



SAPIENZA  
UNIVERSITÀ DI ROMA



## Space Charge Effects and Instabilities

Mauro Migliorati

LA SAPIENZA - *Università di Roma and INFN*

JUAS 2019

# EQUATION OF MOTION

Charged particles in a transport channel or in a circular/linear accelerator are accelerated, guided and confined by external electromagnetic fields. The motion of a single charge is governed by the Lorentz force through the equation:

$$\frac{d(m_0 \gamma \mathbf{v})}{dt} = \mathbf{F}_{e.m.}^{ext} = e(\mathbf{E} + \mathbf{v} \times \mathbf{B})$$

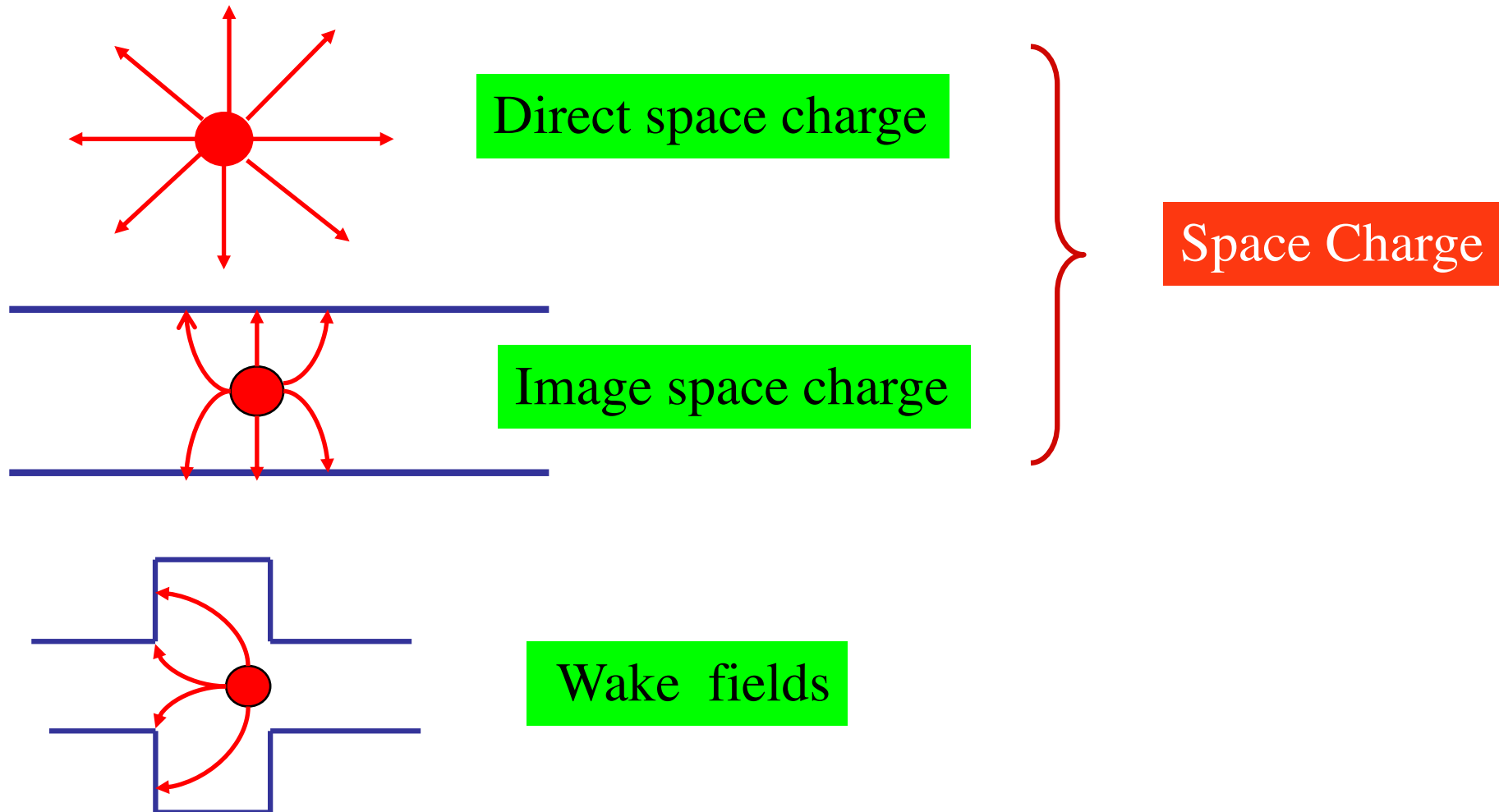
Where  $m_0$  is the rest mass,  $\gamma$  is the relativistic factor and  $\mathbf{v}$  is the particle velocity.

Acceleration is usually provided by the electric field inside of RF cavities. Magnetic fields are produced in the bending magnets for guiding the charges on the reference trajectory (orbit), in the quadrupoles for the transverse confinement, in the sextupoles for the chromaticity correction.

**However, there is another source of e.m. fields, the beam itself...**

# SPACE CHARGE AND WAKE FIELDS

In a real accelerator, in particular at high currents, there is an important source of e.m. fields to be considered, the beam itself, which circulating inside the vacuum chamber, produces additional e.m. fields:



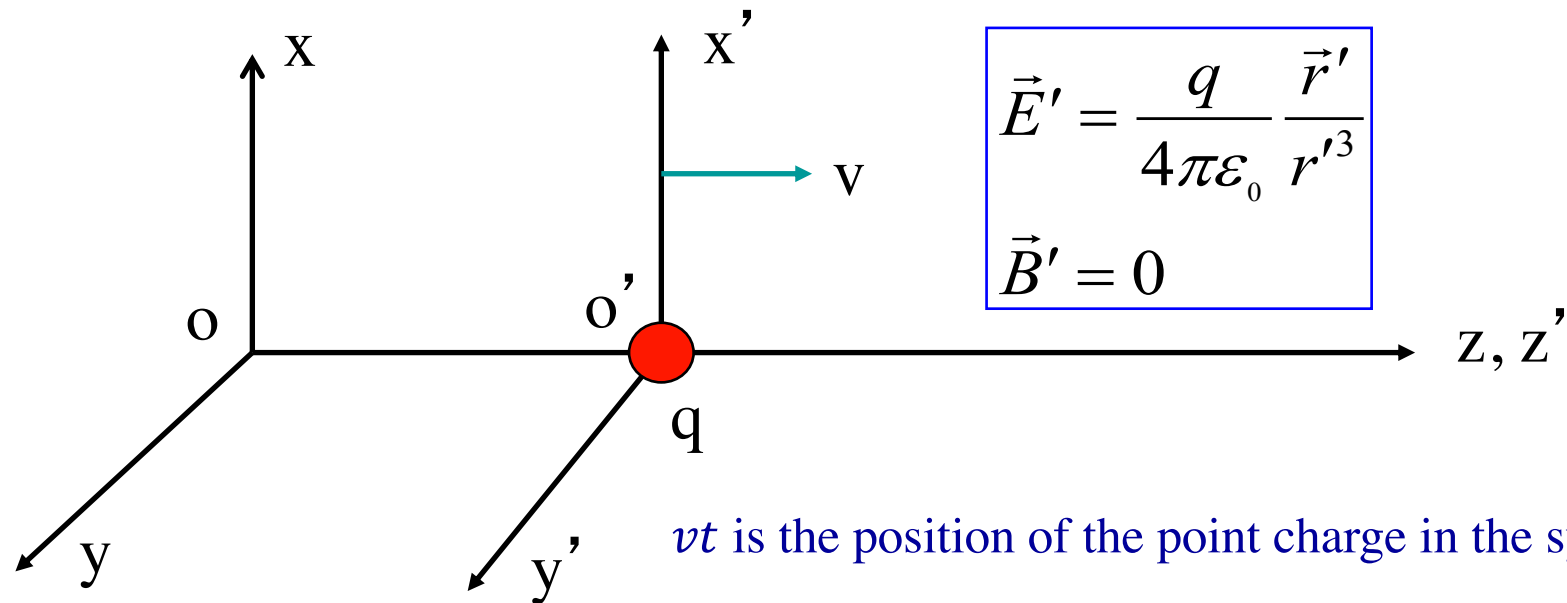
These self induced fields depend on:

- the beam current and beam distribution
- the surrounding geometry and the beam pipe
- the surrounding material.

**They are responsible of many phenomena of beam dynamics:**

- betatron tune shift
- synchrotron tune shift
- energy loss
- energy spread and emittance degradation
- instabilities.

## Fields of a point charge with uniform motion



$$E'_x = \frac{q}{4\pi\epsilon_0} \frac{x'}{r'^3}$$

$$E'_y = \frac{q}{4\pi\epsilon_0} \frac{y'}{r'^3}$$

$$E'_z = \frac{q}{4\pi\epsilon_0} \frac{z'}{r'^3}$$

- In  $O'$  the charge is at rest
- The electric field is radial with spherical symmetry
- The magnetic field is zero

## Relativistic transformations of the fields and coordinates from O' to O

$$\begin{cases} E_x = \gamma(E'_x + vB'_y) \\ E_y = \gamma(E'_y - vB'_x) \\ E_z = E'_z \end{cases} \quad \begin{cases} B_x = \gamma(B'_x - vE'_y/c^2) \\ B_y = \gamma(B'_y + vE'_x/c^2) \\ B_z = B'_z \end{cases} \quad \gamma = \frac{1}{\sqrt{1 - \beta^2}}$$

$$\begin{cases} x' = x \\ y' = y \\ z' = \gamma(z - vt) \end{cases} \quad \begin{aligned} r' &= (x'^2 + y'^2 + z'^2)^{1/2} \\ r' &= [x^2 + y^2 + \gamma^2(z - vt)^2]^{1/2} \end{aligned}$$

$$E_x = \gamma E'_x = \frac{q}{4\pi\epsilon_0} \frac{\gamma x'}{r'^3} = \frac{q}{4\pi\epsilon_0} \frac{\gamma x}{\left[x^2 + y^2 + \gamma^2(z - vt)^2\right]^{3/2}}$$

$$E_y = \gamma E'_y = \frac{q}{4\pi\epsilon_0} \frac{\gamma y'}{r'^3} = \frac{q}{4\pi\epsilon_0} \frac{\gamma y}{\left[x^2 + y^2 + \gamma^2(z - vt)^2\right]^{3/2}}$$

$$E_z = E'_z = \frac{q}{4\pi\epsilon_0} \frac{z'}{r'^3} = \frac{q}{4\pi\epsilon_0} \frac{\gamma(z - vt)}{\left[x^2 + y^2 + \gamma^2(z - vt)^2\right]^{3/2}}$$

The electric field has lost the spherical symmetry but still keeps a symmetry in the x-y plane (with respect the z-axis).

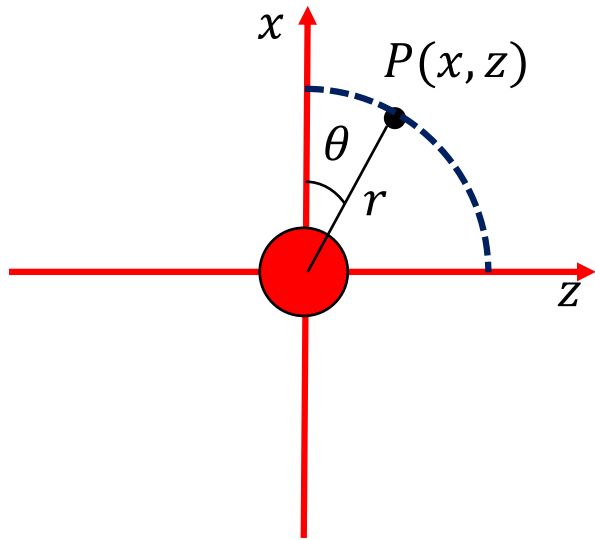
We can consider the properties of the field at time  $t=0$  because the field translates along  $z$  together with the charge.

$$\vec{E} = \frac{q}{4\pi\epsilon_0} \frac{\gamma \vec{r}}{\left[x^2 + y^2 + \gamma^2 z^2\right]^{3/2}}$$

$$\vec{E} = \frac{q}{4\pi\epsilon_0} \frac{\gamma\vec{r}}{(x^2 + y^2 + \gamma^2 z^2)^{3/2}}$$

Due to the  $x - y$  symmetry (cylindrical symmetry) , we can consider  $y = 0$  ( $x - z$  plane) and use

$$x = r \cos \theta, \quad z = r \sin \theta$$



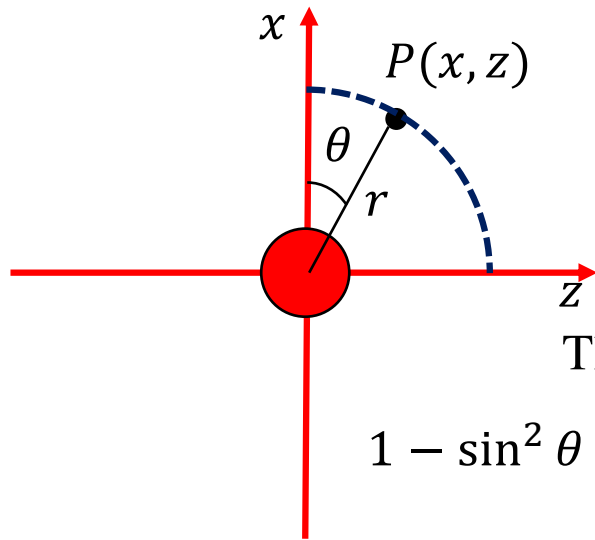
$$|\vec{E}| = \frac{q}{4\pi\epsilon_0 r^2} \frac{\gamma}{(\cos^2 \theta + \gamma^2 \sin^2 \theta)^{3/2}}$$

$$|\vec{E}|_{max} \text{ when } \theta = 0: \quad |\vec{E}|_{max} = \frac{\gamma q}{4\pi\epsilon_0 r^2}$$

$$|\vec{E}|_{min} \text{ when } \theta = \pi/2: \quad |\vec{E}|_{min} = \frac{q}{4\pi\epsilon_0 r^2 \gamma^2}$$



$$|\vec{E}| = \frac{q}{4\pi\epsilon_0 r^2} \frac{\gamma}{(\cos^2 \theta + \gamma^2 \sin^2 \theta)^{3/2}} = \frac{|\vec{E}|_{max}}{(\cos^2 \theta + \gamma^2 \sin^2 \theta)^{3/2}}$$



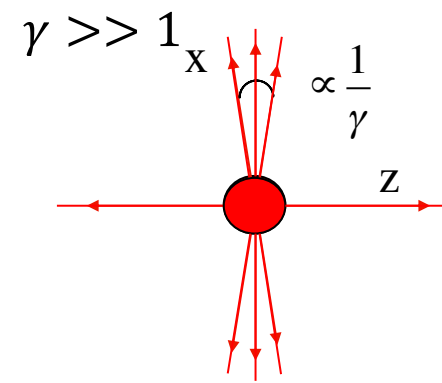
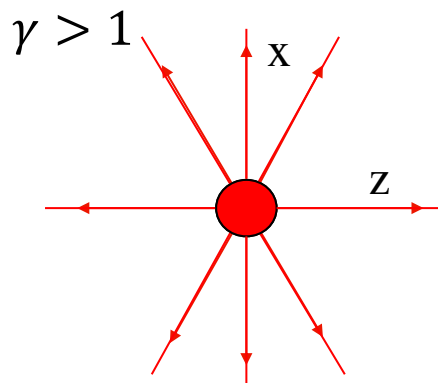
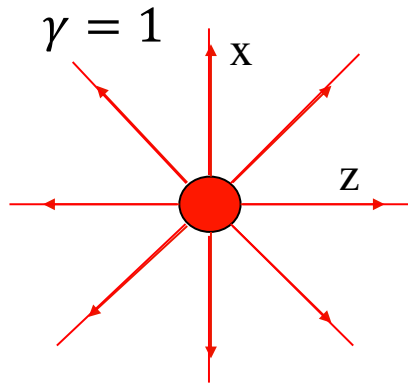
When  $(\cos^2 \theta + \gamma^2 \sin^2 \theta) = 2$ , we have

$$|\vec{E}| = \frac{|\vec{E}|_{max}}{\sqrt{8}} \simeq \frac{|\vec{E}|_{max}}{3}$$

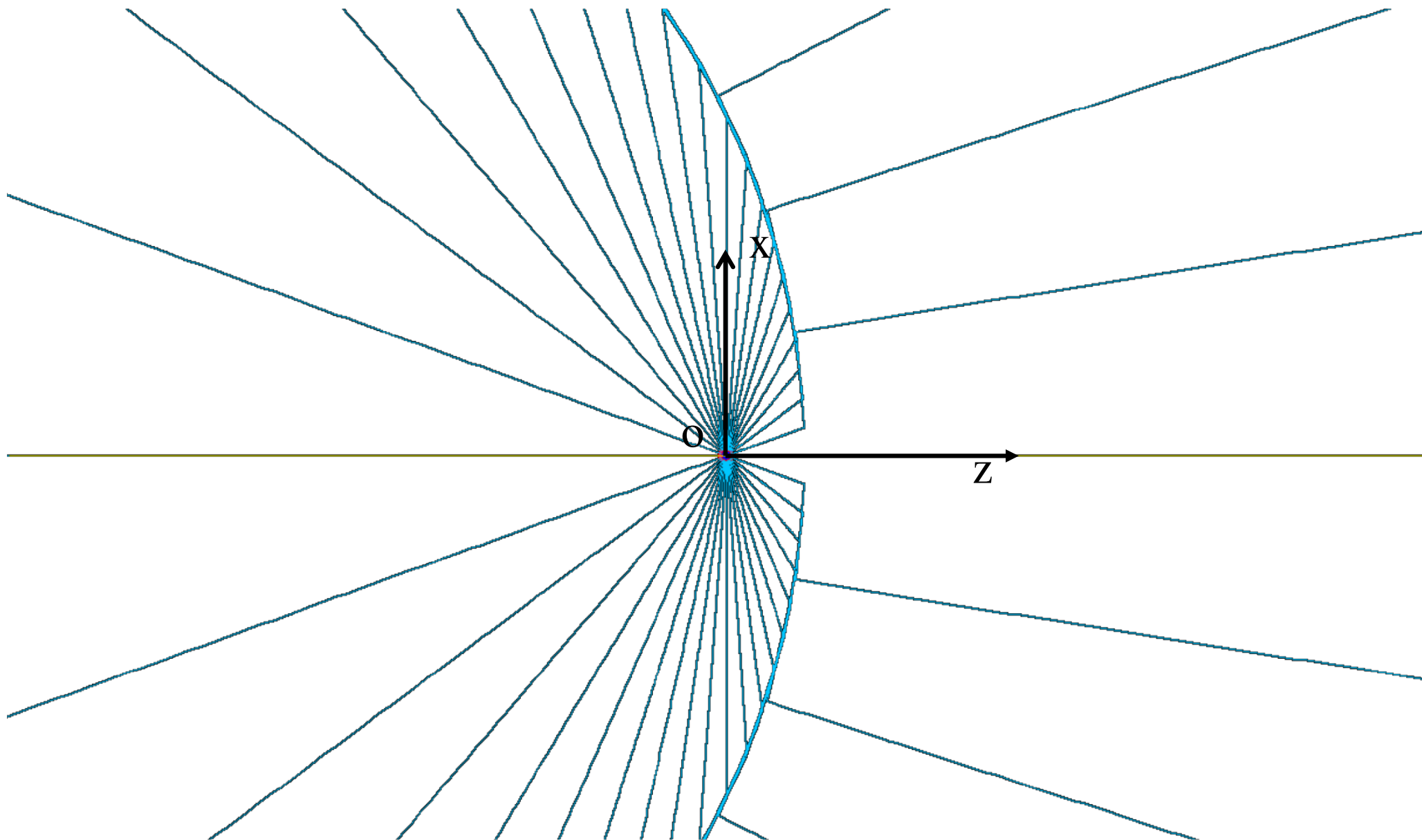
This happens when

$$1 - \sin^2 \theta + \gamma^2 \sin^2 \theta = 2 \rightarrow \sin^2 \theta = \frac{1}{\gamma^2 - 1} \rightarrow (\text{if } \gamma \gg 1) \rightarrow \theta \simeq \frac{1}{\gamma}$$

### Electric field lines



# Electric field lines of a charge moving with velocity $\beta c$



$$E_x = \gamma E'_x = \frac{q}{4\pi\epsilon_0} \frac{\gamma x'}{r'^3} = \frac{q}{4\pi\epsilon_0} \frac{\gamma x}{[x^2 + y^2 + \gamma^2(z - vt)^2]^{3/2}}$$

$$E_y = \gamma E'_y = \frac{q}{4\pi\epsilon_0} \frac{\gamma y'}{r'^3} = \frac{q}{4\pi\epsilon_0} \frac{\gamma y}{[x^2 + y^2 + \gamma^2(z - vt)^2]^{3/2}}$$

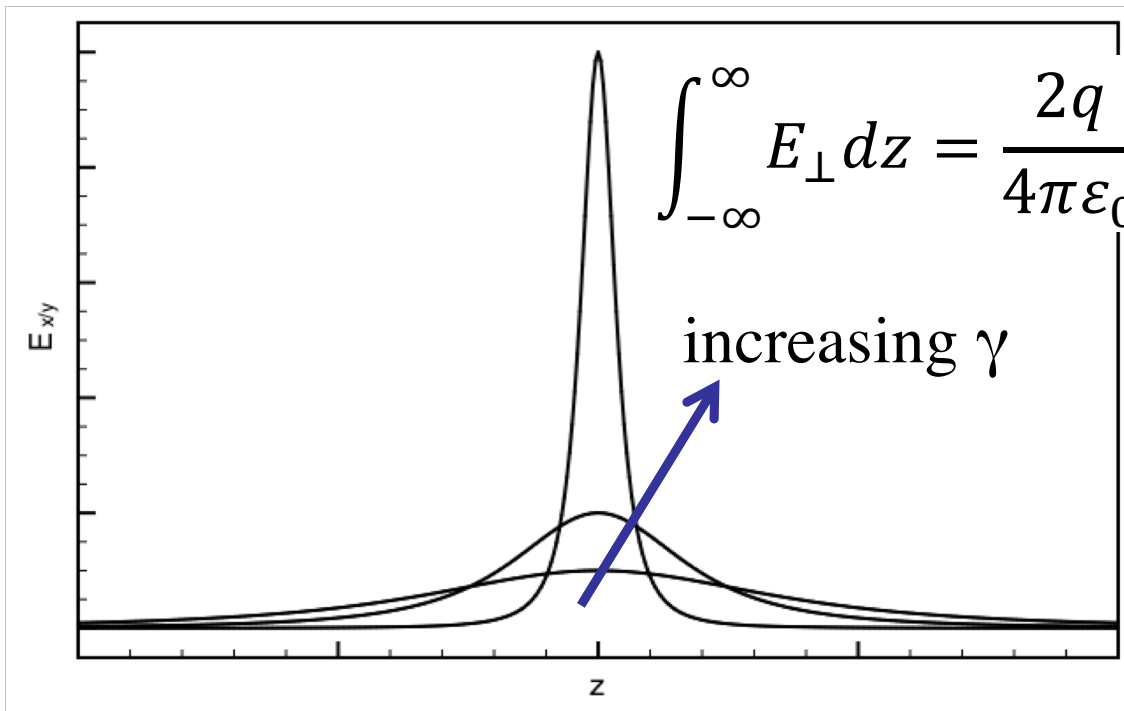
$$E_z = E'_z = \frac{q}{4\pi\epsilon_0} \frac{z'}{r'^3} = \frac{q}{4\pi\epsilon_0} \frac{\gamma(z - vt)}{[x^2 + y^2 + \gamma^2(z - vt)^2]^{3/2}}$$

$\gamma \rightarrow \infty$   
 $v \rightarrow c$

$$\begin{cases} E_x = ? \\ E_y = ? \\ E_z \rightarrow 0 \end{cases}$$

$$z \neq ct \Rightarrow E_{\perp} = 0 \quad (1)$$

$$z = ct \Rightarrow E_{\perp} = \infty \quad (2)$$



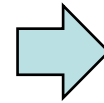
$$\int_{-\infty}^{\infty} E_{\perp} dz = \frac{2q}{4\pi\epsilon_0} \frac{1}{r}$$

independent on  $\gamma$  (3)

$$\Rightarrow E_{\perp} = \frac{2q}{4\pi\epsilon_0} \frac{1}{r} \delta(z - ct)$$

**B is transverse to the motion direction**

$$\begin{aligned}
 E_x &= \gamma(E'_x + vB'_y) & B_x &= \gamma(B'_x - vE'_y/c^2) \\
 E_y &= \gamma(E'_y - vB'_x) & B_y &= \gamma(B'_y + vE'_x/c^2) \\
 E_z &= E'_z & B_z &= B'_z
 \end{aligned}$$

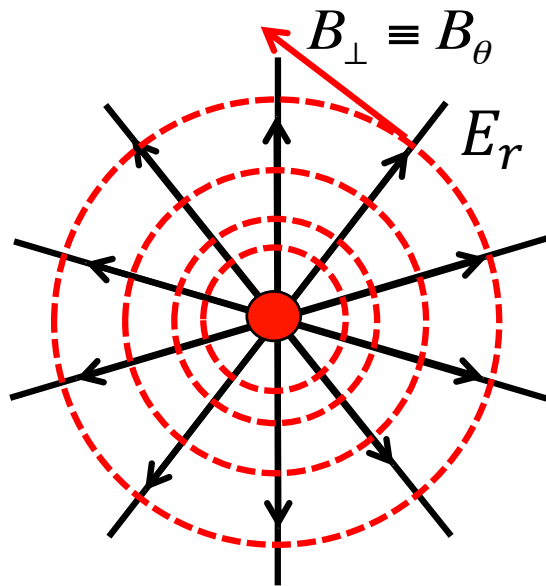


$$\begin{aligned}
 B_z &= 0 \\
 B_x &= -vE_y/c^2 \\
 B_y &= vE_x/c^2
 \end{aligned}$$

$$\vec{B}_\perp = \frac{\vec{v} \times \vec{E}}{c^2}$$

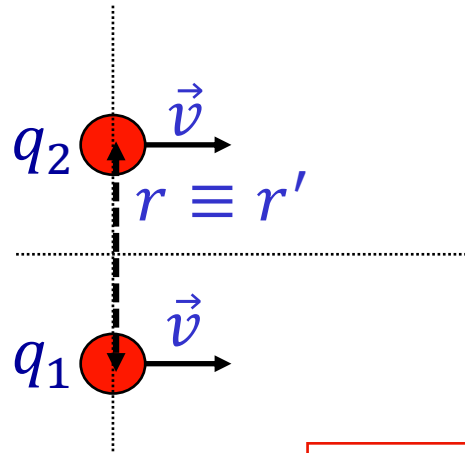


$$B_\theta = \frac{vE_r}{c^2} = \frac{\beta E_r}{c}$$



$$\gamma \gg 1$$

## Two point charges with same velocity on parallel trajectories



In the frame O' in which charges are at rest

$$F_r' = \frac{1}{4\pi\epsilon_0} \frac{q_1 q_2}{r'^2}$$

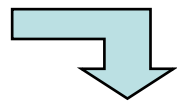
In the frame O in which charges are moving

Relativistic transformations



$$F_r = \frac{1}{\gamma} F_r' = \frac{1}{4\pi\epsilon_0} \frac{q_1 q_2}{\gamma r'^2}$$

Lorentz force

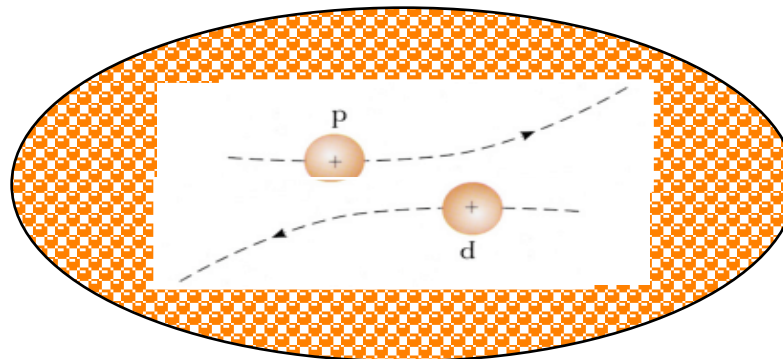


$$F_r = q_2 (E_r - v B_{\perp}) = q_2 \left( E_r - \frac{v^2 E_r}{c^2} \right) = q_2 (E_r - \beta^2 E_r) = \frac{q_2}{\gamma^2} E_r = \frac{1}{4\pi\epsilon_0} \frac{q_1 q_2}{\gamma r^2}$$

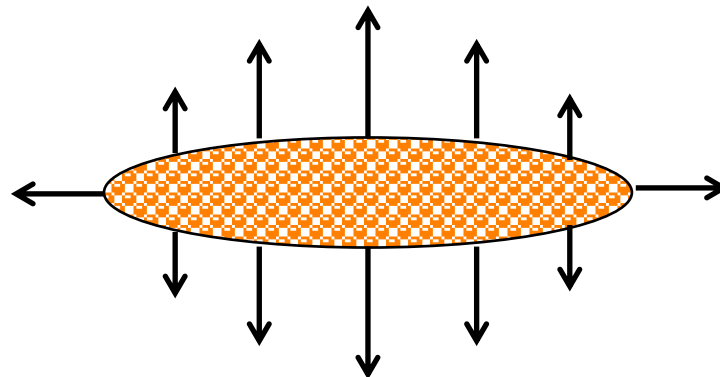
## Space Charge

The effect of the **Coulomb** interactions in a multi-particle system can be classified into two regimes:

- 1) **Collisional Regime** ==> dominated by **binary collisions** between particles ==> **Single Particle Effects (e.g. intra-beam scattering)**



- 2) **Space Charge Regime** ==> dominated by the **self fields** produced by the entire distribution ==> **Collective Effects**



## Collisional and Space Charge regimes

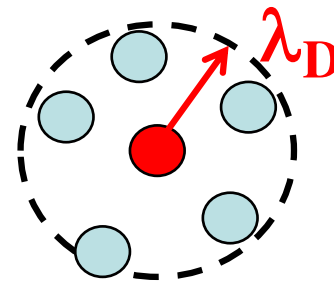
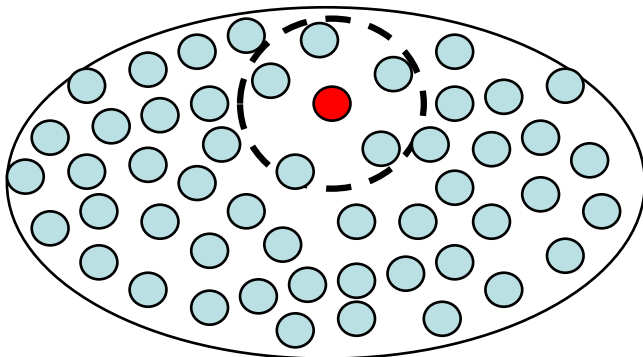
- The interaction of the charged particles in a beam can be represented by the sum of a “collisional” and a “smooth” force. The collisional part of the interaction force arises when a particle “sees” its immediate neighbours and is affected by their individual positions. This force will cause small random displacements of the particle’s trajectory and statistical fluctuations in the particle distribution as a whole. In most practical beams, however, this is a small effect, and the mutual interaction between particles is described largely by a smoothed force.
- A measure for the relative importance of collisional versus smoothed interaction, of single-particle versus collective effects, is the *Debye length*,  $\lambda_D$ : it is a distance over which a local perturbation in the equilibrium charge distribution of a beam with transverse temperature  $T$  and density  $n$ , confined by external focusing fields, is screened off.

## Collisional and Space Charge regimes

If the Debye length is large compared with the beam radius ( $\lambda_D \gg a$ ), the screening will be ineffective and single-particle behaviour will dominate (motion of particles is influenced by local perturbations): **collisional regime**.

On the other hand, if the Debye length is small compared to the beam radius ( $\lambda_D \ll a$ ), smooth functions for the charge and field distributions can be used, and collective effects due to the self fields of the entire beam will play an important role: **space charge regime**.

The charges surrounding a test particle have a screening effect at a distance  $\lambda_D$



$$\lambda_D = \sqrt{\frac{\epsilon_o k_B T}{e^2 n}}$$

$k_B$  = Boltzmann constant

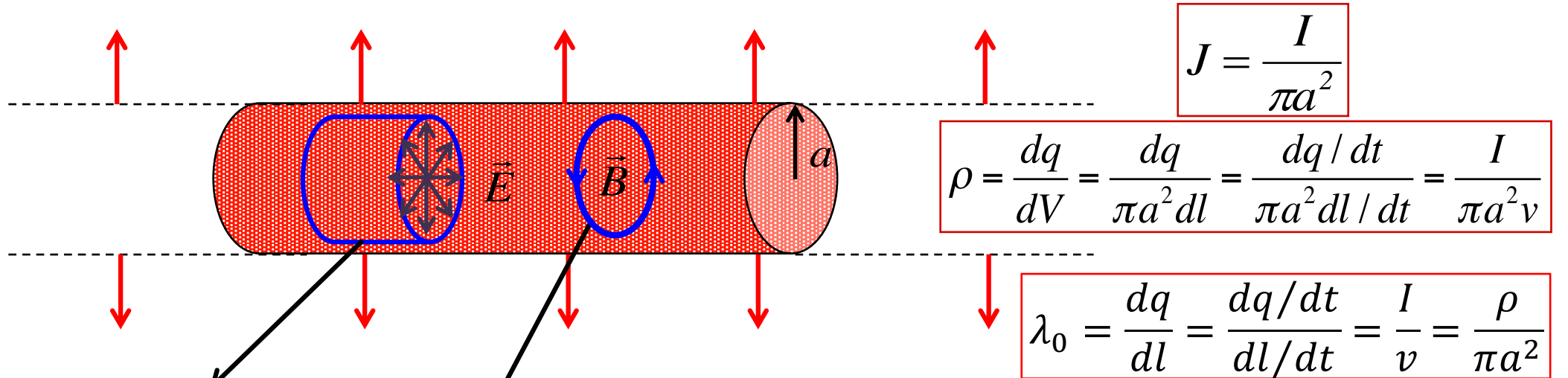
T = Temperature

$k_B T$  = average kinetic energy of the particles =  $\gamma m_o \langle v_{\perp}^2 \rangle$

n = particle density (N/V)



# Example 1. Relativistic Uniform Cylindrical Beam



Gauss' s law

$$\epsilon_0 \int \vec{E} \cdot d\vec{S} = \int \rho dV$$

$$2\pi r l \epsilon_0 E_r = \rho \pi r^2 l$$

$$E_r = \frac{\rho r}{2\epsilon_0} = \frac{I r}{2\pi\epsilon_0 a^2 v} = \frac{\lambda_0 r}{2\pi\epsilon_0 a^2} \quad \text{for } r \leq a$$

**Linear**

Ampere' s law

$$\oint \vec{B} \cdot d\vec{l} = \mu_0 \int \vec{J} \cdot d\vec{S}$$

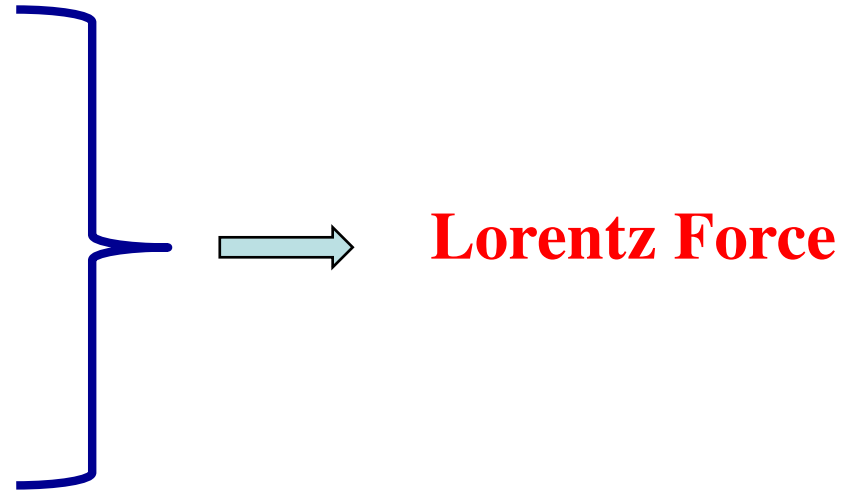
$$2\pi r B_\theta = \mu_0 J \pi r^2$$

$$B_\theta = \frac{\mu_0 J r}{2} = \mu_0 \frac{I r}{2\pi a^2} = \frac{1}{\epsilon_0 c^2} \frac{I r}{2\pi a^2} \frac{v}{v} = \frac{\beta}{c} \frac{I r}{2\pi\epsilon_0 a^2 v} \quad \text{for } r \leq a$$

$$B_\theta = \frac{\beta}{c} E_r$$

$$E_r(r) = \frac{Ir}{2\pi\epsilon_0 a^2 v} = \frac{\lambda_0}{2\pi\epsilon_0 a^2} r$$

$$B_\theta(r) = \frac{\beta}{c} E_r(r) = \frac{\lambda_0}{2\pi\epsilon_0 a^2} \frac{\beta}{c} r$$



$$F_r(r) = e(E_r - \beta c B_\theta) = e(1 - \beta^2) E_r = \frac{e E_r(r)}{\gamma^2}$$

- has only **radial** component
- is a **linear** function of the transverse coordinate

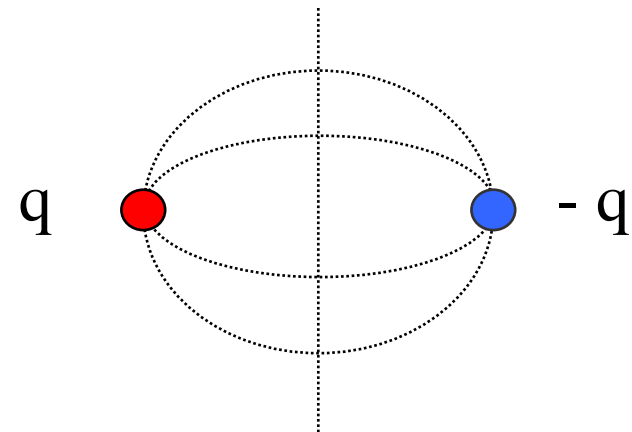
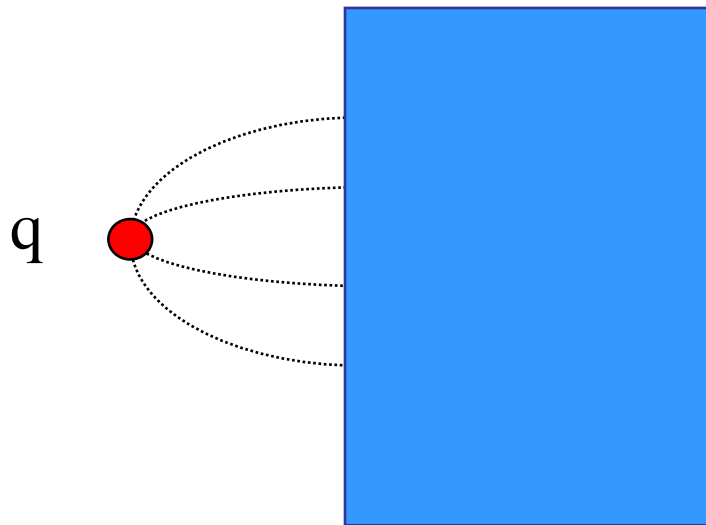
The attractive magnetic force, which becomes significant at high velocities, tends to compensate the repulsive electric force. Therefore, space charge defocusing is primarily a non-relativistic effect.

# **Space charge with image charges/currents**

## Static Fields: conducting or magnetic screens

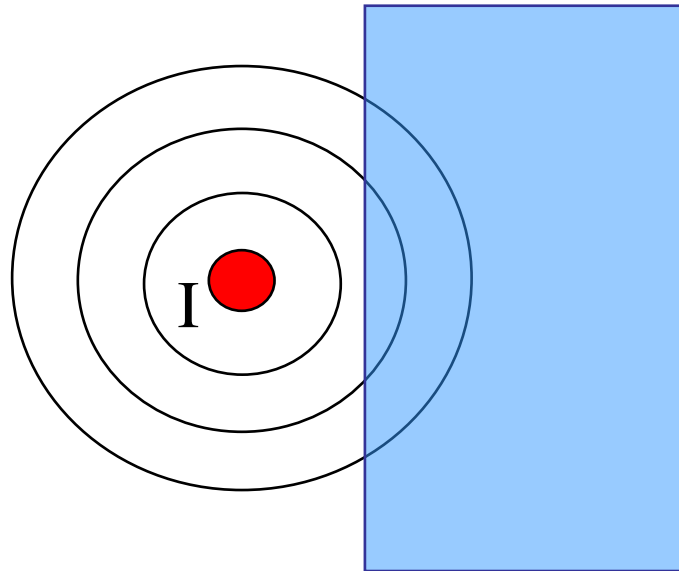
Let us consider a point charge  $q$  close to a conducting screen.

The electrostatic field can be derived through the "image method". Since the metallic screen is an equi-potential plane, it can be removed provided that a "virtual" charge is introduced such that the potential is constant at the position of the screen



A constant current in the free space produces a circular magnetic field.

**If  $\mu_r \approx 1$ , the material, even in the case of a good conductor, does not affect the field lines.**

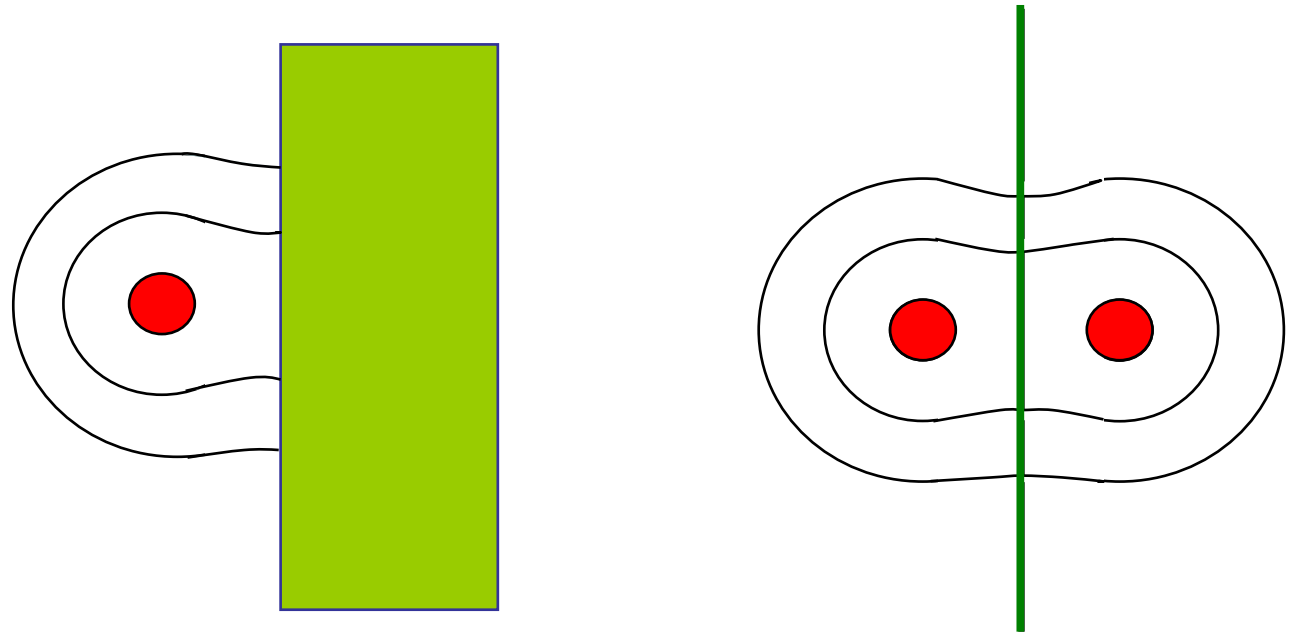


For **ferromagnetic materials**, with  $\mu_r \gg 1$ , the very high magnetic permeability makes the tangent magnetic field zero at the boundary so that the magnetic field is perpendicular to the surface, just like the electric field lines close to a conductor.

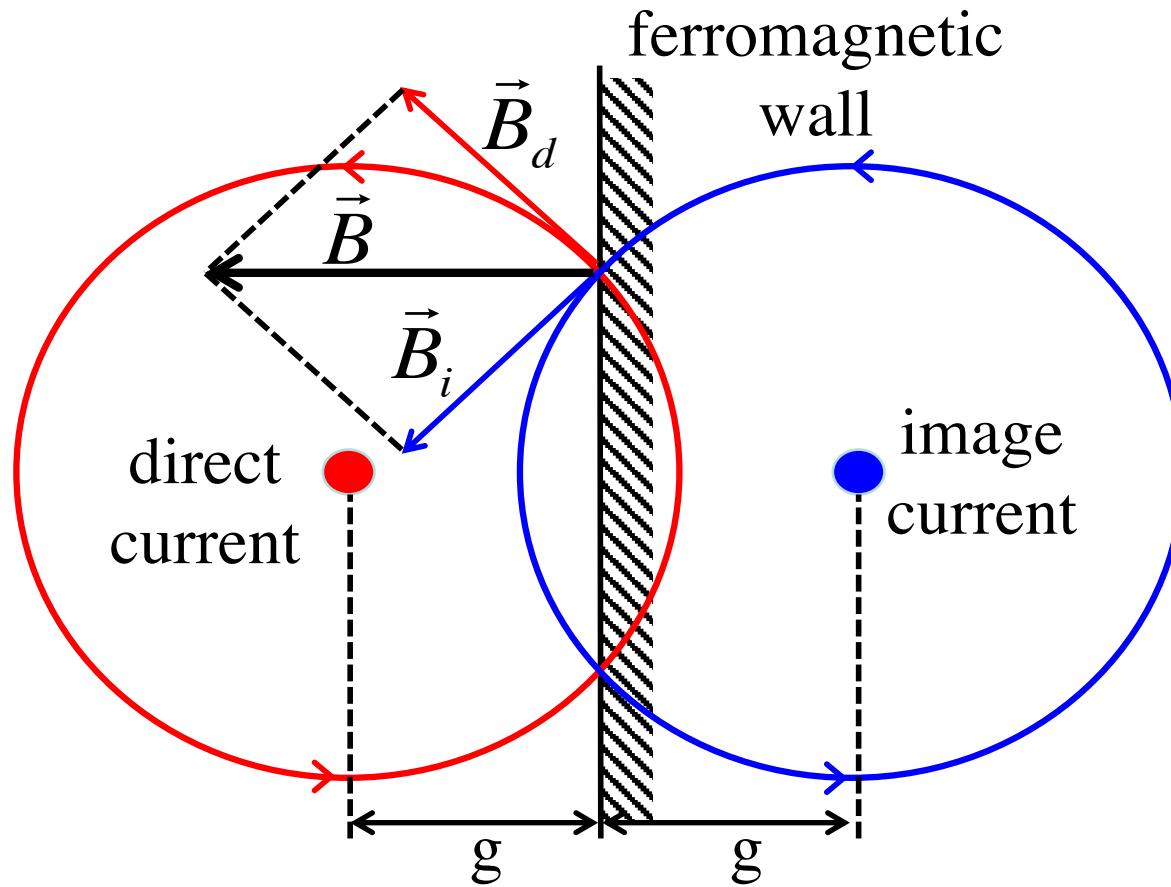
Law of refraction of magnetic field lines:

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{\mu_{r1}}{\mu_{r2}}$$

$$\mu_{r2} \rightarrow \infty \Rightarrow \theta_1 \rightarrow 0$$



In analogy with the image method we get the magnetic field, in the region outside of the material, as superposition of the fields due to two symmetric equal currents flowing in the same direction.



Satisfying a magnetic boundary condition by an image current.

## Time-varying fields

Static electric fields vanish inside a conductor for any finite conductivity, while magnetic fields pass through unless of high permeability.

This is no longer true for time changing fields, which can penetrate inside the material in a region characterized by a quantity called skin depth  $\delta_w$ . Inside the conducting material we write the following Maxwell's equations:

$$\left\{ \begin{array}{l} \nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t} \\ \nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t} \end{array} \right. \quad \left\{ \begin{array}{l} \mathbf{B} = \mu \mathbf{H} \\ \mathbf{D} = \epsilon \mathbf{E} \\ \mathbf{J} = \sigma \mathbf{E} \end{array} \right. \longrightarrow \boxed{\text{Constitutive relations}}$$

Copper  $\sigma = 5.8 \cdot 10^7 \text{ (}\Omega\text{m)}^{-1}$

Aluminium  $\sigma = 3.5 \cdot 10^7 \text{ (}\Omega\text{m)}^{-1}$

Stainless steel  $\sigma = 1.4 \cdot 10^6 \text{ (}\Omega\text{m)}^{-1}$



$$\nabla^2 \mathbf{E} = \mu\sigma \frac{\partial \mathbf{E}}{\partial t} + \mu\epsilon \frac{\partial^2 \mathbf{E}}{\partial t^2} \qquad \nabla^2 \mathbf{H} = \mu\sigma \frac{\partial \mathbf{H}}{\partial t} + \mu\epsilon \frac{\partial^2 \mathbf{H}}{\partial t^2}$$

Consider a plane wave ( $H_y, E_x$ ) propagating in the material

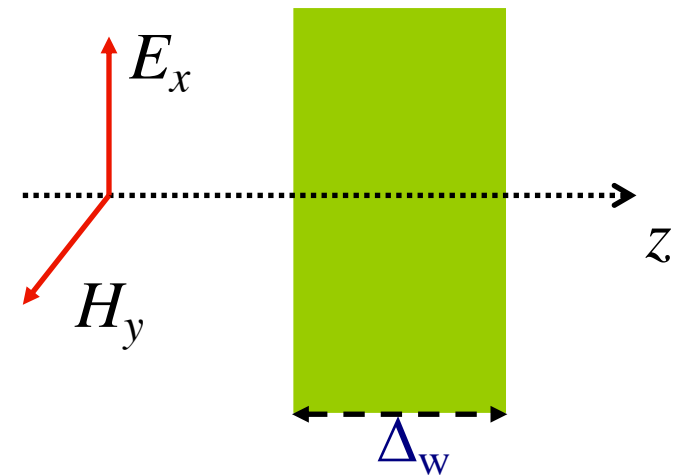
$$\frac{\partial^2 E_x}{\partial z^2} - \epsilon\mu \frac{\partial^2 E_x}{\partial t^2} - \sigma\mu \frac{\partial E_x}{\partial t} = 0$$

(the same equation holds for  $H_y$ ). Assuming that fields propagate in the z-direction with the law:

$$H_y = \tilde{H}_0 e^{i\omega t - kz}$$

$$E_x = \tilde{E}_0 e^{i\omega t - kz}$$

$$(k^2 + \epsilon\mu\omega^2 - i\omega\mu\sigma)\tilde{E}_0 e^{i\omega t - kz} = 0$$

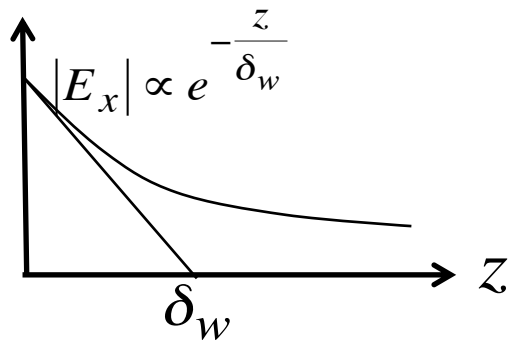


We say that the material behaves like a conductor if  $\sigma \gg \omega\epsilon$  thus:

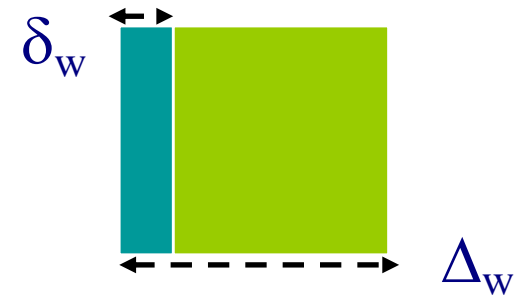
$$k \cong (1 + i) \sqrt{\frac{\sigma\mu\omega}{2}} \qquad \Re(k) = \sqrt{\frac{\sigma\mu\omega}{2}} \quad \Rightarrow \quad \text{Exponential decay}$$

Fields propagating along “z” are attenuated.

The attenuation constant measured in meters is called skin depth  $\delta_w$ :



$$\delta_w \cong \frac{1}{\Re(k)} = \sqrt{\frac{2}{\omega\sigma\mu}}$$

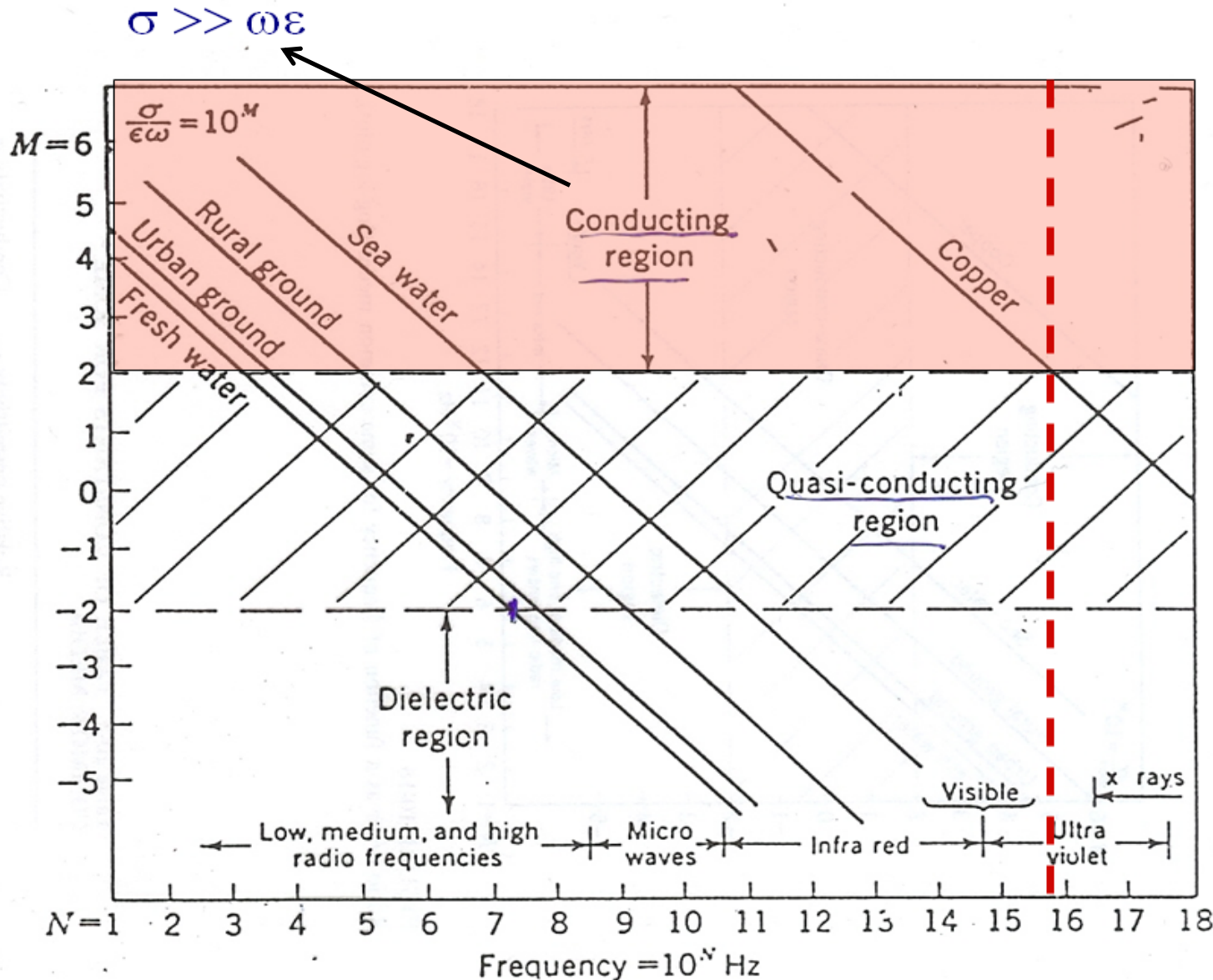


The skin depth depends on the material properties and on the frequency. Fields pass through the conductor wall if the skin depth is larger than the wall thickness  $\Delta_w$ . This happens at relatively low frequencies.

At higher frequencies, for a good conductor  $\delta_w \ll \Delta_w$  and both electric and magnetic fields vanish inside the wall.

For the copper 
$$\delta_w \cong \frac{6.6}{\sqrt{f(Hz)}} (cm); \quad \omega = 2\pi f$$

For a pipe 2mm thick, the fields pass through the wall up to 1 kHz.  
(Skin depth of Aluminium is larger by a factor 1.28)

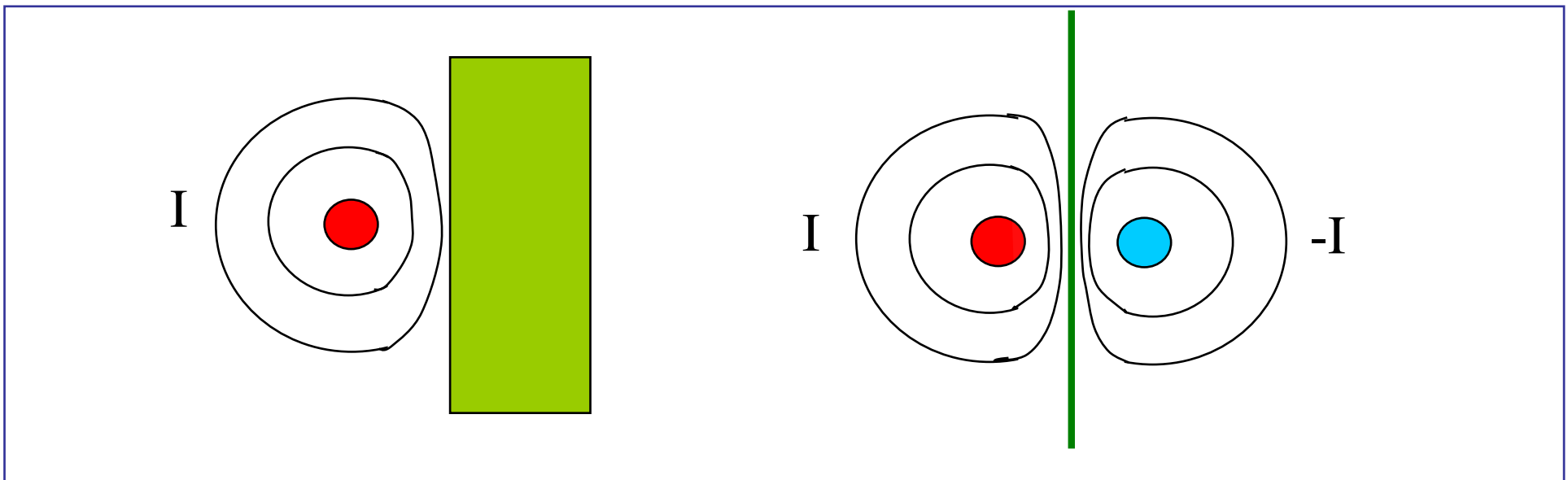


Note that copper behaves like a conductor at frequencies far above the microwave region. On the other hand, fresh water acts like a dielectrics at frequencies above about 10MHz

$$\begin{aligned}
 M &= \log \frac{\sigma}{\epsilon\omega} = \\
 &= \log \frac{\sigma}{\epsilon 2\pi} - \log f \\
 &= \log \frac{\sigma}{\epsilon 2\pi} - N
 \end{aligned}$$

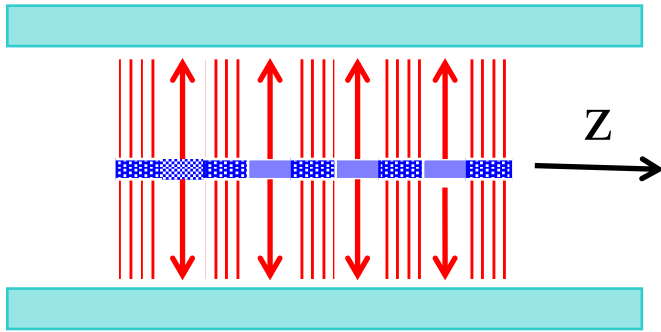
**Ratio  $\sigma/\omega\epsilon$  as a function of frequency  $f$  for some common media (log-log plot)**

- Compare the wall thickness and the skin depth (region of penetration of the e.m. fields) in the conductor.
- If the fields penetrate and pass through the material, they can interact with bodies in the outer region.
- If the skin depth is very small (rapidly varying fields), fields do not penetrate, the electric field lines are perpendicular to the wall, as in the static case, while the magnetic field lines are tangent to the surface.



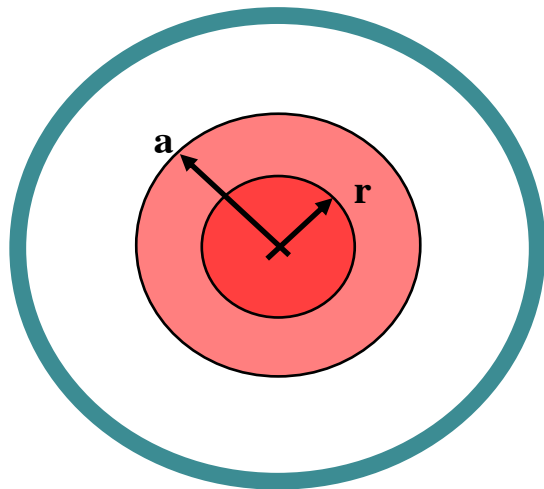
## Example 2: Circular Perfectly Conducting Pipe

(Uniform Beam at Center)



If we take the previous uniform cylindrical beam and enclose it into a cylindric perfectly conducting pipe, the field lines are not perturbed because the electric ones are already radial and then perpendicular to the pipe, and the magnetic ones remain circular. The presence of the pipe does not affect the fields.

In the case of cylindrical charge distribution, with  $\gamma \gg 1$ , the electric field lines can be considered perpendicular to the direction of motion. The intensities of the transverse fields can be computed as in the static case, applying the Gauss's and Ampere's laws.



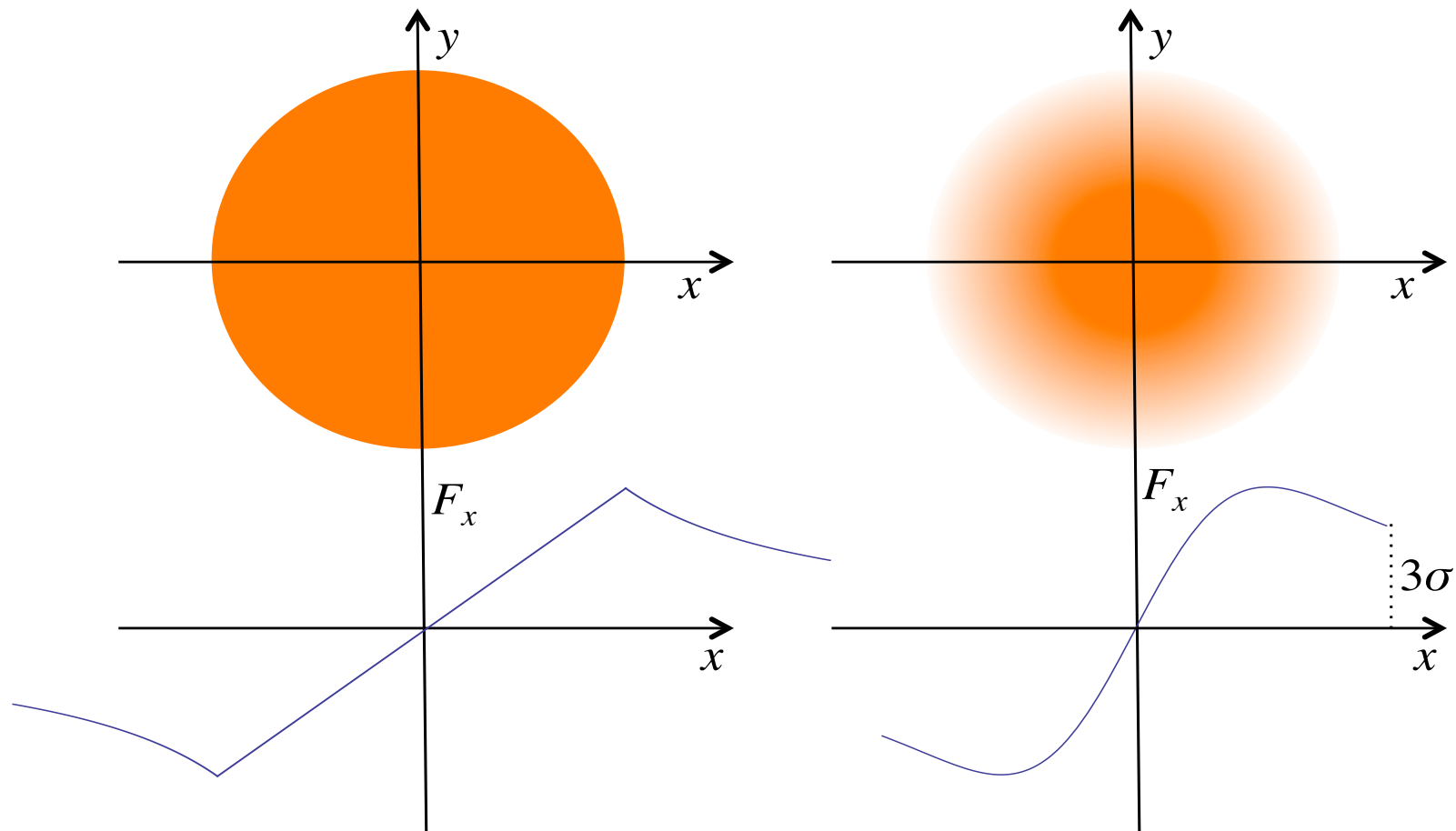
$$E_r(r) = \frac{\lambda_0}{2\pi\epsilon_0 a^2} r; \quad B_\theta(r) = \frac{\beta}{c} E_r(r) = \frac{\lambda_0 \beta}{2\pi\epsilon_0 a^2 c} r$$

$$F_\perp(r) = e(E_r - \beta c B_\theta) = \frac{e}{\gamma^2} \frac{\lambda_0}{2\pi a^2 \epsilon_0} r$$

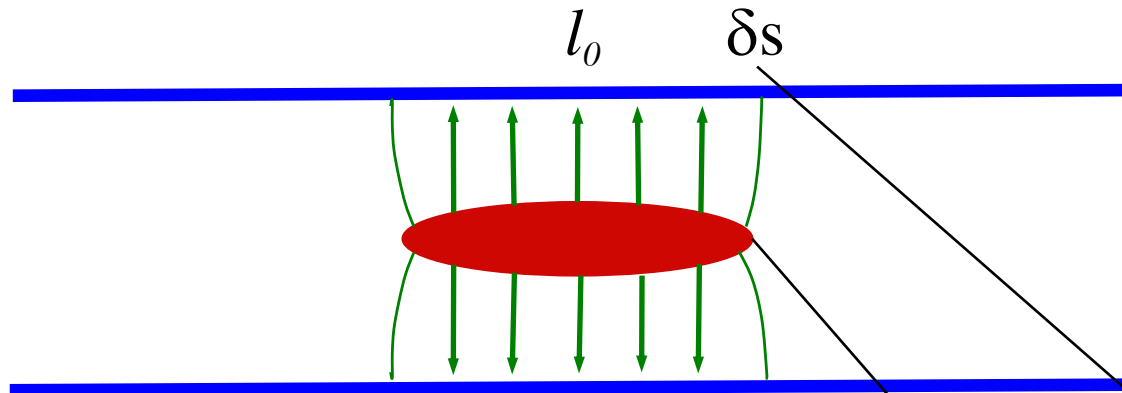
This direct space charge force does not depend on the longitudinal position along the beam. If  $\lambda$  is not constant, one should consider the local charge density  $\lambda(z)$  (some examples in the exercises).

If the transverse distribution is not uniform, we can still apply Gauss's and Ampere's laws (example in the exercises).

Defocusing transverse self induced forces produced by direct space charge in case of uniform (left) and Gaussian (right) distributions.



# Relativistic Uniform Cylindrical Beam – finite length



Beam pipe radius  $b$   
 Bunch length  $l_0$   
 Widening at the wall  $\delta s$

$$\delta s \cong \frac{b}{\gamma}$$

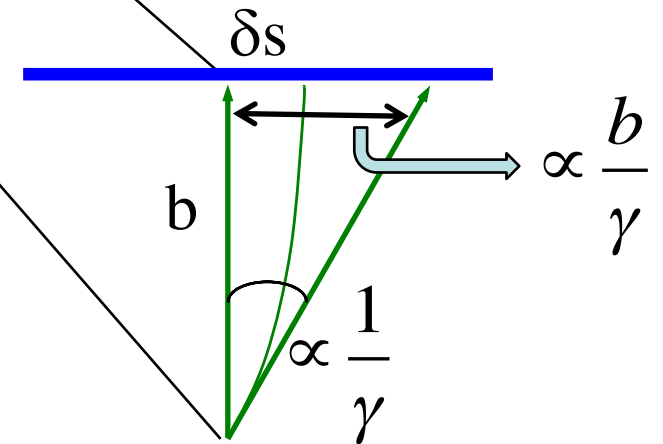
$$l_0 \gg \delta s$$

$$\gamma \gg \frac{b}{l_0}$$

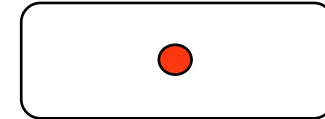
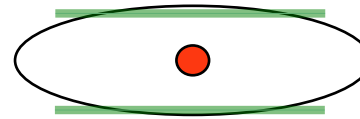
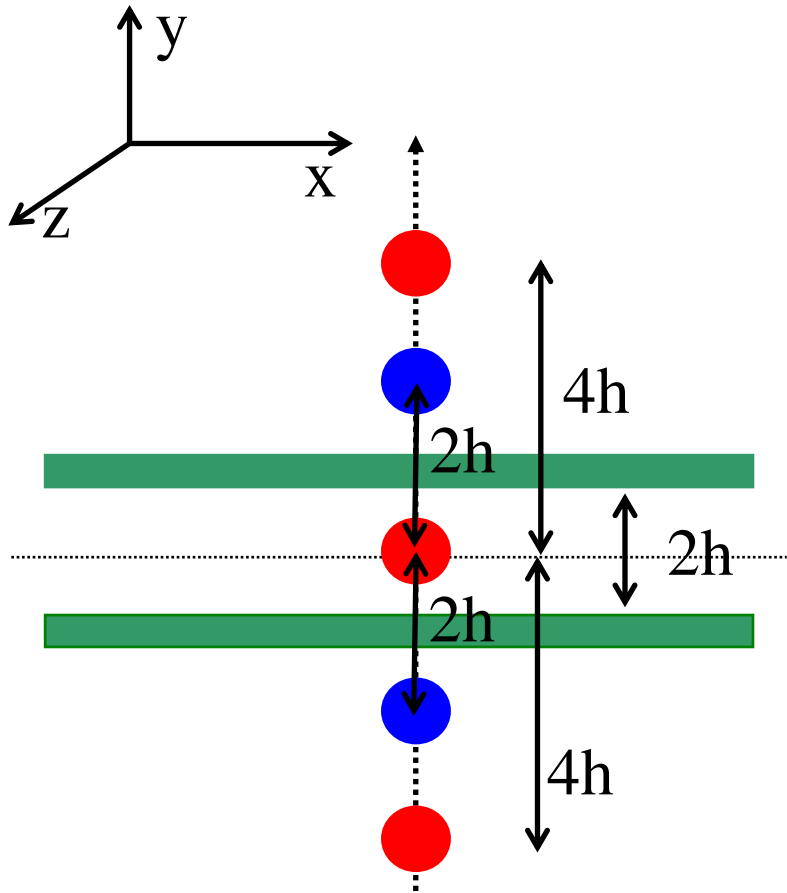
e.g.:  
 $b = 1 \text{ cm}$   
 $l_0 = 100 \mu\text{m}$



$\gamma \gg 100$



## Parallel Plates (Beam at Center)



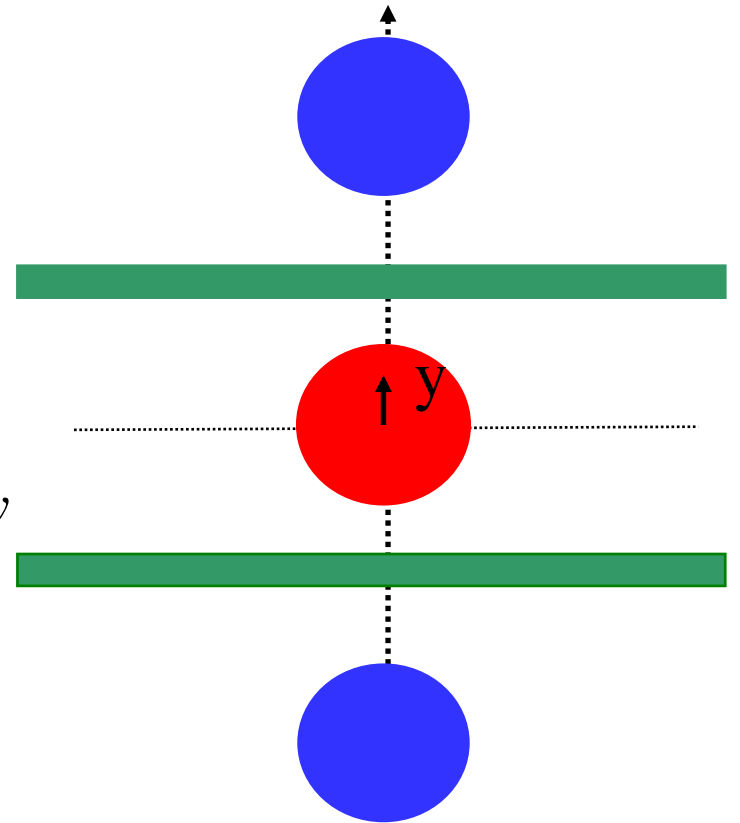
In some cases, the beam pipe cross section is such that we can consider only the surfaces closer to the beam, which behave like two parallel plates. In this case, we use the image method to a charge distribution of radius  $a$  between two conducting plates  $2h$  apart. By applying the superposition principle we get the total image field at a position  $y$  inside the beam.



$$E_y^{im}(z,y) = \frac{\lambda(z)}{2\pi \epsilon_0} \sum_{n=1}^{\infty} (-1)^n \left[ \frac{1}{2nh + y} - \frac{1}{2nh - y} \right]$$

$$E_y^{im}(z,y) = \frac{\lambda(z)}{2\pi \epsilon_0} \sum_{n=1}^{\infty} (-1)^n \frac{-2y}{(2nh)^2 - y^2} \cong \frac{\lambda(z)}{4\pi \epsilon_0 h^2} \frac{\pi^2}{12} y$$

Where we have assumed  $h \gg a \geq y$ .



For d.c. or slowly varying currents, the boundary conditions imposed by the conducting plates do not affect the magnetic field.

There is no magnetic field which can compensate the electric field due to the "image" charges.

$$F_y(y) = \frac{e}{\gamma^2} E_y^{dir} + eE_y^{im} = \frac{e}{\gamma^2} \frac{\lambda(z)}{2\pi \epsilon_0} \frac{y}{a^2} + \frac{e\lambda(z)}{4\pi \epsilon_0 h^2} \frac{\pi^2}{12} y$$

From the divergence equation  $\left( \nabla \cdot \mathbf{E}^{im} = \frac{\rho^{im}}{\epsilon_0} = 0 \right)$  we derive also the other transverse component:

$$\frac{\partial}{\partial x} E_x^{im} = -\frac{\partial}{\partial y} E_y^{im} \Rightarrow E_x^{im}(z, x) = \frac{-\lambda(z)}{4\pi\epsilon_0 h^2} \frac{\pi^2}{12} x$$

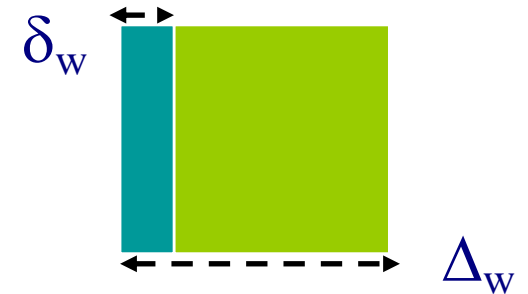
Including also the direct space charge force, we get:

$$F_x(z, x) = \frac{e\lambda(z)x}{\pi\epsilon_0} \left( \frac{1}{2a^2\gamma^2} - \frac{\pi^2}{48h^2} \right)$$

$$F_y(z, y) = \frac{e\lambda(z)y}{\pi\epsilon_0} \left( \frac{1}{2a^2\gamma^2} + \frac{\pi^2}{48h^2} \right)$$

Therefore, for  $\gamma \gg 1$ , and for d.c. or slowly varying currents the cancellation effect applies only for the direct space charge forces. There is no cancellation of the electric and magnetic forces due to the "image" charges.

## Parallel Plates (Beam at Center) a.c. currents



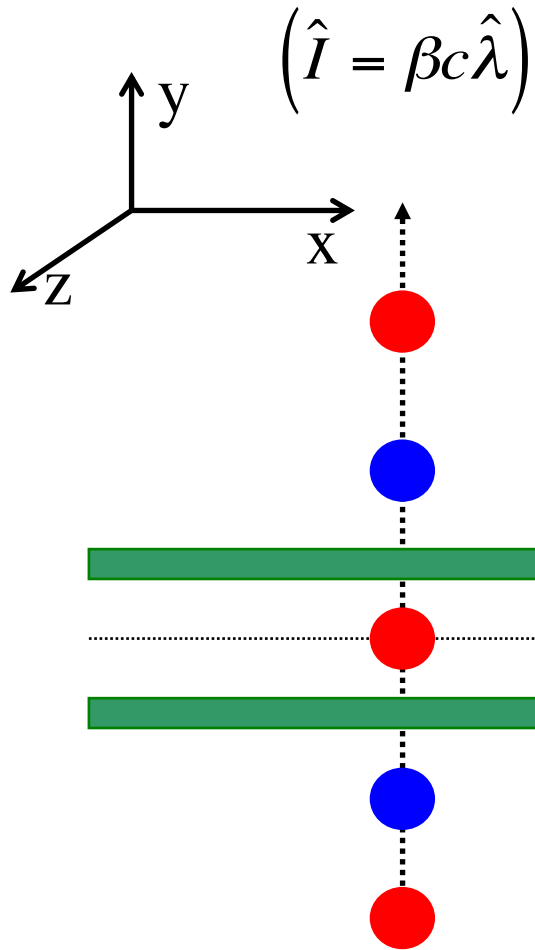
Usually, the frequency spectrum of a beam is quite rich of harmonics, especially for bunched beams.

To simplify our study it is convenient to decompose the current into a d.c. component,  $I$ , and an a.c. component,  $\hat{I}$ , for which we consider  $\delta_w \ll \Delta_w$ .

The d.c. component of the magnetic field is not affected by the presence of the material, and only the ‘image’ electric field must be considered.

The a.c. component of the magnetic field must be tangent to the pipe wall, and it can be obtained by using an infinite sum of image currents with alternating directions as we did for the electric field.

We can see that this magnetic field is able to cancel the effect of the electric force.



$$\hat{E}_y(z, y) = \frac{\hat{\lambda}(z)y}{\pi \epsilon_0} \frac{\pi^2}{48h^2}; \quad \hat{B}_x(z, y) = -\frac{\beta}{c} \hat{E}_y(z, y)$$

$$\hat{F}_y(z, y) = \frac{e\hat{\lambda}(z)y}{\pi \epsilon_0 \gamma^2} \frac{\pi^2}{48h^2}$$

$$\hat{F}_y(z, y) = \frac{e\hat{\lambda}(z)y}{\pi \epsilon_0 \gamma^2} \left( \frac{1}{2a^2} + \frac{\pi^2}{48h^2} \right)$$

$$\hat{F}_x(z, x) = \frac{e\hat{\lambda}(z)x}{\pi \epsilon_0 \gamma^2} \left( \frac{1}{2a^2} - \frac{\pi^2}{48h^2} \right)$$

For the a.c. current there is cancellation of the electric and magnetic forces.

## Parallel Plates - General expression of the force

Taking into account all the boundary conditions for d.c. and a.c. currents, considering also the presence of ferromagnetic materials in dipoles, we can write the expression of the force as:

$$F_u = \frac{e}{\pi \varepsilon_0} \left[ \frac{1}{\gamma^2} \left( \frac{1}{2a^2} \mp \frac{\pi^2}{48h^2} \right) \lambda \mp \beta^2 \left( \frac{\pi^2}{48h^2} + \frac{\pi^2}{24g^2} \right) \bar{\lambda} \right] u$$

$$u = x, y$$

where  $\lambda$  is the total current divided by  $\beta c$ ,  $\bar{\lambda}$  its d.c. part,  $g$  the gap in a dipole, and we take the sign (+) if  $u=y$ , and the sign (-) if  $u=x$ .

It is interesting to note that these forces are linear in the transverse displacement  $x$  and  $y$ .

## Space Charge Force - General expression

One often finds the space charge force written in terms of the Laslett form factors  $f_0, f_1$  and  $f_2$

$$F_u = \frac{e}{\pi\epsilon_0} \left[ \frac{1}{\gamma^2} \left( \frac{f_0}{a^2} \mp \frac{f_1}{h^2} \right) \lambda \mp \beta^2 \left( \frac{f_1}{h^2} + \frac{f_2}{g^2} \right) \bar{\lambda} \right] u$$

where the Laslett form factors have been obtained for different pipe geometries (as elliptical and rectangular, with more complicated reasoning).

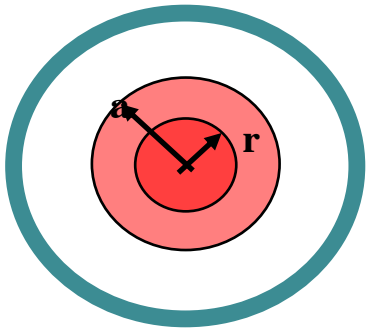
For example, for our case of parallel plates, we have:

$$f_0=1/2, f_1=\pi^2/48, f_2=\pi^2/24$$

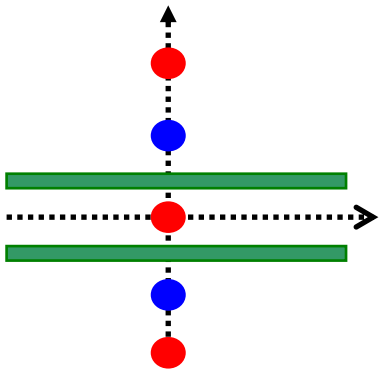
$$\lambda(z) = \lambda_0 + \hat{\lambda} \cos(k_z z) \quad ; \quad k_z = 2\pi / l_w$$

D.C.

A.C.  $(\delta_w \ll \Delta_w)$



$$F_{\perp}(r) = \frac{e}{\gamma^2} \frac{\lambda(z)}{2\pi \epsilon_0} \frac{r}{a^2}$$



$$F_x(z, x) = \frac{e\lambda_0 x}{2\pi \epsilon_0} \left( \frac{1}{a^2 \gamma^2} - \frac{\pi^2}{24h^2} \right)$$

$$F_y(z, y) = \frac{e\lambda_0 y}{2\pi \epsilon_0} \left( \frac{1}{a^2 \gamma^2} + \frac{\pi^2}{24h^2} \right)$$

$$\hat{F}_x(z, x) = \frac{e\hat{\lambda}(z)x}{2\pi \epsilon_0 \gamma^2} \left( \frac{1}{a^2} - \frac{\pi^2}{24h^2} \right)$$

$$\hat{F}_y(z, y) = \frac{e\hat{\lambda}(z)y}{2\pi \epsilon_0 \gamma^2} \left( \frac{1}{a^2} + \frac{\pi^2}{24h^2} \right)$$

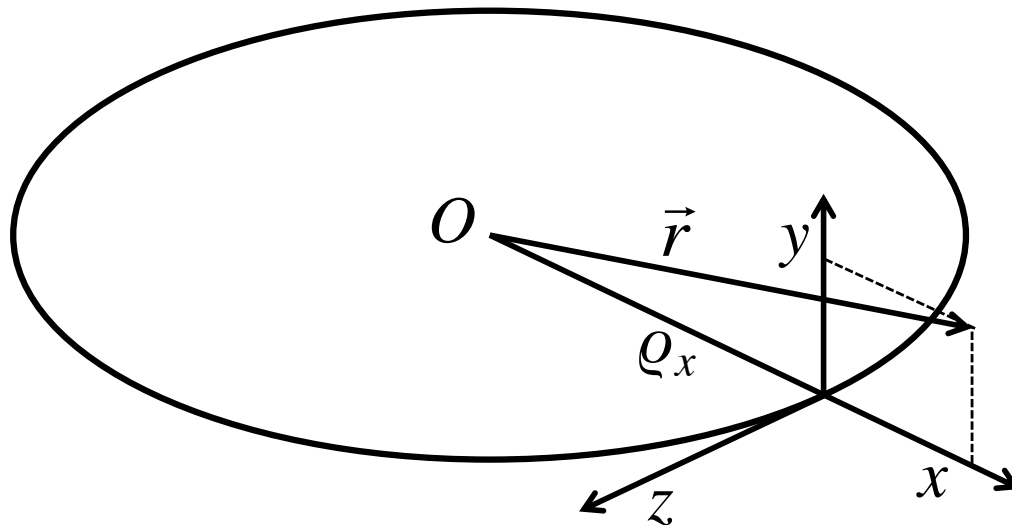
# **Space charge effects in circular accelerators**



## Self fields and betatron motion

Consider a perfectly circular accelerator with radius  $\rho_x$ . The beam circulates inside the beam pipe. The transverse single particle motion in the linear regime, is derived from the equation of motion. Including the self field forces in the motion equation, we have:

$$\frac{d(m\gamma \mathbf{v})}{dt} = \mathbf{F}^{ext}(\vec{r}) + \mathbf{F}^{self}(\vec{r}) \qquad \frac{d\mathbf{v}}{dt} = \frac{\mathbf{F}^{ext}(\vec{r}) + \mathbf{F}^{self}(\vec{r})}{m\gamma}$$



Following the same steps of the "transverse dynamics" lectures, we write:

$$\vec{r} = (\rho_x + x)\hat{e}_x + y\hat{e}_y$$

$$\vec{v} = \dot{x}\hat{e}_x + \dot{y}\hat{e}_y + \omega_0(\rho_x + x)\hat{e}_z$$

$$\vec{a} = \left[ \ddot{x} - \omega_0^2(\rho_x + x) \right] \hat{e}_x + \ddot{y}\hat{e}_y + \left[ \dot{\omega}_0(\rho_x + x) + 2\omega_0\dot{x} \right] \hat{e}_z$$

For the motion along x:

$$\ddot{x} - \omega_0^2(\rho_x + x) = \frac{1}{m\gamma} \left( F_x^{ext} + F_x^{self} \right)$$

which is rewritten with respect to the azimuthal position  $s = v_z t$ :

$$\ddot{x} = v_z^2 x'' = \omega_0^2 (\rho_x + x)^2 x''$$

$$x'' - \frac{1}{\rho_x + x} = \frac{1}{mv_z^2 \gamma} \left( F_x^{ext} + F_x^{self} \right)$$

We assume a small transverse displacement  $x$  so that:

$$x'' - \frac{1}{\rho_x} + \frac{1}{\rho_x^2} x = \frac{1}{m_0 v_z^2 \gamma} \left( F_x^{ext} + F_x^{self} \right)$$

The external force is due to the magnetic guiding fields. We suppose to have only dipoles and quadrupoles, or, equivalently, we expand the external guiding fields in a Taylor series up to the quadrupole component:

$$-F_x^{ext} = qv_z B_y = qv_z B_{y0} + qv_z \left( \frac{\partial B_y}{\partial x} \right)_0 x + \dots$$

the dipolar magnetic field  $B_{y0}$  is responsible of the circular motion along the reference trajectory of radius  $\rho_x$  according to the equation :

$$qv_z B_{y0} = \frac{m_0 \gamma v_z^2}{\rho_x}$$

We finally get:

$$x'' + \left[ \frac{1}{\rho_x^2} + \frac{q}{m_0 v_z \gamma} \left( \frac{\partial B_y}{\partial x} \right)_0 \right] x = \frac{1}{m_0 v_z^2 \gamma} F_x^{self}$$

which can also be written as:

$$x'' + \left[ \frac{1}{\rho_x^2} - k \right] x = \frac{1}{m_0 v_z^2 \gamma} F_x^{self}$$

where we have introduced the normalized gradient

$$k = \frac{g}{p/q} = - \frac{q}{m_0 v_z \gamma} \left( \frac{\partial B_y}{\partial x} \right)$$

with  $g$  the quadrupole gradient in [T/m] and  $p$  the charge momentum

Both the curvature radius and the normalized gradient depend on the azimuthal position 's'. By using the focusing constant  $K_x(s)$  we then can write:

$$x''(s) + K_x(s)x(s) = \frac{1}{m_0 v_z^2 \gamma} F_x^{self}(x, s)$$

In absence of self fields, the solution of the free equation, known as Hill's equation gives the betatron oscillations.

Putting  $v_z = \beta_z c \cong \beta c$  (small beam divergence), we get

$$x''(s) + K_x(s)x(s) = \frac{1}{\beta^2 E_0} F_x^{self}(x, s)$$

where  $E_0$  is the particle energy.

- In the analysis of the motion of the particles in presence of the self fields, we will adopt a simplified model where particles execute simple harmonic oscillations around the reference orbit.
- This is the case for which the focusing term is constant along the machine. Although this condition is never fulfilled in a real accelerator, it provides a reliable model for the description of the effects due to the self fields .

$$x''(s) + K_x x(s) = \frac{1}{\beta^2 E_0} F_x^{self}(x)$$

Free betatron motion:

$$x''(s) + K_x x(s) = 0 \quad \longrightarrow$$

Perturbed motion:

$$x''(s) + \left(\frac{Q_{x0}}{\rho_x}\right)^2 x(s) = \frac{1}{\beta^2 E_0} F_x^{self}(x, s)$$

$$\left\{ \begin{array}{l} x(s) = A_x \cos[\sqrt{K_x} s - \varphi_x] \\ \lambda_\beta = \frac{2\pi}{\sqrt{K_x}} \\ Q_{x0} = \frac{2\pi\rho_x}{\lambda_\beta} = \frac{2\pi\rho_x\sqrt{K_x}}{2\pi} = \rho_x\sqrt{K_x} \\ K_x = \left(\frac{Q_{x0}}{\rho_x}\right)^2 \end{array} \right.$$

# Transverse incoherent effects

We take the linear term of the self induced transverse force in the betatron equation:

$$F_x^{self}(x, s) = F_x^{s.c.}(x, s) \cong \left( \frac{\partial F_x^{s.c.}}{\partial x} \right)_{x=0} x \quad \Rightarrow \quad x'' + \left( \frac{Q_{x0}}{\rho_x} \right)^2 x = \frac{1}{\beta^2 E_0} \left( \frac{\partial F_x^{s.c.}}{\partial x} \right)_{x=0} x$$

$$x'' + \left[ \left( \frac{Q_{x0}}{\rho_x} \right)^2 - \frac{1}{\beta^2 E_0} \left( \frac{\partial F_x^{s.c.}}{\partial x} \right)_{x=0} \right] x = 0 \quad \Rightarrow \quad x'' + \left( \frac{Q_{x0} + \Delta Q_x}{\rho_x} \right)^2 x = 0$$

$$x'' + \left[ \frac{Q_{x0}^2 + 2Q_{x0}\Delta Q_x + \cancel{\Delta Q_x^2}}{\rho_x^2} \right] x = 0 \quad \Rightarrow \quad x'' + \left[ \frac{Q_{x0}^2}{\rho_x^2} + \frac{2Q_{x0}\Delta Q_x}{\rho_x^2} \right] x = 0$$

$$\Delta Q_x = - \frac{\rho_x^2}{2\beta^2 E_0 Q_{x0}} \left( \frac{\partial F_x^{s.c.}}{\partial x} \right)_{x=0}$$

## Transverse incoherent effects

$$\Delta Q_x = - \frac{\rho_x^2}{2\beta^2 E_0 Q_{x0}} \left( \frac{\partial F_x^{s.c.}}{\partial x} \right)$$

The shift of betatron wave number (tune shift) is negative since the space charge forces are defocusing on both planes (the betatron wavelength increases). Remember that the space charge force, and then the tune shift, is, in general, function of “z”,  $\lambda(z)$ , therefore this expression represents a tune spread inside the beam. This is why we call it incoherent. This conclusion is generally true also for more realistic non-uniform transverse beam distributions, which are characterized by a tune shift dependent also on the betatron oscillation amplitude. When  $\Delta Q_x$  is not constant in the beam, instead of tune shift the effect is called tune spread.



**Example 3: incoherent betatron tune shift for a uniform electron beam of radius  $a=100\mu\text{m}$ , length  $l_o=100\mu\text{m}$ , inside a circular perfectly conducting pipe (energy  $E_0=1\text{GeV}$ ,  $N=10^{10}$ ,  $Q_x=20\text{m}$ ,  $Q_{x0}=4.15$ )**

$$\left(\frac{\partial F_x^{s.c.}}{\partial x}\right) = \frac{\partial}{\partial x} \left(\frac{e\lambda_0 x}{2\pi\epsilon_0\gamma^2 a^2}\right) = \frac{e\lambda_0}{2\pi\epsilon_0\gamma^2 a^2}$$

$$\Delta Q_x = -\frac{\rho_x^2 N e^2}{4\pi\epsilon_0 a^2 \beta^2 \gamma^2 E_0 Q_{x0} l_o}$$

$$r_{e,p} = \frac{e^2}{4\pi\epsilon_0 m_o c^2} \quad (\text{electrons : } 2.82 \cdot 10^{-15} \text{ m, protons : } 1.53 \cdot 10^{-18} \text{ m})$$

$$\Delta Q_x = -\frac{\rho_x^2 N r_{e,p}}{a^2 \beta^2 \gamma^3 Q_{x0} l_o} \approx -0.36$$

Remember that for real bunched beams the space charge forces depend on the longitudinal and radial position of the charge => tune spread.

## ΔQ as function of beam emittance and filling factor of the ring

$$\Delta Q_x = -\frac{\rho_x^2 N r_{e,p}}{a^2 \beta^2 \gamma^3 Q_{x0} l_o}$$

$$a^2 = \varepsilon_x \beta_x$$

$$\beta_x = \frac{\lambda_\beta}{2\pi} = \frac{1}{\sqrt{K_x}}$$

$$K_x = \left( \frac{Q_{x0}}{\rho_x} \right)^2$$

$$Q_{x0} = \rho_x \sqrt{K_x} = \frac{\rho_x}{\beta_x}$$

$$\Delta Q_x = -\frac{\cancel{\rho_x^2} N r_{e,p}}{\varepsilon_x \cancel{\beta_x} \beta^2 \gamma^3 \frac{\cancel{\rho_x} l_o}{\cancel{\beta_x}}}$$

$$\Delta Q_x = -\frac{N r_{e,p}}{2\pi \varepsilon_x \beta^2 \gamma^3} \left( \frac{2\pi \rho_x}{l_o} \right)$$

This expression is valid also in the general case of non-uniform focusing along the accelerator for a uniform beam inside a circular pipe.

## General expression of the incoherent tune shift

We have seen that the equation of the betatron oscillations in presence of self forces is

$$x''(s) + K_x x(s) = \frac{1}{\beta^2 E_0} F_x^{self}(x) = \frac{1}{\beta^2 E_0} \left( \frac{\partial F_x^{self}}{\partial x} \right)_{x=0} x$$

which we can also write as

$$x''(s) + \left[ K_x - \frac{1}{\beta^2 E_0} \left( \frac{\partial F_x^{self}}{\partial x} \right)_{x=0} \right] x(s) = 0$$

From beam optics, it is possible to demonstrate that, having a circular machine with design quadrupole strength  $K_x(s)$  and gradient errors  $\Delta K_x(s)$  distributed along the machine, these errors lead to a tune shift of

$$\Delta Q_x = \frac{1}{4\pi} \oint \beta_x(s) \Delta K_x(s) ds = - \frac{1}{4\pi \beta^2 E_0} \oint \beta_x(s) \left( \frac{\partial F_x^{self}}{\partial x} \right)_{x=0} ds$$

## General expression of the incoherent tune shift

$$\Delta Q_x = \frac{1}{4\pi} \oint \beta_x(s) \Delta K_x(s) ds = - \frac{1}{4\pi\beta^2 E_0} \oint \beta_x(s) \left( \frac{\partial F_x^{self}}{\partial x} \right)_{x=0} ds$$

This is a general expression. The only assumption is the linearization of the self field forces. For a uniform transverse distribution,  $\beta_x(s) = a^2 / \varepsilon_x$

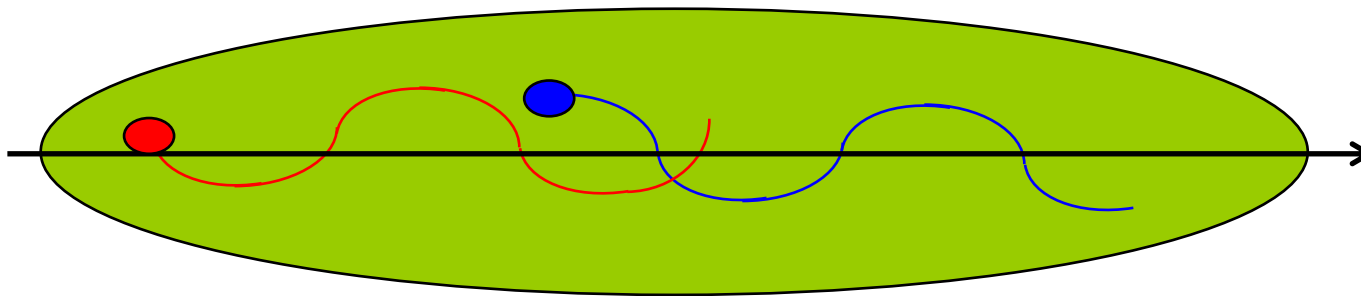
$$\Delta Q_x = - \frac{1}{4\pi\beta^2 \varepsilon_x E_0} \oint a^2 \left( \frac{\partial F_x^{self}}{\partial x} \right)_{x=0} ds$$

$$\Delta Q_x = - \frac{2\pi\rho_x}{4\pi\beta^2 \varepsilon_x E_0} \left\langle a^2 \left( \frac{\partial F_x^{self}}{\partial x} \right)_{x=0} \right\rangle$$

where  $\langle \rangle$  means averaged over the machine circumference. With this expression we can account for the variation of the beam dimensions along the machine due to the betatron function.

## Shift and spread of the incoherent tunes

If the beam is located at the centre of symmetry of the pipe, the e.m. forces due to space charge and images cannot affect the motion of the centre of mass (coherent), but change the trajectory of individual charges in the beam (incoherent).



These forces may have a complicate dependence on the charge position. Our simple analysis is done by considering only the linear expansion of the self-fields forces around the equilibrium trajectory.

The consequences are a shift and a spread of the incoherent tunes.

## Consequences of the space charge tune spreads

In circular accelerators the values of the betatron tunes should not be close to rational numbers in order to avoid the crossing of linear and non-linear resonances where the beam becomes unstable. The spread induced by the space charge force can make hard to satisfy this basic requirement. Typically, in order to avoid major resonances the stability requires

$$|\Delta Q_u| < 0.5^*$$

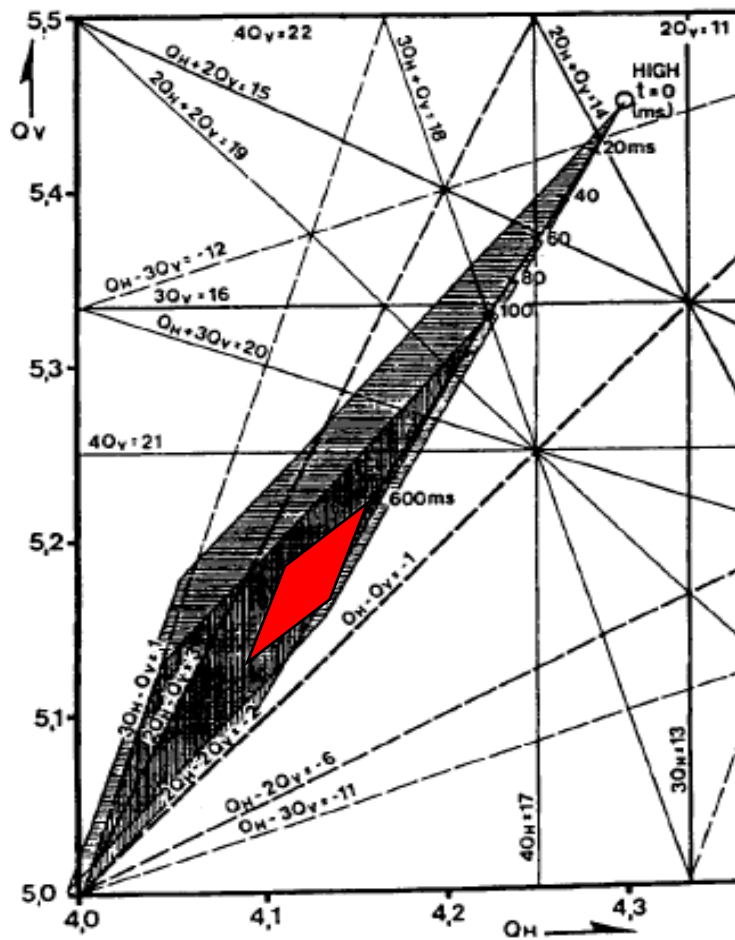
If the tune spread exceeds this limit, it is possible to reduce the effects of space charge tune spread, e.g. by increasing the injection energy or the transverse beam size.

The incoherent tune spread produces also a beneficial effect, called Landau damping, which can cure the coherent instabilities, provided that the coherent tune remains inside the incoherent spread.

\*See, for example, J. Rossbach, P. Schmüser, 'Basic course on accelerator optics', CAS Jyväskylä 1992, CERN 94-01, p. 76.

J. P. Delahaye, et al., Proc. 11<sup>th</sup> Int. Conf. on High Energy Accelerators, Geneva, 1980, p. 299.

## Example from A. Hofmann in CAS 1992 (General Course - Jyväskylä Finland)

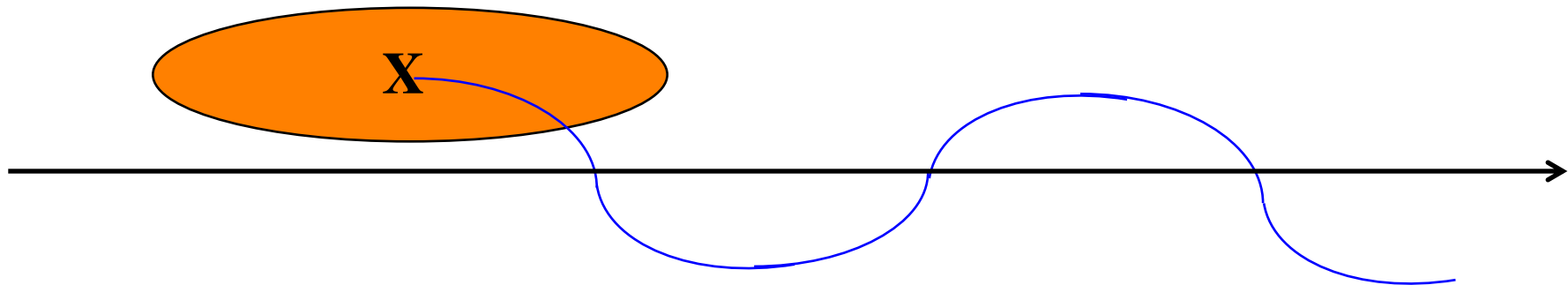


CERN PS Booster accelerated proton bunches from 50 to 800 MeV in about 0.6 s. The tunes occupied by the particles are indicated in the diagram by the shaded area. As time goes on, the energy increases and the space charge tune spread gets smaller covering at  $t=100$  ms the tune area shown by the darker area. The point of highest tune corresponds to the particles which are least affected by the space charge. This point moves in the  $Q$  diagram since the external focusing is adjusted such that the reduced tune spread lies in a region free of harmful resonances.

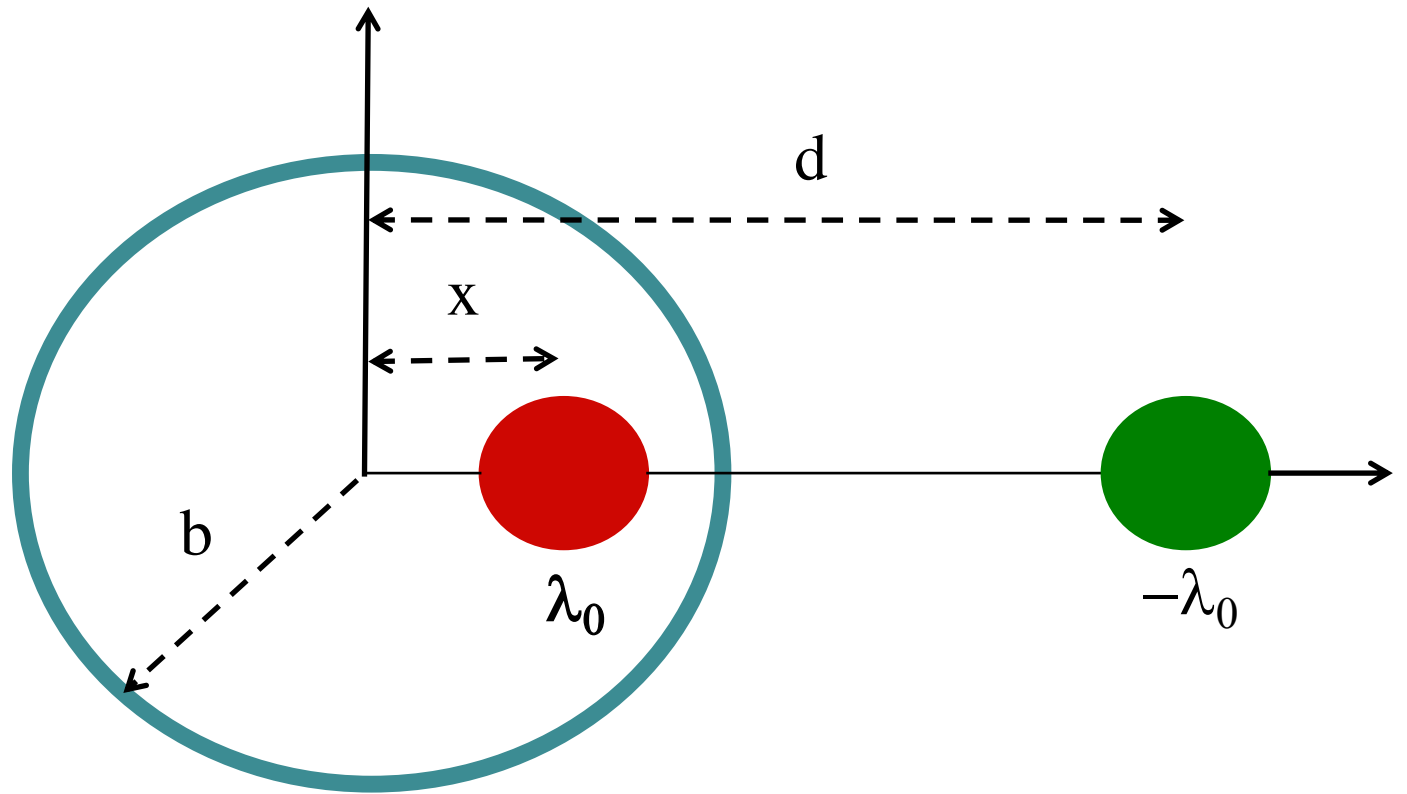
The small red area shows the situation at  $t=600$  ms when the beam has reached the energy of 800 MeV. The tune spread reduction is lower than expected with the energy increase ( $1/\gamma^3$ ) dependence since the bunch dimensions also decrease during the acceleration.

## Transverse coherent effects

If the beam experiences a transverse deflection kick, it starts to perform betatron oscillations as a whole. The beam, source of the space charge fields moves transversely inside the pipe, but its centre of mass ( $X$ ), due to symmetry, cannot be affected by the direct space charge. Only image space charge can affect its motion.



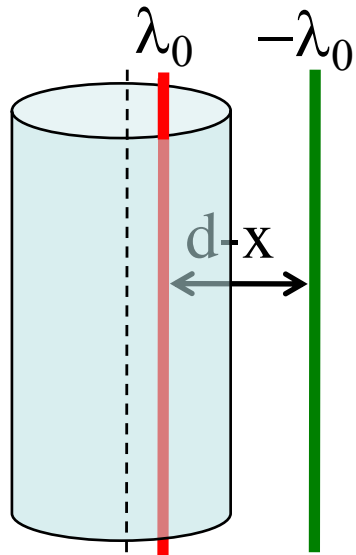




$$d = \frac{b^2}{x}$$

The image charge is at a distance “ $d$ ” such that the pipe surface is at constant voltage, and pulls the beam away from the center of the pipe.

The effect is defocusing: the horizontal electric image field  $E$  and the horizontal force  $F$  are:



$$E_{xc}(\mathbf{x}) = \frac{\lambda_0}{2\pi\epsilon_0} \frac{1}{d-x} \approx \frac{\lambda_0}{2\pi\epsilon_0} \frac{1}{d} = \frac{\lambda_0}{2\pi\epsilon_0} \frac{x}{b^2}$$

$$F_{xc}(x) \approx \frac{e\lambda_0}{2\pi\epsilon_0} \frac{x}{b^2}$$

$$\Delta Q_{xc} = -\frac{\rho_x^2}{2\beta^2 E_o Q_{x0}} \left( \frac{\partial F_{xc}}{\partial x} \right) = -\frac{\rho_x^2}{2\beta^2 E_o Q_{x0}} \frac{e\lambda_0}{2\pi \epsilon_o b^2}$$

$$r_{e,p} = \frac{e^2}{4\pi\epsilon_0 m_0 c^2}$$

$$\Delta Q_{xc} = -\frac{r_e \rho_x^2}{\beta^2 \gamma Q_{x0}} \frac{N}{b^2 l_0}$$

**Example 4: coherent betatron tune shift for a uniform electron beam of length  $l_0=100\mu\text{m}$ , inside a circular perfectly conducting pipe of radius  $b=14\text{cm}$ , (energy  $E_0=1\text{GeV}$ ,  $N=10^{10}$ ,  $Q_x=20\text{m}$ ,  $Q_{x0}=4.15$ )**

$$r_e = \frac{e^2}{4\pi\epsilon_0 m_0 c^2} = 2.82 \times 10^{-15} \text{m}$$

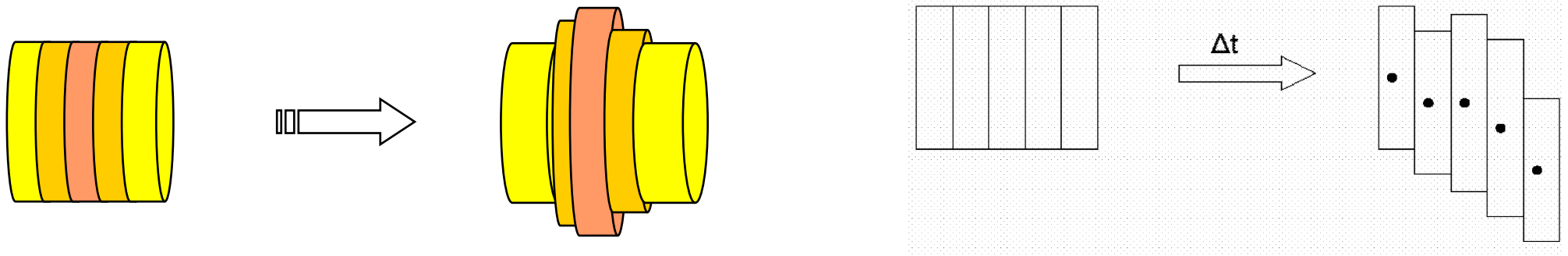
$$\Delta Q_{xc} = -\frac{r_e \rho_x^2}{\beta^2 \gamma Q_{x0}} \frac{N}{b^2 l_0} \approx -0.7$$

# Consequences of the space charge forces on LINACS

In a LINAC or a beam transport line, the space charge forces cause energy spread and perturb the equilibrium beam size.

They can also lead to a significant longitudinal-transverse correlation of the bunch parameters, which may produce mismatch with the focusing and accelerating devices, thus contributing to emittance growth.

The dynamics can be studied by considering the beam as an ensemble of longitudinal slices, for each of which it is possible to write a differential equation giving the behaviour of the transverse dimension along the machine (**envelope equation**).



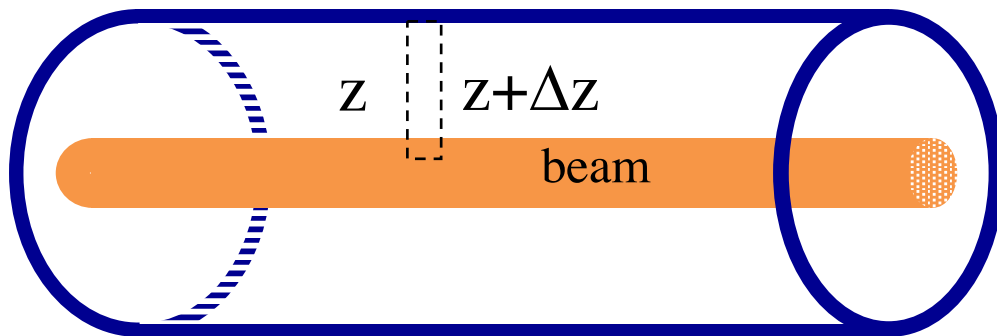
For the stability it is required anyway that the defocusing space charge forces must not be larger than the external focusing forces.

## LONGITUDINAL FORCES

Longitudinal forces can be obtained from the knowledge of the transverse ones.

In order to derive the relationship between the longitudinal and transverse forces inside a beam, let us consider the case of cylindrical symmetry and ultra-relativistic bunches. We know from Faraday's law of induction that a varying magnetic field produces a rotational electric field:

$$\oint \mathbf{E} \cdot d\mathbf{l} = -\frac{\partial}{\partial t} \int_S \mathbf{B} \cdot \mathbf{n} dS$$



We choose as path a rectangle going through the beam pipe and the beam, parallel to the axis.

$$\begin{aligned}
 E_z(r, z)\Delta z + \int_r^b E_r(r', z + \Delta z)dr' - E_z(b, z)\Delta z - \int_r^b E_r(r', z)dr' &= \\
 = -\Delta z \frac{\partial}{\partial t} \int_r^b B_\theta(r', z)dr' & \quad \begin{array}{l} \nearrow \\ \searrow \end{array} \quad \begin{array}{l} E_r(r', z + \Delta z) - E_r(r', z) = \frac{\partial E_r(r', z)}{\partial z} \Delta z \end{array}
 \end{aligned}$$

$$E_z(r, z) = E_z(b, z) - \int_r^b \left[ \frac{\partial E_r(r', z)}{\partial z} + \frac{\partial B_\theta(r', z)}{\partial t} \right] dr' \quad \begin{array}{l} \nearrow \\ \searrow \end{array} \quad \boxed{dz = -vdt}$$

$$E_z(r, z) = E_z(b, z) - \frac{\partial}{\partial z} \int_r^b [E_r(r', z) - vB_\theta(r', z)] dr' \quad \begin{array}{l} \nearrow \\ \searrow \end{array}$$

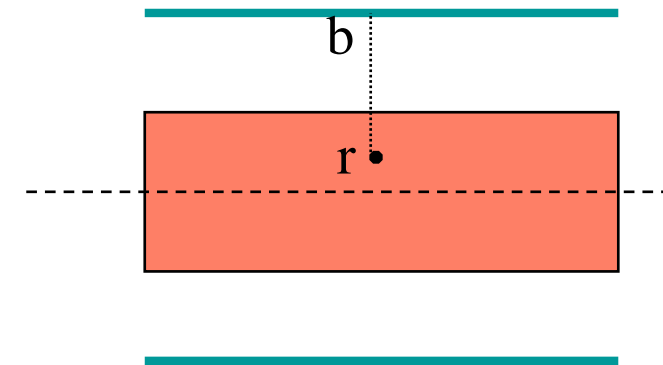
$$E_z(r, z) = E_z(b, z) - \frac{\partial}{\partial z} \int_r^b [E_r(r', z) - \beta^2 E_r(r', z)] dr'$$

$$E_z(r, z) = E_z(b, z) - (1 - \beta^2) \frac{\partial}{\partial z} \int_r^b E_r(r', z) dr'$$

where  $(1 - \beta^2) = 1/\gamma^2$ . For perfectly conducting walls  $E_z = 0$ .

$$E_z(r, z) = -\frac{1}{\gamma^2} \frac{\partial}{\partial z} \int_r^b E_r(r', z) dr'$$

Transverse uniform beam in a circular p.c. pipe.



$$F_z(r, z) = -\frac{e}{4\pi\epsilon_0\gamma^2} \left(1 - \frac{r^2}{a^2} + 2 \ln \frac{b}{a}\right) \frac{\partial \lambda(z)}{\partial z}$$

## Longitudinal self fields and synchrotron motion

Longitudinal equations of motion for constant energy and circular machine, ignoring radiation damping

$$\frac{d\phi}{dt} = -\frac{2\pi h\eta}{\beta^2 T_0} \frac{\Delta E}{E_0} \quad \frac{d(\Delta E)}{dt} = \frac{qV_{rf}}{T_0} (\sin\phi - \sin\phi_s) \quad \eta = \frac{1}{\gamma^2} - \alpha_c$$

$\phi$  is the RF phase,  $h$  the harmonic number,  $\eta$  the slippage factor,  $\Delta E$  the energy difference with respect to the synchronous particle

$$\Delta\phi'' + \left(\frac{Q_s}{\rho_x}\right)^2 \Delta\phi = 0; \quad Q_s = \frac{\omega_s}{\omega_0} = \sqrt{\frac{e\eta h V_{RF} \cos\phi_s}{2\pi\beta^2 E_0}}$$

$\Delta\phi$  is the phase difference with respect to the synchronous particle. Including longitudinal space charge forces the equation becomes:

$$\Delta\phi'' + \left(\frac{Q_s}{\rho_x}\right)^2 \Delta\phi = \frac{h\eta F_z^{self}}{\rho_x \beta^2 E_0}$$



# Numerical Analysis - 1

There are numerical codes used to evaluate the space charge effects in circular accelerators and Linacs:

## ORBIT: Objective Ring Beam Injection and Tracking Code

[https://oraweb.cern.ch/pls/hhh/code\\_website.disp\\_code?code\\_name=ORBIT](https://oraweb.cern.ch/pls/hhh/code_website.disp_code?code_name=ORBIT)

ORBIT is a computer code designed for beam dynamics calculations in high-intensity rings. Its intended use is the detailed simulation of realistic accelerator problems, although it is equally applicable to idealized situations. ORBIT is a particle-in-cell tracking code in 6D phase space that transports bunches of interacting particles through a series of nodes representing elements, dynamic effects, or diagnostics that occur in the accelerator lattice. It can be used in combination with PTC, a 6D integrator as tracker.

## GPT: General Particle Tracer

<http://www.pulsar.nl/gpt/>

GPT is based on full 3D particle tracking techniques, providing a basis for the study of all 3D and non-linear effects of charged particles dynamics in electromagnetic fields. All built-in beam line components and external 2D/3D field-maps can be arbitrarily positioned and oriented to simulate a complicated setup-up and study the effects of misalignments. An embedded fifth order Runge-Kutta driver with adaptive stepsize control ensures accuracy while computation time is kept to a minimum. GPT provides various 2D and 3D space-charge models.

## Numerical Analysis - 2

### PARMELA: Phase and Radial Motion in Electron Linear Accelerators

[http://laacg.lanl.gov/laacg/services/serv\\_codes.phtml#parmela](http://laacg.lanl.gov/laacg/services/serv_codes.phtml#parmela)

PARMELA is a multi-particle beam dynamics code used primarily for electron-linac beam simulations. It is a versatile code that transports the beam, represented by a collection of particles, through a user-specified linac and/or transport system. It includes several space-charge calculation methods. Particle trajectories are determined by numerical integration through the fields. This approach is particularly important for electrons where some of the approximations used by other codes (e.g. the "drift-kick" method commonly used for low-energy protons) would not hold.

### PARMILA: Phase And Radial Motion in Ion Linear Accelerators

<http://www.lanl.gov/projects/feynman-center/technologies/software/parmila.php>

Parmila has been the standard code for the design of RF linacs for many years. The enhanced, second generation, PARMILA 2 program is utilized in the PBO Lab PARMILA-2 Module. The Module is ideally suited for the design of complex ion accelerator components such as drift tube linacs (DTLs), coupled cavity linacs (CCLs), coupled-cavity drift tube linacs (CC-DTLs) and superconducting linacs (SCLs). The program offers two different multi-particle space charge algorithms which permits comparing different high beam current modeling approximations. The PARMILA-2 Module is also useful for the simulation of intense beams in transport channels and for studying beam loss, misalignments, cavity mispowering, and similar off-nominal operation.