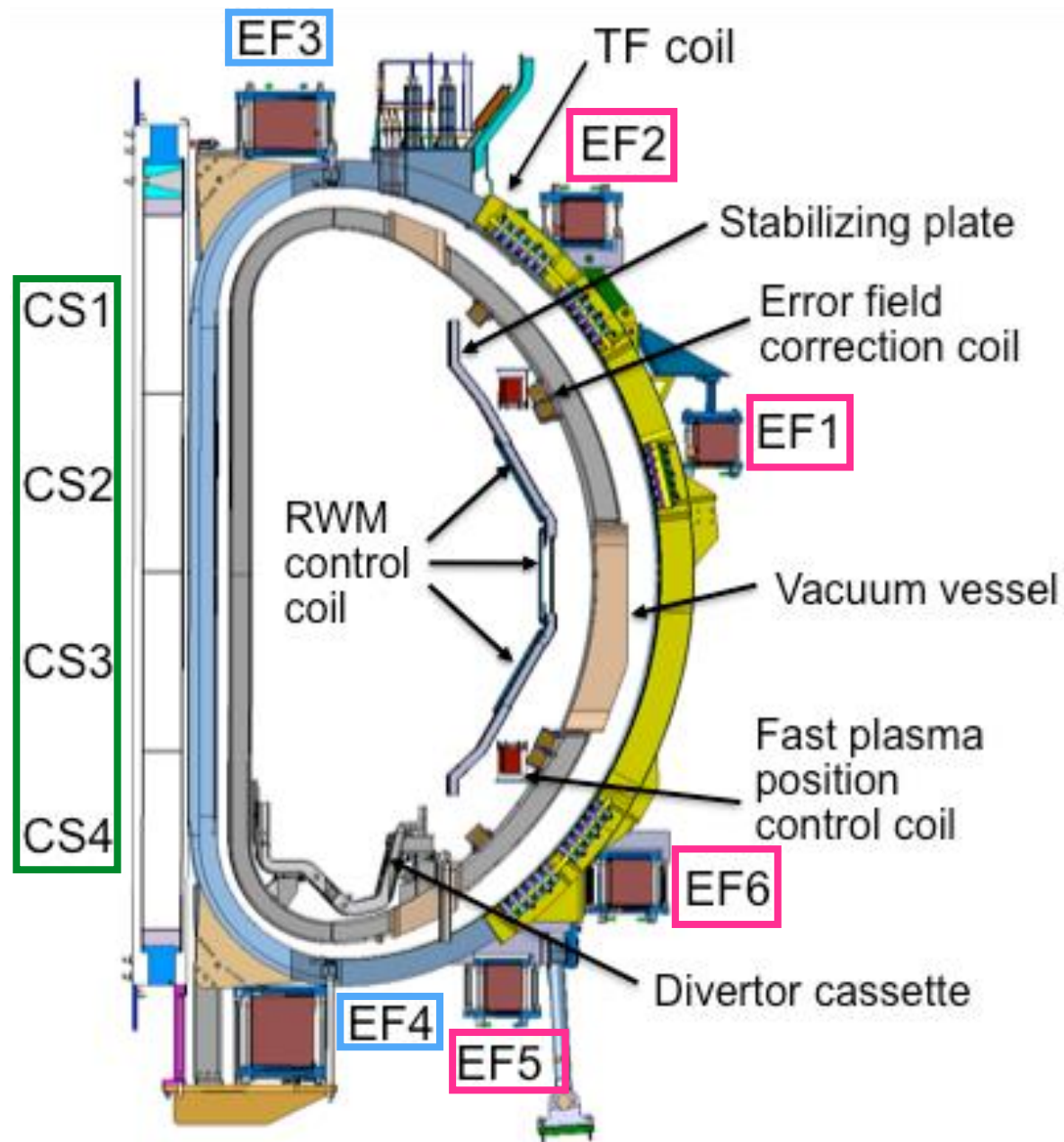
Y. Kamada. et al., Nucl. Fusion, 55, No.10

- **Main magnets are super conducting** for long operation (~ 180 s)
- 10 Poloidal field coils (4 CS, 6 EF coils)
- 18 Toroidal field coils (2.25 T@center of plasma, stored energy 1 GJ)



# Current waveforms in the operation

## Drastic current change around plasma ignition and ramp-up



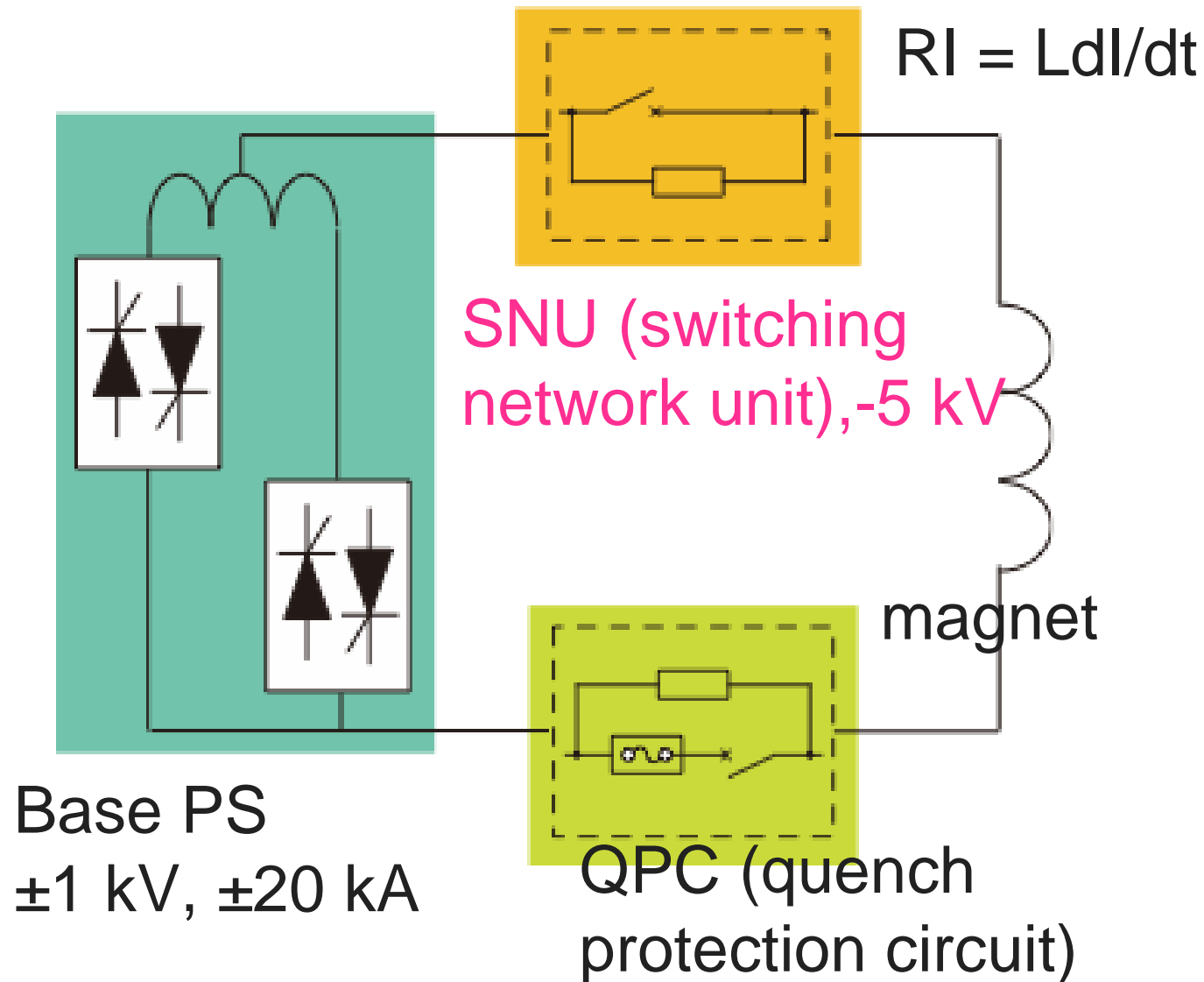
PID (v3.8) Scenario #1. Full current, Inductive, DN, 41 MW

- CSs induce current in plasma for heating and confinement
- EF coils control shape and position of plasma
- High voltage ( $< 5$  kV) is necessary only at ignition and ramp-up phase.

# Circuit Configuration for PF magnets

## High voltage converter needs large reactive power

for CS,EF3,4



Base PS  
 $\pm 1$  kV,  $\pm 20$  kA

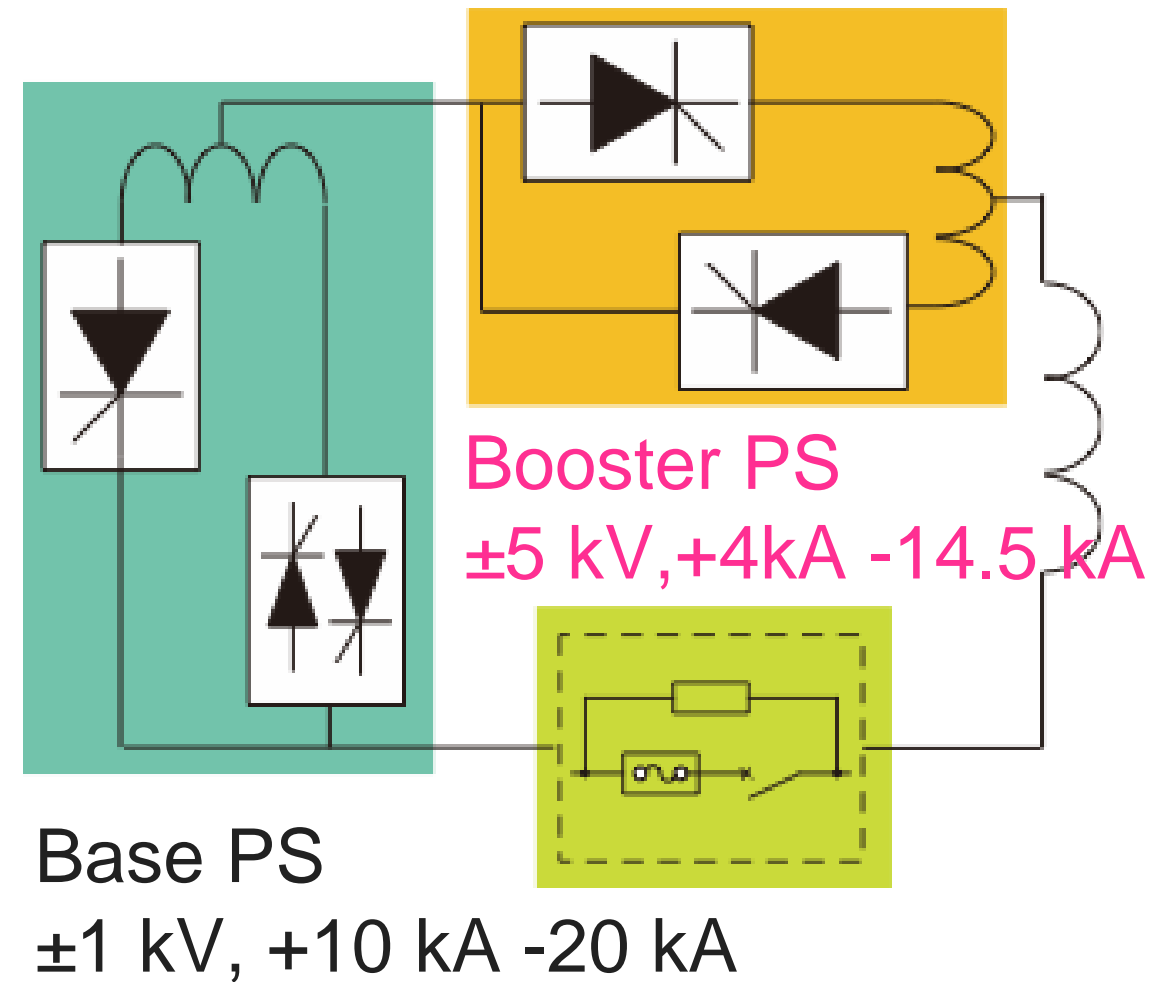
SNU (switching network unit), -5 kV

QPC (quench protection circuit)

magnet

- Resistor is inserted for induction and initiation of plasma
- The resistor is bypassed at 5 s after the ignition

for EF1,2,5,6



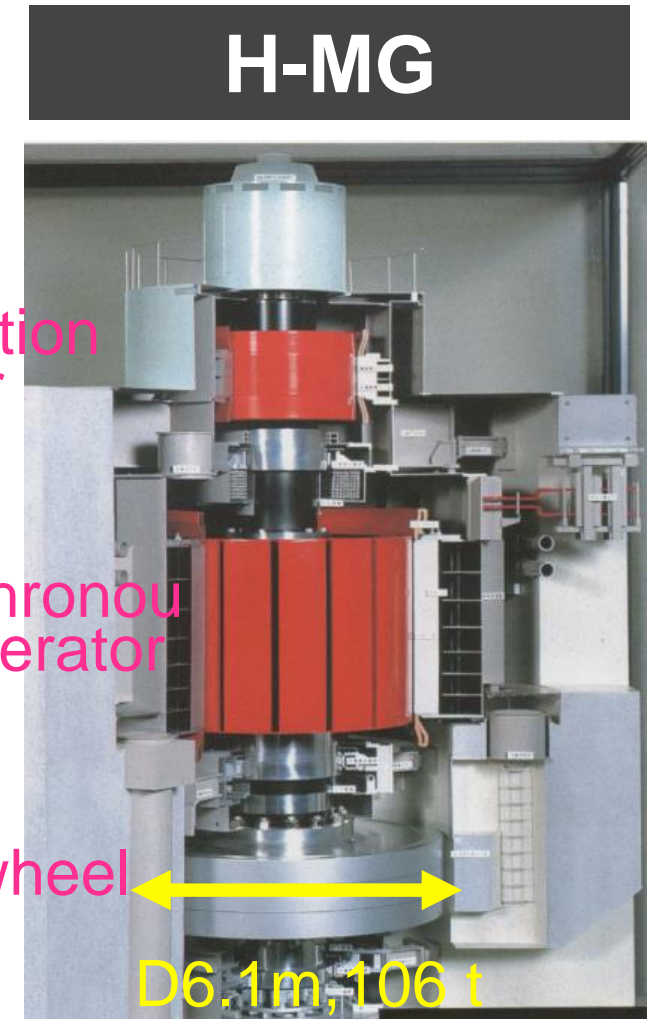
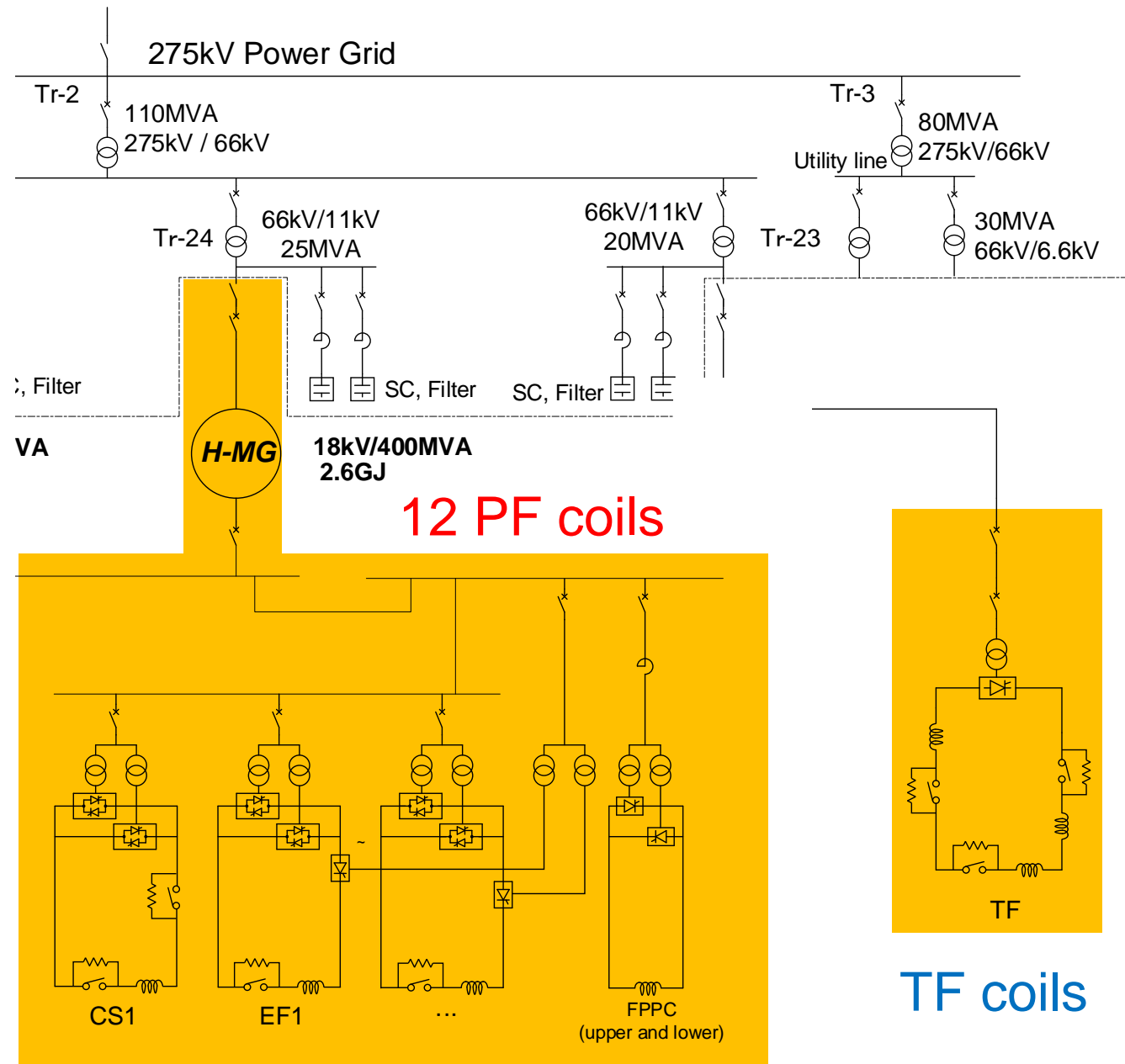
Base PS  
 $\pm 1$  kV, +10 kA -20 kA

Booster PS  
 $\pm 5$  kV, +4kA -14.5 kA

- Booster PS is used for highspeed control of plasma shaping
- **Low voltage operation** of Booster PS cause large reactive power

# Dedicated motor-generator for PF Magnets

250 MVA is required for PF magnets power supplies in total



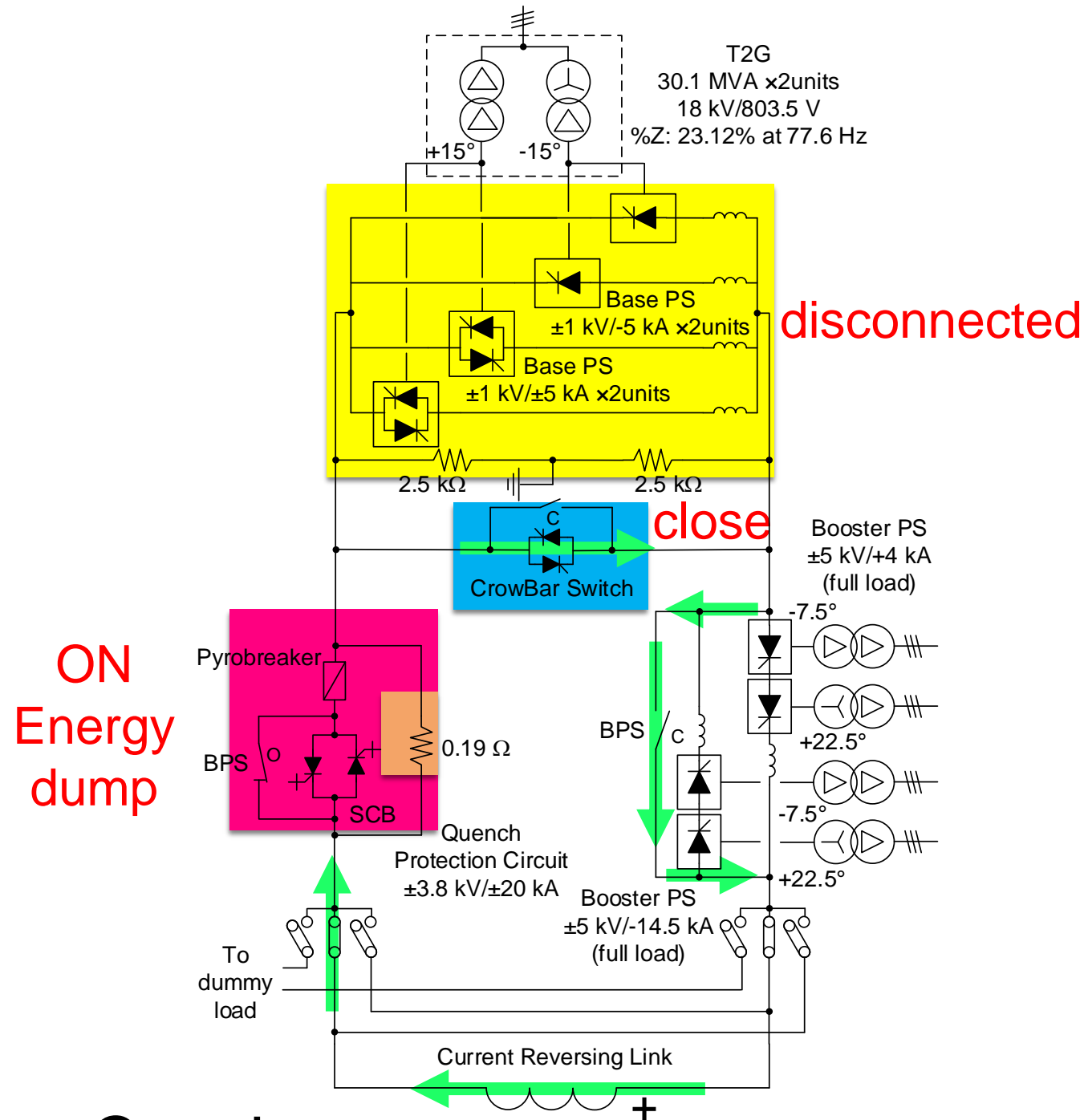
Output Power	400 MVA
Voltage	18,000 V
Current	12,830 A
Power Factor	0.62
Rotation	582~406.5 rpm
Frequency	77.6~54.2 Hz
Discharge Energy	2.650 GJ

## Issues

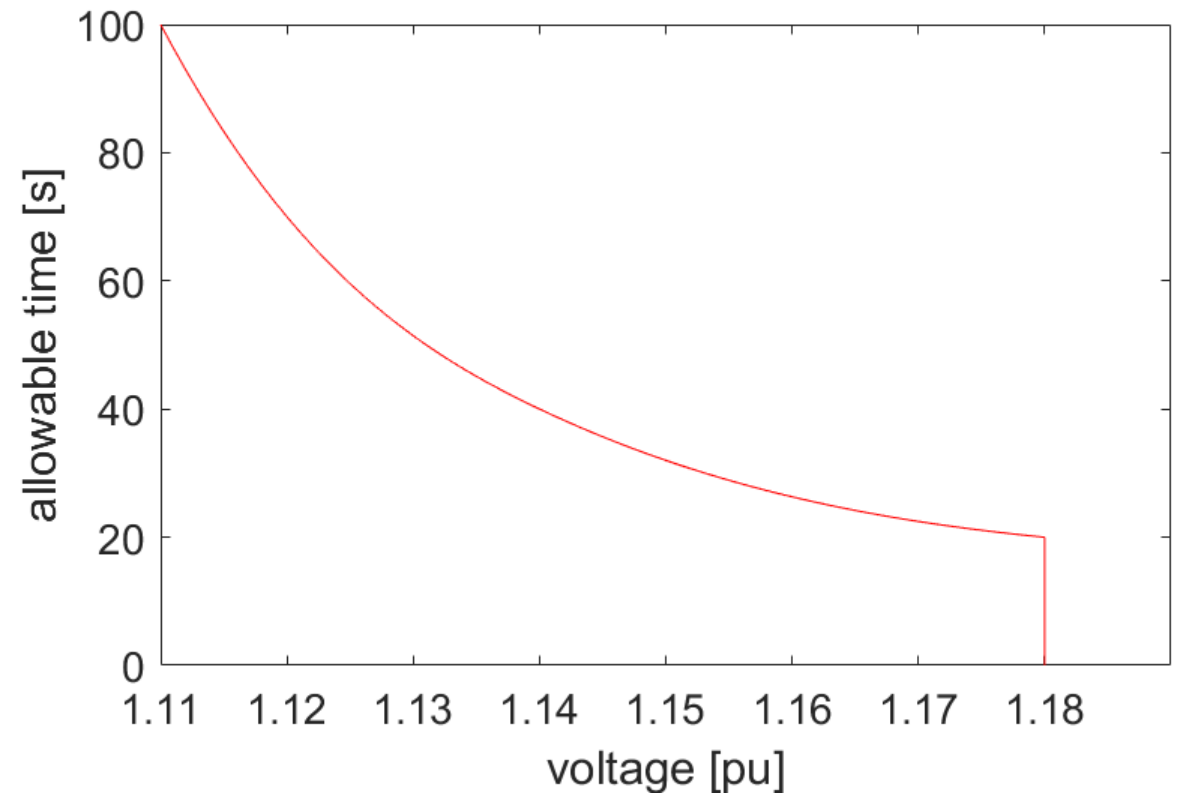
- **Over voltage** due to breaking large power
- **Harmonic current** (heating in damper winding)

# Issue1. Over voltage due to magnet quench

All PF circuits start fast discharge even when only one magnet quench



## Criteria



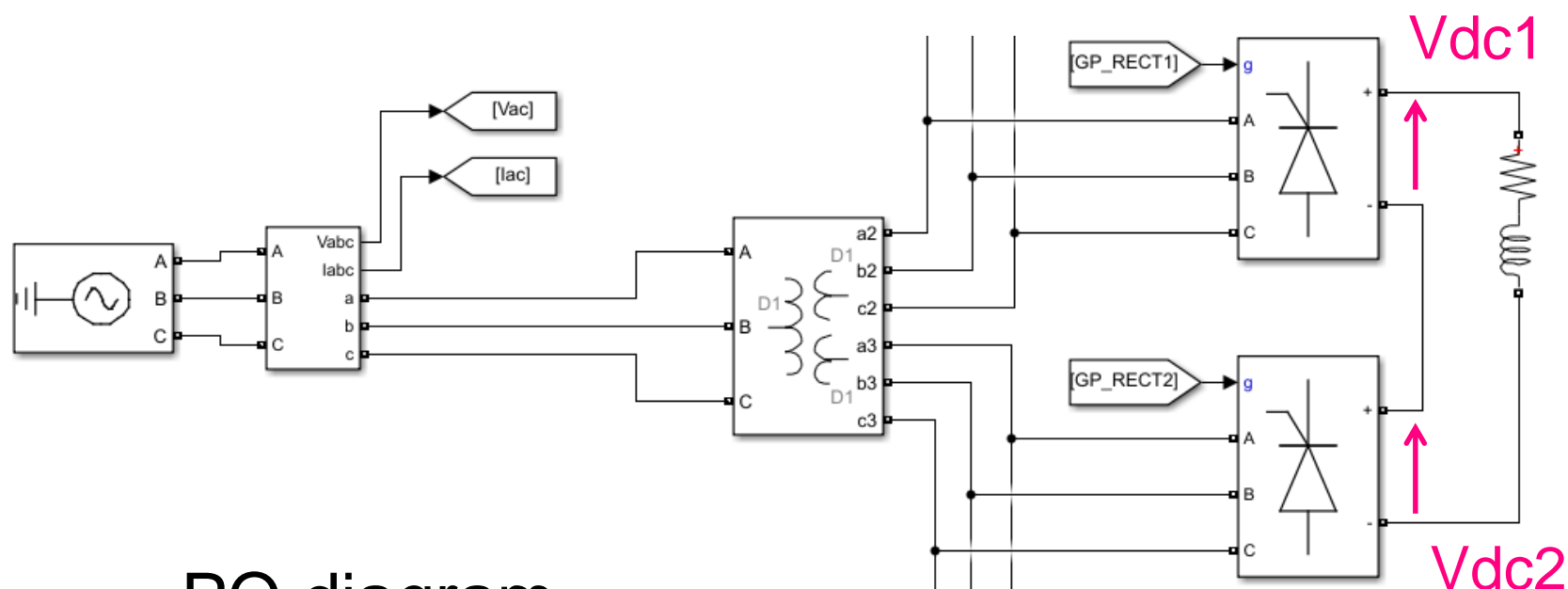
- inverse time characteristics
- definite time characteristics

- Crowbar (thyristor and mechanical hybrid) breaks load in a moment (~ ms)
- Voltage controller of H-MG can not suppress the rapid change
- **Power reduction** is only way to reduce the over voltage

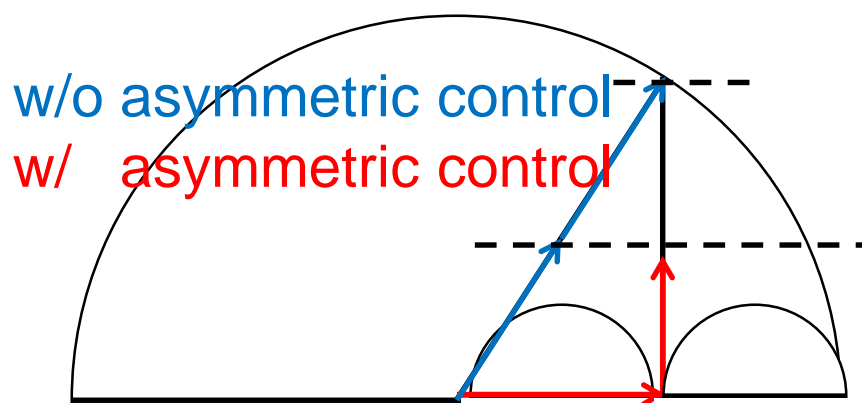
# Issue 2. Harmonics due to reactive power reduction

## “Asymmetric control” reduces reactive power of series converters

### How to split Vdc



### PQ diagram



### Output voltage

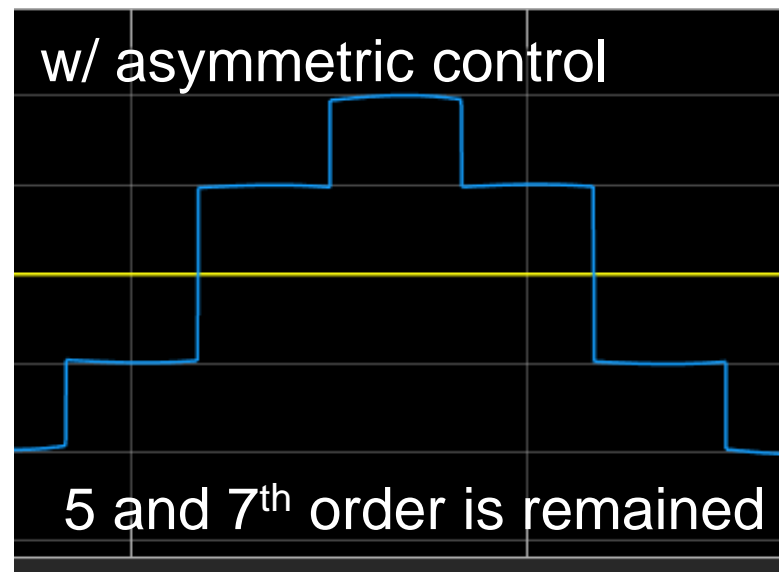
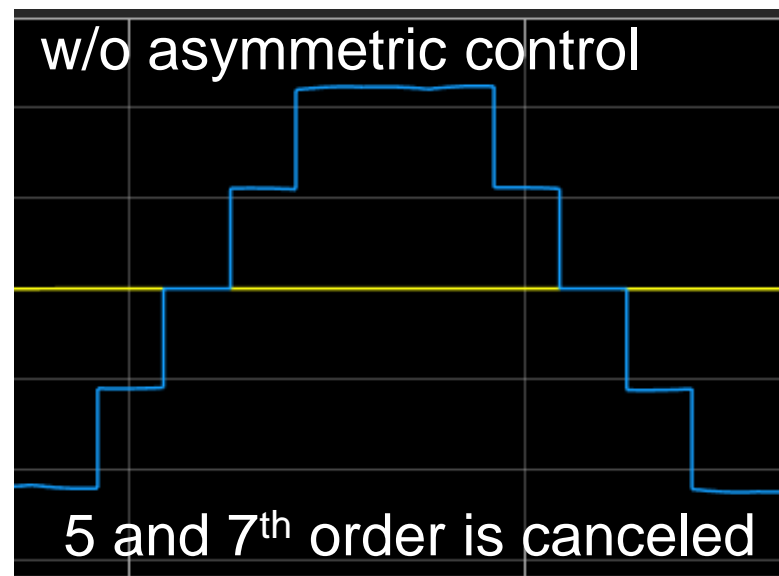
$$V_{DC} = 1.35 \times V_{ac} \times \cos(\alpha)$$

### Active and reactive power

$$P = 1.35 \times V_{ac} \times I_{DC} \cos(\alpha)$$

$$Q = 1.35 \times V_{ac} \times I_{DC} \sin(\alpha)$$

### Current in primary side

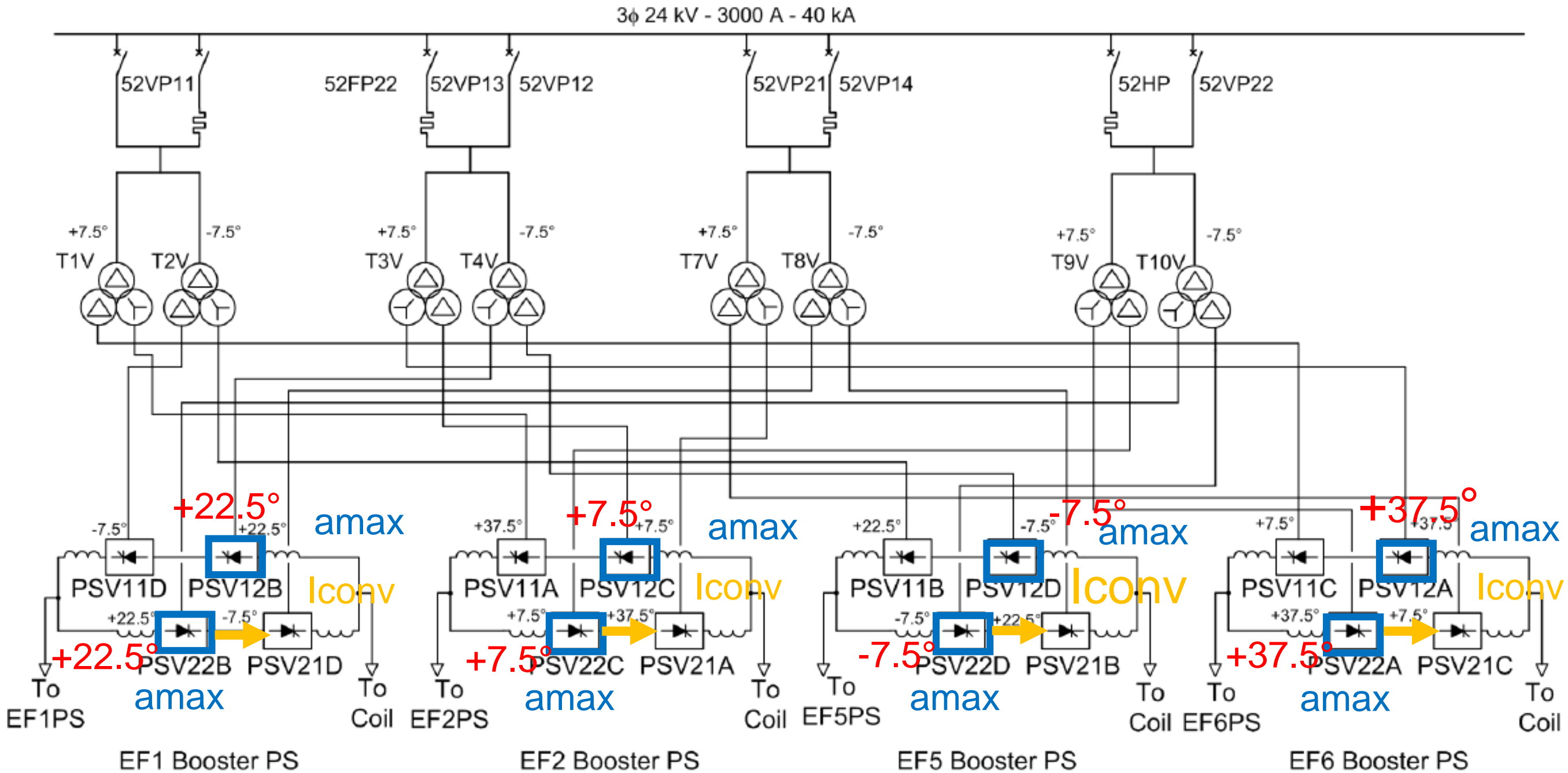


- Vdc is proportional to active power P and reactive power Q
- Reactive power can be reduced by changing distribution of Vdc
- **Criteria of harmonics is  $I_{eq2} = \sqrt{\sum \frac{N}{2} \times I_N^2} < 15\%$  of nominal current**



# How to reduce harmonic current

## Difference power supplies cancel harmonics together



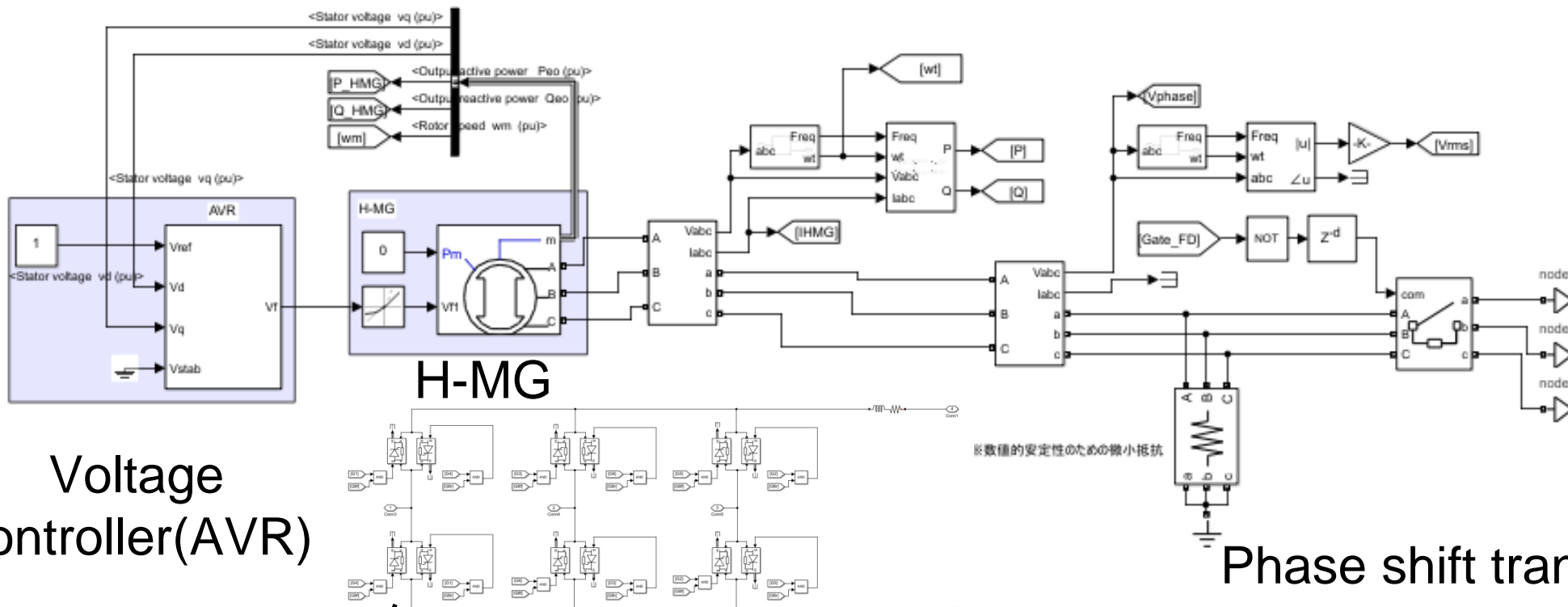
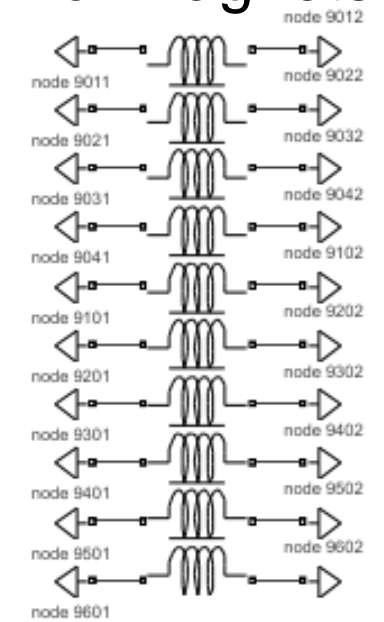
- This assumption depends on command phase angles and amplitude of current for each converters during discharge
- The effect should be confirmed by integrated model of PS system



# Integration model

All components are implemented without simplification in simulink

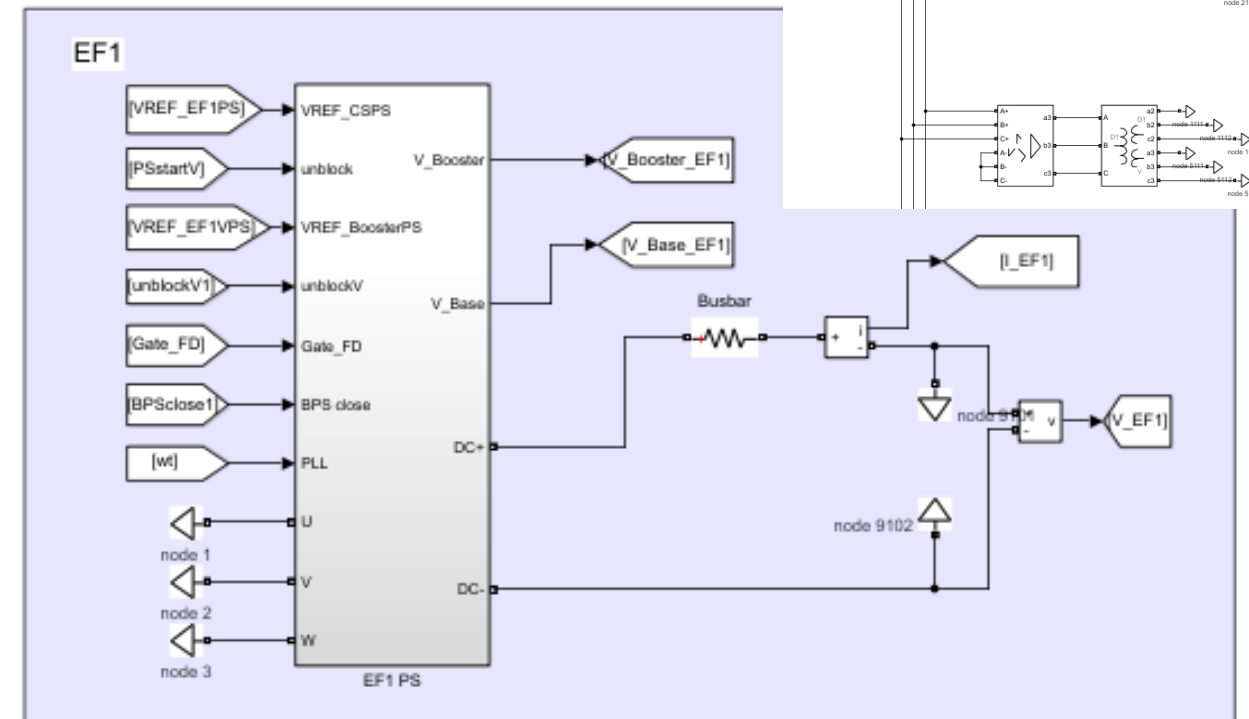
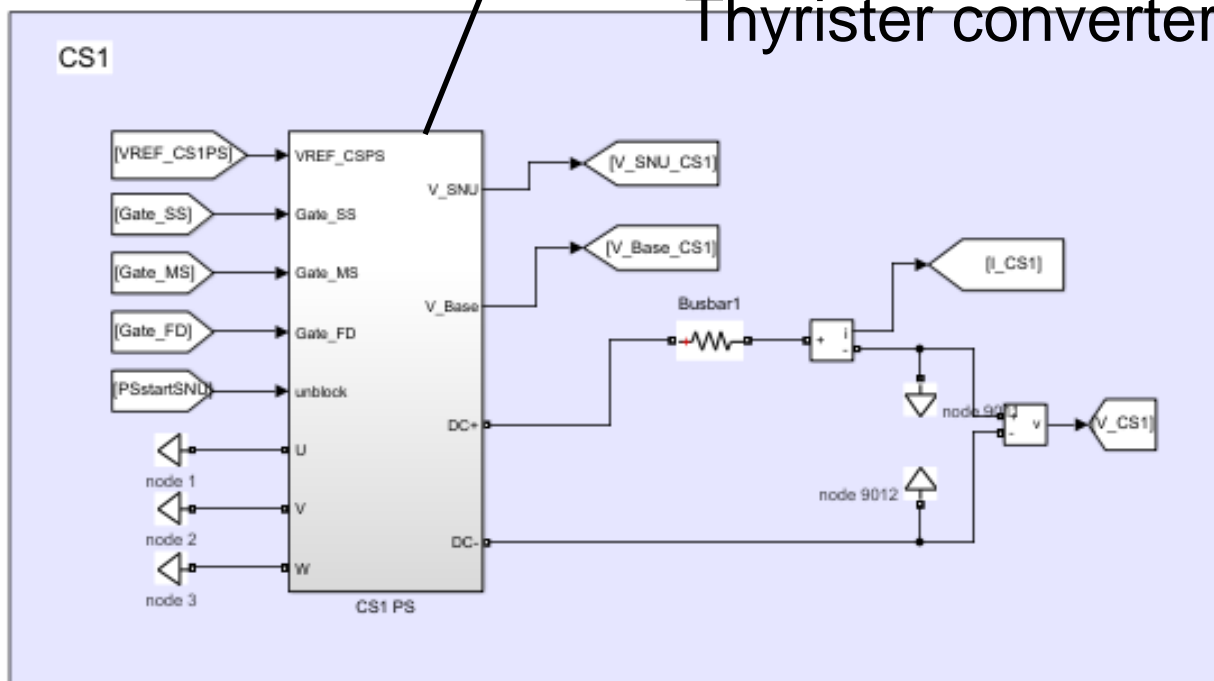
Mutual coupling of magnets



Voltage controller(AVR)

Phase shift transformers

Thyristor converters

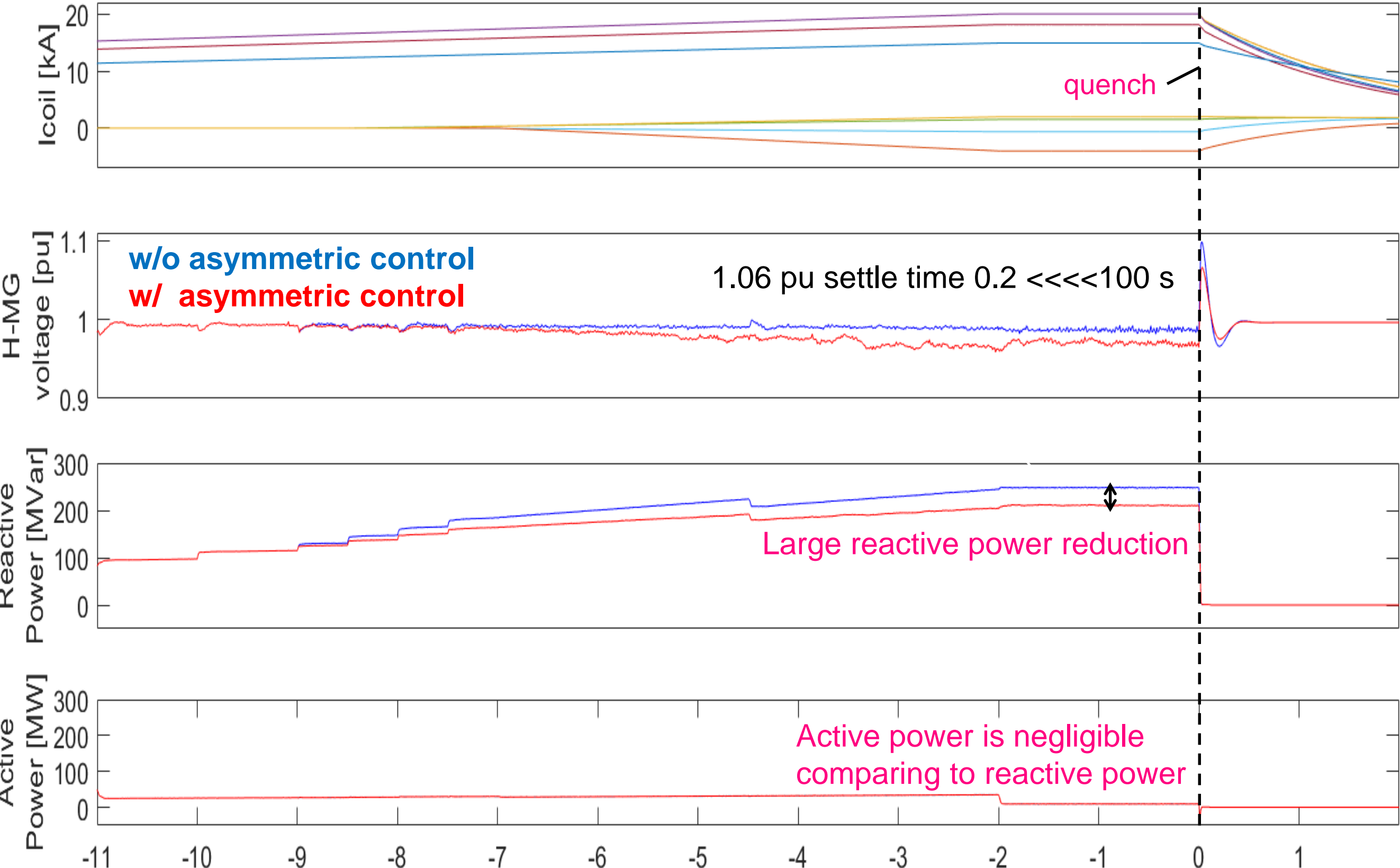


Booster PS type x 4 (EF1-4)

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# Overvoltage estimation at quench

Pass criteria +6 % < +18 % (definite time)

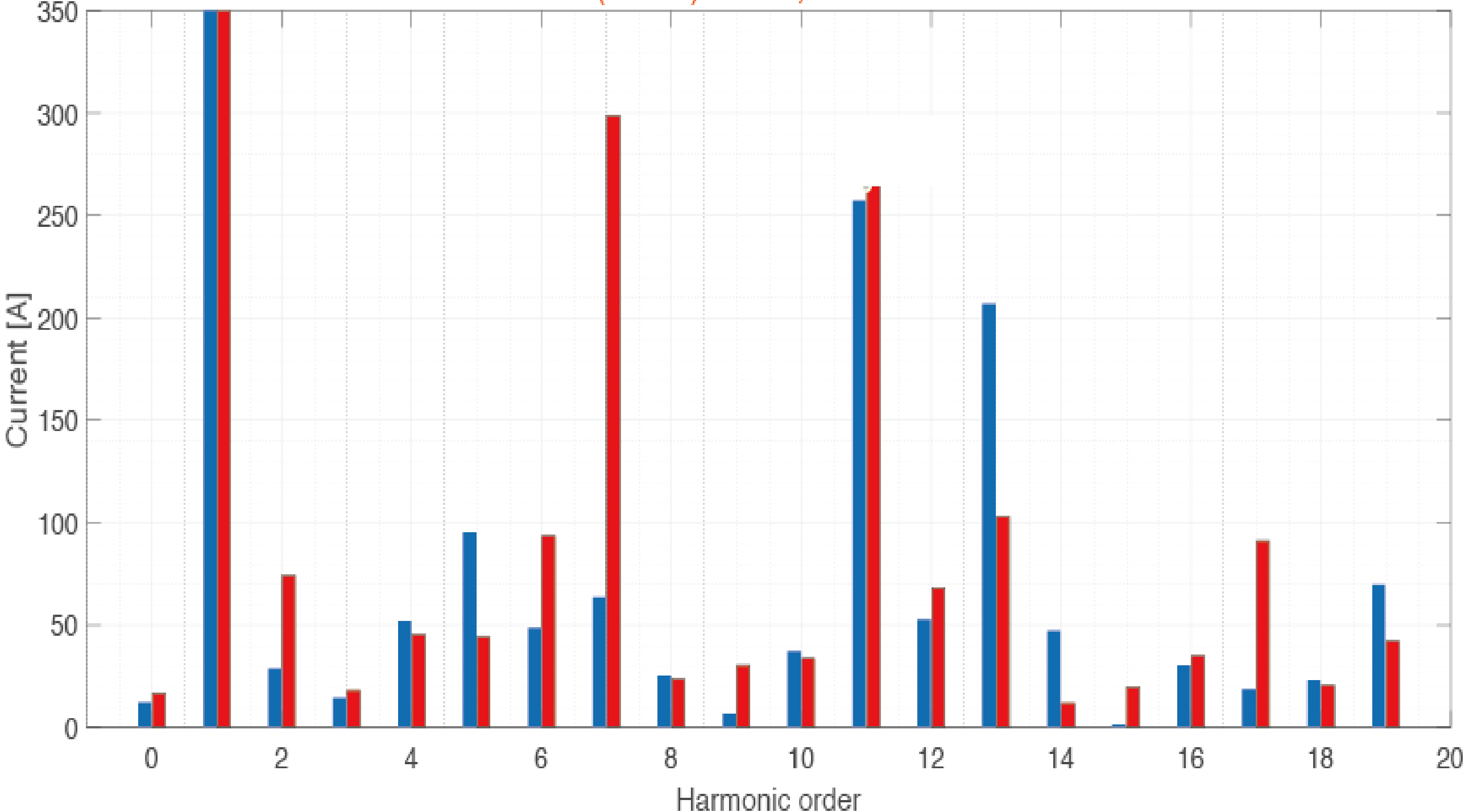


# Harmonic current estimation

**$I_{2eq} = 5.96\% \llll 15\%$  @  $t = 0.1\text{ s}$  (around ignition)**

Fundamental (71.7Hz) = 9518 , THD= 5.00% @  $t = 0.1\text{ s}$

Fundamental (71.7Hz) = 8915 , THD= 6.04% @  $t = 0.1\text{ s}$



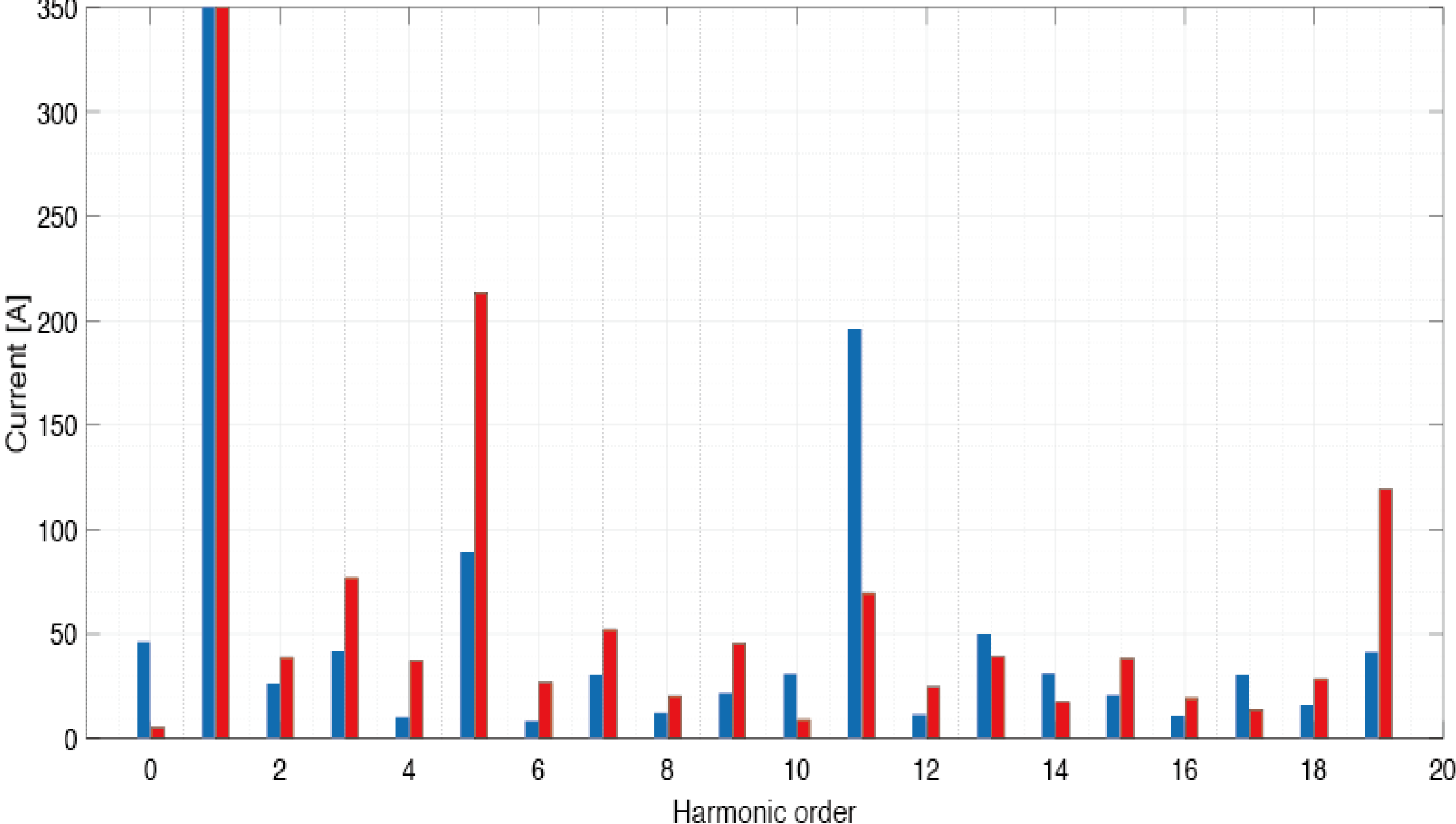


# Harmonic current estimation

**$I_{2eq} = 3.51\% \lll 15\%$  @  $t = 4.9\text{ s}$  (just before Booster PS stop)**

Fundamental (72.2Hz) = 9159 , THD= 4.26% @  $t = 4.9\text{ s}$

Fundamental (72.2Hz) = 7411 , THD= 5.48% @  $t = 4.9\text{ s}$



# Conclusion

- Large reactive power is required for PF magnet system in JT-60SA
- At magnet quench, over voltage of H-MG is happened due to load breaking
- Asymmetric control can reduce reactive power
- However, asymmetric control causes harmonic current
- In JT-60SA, phase shift transformer is optimized for reduction of harmonics
- Series connected converters for each magnet can reduce the harmonics together
- Over voltage and harmonic current is estimated using integration model of PS system
- Over voltage is suppressed less than 6 % (criteria < 18 %)
- Harmonic current is also suppressed less than 6 % (criteria < 15 %)