

Investigation of multipole components in MCBRD

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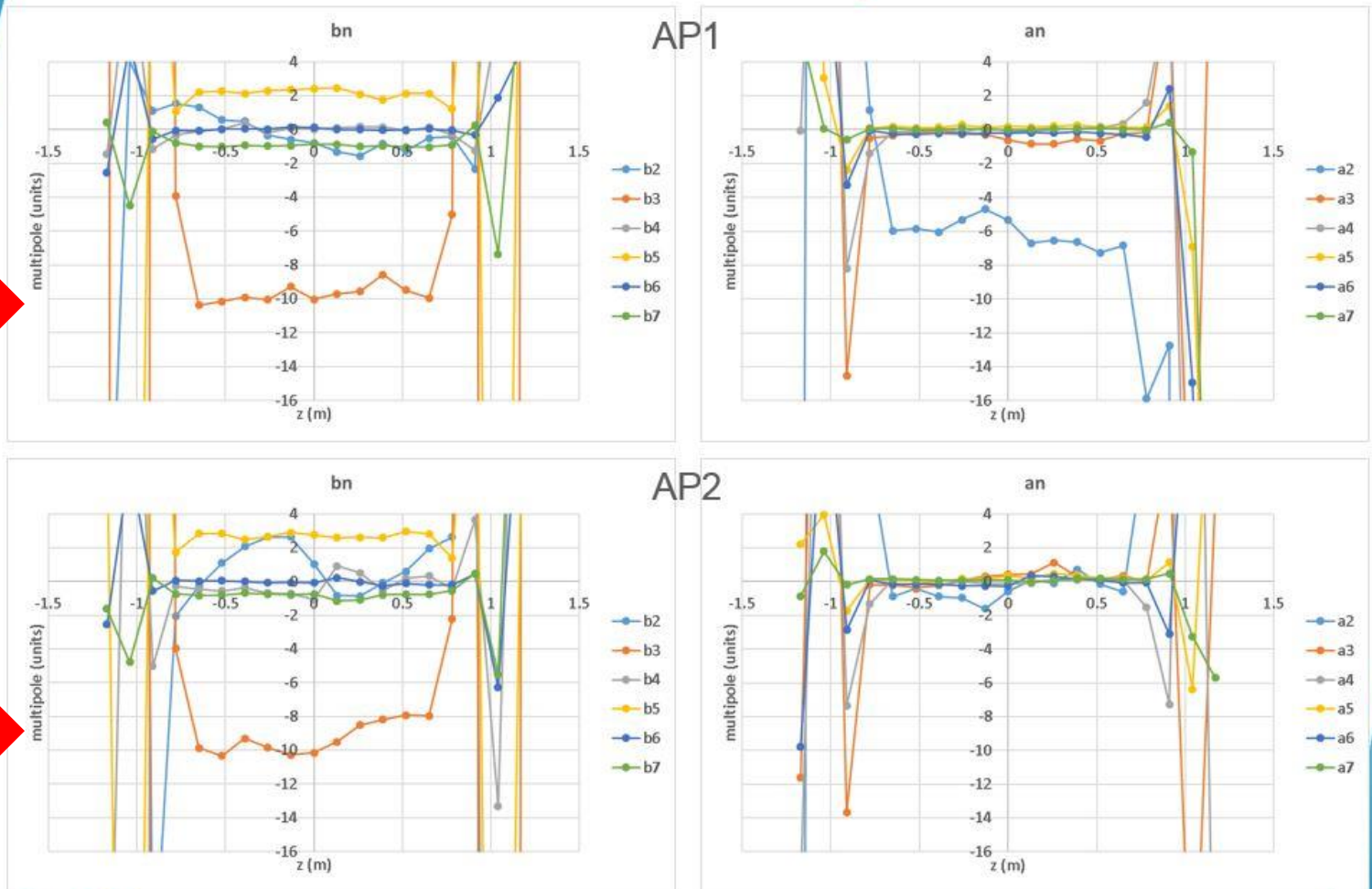
18/9/2018

The issue

- When measuring the field quality at warm of MCBRD, a large component of B3 was seen
- The measurement was confirmed by two methods, so I will assume it is real
- Although this component is still within specification, it would be nice to understand why it is there

Effect seen at both apertures

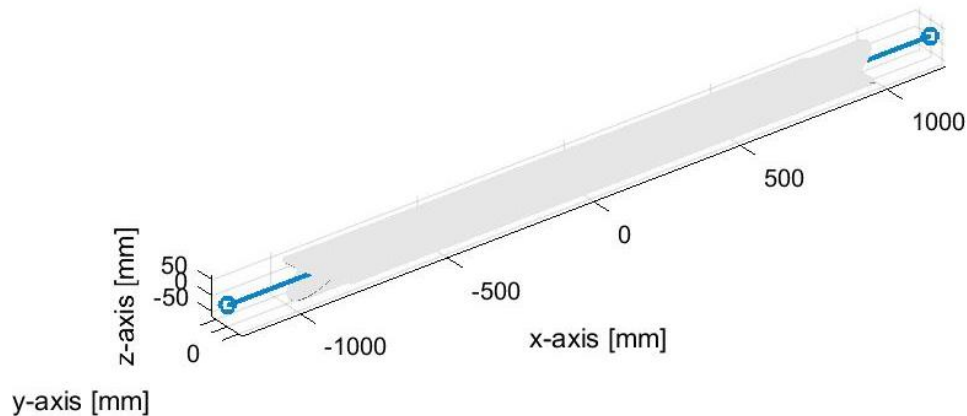
MCBRDP1 at room temperature 3



“allowed multipoles are larger than expected but field quality is within specifications”

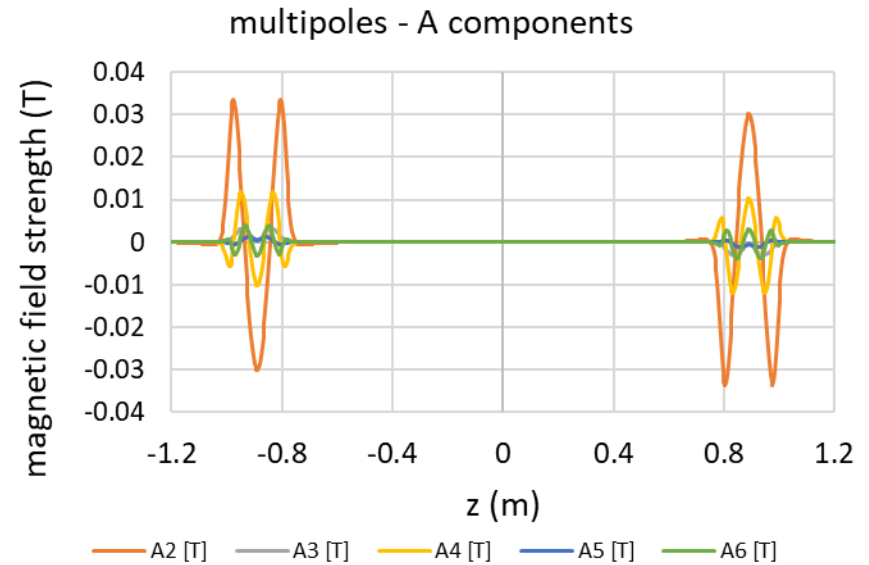
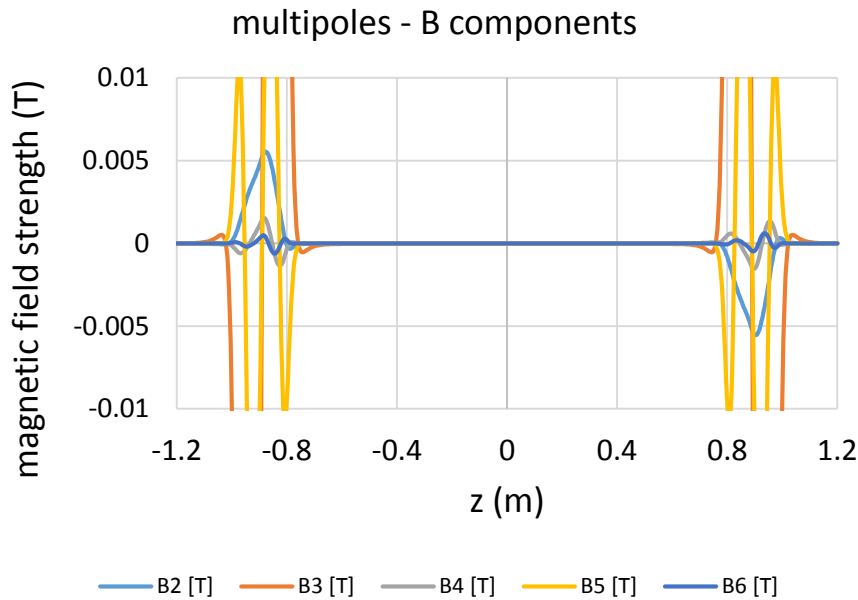
...but first, look at the ideal case

- CCT design: it has the virtue of excellent field quality
- How does the field look like?

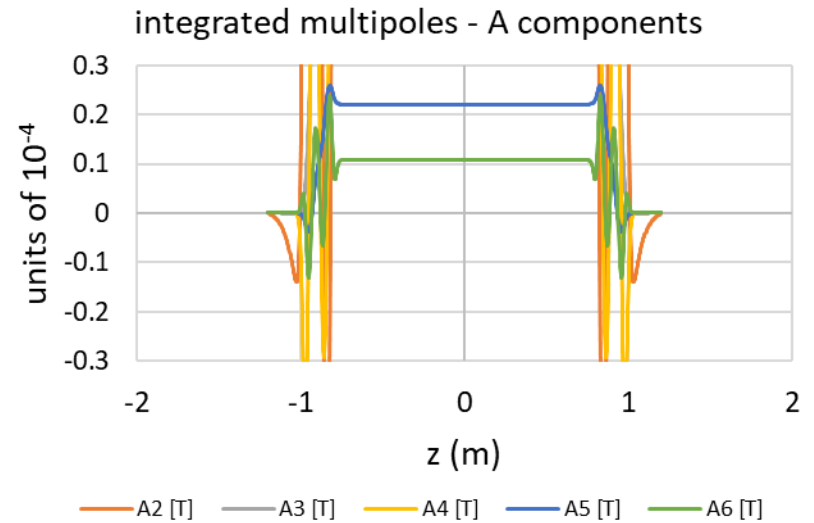
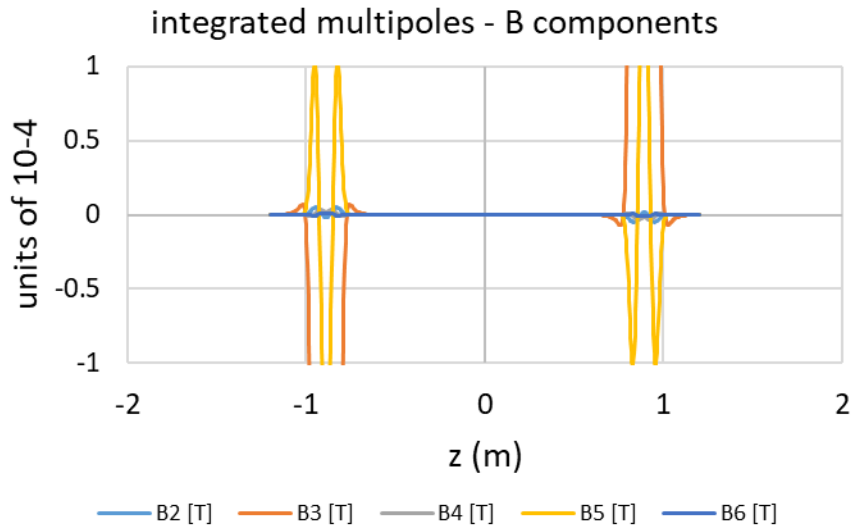


Field quality with ideal positioning of both coils

- Small effects at the edges that cancel out when integrating

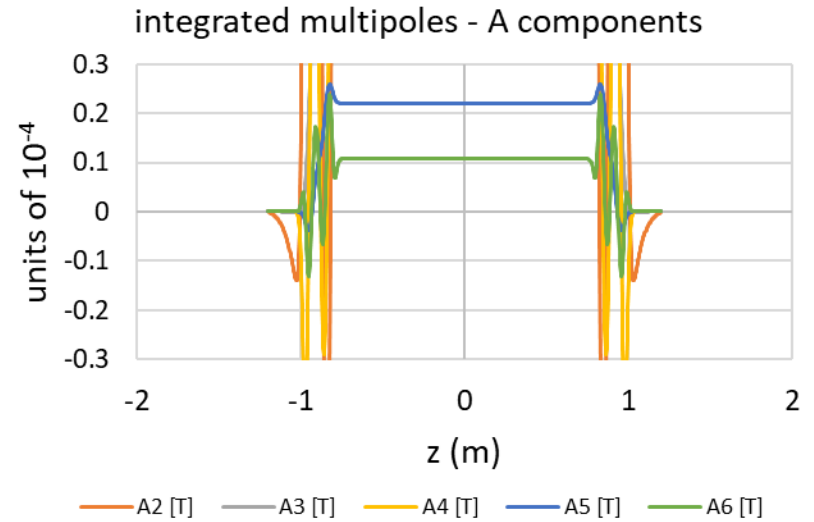
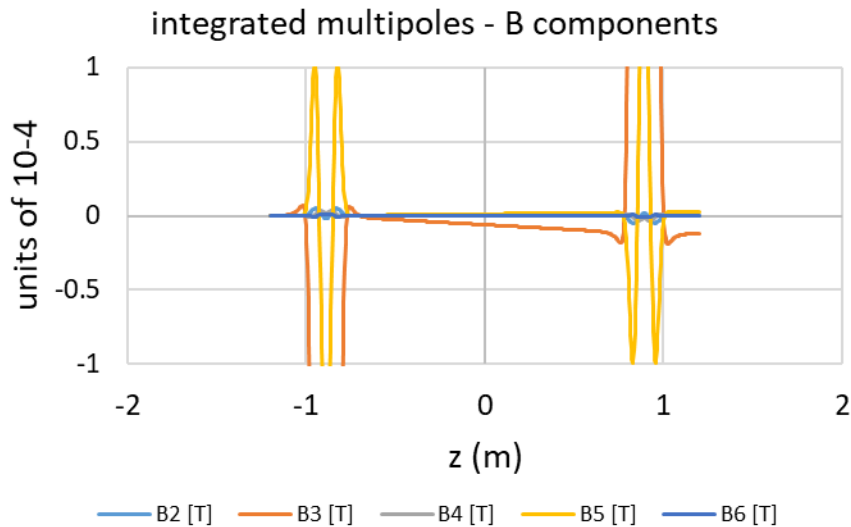


And if we integrate...



- This is for infinitely thin wires

Now, take into account the fact that the cable is 2mm wide



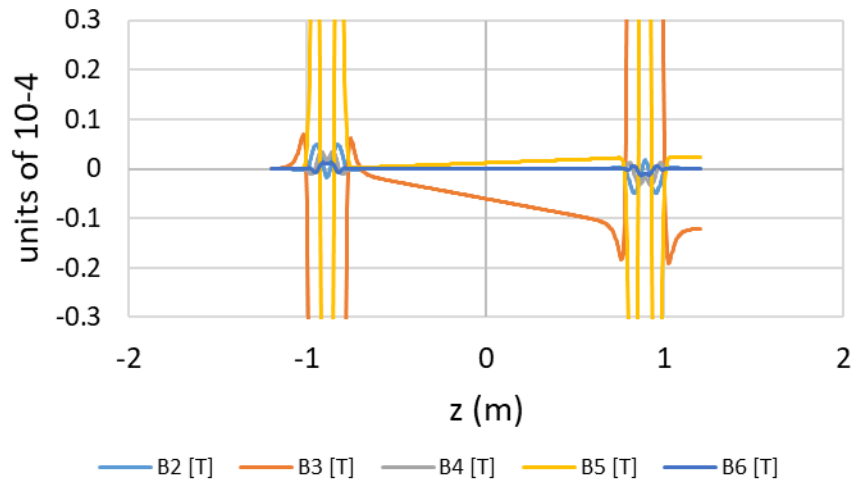
- This introduces a minute B3 component

Now, calculate the effect of misalignment

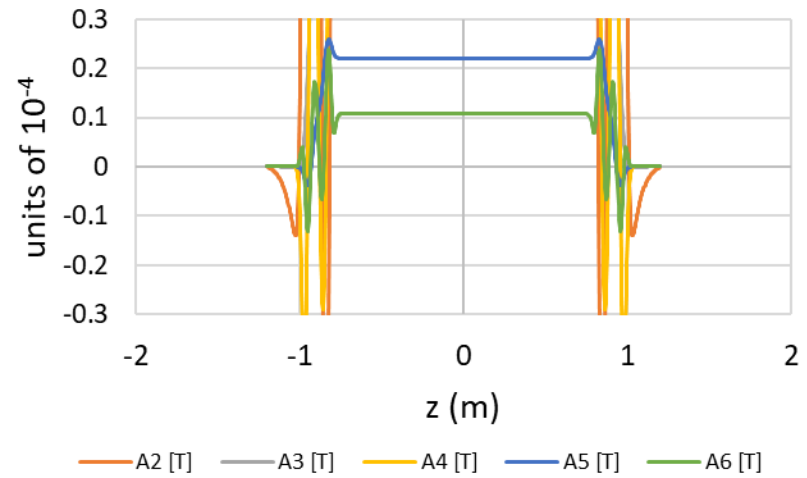
- Translation in x , y , z of the inner wrt the outer coil
- Rotation wrt all angles
- Simplifications: No iron, no cross talk, standalone magnet in air

Reference

integrated multipoles - B components

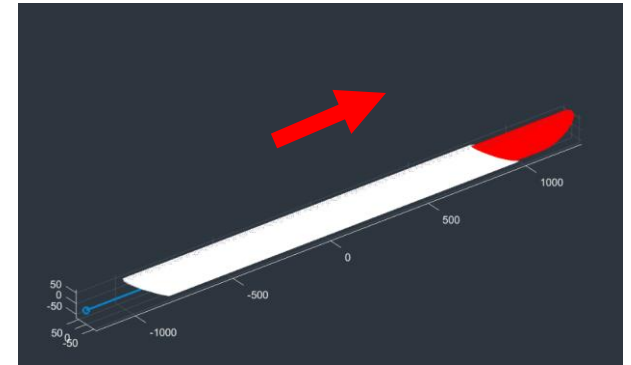


integrated multipoles - A components

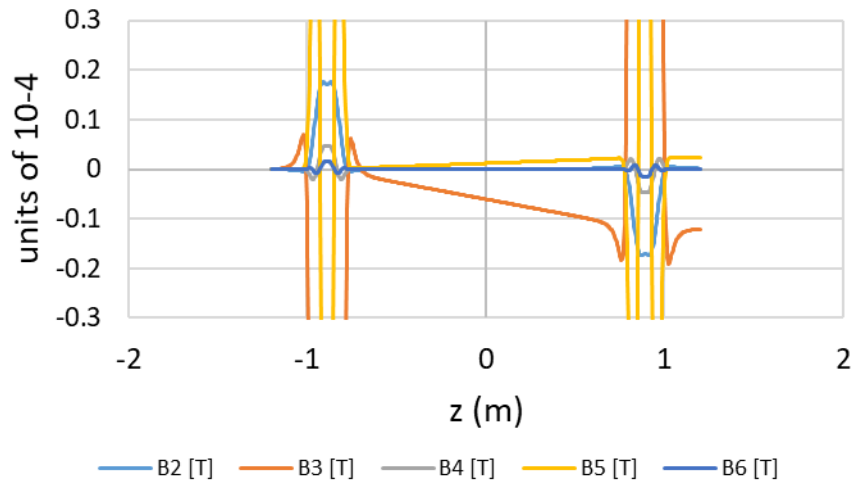


Misalignment along the beam

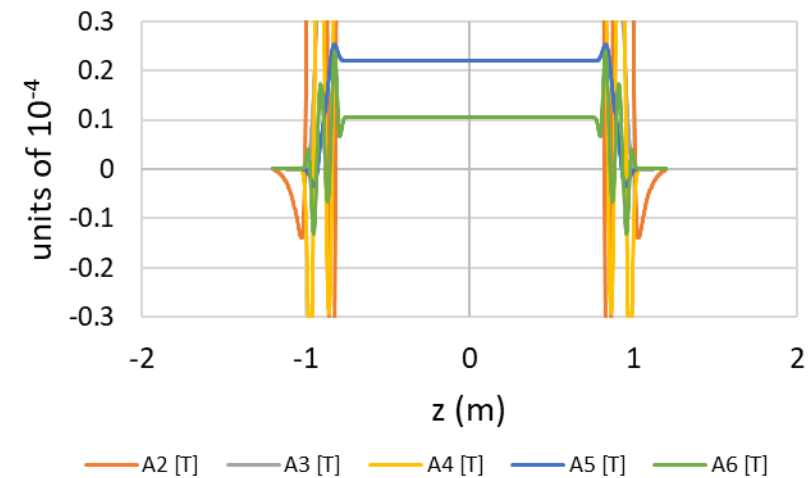
- By 3mm – no effect



integrated multipoles - B components

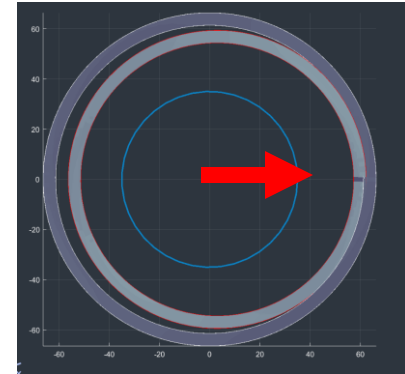


integrated multipoles - A components

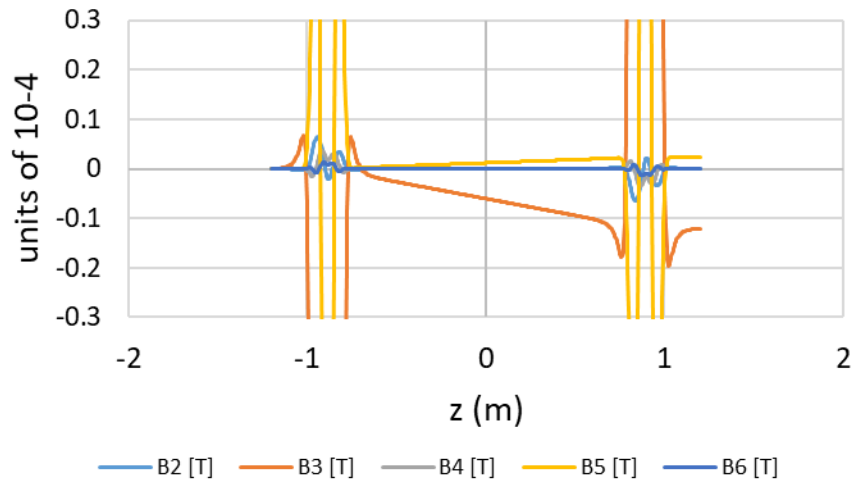


Misalignment horizontally

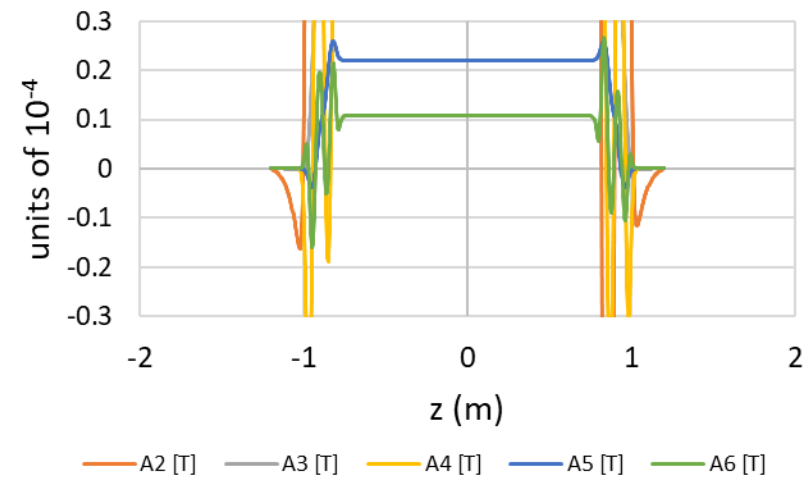
- By 200 μm – no effect



integrated multipoles - B components

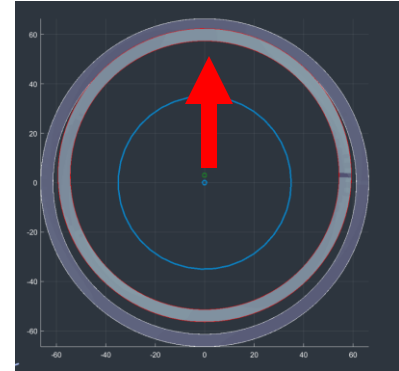


integrated multipoles - A components

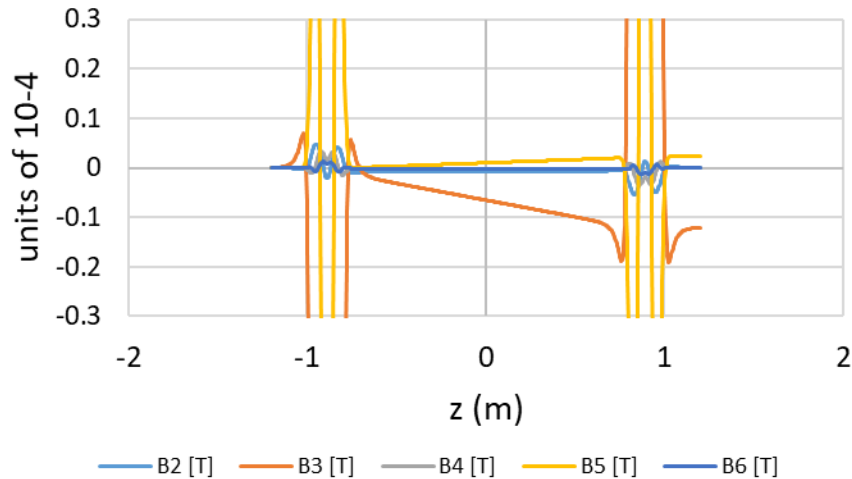


Misalignment vertically

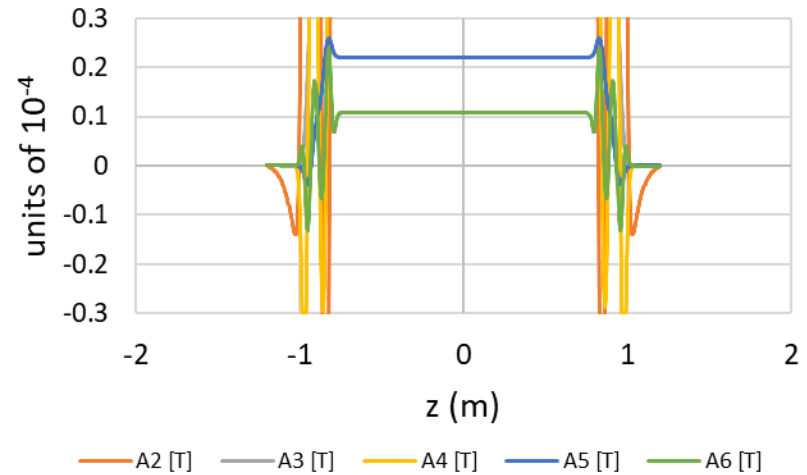
- By 200 μm – no effect



integrated multipoles - B components

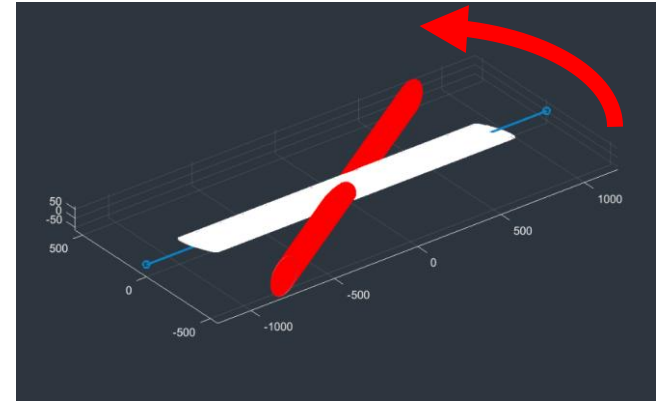


integrated multipoles - A components

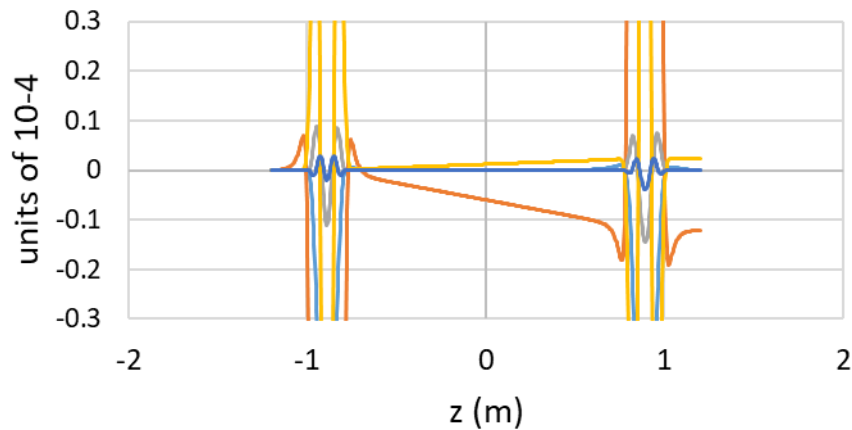


Twist horizontally

- By 1mrad – no effect

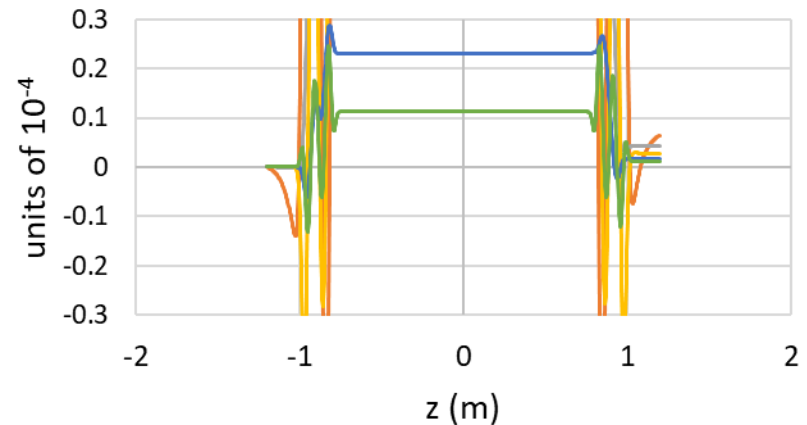


integrated multipoles - B components



— B2 [T] — B3 [T] — B4 [T] — B5 [T] — B6 [T]

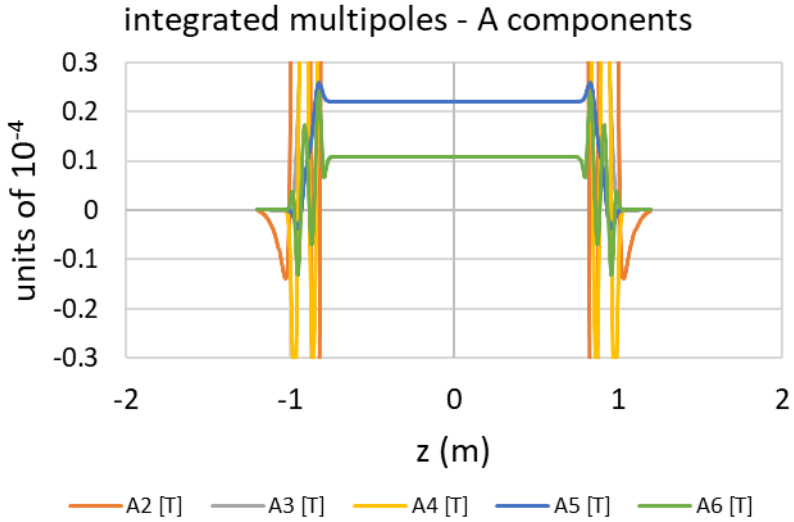
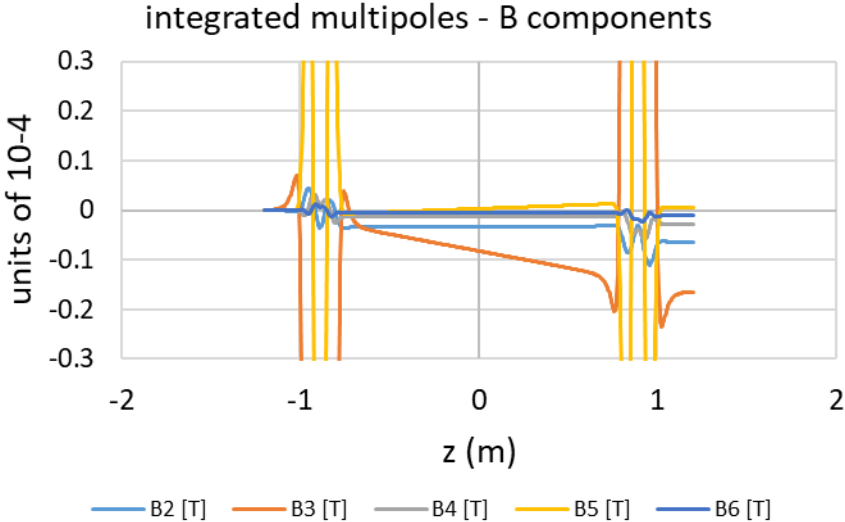
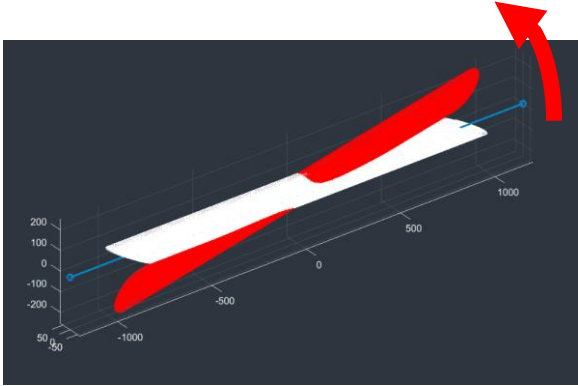
integrated multipoles - A components



— A2 [T] — A3 [T] — A4 [T] — A5 [T] — A6 [T]

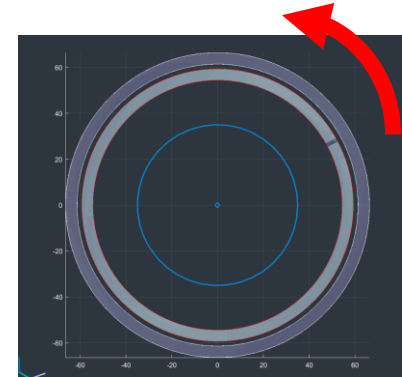
Twist vertically

- By 1mrad – no effect

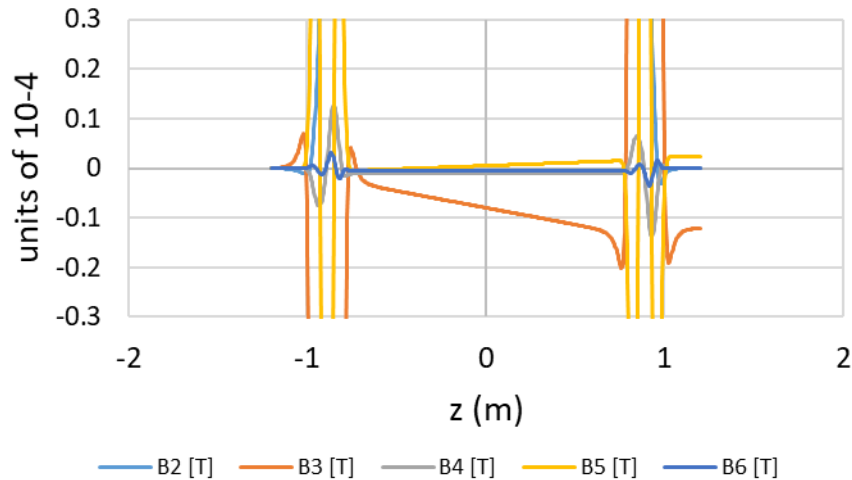


Rotate along beam

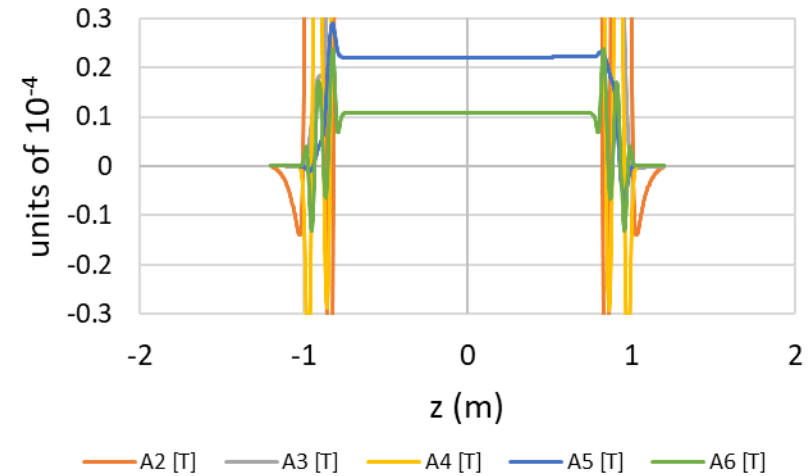
- By 10mrad – no effect



integrated multipoles - B components



integrated multipoles - A components



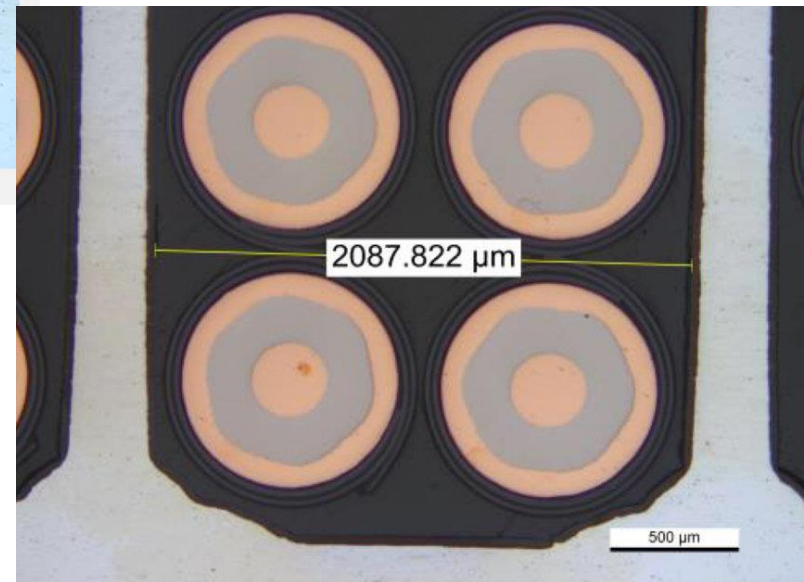
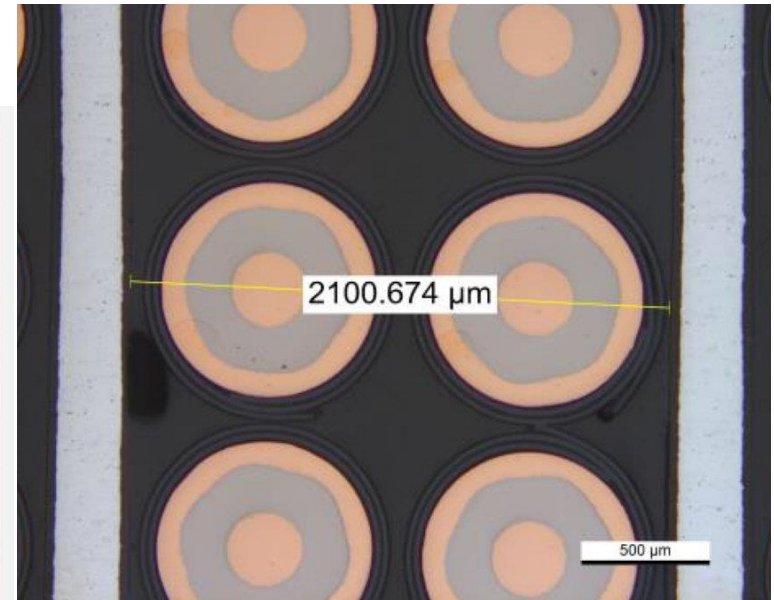
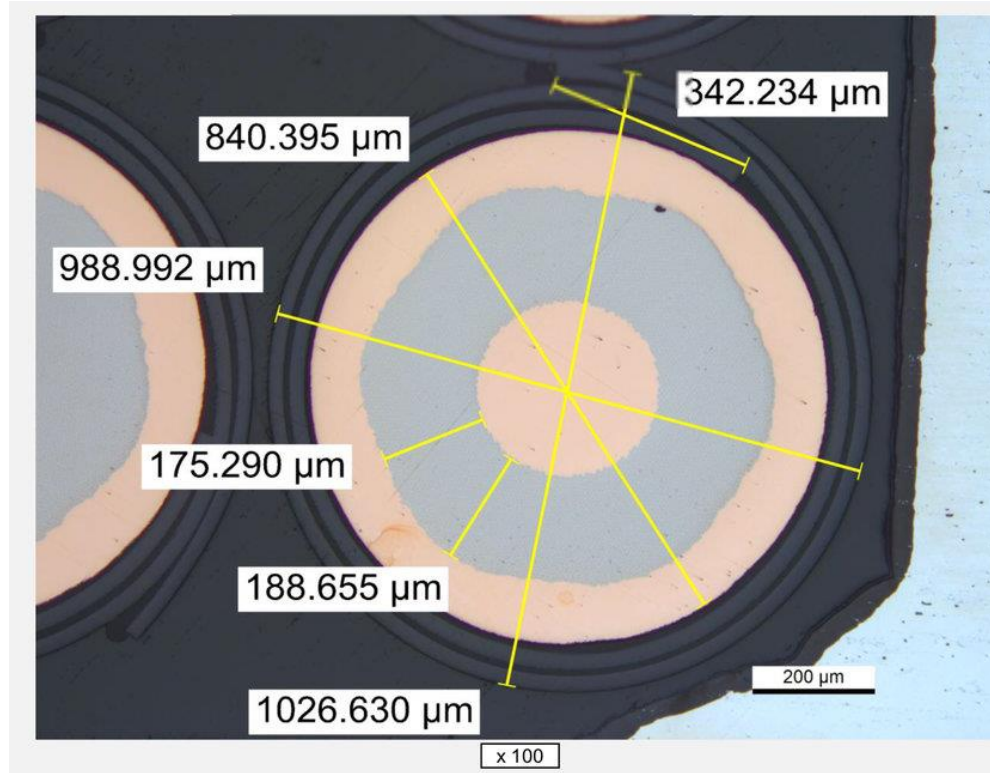
recap

- The CCT design is very forgiving when it comes to mechanical tolerances (when we talk about the integral of the multipoles)
- So where does the 10 unit B3 component come from?

Possible culprits:

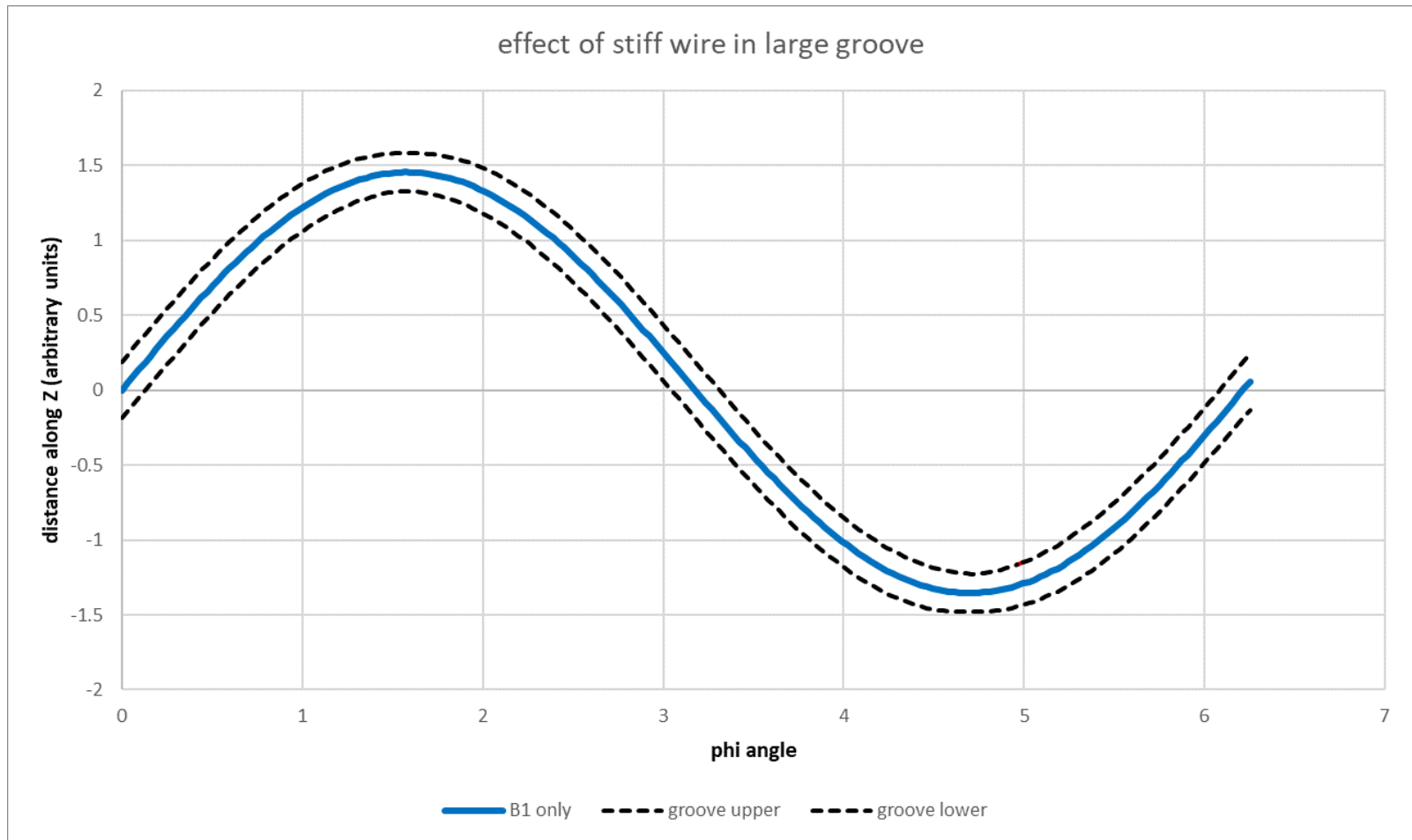
- Some error creeping in from the electrical design till the manufacturing process
 - I was unable to test this
- I will offer one more possible explanation...

Groove size vs cable size

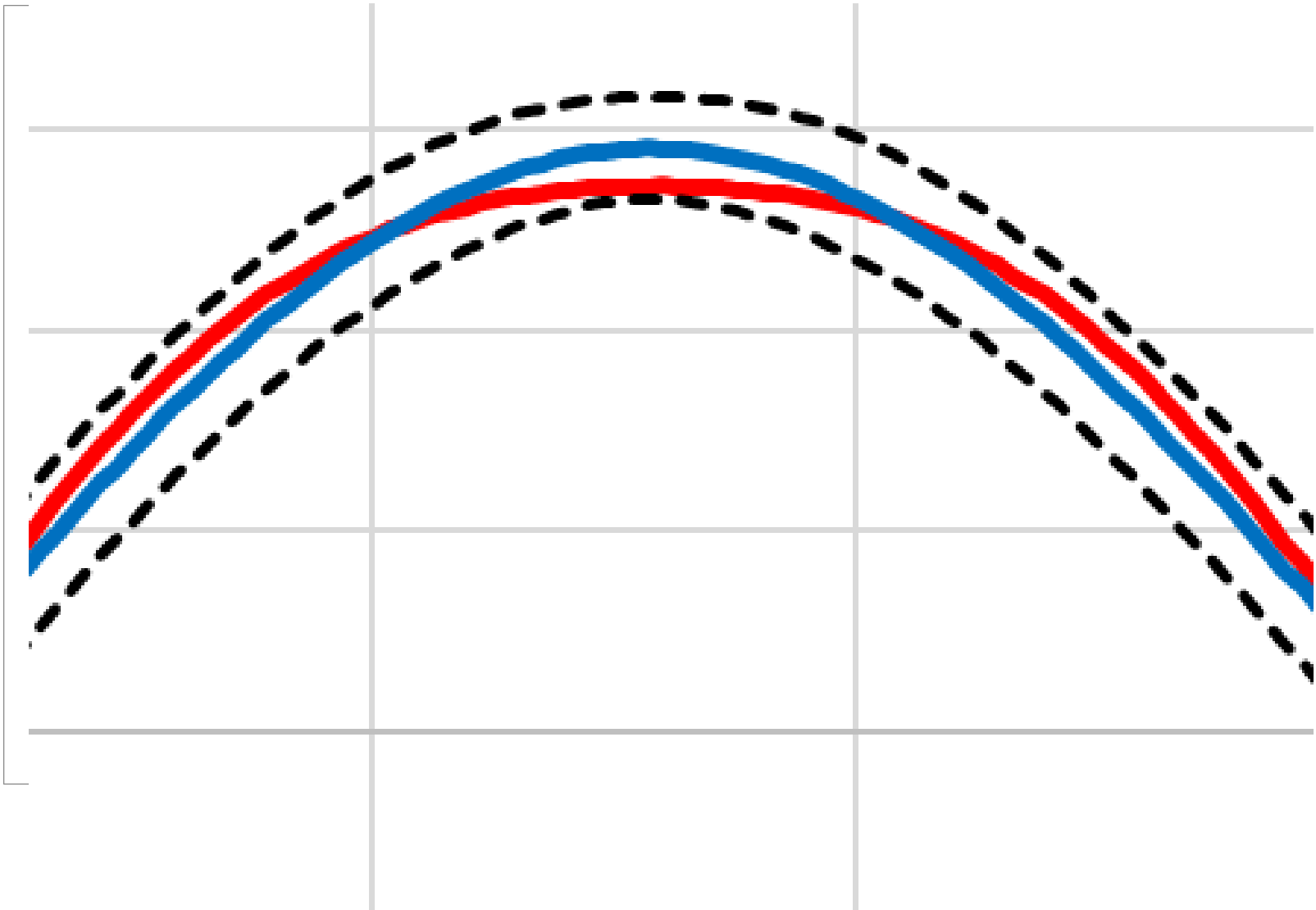


2100 μm vs $2 \times 990 \mu\text{m}$:
there is an empty space
of $\pm 60 \mu\text{m}$

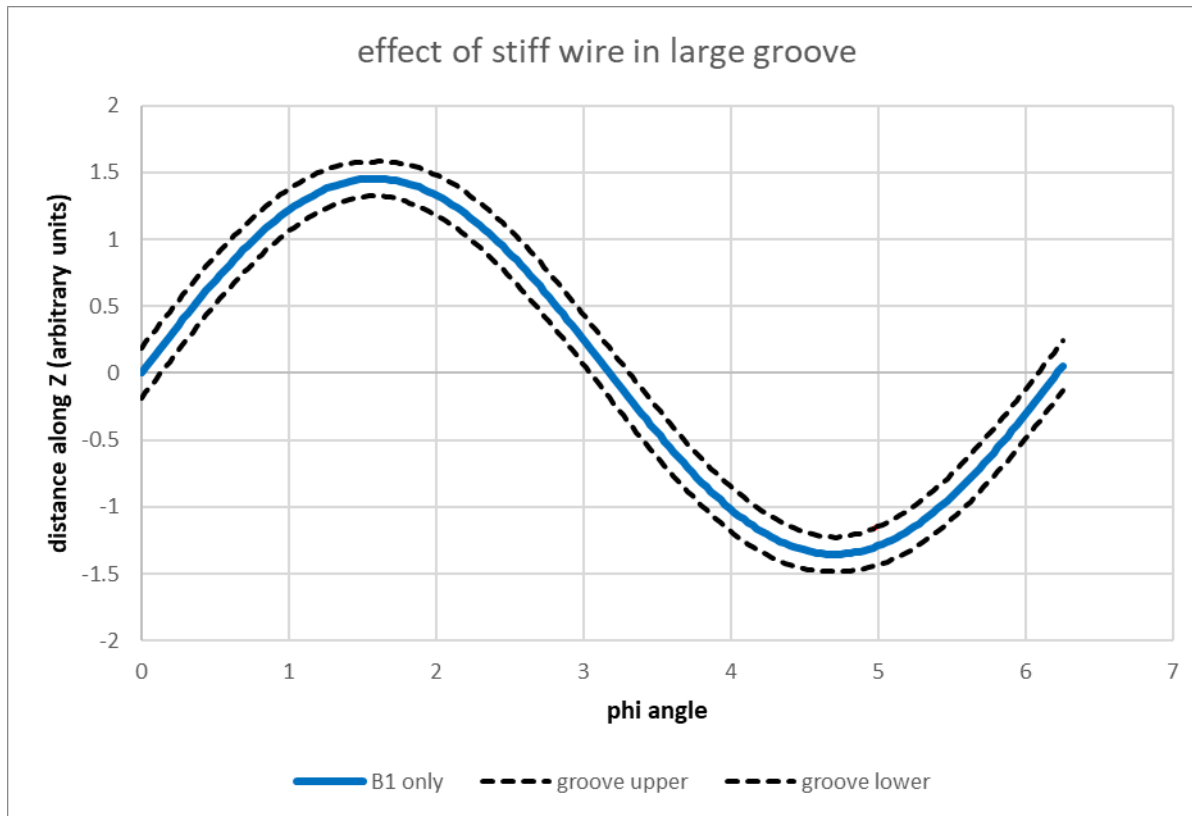
Slot around ideal position – B1 (dipole) case



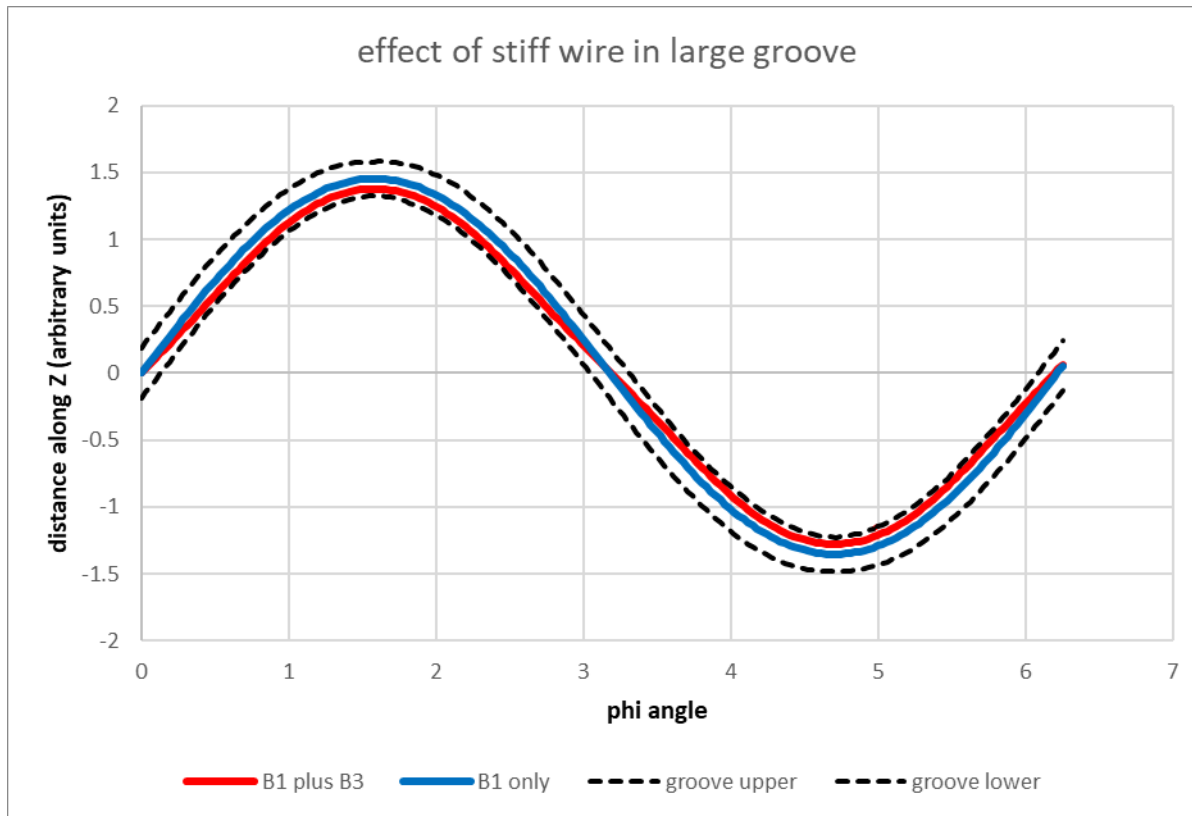
Positioning of a stiff wire in a larger groove



...or is it like this



...or is it like this

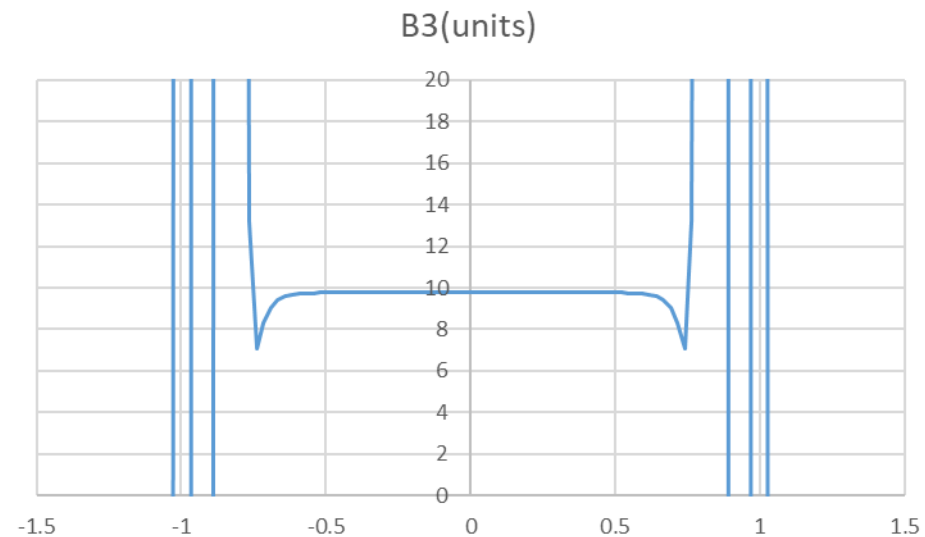
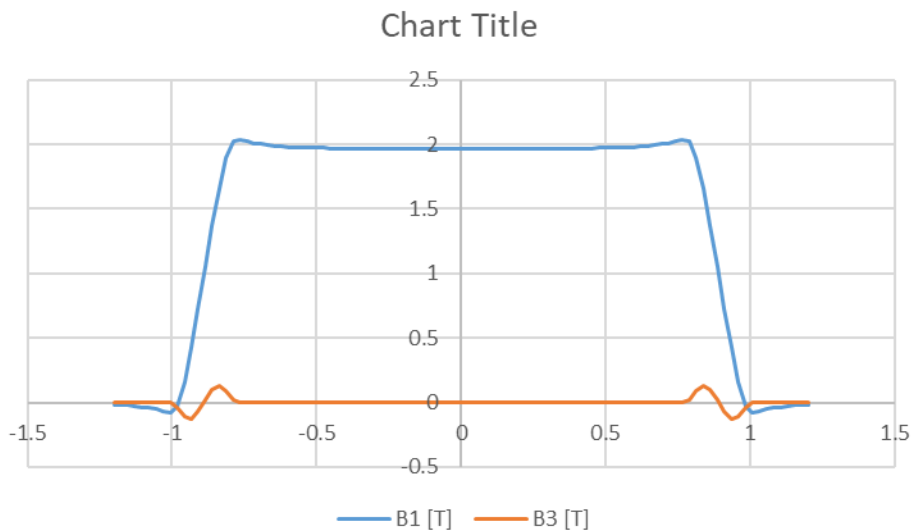


What does this have to do with B3?

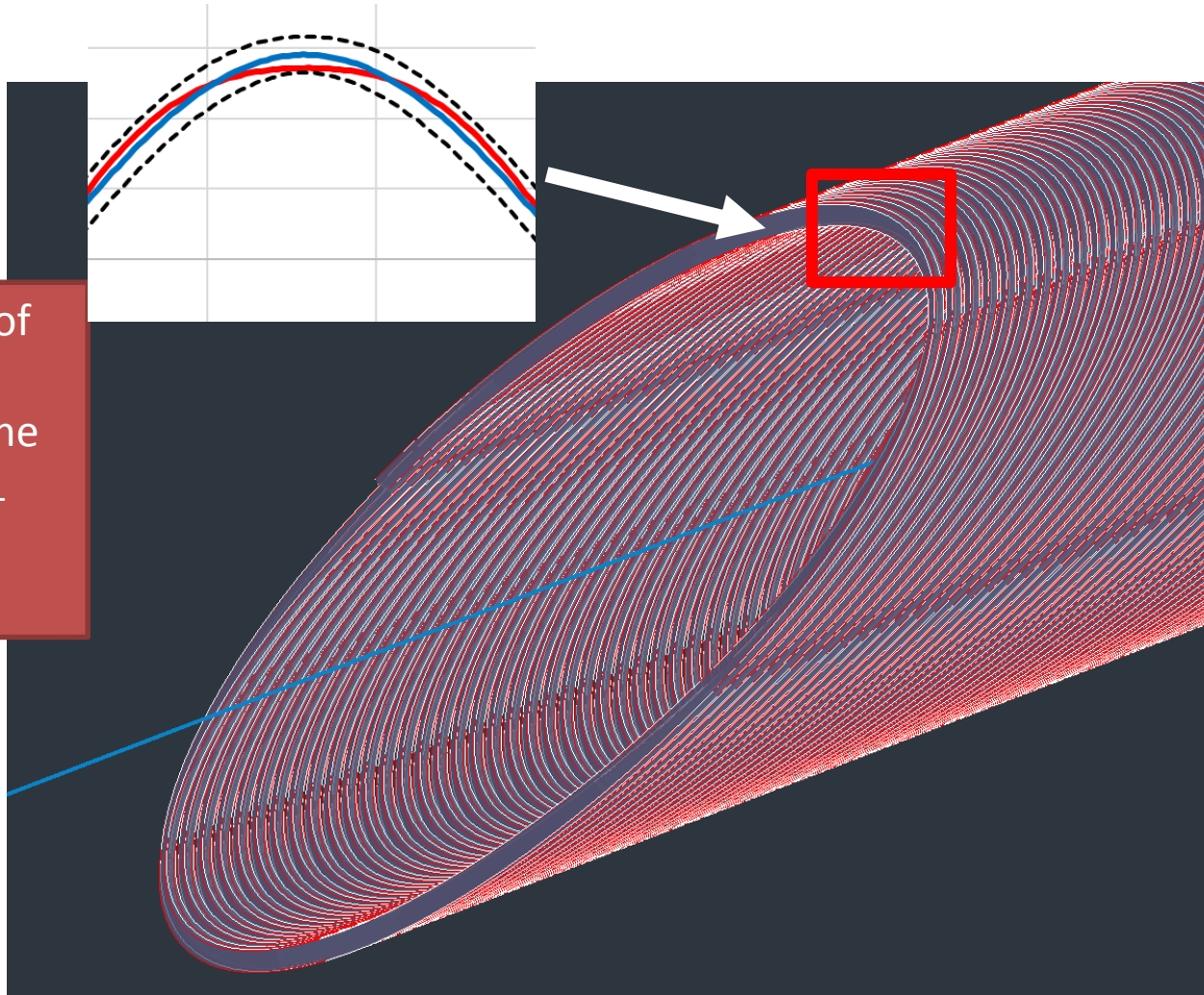
- Actually, I have cheated. I do not (yet) have a model for the position of a stiff wire inside a groove. What you saw in the previous slides is the addition of a B3 component to the existing B1 component
- In the first plot, a B3 component of the same sign as the B1 component was added
- In the second plot, a B3 and B5 component of the opposite sign were added
- In both cases, the result is that around the bend the wire sits in the lowest allowed region of the groove
- Question is: how many microns of wiggle do we need to get 10 units of B3?
- Use Jeroen's field program

Model used

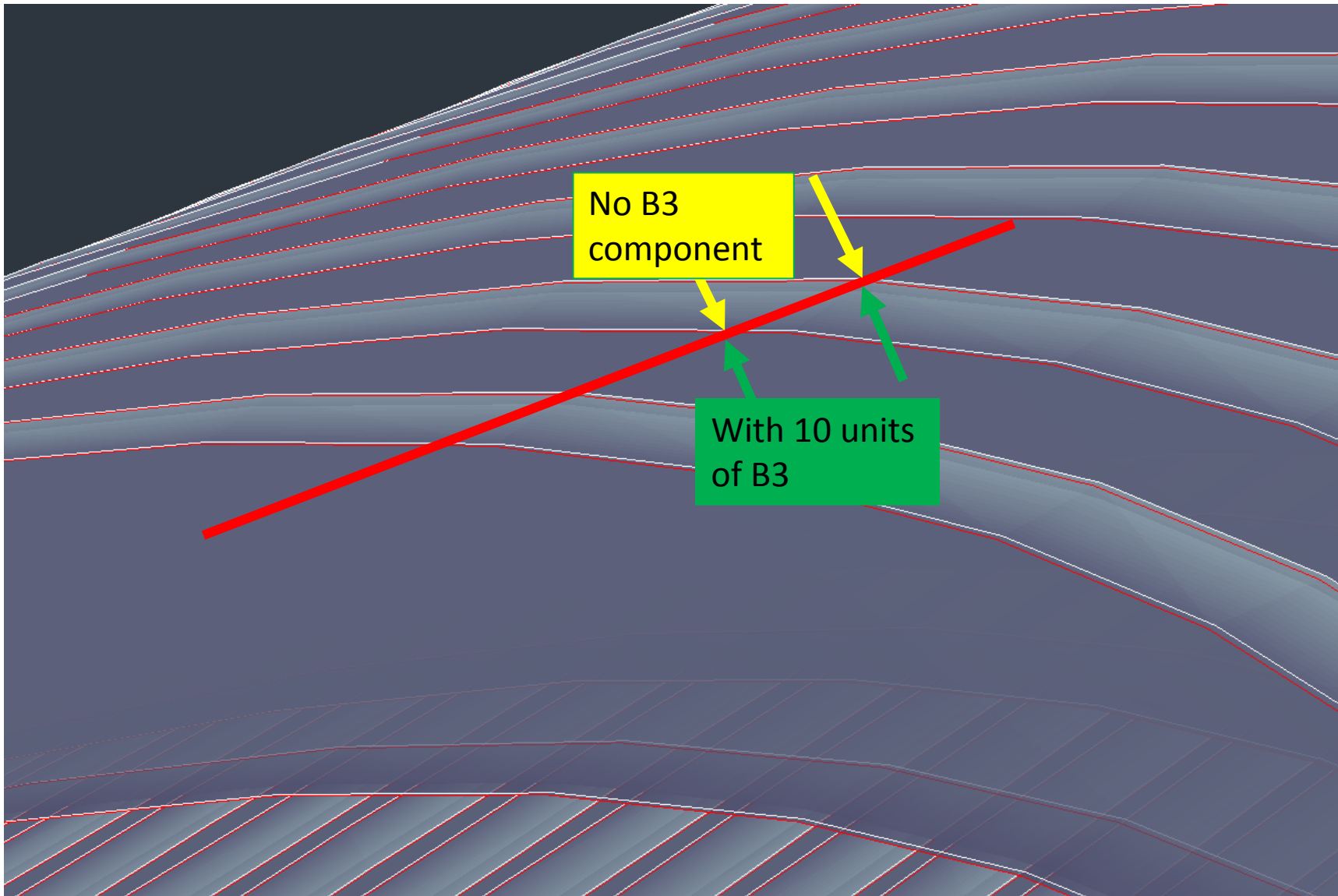
- Inner radius of inner cable: 54.35; cable size 2X5mm; outer cable inner radius: 61.35
- Strength of B1: maximum (60 degrees)
- Strength of B3: 1/200th of maximum (0.3 degrees)



Effect on position of cable

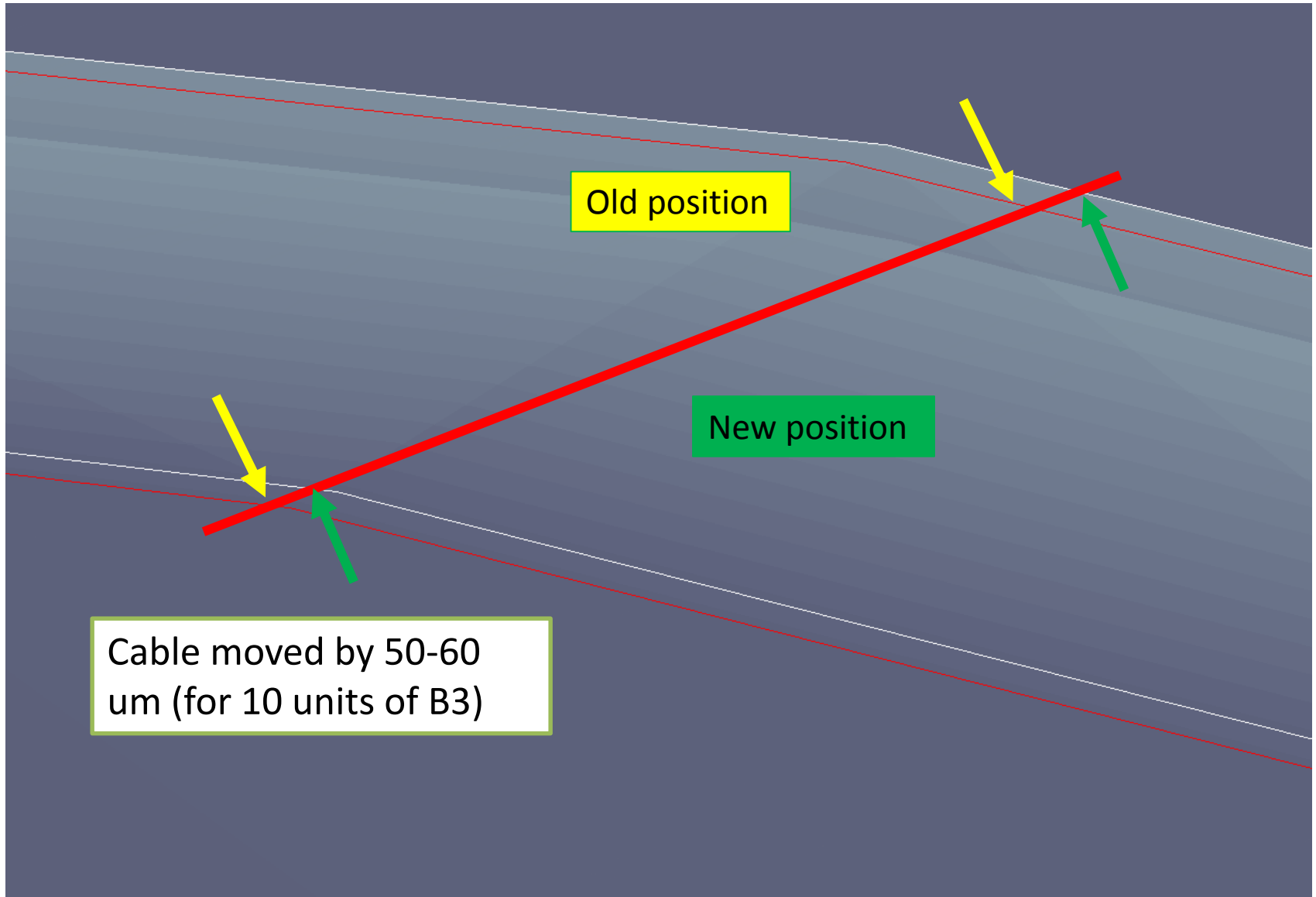


Superposition of two coils: one with only B1, the second with B1 and B3 components



No B3
component

With 10 units
of B3



Old position

New position

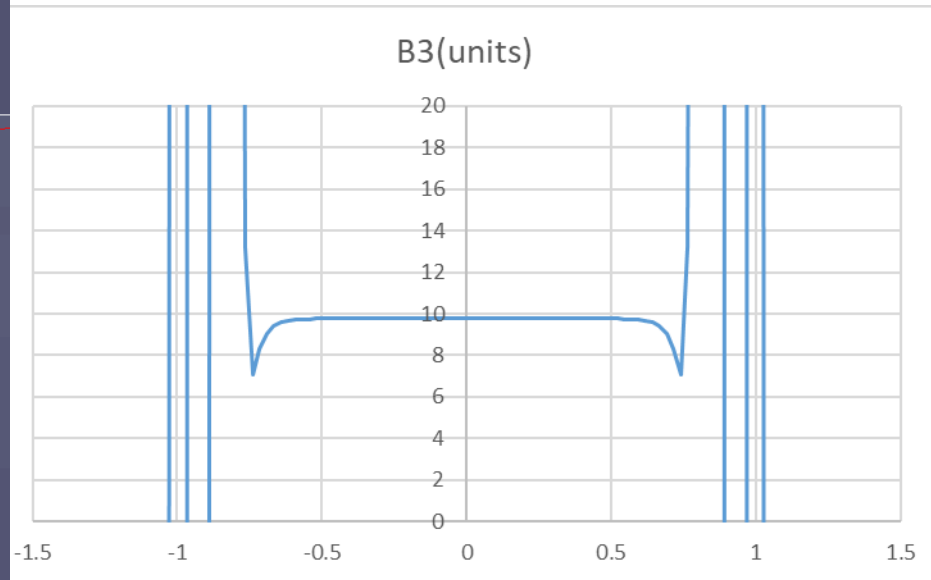
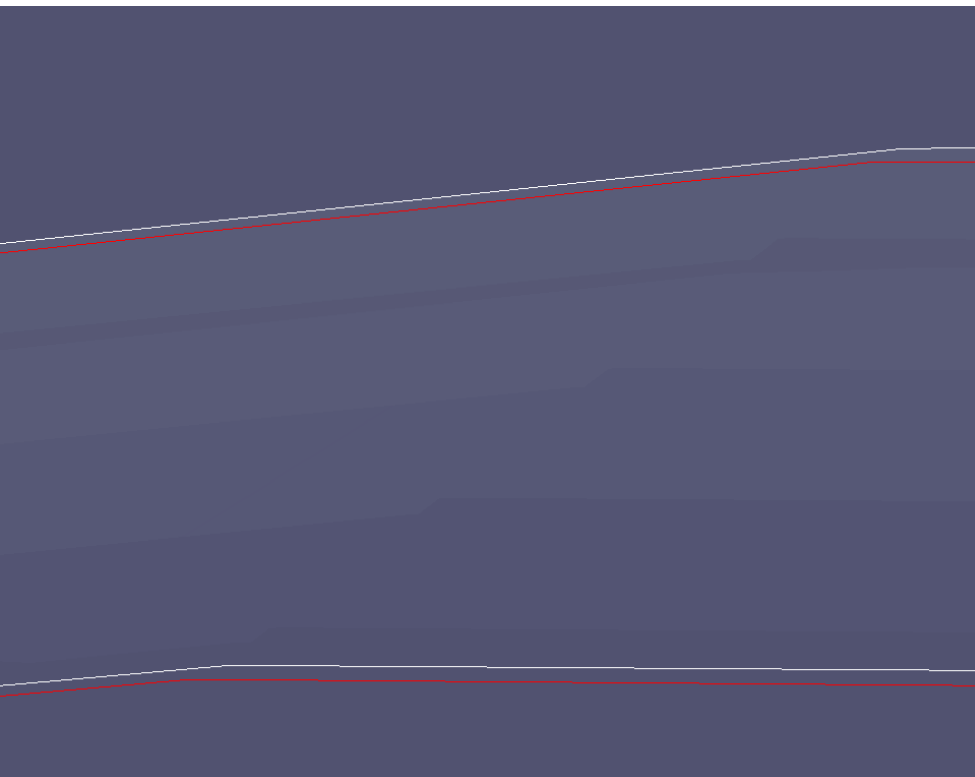
Cable moved by 50-60 um (for 10 units of B3)

Max. displacement of cable and B3 component

50 μm movement

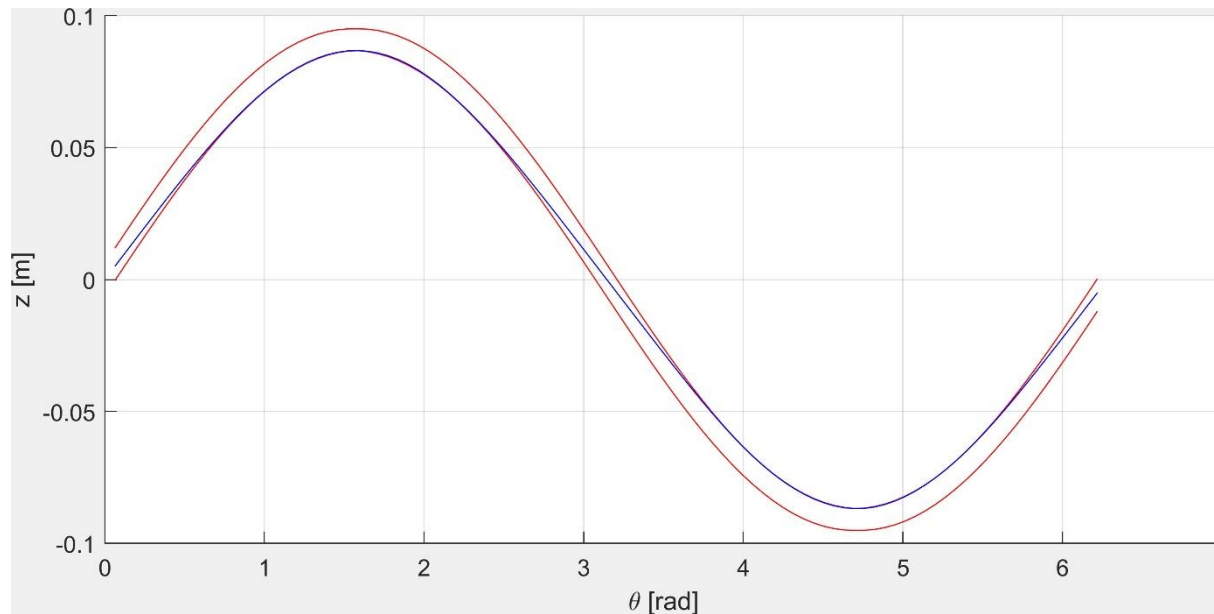


10 units of B3



Model of a stiff wire in a groove

- Work just started... modeling of the wire inside the groove, minimizing the potential energy of the wire
- Following is a sneak preview of this work (that even gives the correct strength of B3 (10 units in a groove of 2.1 mm where the wire width is 2X1mm))



Jeroen van Nugteren

Possible mitigation strategies

- Introduce a -10 units of B3 component
- Tighter fitting cable in slot
- Tension during winding ?? – this still has a few question marks until we understand the model well.

What about the 6 units of A2 found in one of the two apertures?

- Best theory is that one of the apertures is not centered wrt to the iron yoke, but I have not tested it

Conclusions

- I found a possible explanation for the large B3 component: it could be the combination of a stiff wire and a larger groove than the cable dimensions
- The numbers match: B3 component magnitude is what is expected by the size of the groove (2100um) and the size of the cables (2X990um)

End