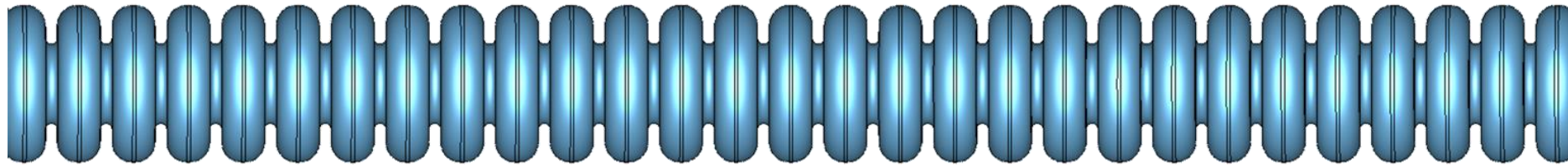




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# K-Band RF Linearizer Design

A. Castilla\*, G. Burt, W.L. Millar - Lancaster University

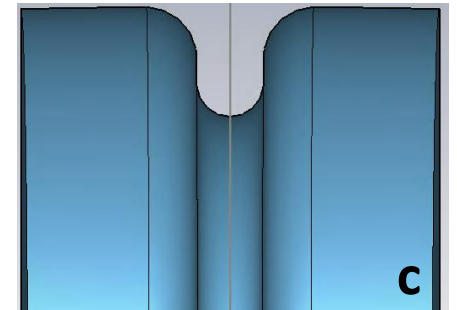
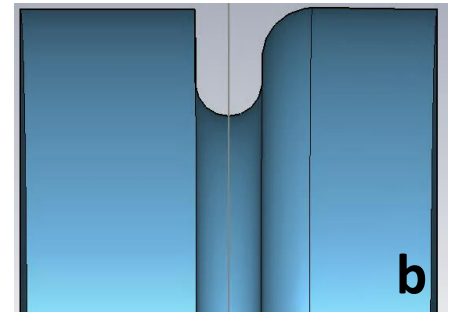
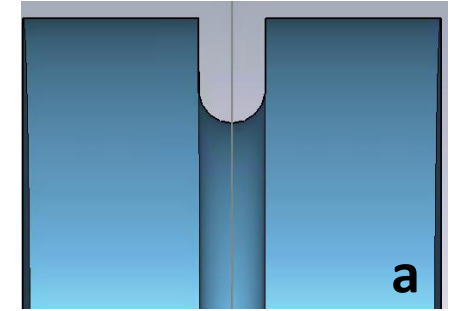
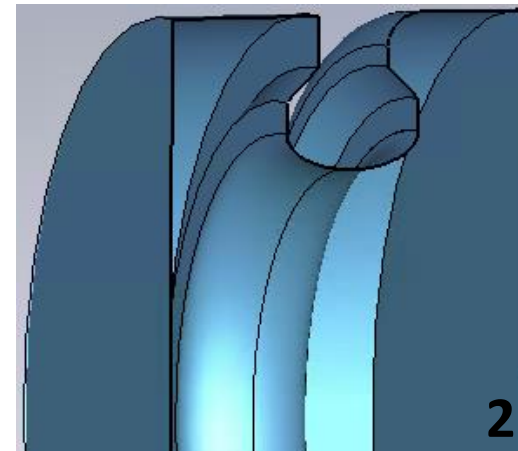
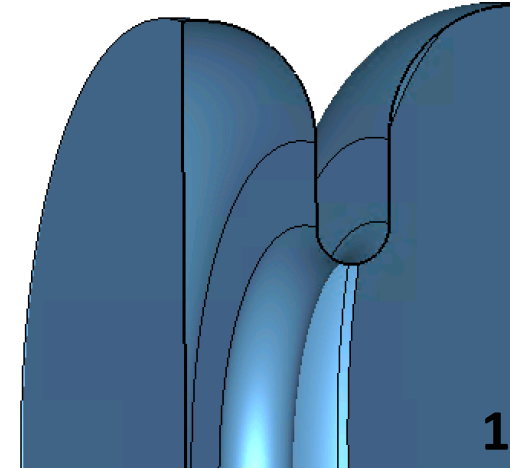
X. Wu, X. Liu, A. Latina, W. Wuensch - CERN

A. Cross - University of Strathclyde

\* [a.castilla@cern.ch](mailto:a.castilla@cern.ch)

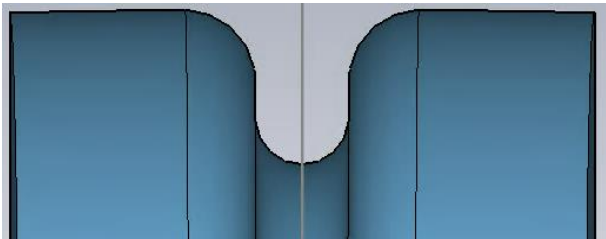
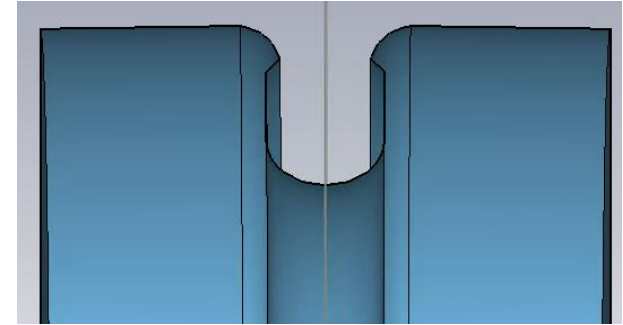
# Single Cell Revisited: Candidates

- 2 basic geometries studied:
  1. Simple.
  2. Reentrant.
- For each of this geometries, 3 variations were evaluated:
  - a. No-blends at the equator (“Pillbox”).
  - b. 1-blend at the equator (“CLARA-style”).
  - c. 2-blends at equator (“Classic”).
- Each for 2 phase advances:
  - $2\pi/3$ .
  - $5\pi/6$ .

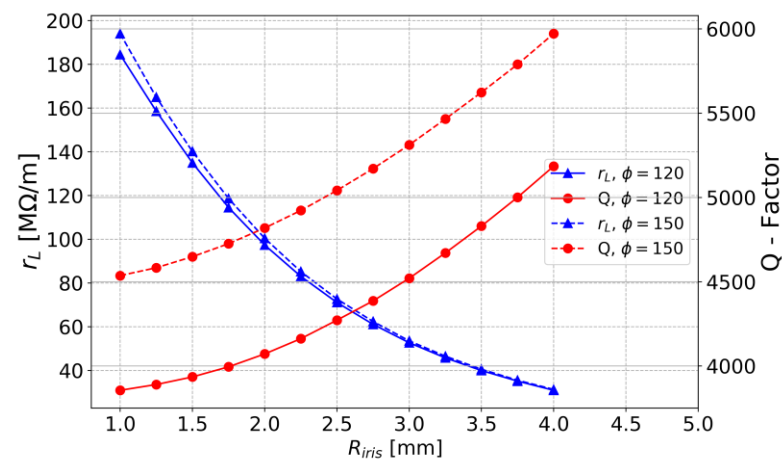


# Single Cell Revisited: Comparison

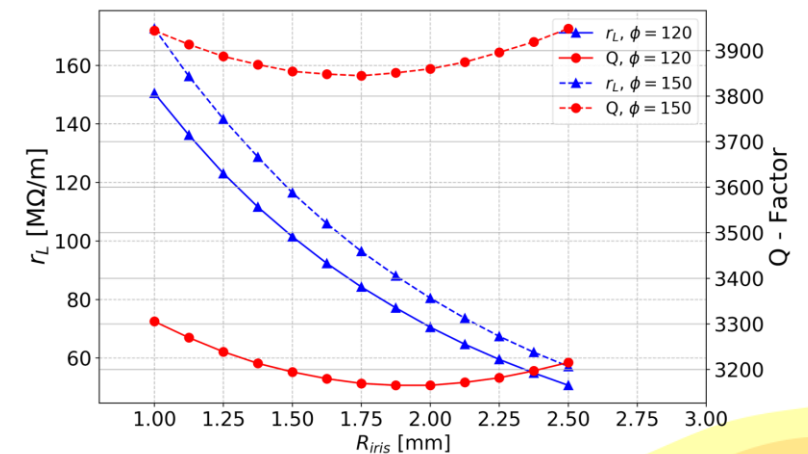
- Shunt Impedance:
  - Higher for simple cells and low iris apertures.
- Intrinsic Q-Factor:
  - On average, higher for simple cells.



## 2-Blends Simple Cell

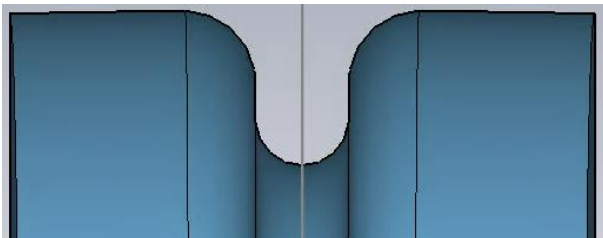
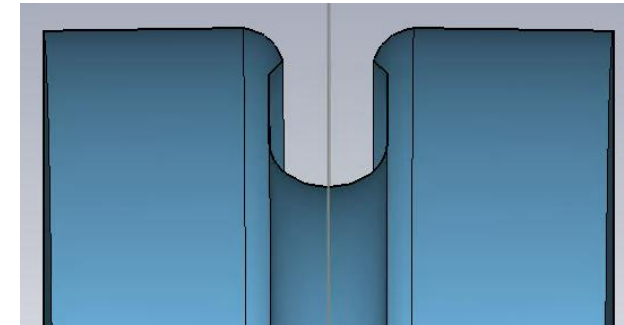


## 2-Blends Reentrant Cell

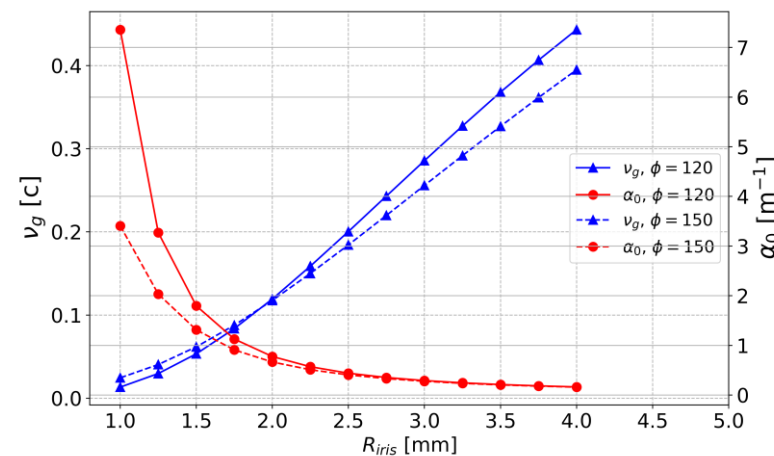


# Single Cell Revisited: Comparison

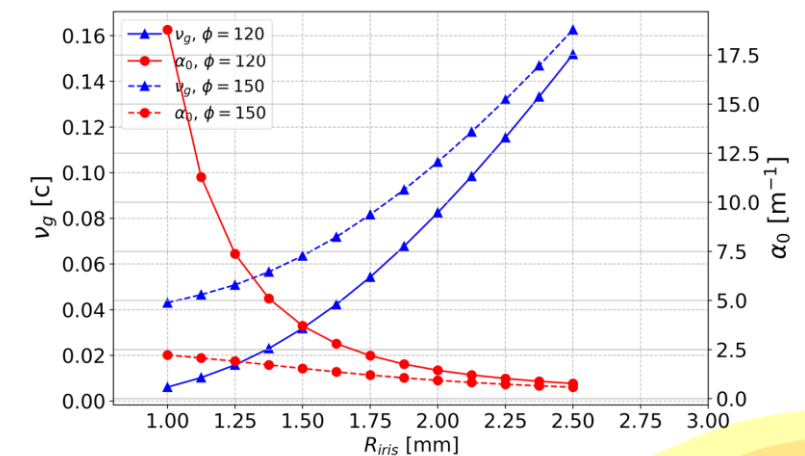
- Group velocities:
  - Lower for the reentrant cell.
- Attenuation:
  - Higher for the reentrant cells.



## 2-Blends Simple Cell

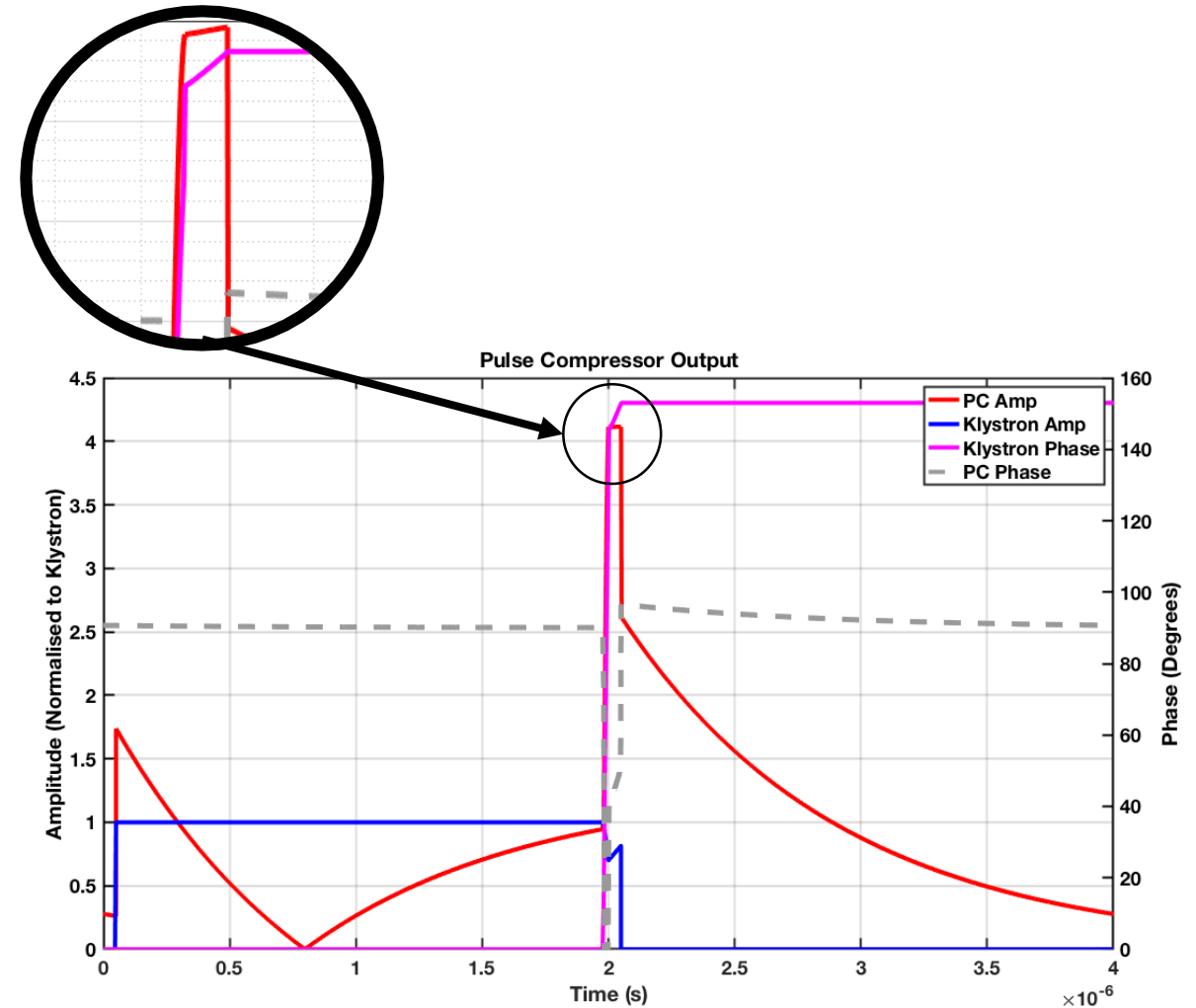


## 2-Blends Reentrant Cell



# Power Considerations

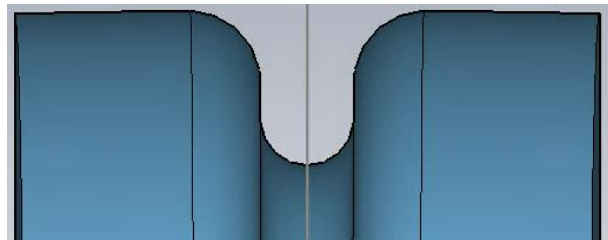
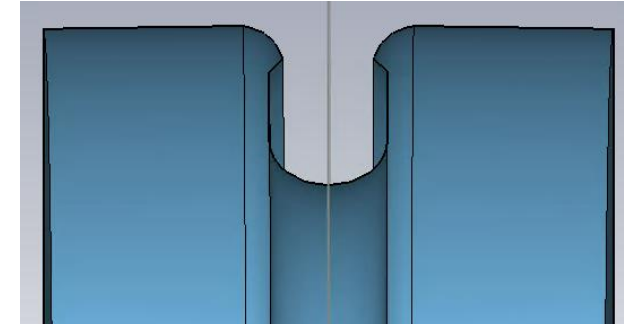
- 36GHz Gyro-klystron:
  - $2\mu\text{s}$  pulse length.
  - $\geq 2$  MW amplitude.
- SLEDI Pulse Compressor:
  - 50ns flat top.
  - $\sim 4\times$  power gain.
    - Needs both Amp. & Phase ramps to have flat Amp. & Phase outputs.
    - Higher gains are possible w/o flat phase (not useful for beam operations).



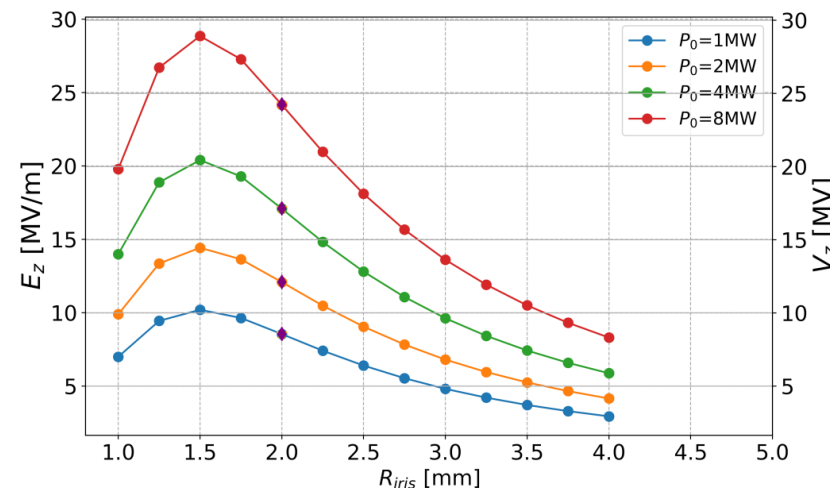
W.L. Millar - ULANC

# Single Cell: 1m Structure Performance

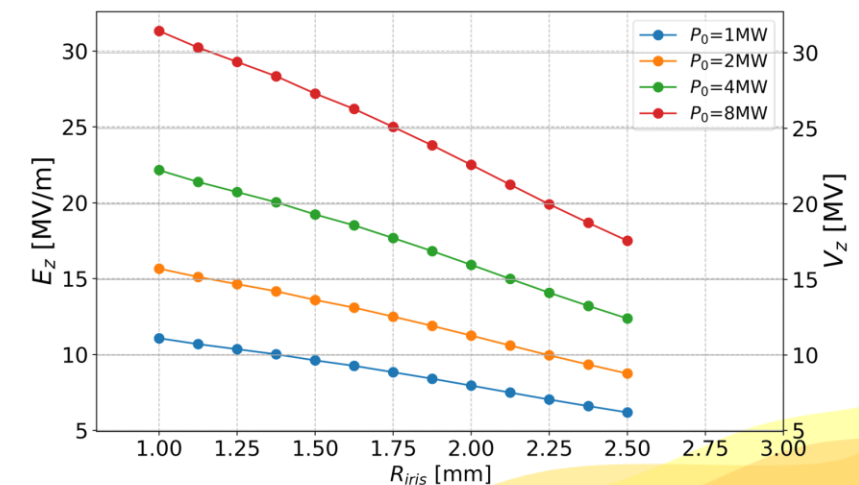
- For 2mm iris radius:
  1. Simple and reentrant cells have comparable performances.
  2.  $2\pi/3$  and  $5\pi/6$  also perform similarly.



## 2-Blends Simple Cell @120deg

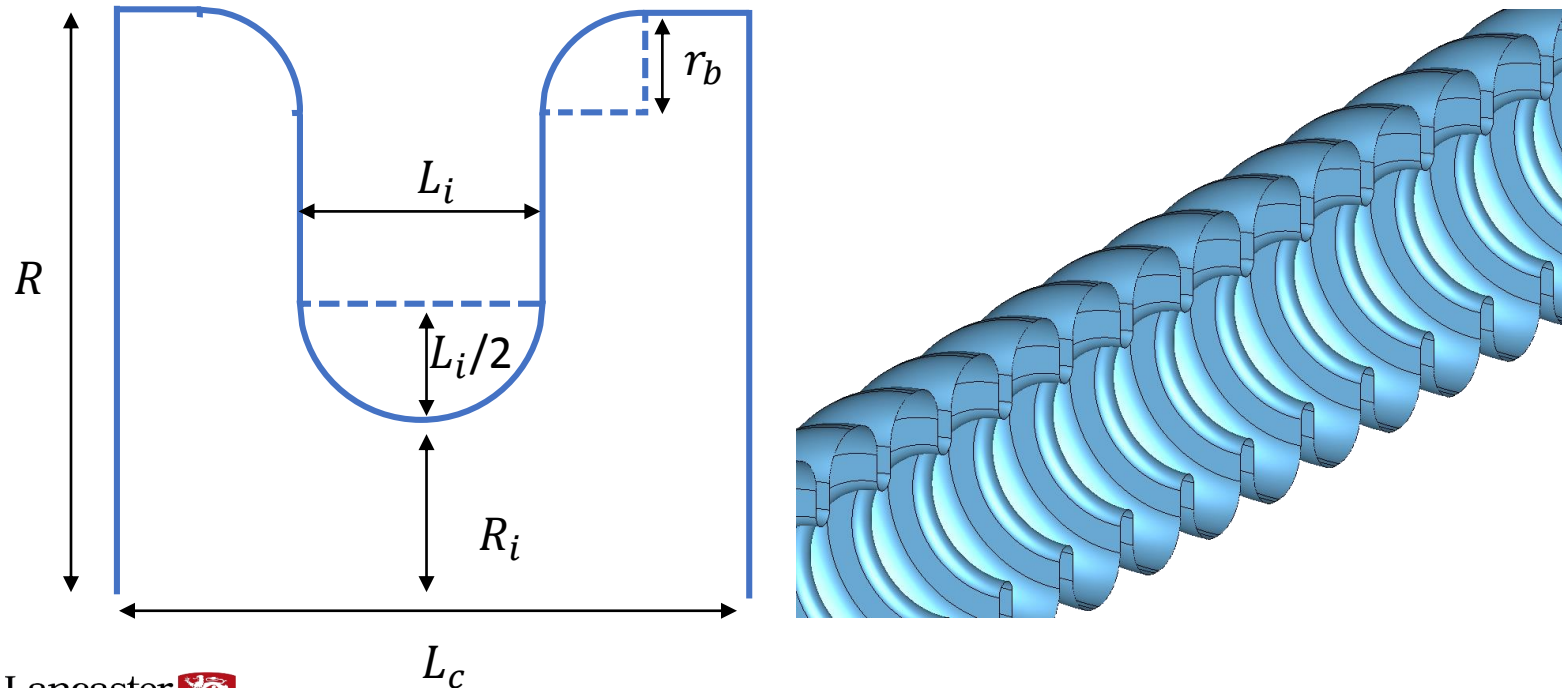


## 2-Blends Reentrant Cell @150deg



# Cell Design

- Simple cell = less manufacturing constraints.
- A geometry is proposed.
- $H_p \approx 90\text{kA/m}$  and  $E_p \approx 65\text{MV/m}$  @  $25\text{MV/m}$



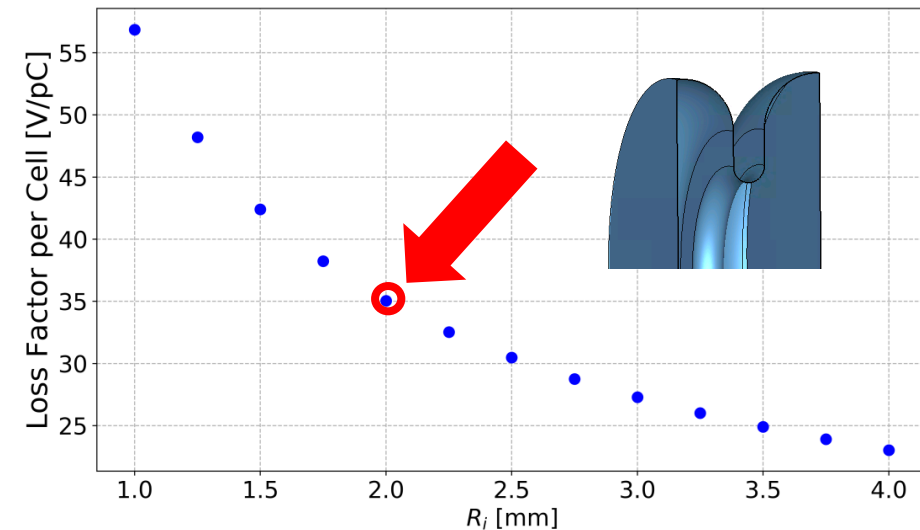
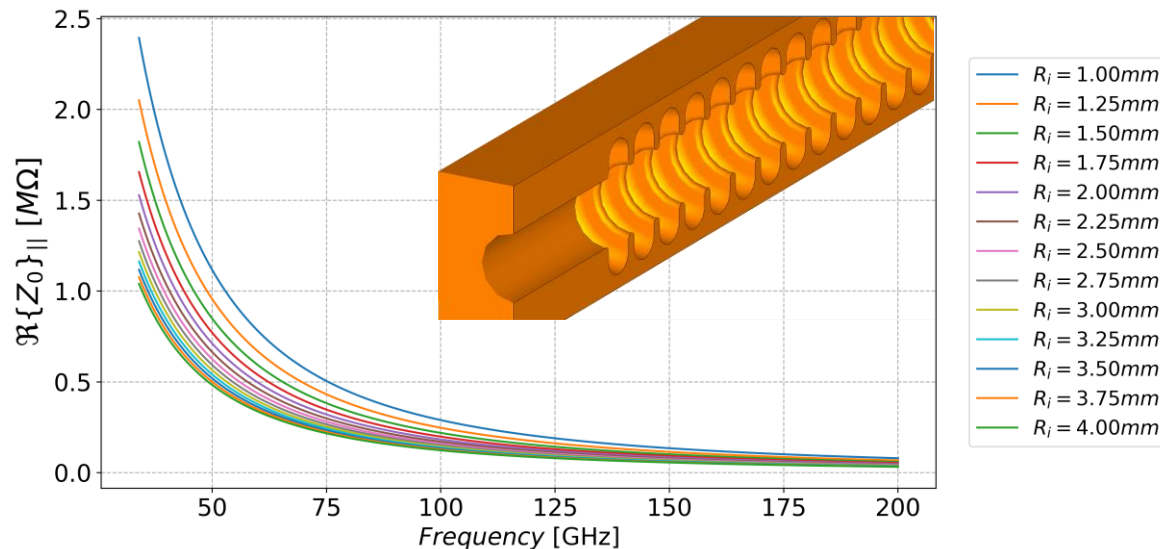
Parameter	Value	Units
Freq.	36	GHz
Q	4392	--
$r_L$	106	$\text{M}\Omega/\text{m}$
$v_g$	0.12	c
$\alpha_0$	0.7	$\text{m}^{-1}$
$E_p^*$	2.6	$\text{MV/m}$
$R$	3.96	mm
$R_i$	2.00	mm
$L_c$ ( $\varphi = 2\pi/3$ )	2.78	mm
$L_i$	0.60	mm
$r_b$	1.00	mm

\*normalized to  $E_z = 1\text{ MV/m}$



# A Quick Look Into The Wakes

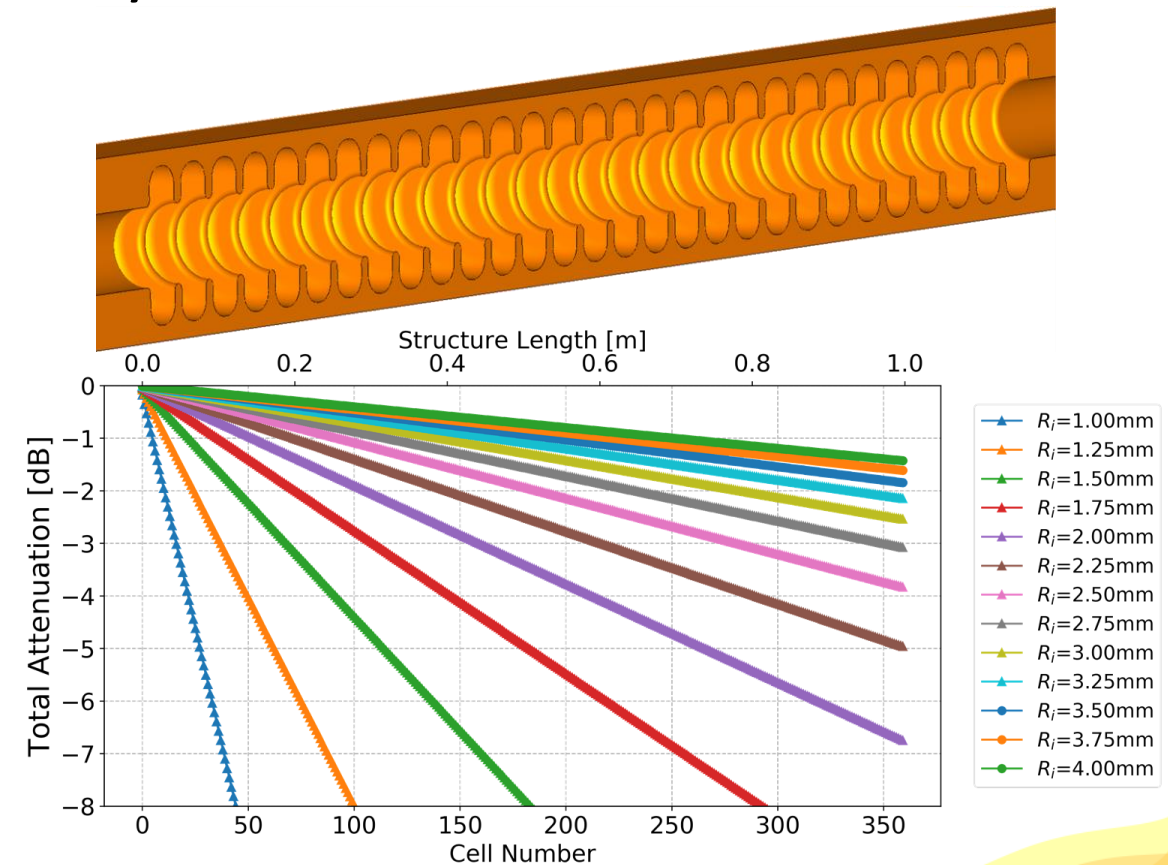
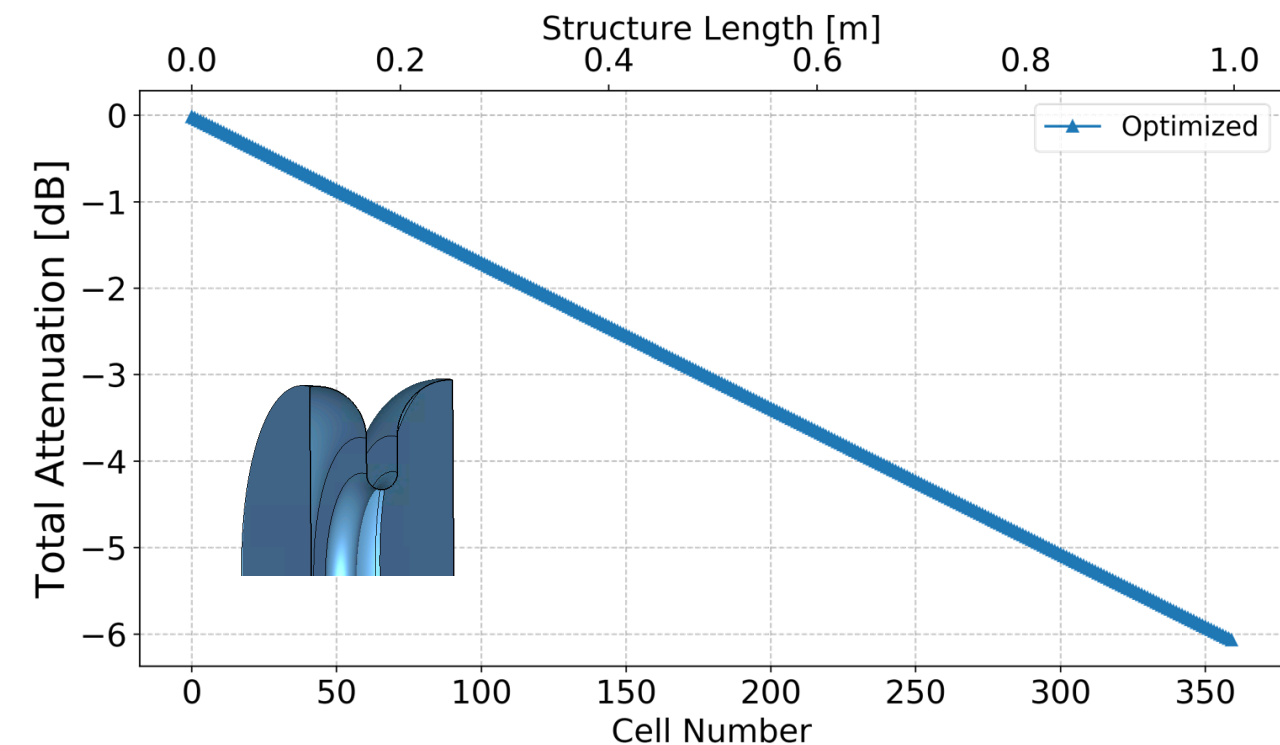
- Considering a 1 meter structure for  $2\pi/3$  mode (i.e. 360 cells).
- The longitudinal loss factor per cell decreases with the iris aperture.
- Effect of the transverse wakes even more significant.





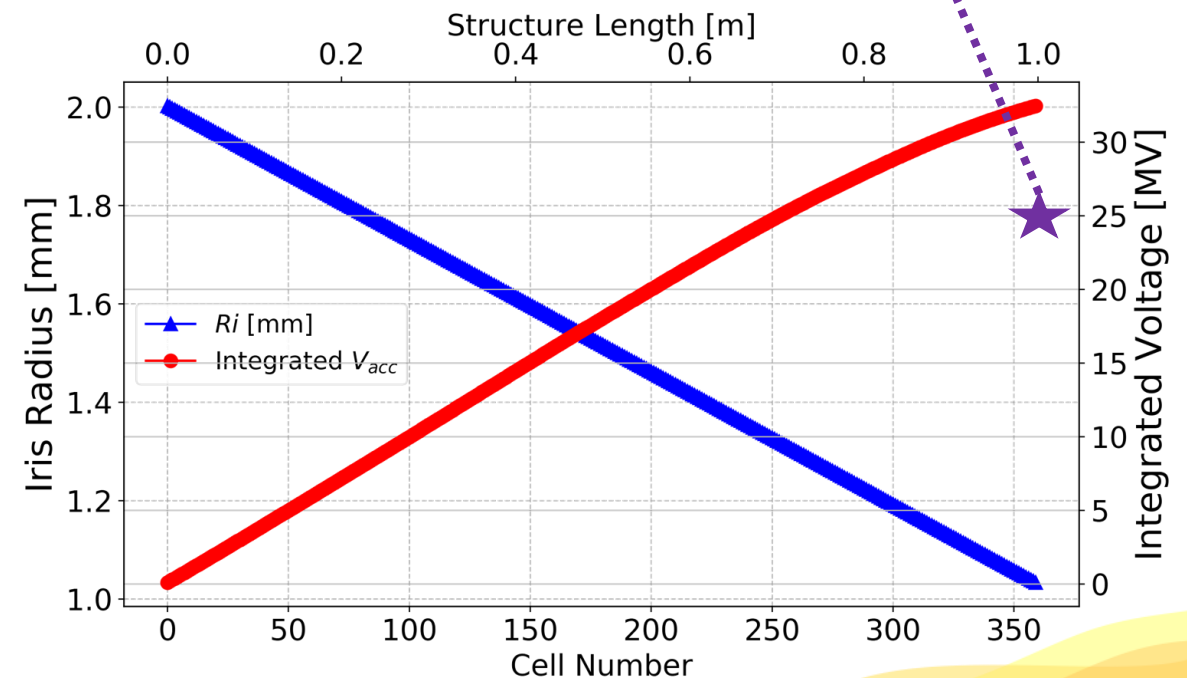
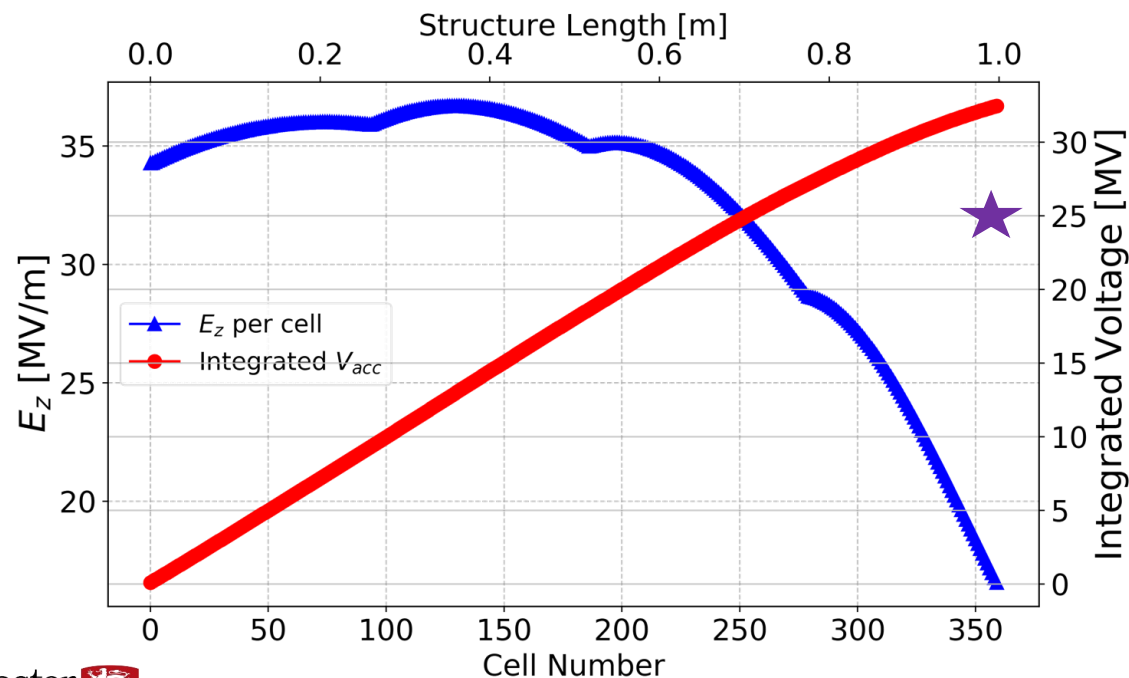
# Other Options

- Power recirculation advantages bounded by the total structure attenuation:
  - It may be challenging for this aperture.



# Simple Cell: 'Constant Gradient' (@8MW)

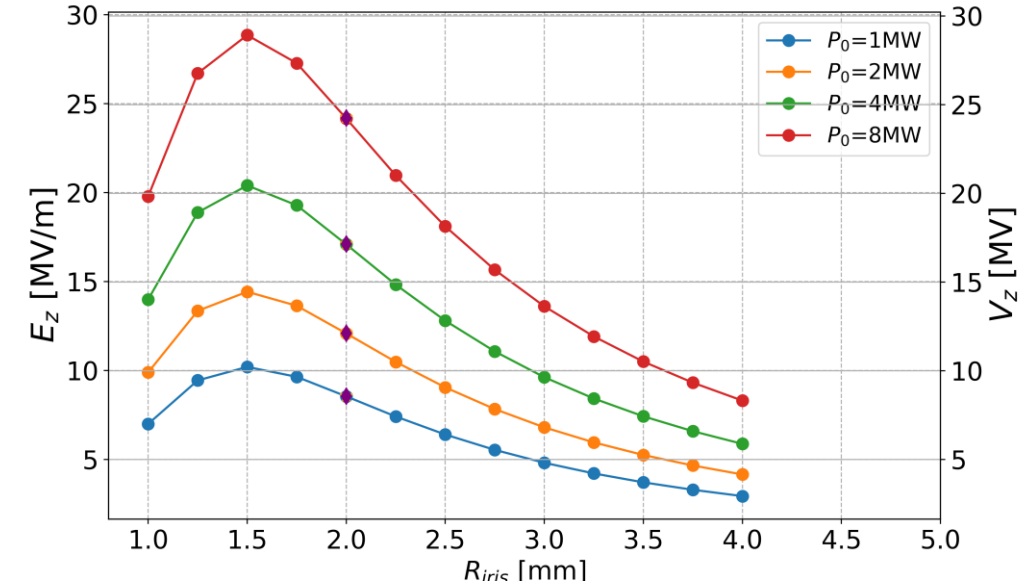
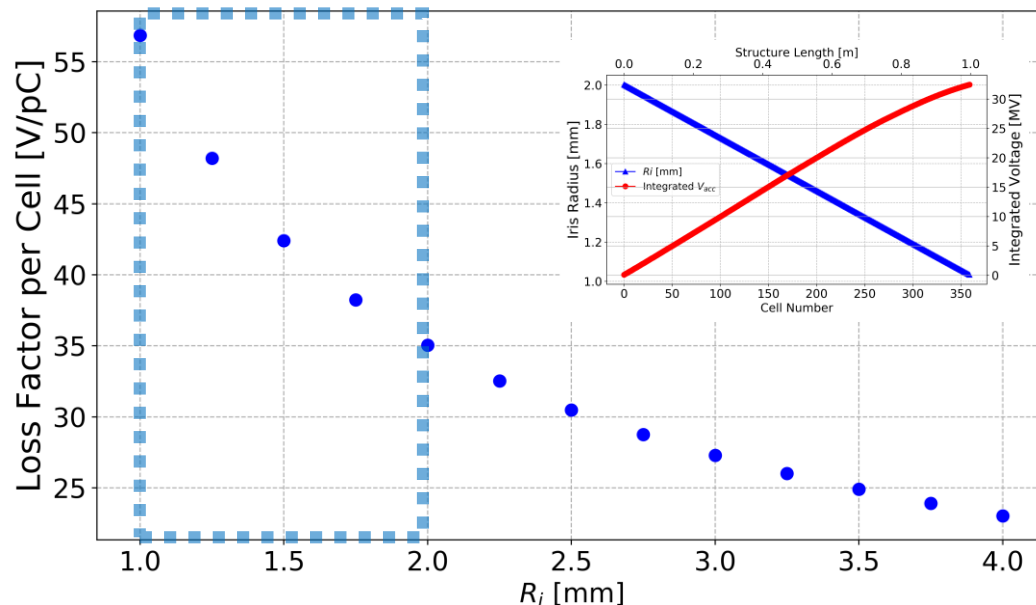
- Improved gains at the expense of tapering the iris:
  - Higher loss factor.
  - ~32MV integrated voltage.



Constant  
Impedance

# Simple Cell: 'Constant Gradient' (@8MW)

- Improved gains at the expense of tapering the iris:
  - Higher loss factor: Sweeping between 2 and 1mm.
  - Slightly higher integrated voltage (~32MV).



# Summary

- **Detailed exploration of the parameter space revisited:**
  - Wakes constrain the minimum iris aperture.
  - RF performance constrains the maximum iris aperture.
  - **A simple cell geometry is proposed with 2mm iris radius.**
- **Performance of a 1m structure:**
  - ~25MV achievable with reasonable power considerations.
- **Power recirculation option:**
  - More efficient for higher iris apertures (i.e. lower attenuation factors).
- **Constant gradient structure option:**
  - Higher integrated voltages than the constant impedance option.
  - Higher loss factors from wakes due to reduction on the iris aperture.



# Thanks!