



**Methodical Accelerator Design - Next Generation**  
**Tilt or not Tilt? *Notes about frames, patches and angles.***  
**ABP-HSS meeting**

**Laurent Deniau**  
**CERN-BE/ABP**

**16<sup>th</sup> January 2019**

# PLAN

1. **Overview: Survey, Track, Cofind, Twiss, Match, Plot**  
Unification and (re)use of the command interfaces.
2. **Survey command and Plot command.**  
Geometrical tracking.
3. **Track command and Beam command.**  
Dynamical tracking.
4. **Twiss command and Cofind command.**  
Tracking DA maps, computing optical functions.
5. **Match command.**  
Optimising lattices, functions optima.

Clarifications needed here!

## Annexes

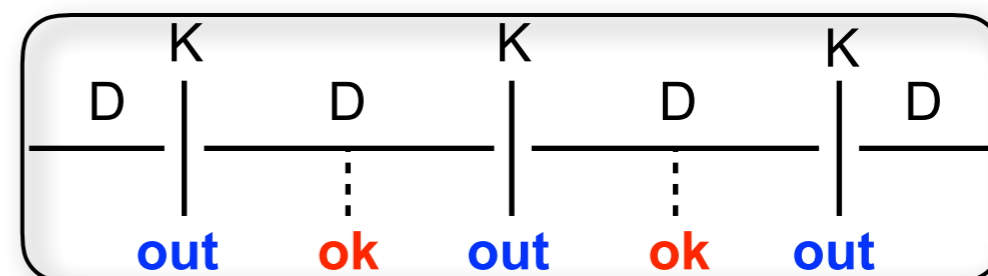
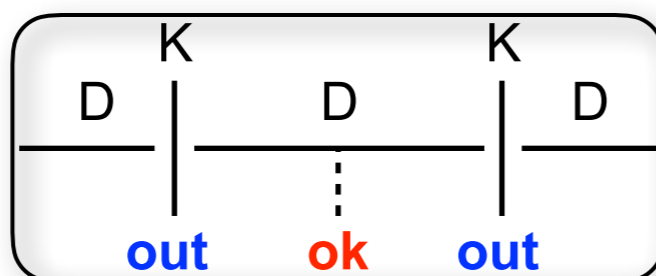
- I. Object model, Commands, Environments.
- II. MTable, Sequence, Elements.
- III. Symplectic integrators.
- IV. DA maps, GTPSA.
- V. Linear Algebra.

- Recommendations for unified use of MAD-X (main) commands:
  - ➔ Use SEQUENCE with refer=centre for MAKETHIN compatibility.
  - ➔ Use TWISS with centre=false for SURVEY compatibility.
  - ➔ Use MAKETHIN with slice>=2 in SBEND for SURVEY and TWISS compatibility at exit.
  - ➔ Use “**thin lens**” physics at centre (even slices) or exit of thick elements (**ok tags below**).
    - ▶ Install markers on **ok tags** or exit to save values at valid s-positions.

slice=even

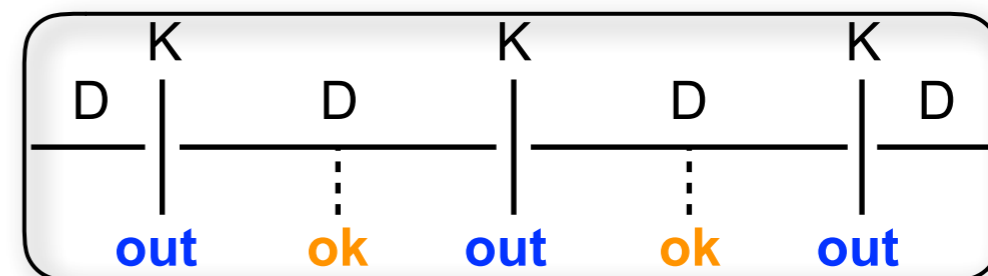
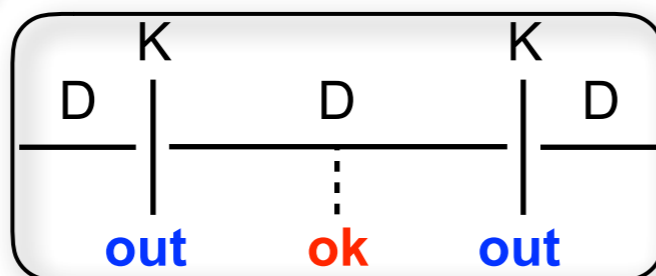
slice=odd

style=simple



**MAD-NG slices are at ok positions**

style=teapot



**Track:** shouldn't be problem as “observe” points are usually at well defined s-positions.  
**Twiss:** save optical functions at MULTIPOLE **out** s-positions, consider results with care.  
**Space Charge:** should take care about “SC kicks” s-positions.

```
n=4 ; e1=1.5 ; c1=e1/2 ; ang=pi/2 ; tlt=pi/6 ;

seq: sequence, l=(2*n+1)*e1 ;
!s1: srotation, at=0, angle=-tlt; ! <x,z> only
m1: sbend, at=c1+1*e1, l=e1, angle=-ang, tilt=+tlt ;
m2: sbend, at=c1+3*e1, l=e1, angle=+ang, tilt=+tlt ;
m3: sbend, at=c1+5*e1, l=e1, angle=+ang, tilt=+tlt ;
m4: sbend, at=c1+7*e1, l=e1, angle=-ang, tilt=+tlt ;
endsequence ;

beam ;
use sequence=seq ;
survey, file="srv_chicane_30.tfs" ;
plot, table=survey, haxis=z, vaxis={x,y} ;
```

```
! sbend-like patches for survey z->x,y
d1=e1*sinc(ang/2) ; ! cord length

pbend: sequence, l=d1 ;
ms1: srotation, at= 0, angle=+tlt;
my1: yrotation, at= 0, angle=+ang/2;
my2: yrotation, at=d1, angle=+ang/2;
ms2: srotation, at=d1, angle=-tlt;
endsequence ;
```

→  
patches  
version

convert to thin lens



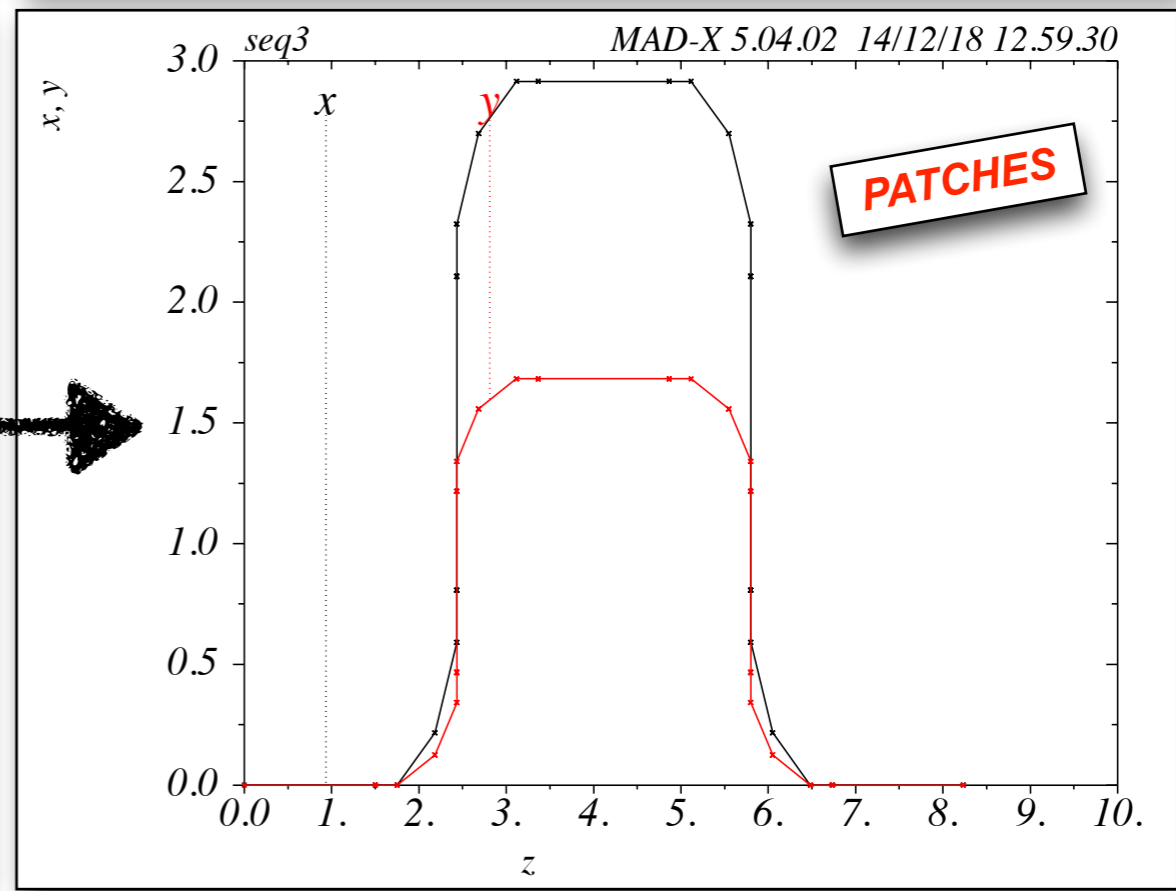
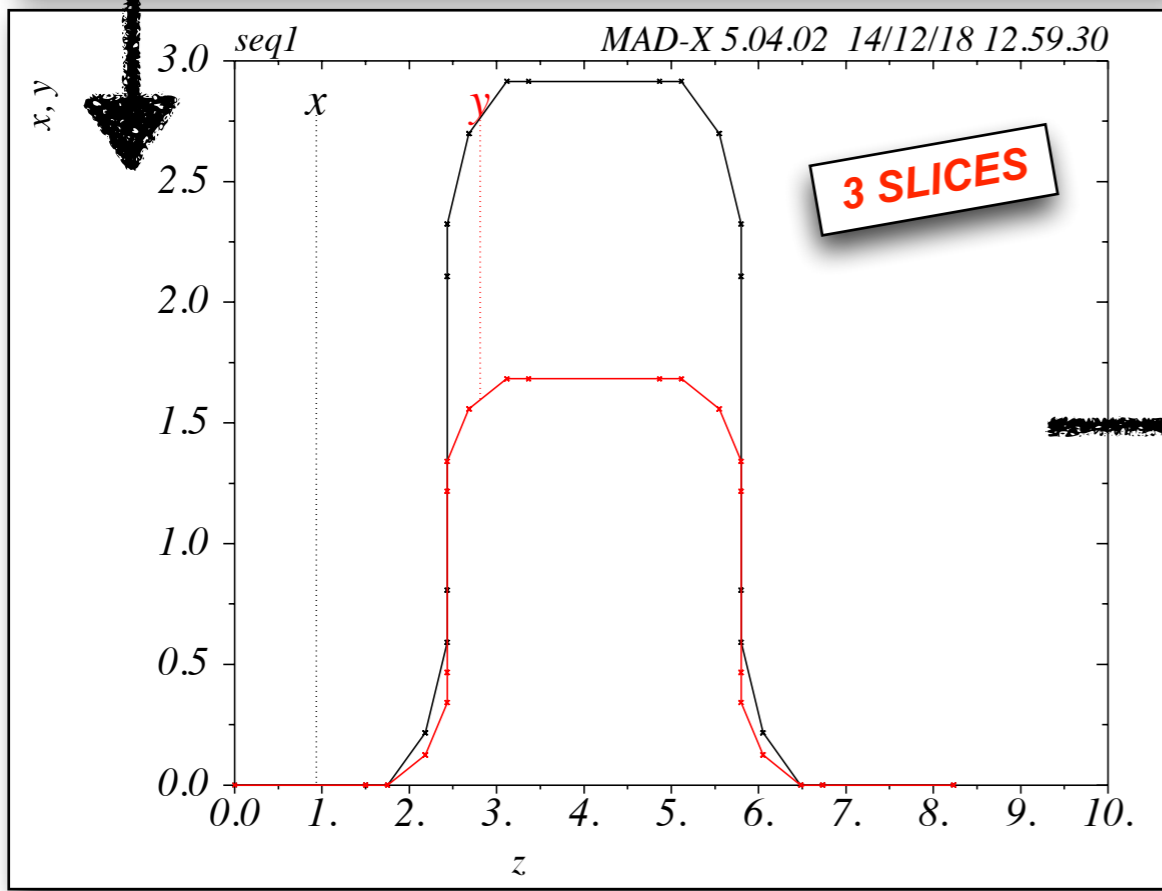
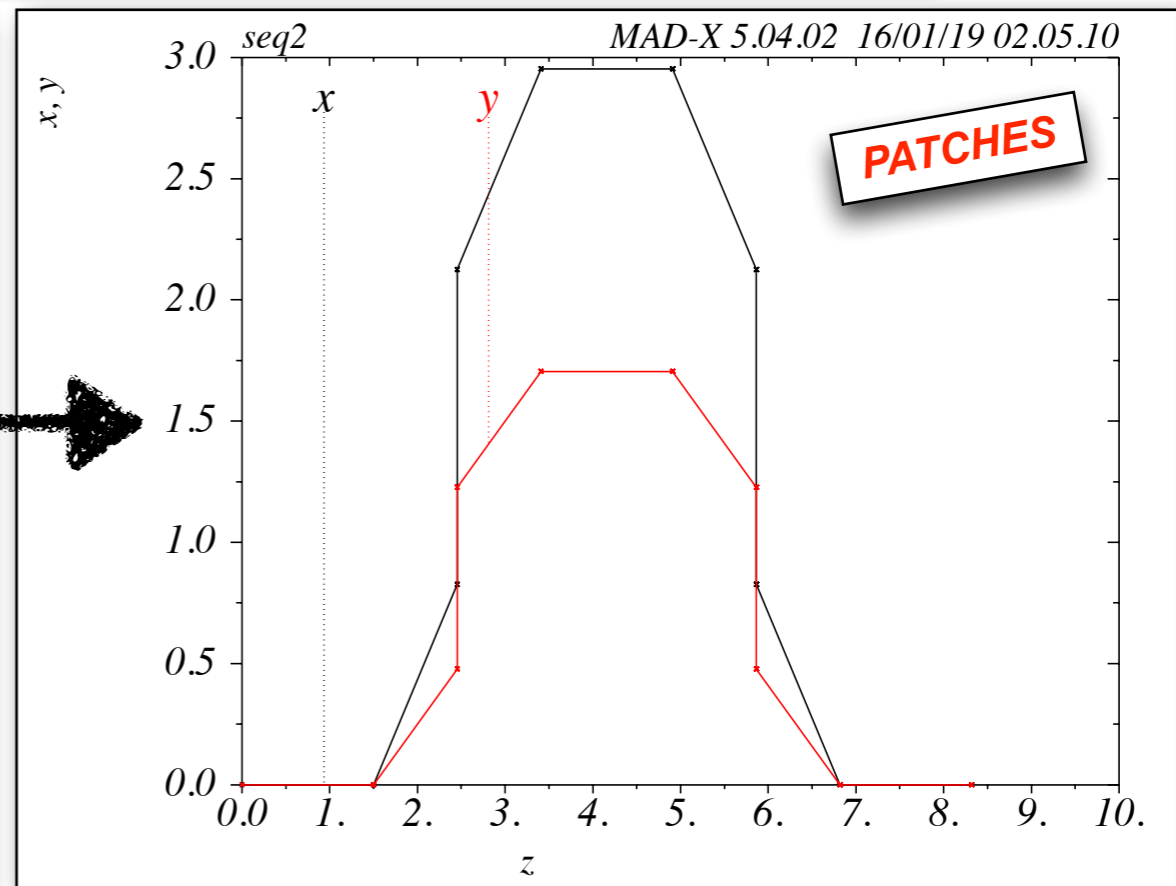
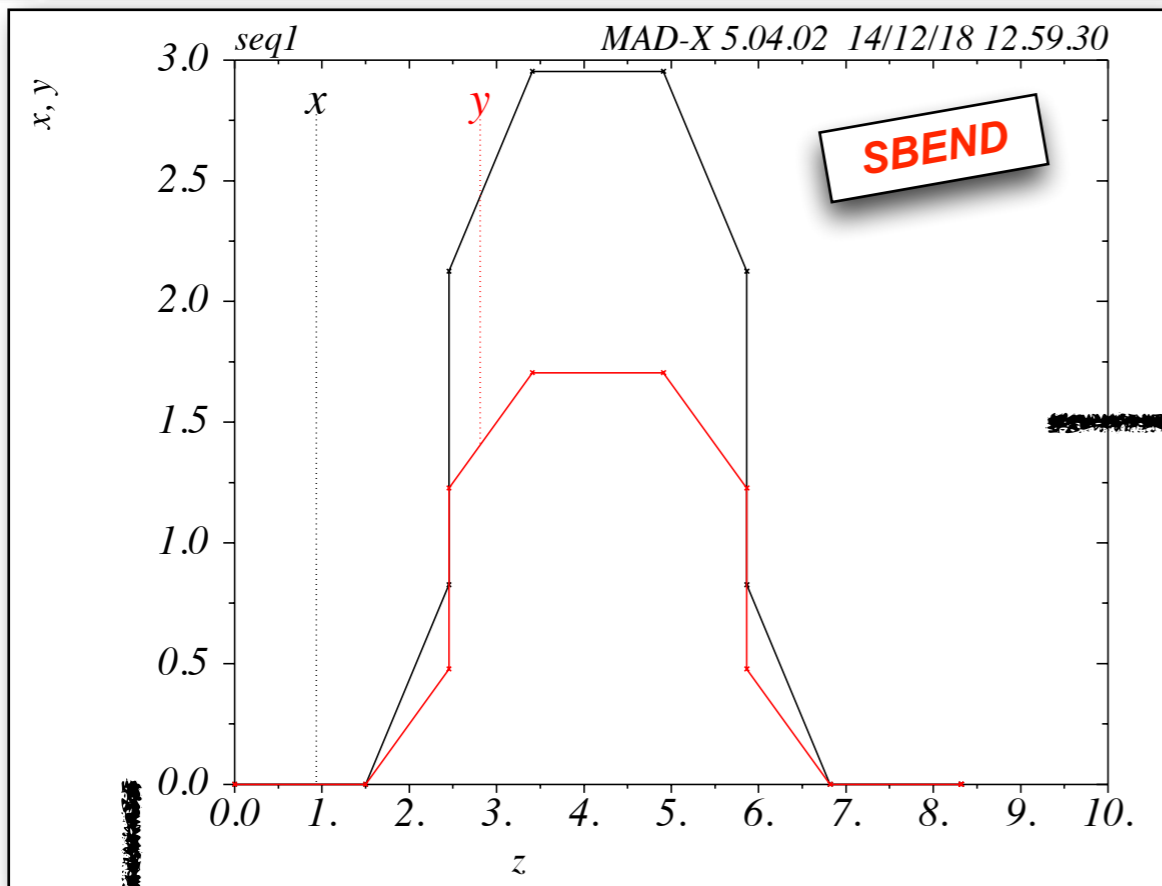
**In SURVEY, elements change the reference frame, i.e. act as patches:  
SBEND->angle/2 = YROTATION->angle**

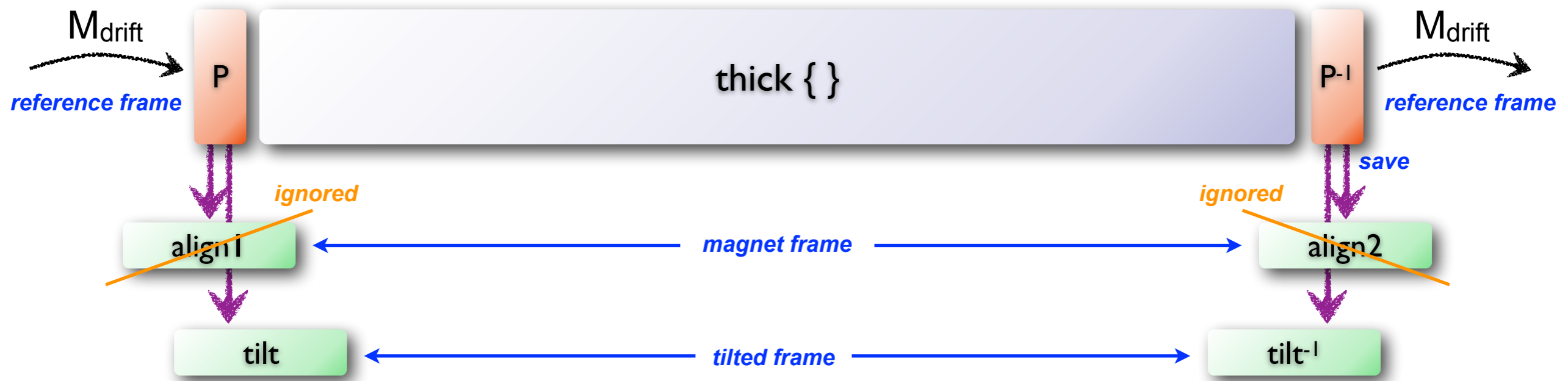
pbend replaces sbend in seq

```
! thin-sbend for survey z->x,y
select, flag=makethin, slice=3 ;
makethin, sequence=seq, style=simple ;
```

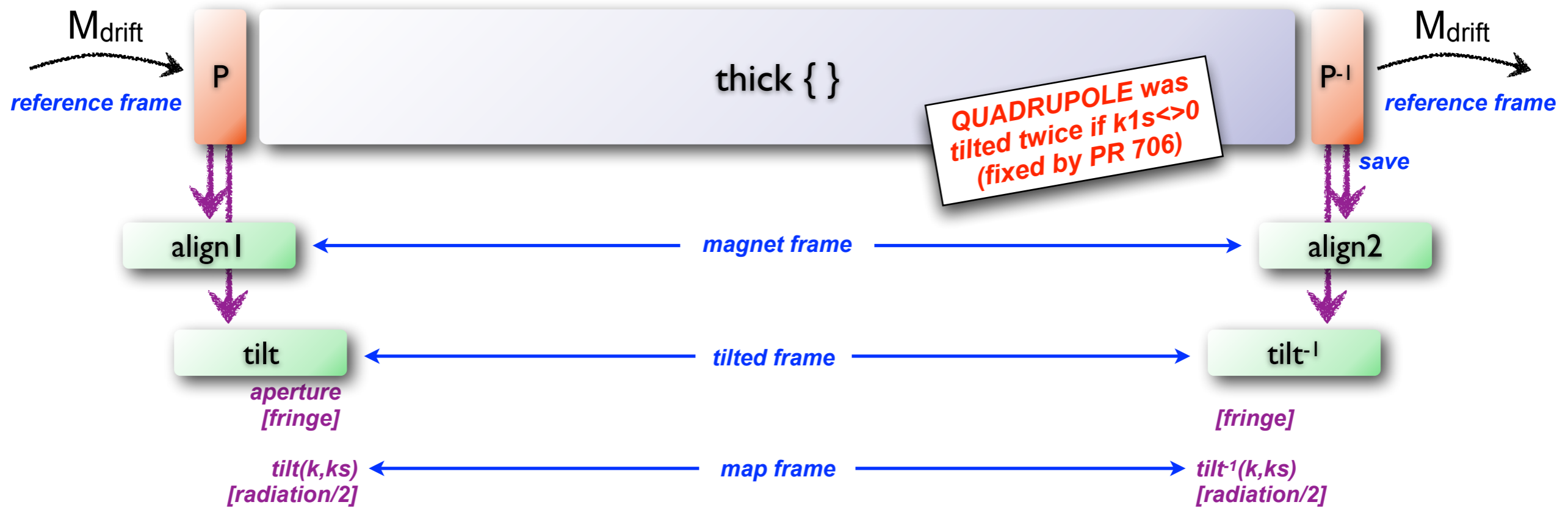
```
! thin-like patches for survey z->x,y
pbend: sequence, l=e1 ;
mt1: srotation, at=0, angle=+tlt ;
my1: yrotation, at=e1/6, angle=+ang/3;
my2: yrotation, at=e1/2, angle=+ang/3;
my3: yrotation, at=5*e1/6, angle=+ang/3;
mt2: srotation, at=e1, angle=-tlt ;
endsequence ;
```

→  
patches  
version





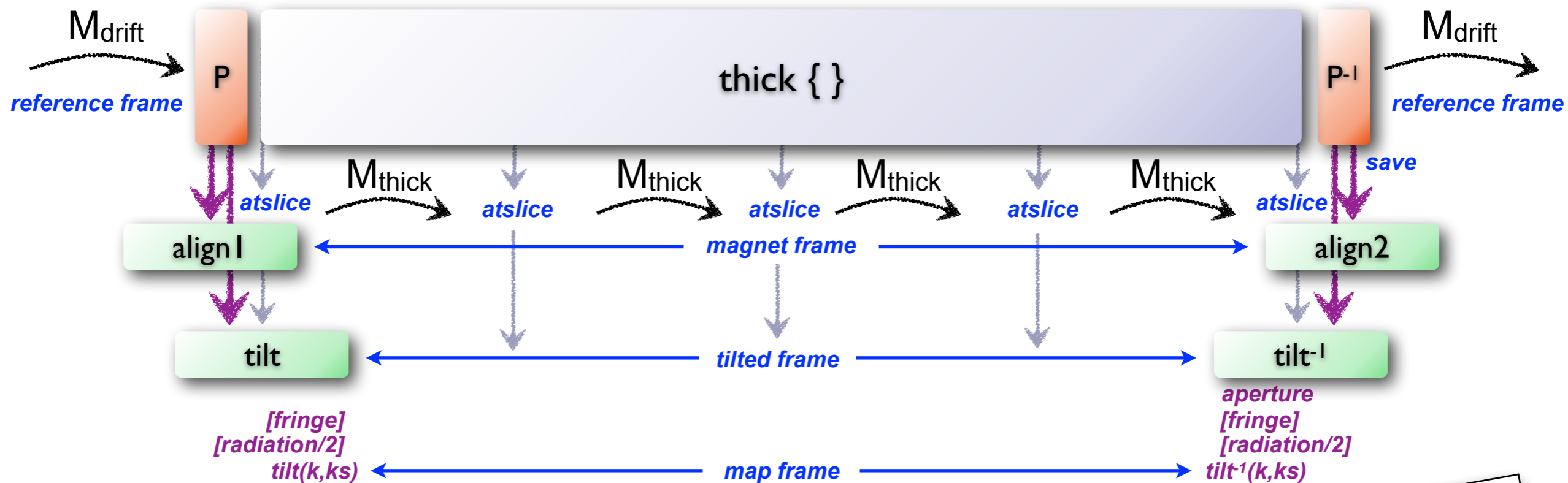
- ~~psi: s-rotation from reference frame to magnet frame.~~
- **tilt: s-rotation from magnet frame to tilted frame.**
- **angle: y-rotation in the tilted frame.**



- **psi**: *s*-rotation from reference frame to magnet frame.
- **tilt**: *s*-rotation from magnet frame to tilted frame.
- **angle**: *y*-rotation in the tilted frame (e.g. SBEND).
- **aperture tilt**: *s*-rotation in the tilted frame (e.g. aperture frame).
- $k_i + dk_{ni}/l$ ,  $ks_i + dk_{si}/l$ : magnet main *i*-strengths in the tilted frame,  $i > 0$ .
- $k$ : magnet main *i*-strength in the (untilted) map frame.

Radiation occurs in map frame.

Multipoles and field errors are ignored, except by MULTIPOLE.



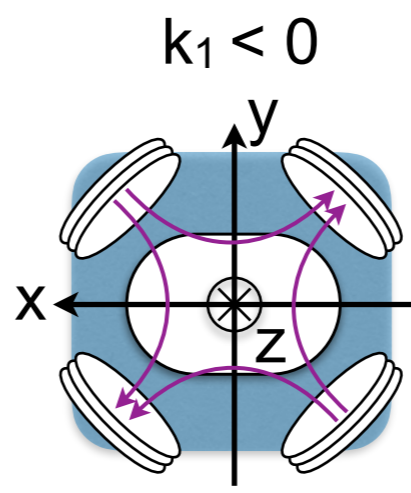
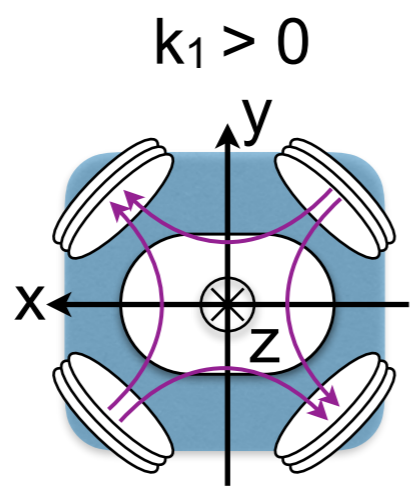
- ⦿ **psi:** *s-rotation* from **reference frame** to **magnet frame**.
- ⦿ **tilt:** *s-rotation* from **magnet frame** to **tilted frame**.
- ⦿ **angle:** *y-rotation* in the **tilted frame** (e.g. SBEND).
- ⦿ **aperture tilt:** *s-rotation* in the **tilted frame** (e.g. aperture frame).
- ⦿  $k_i + (k_{nl_i} + dk_{nl_i})/l$ ,  $ks_i + (ks_l + dks_l)/l$ : magnet main *i*-strengths in the **tilted frame**,  $i > 0$ .
- ⦿  $k$ : magnet main *i*-strength in the (untilted) **map frame**.
- ⦿  $k_{nl_j} + dk_{nl_j}$ ,  $ks_l + dks_l$ : magnet integrated multipole strengths ( $j \neq i$ ) in the **tilted frame**.

**“atslice” actions and thin subelements act in tilted frame.**

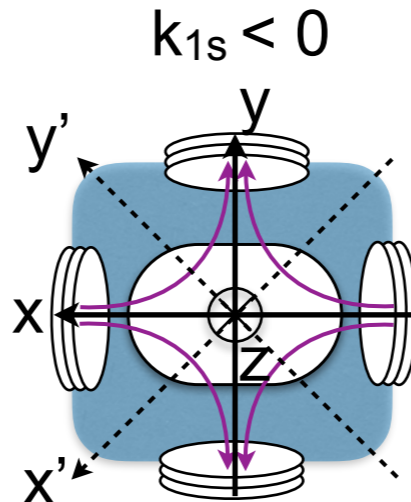
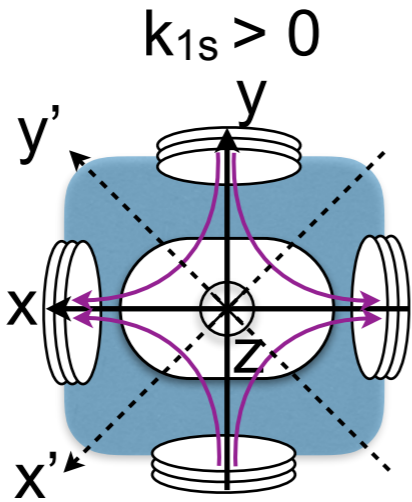
**Multipoles and field errors are considered.**



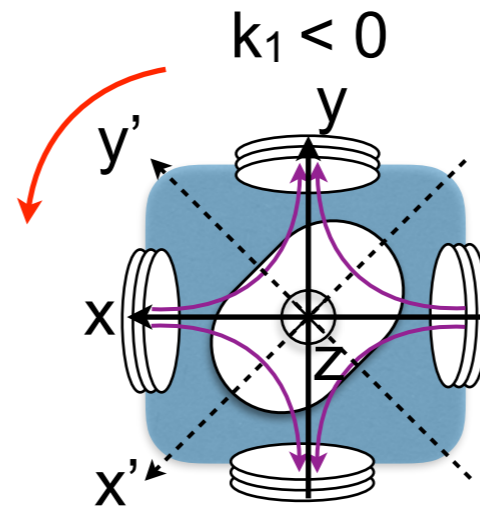
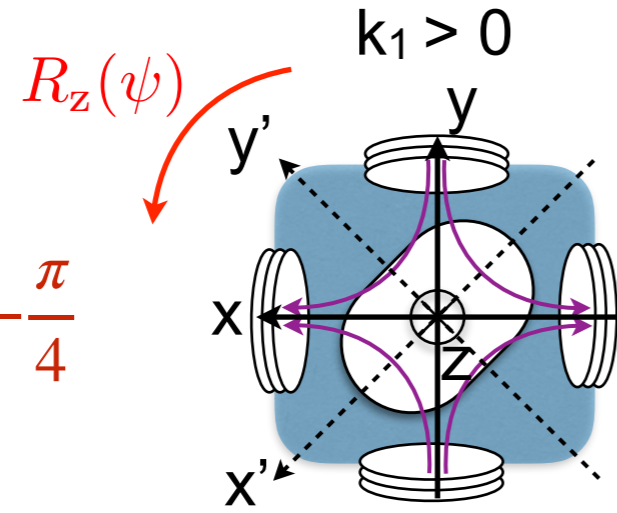
Quad:



Skew Quad:



Quad tilt =  $-\frac{\pi}{4}$



$$k_1 = \frac{\partial B_y}{\partial x} B_\rho^{-1}$$

$$k_{1s} = \frac{1}{2} \left( \frac{\partial B_x}{\partial x} - \frac{\partial B_y}{\partial y} \right) B_\rho^{-1}$$

x,y: magnet frame  
x',y': map frame

**Aperture checks are in tilted frame.**

- Tilt the map by angle  $\alpha$  to cancel the tilt  $\psi$  and the  $i$ -skew component  $ks_i$ ,  $i > 0$ .

$$k_m = k_i + (knl_i + dknl_i)/l$$

$$ks_m = ks_i + (ksl_i + dksl_i)/l$$

$$k = \sqrt{k_m^2 + ks_m^2}$$

$$\alpha = \psi - \frac{1}{m} \arctan \frac{ks_m}{k_m}$$

**MAD-X ignores  $knl_i$  and  $ksl_i$ .**

- Use the tilted (untitled) map (i.e. only T in TKT model in MAD-NG)

$$\mathbf{x}_2 = R_z(\alpha) \cdot \mathcal{M}_\perp(k) \cdot R_z(-\alpha) \mathbf{x}_1$$

- MAD-X remarks for Track and Twiss:

- ➔ Tilted frame and map frame are intermixed, physics must be correct in both.
- ➔ Thick maps discard integrated strength  $knl$ ,  $ksl$ ,  $dknl_j$  and  $dksl_j$  for  $j \neq i$  (required!).
- ➔ SBEND and RBEND consider *angle*,  $k_0 + dknl_0/l$ ,  $k_1 + dknl_1/l$  [,  $k_2 + dknl_2/l$ ](twiss only).
- ➔ MULTIPOLE expects  $knl$ ,  $ksl$ ,  $dknl$  and  $dksl$  in the tilted frame.

- MAD-NG remarks:

- ➔ Tilted frame and (thick untilted) map frame are NOT intermixed, tilted frame is used for everything but T in TKT model, i.e. multipole kicks K are in the **tilted frame**.

- EALIGN angles  $d\theta$ ,  $-d\phi$  and  $d\psi$  are right handed.

→  $d\theta$  = azimuthal angle ( $d\theta \rightsquigarrow -\theta$  of SBEND)

→  $d\phi$  = elevation angle ( $d\phi > 0 \rightsquigarrow dy > 0$ )

→  $d\psi$  = roll angle

Compatible with reversed sequence (e.g. LHCB2).

Angles can be "large" in MAD-NG and computed to full order (as in PTC).

- At **entry**, an element is rotated by  $R(d\theta, d\phi, d\psi)$  and translated by  $T(dx, dy, ds)$ .

$$\mathbf{x}'_1 = R \mathbf{x}_1 + T \quad (\text{transform the frame})$$

$$\mathbf{x}_1 = R^t (\mathbf{x}'_1 - T) \quad (\text{transform the coordinates})$$

$$R = R_y(d\theta) \cdot R_x(-d\phi) \cdot R_z(d\psi)$$

$$R^t = R_z(-d\psi) \cdot R_x(d\phi) \cdot R_y(-d\theta) \quad (\text{inverse})$$

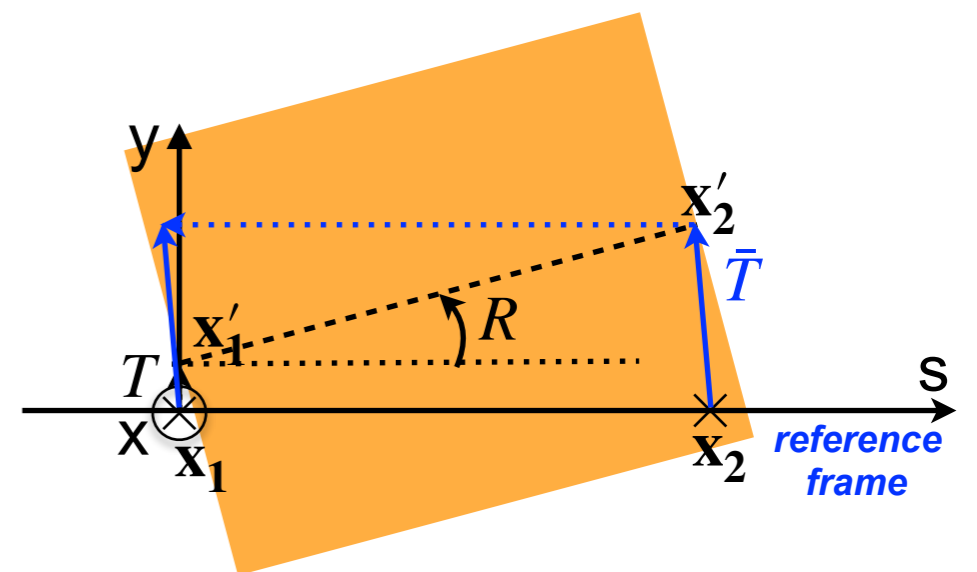
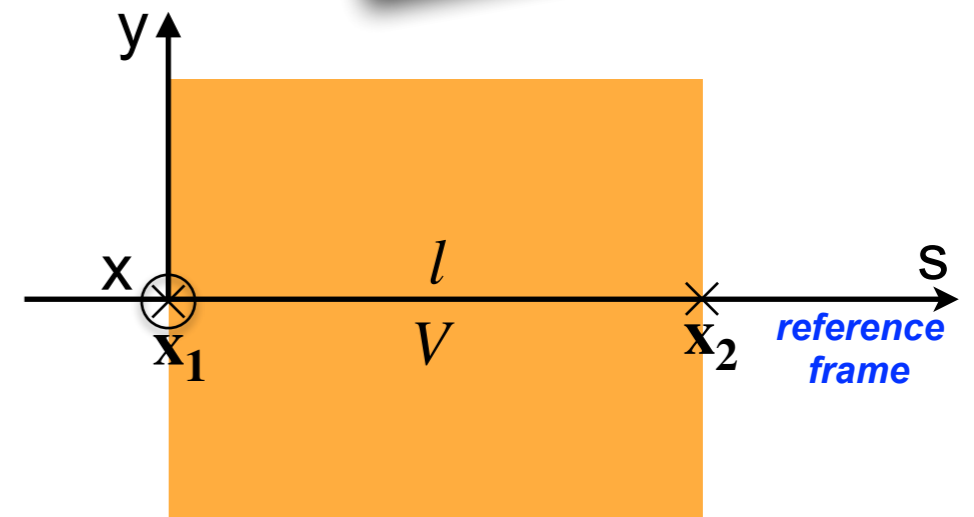
- At **exit**, using  $V = \overrightarrow{\mathbf{x}_1 \mathbf{x}_2} = [0, 0, l]^t$  (displacement) and  $W = I$  (rotation) of an element with a length  $l$ .

$$\mathbf{x}'_2 = \bar{R} \mathbf{x}_2 + \bar{T}$$

$$\mathbf{x}_2 = \bar{R}^t (\mathbf{x}'_2 - \bar{T})$$

$$\bar{T} = W^t (RV + T - V) = W^t (\overrightarrow{\mathbf{x}'_1 \mathbf{x}'_2} - \overrightarrow{\mathbf{x}_1 \mathbf{x}_2})$$

$$\bar{R} = W^t R W ; \bar{R}^t = W R^t W^t$$



- At **entry**, an element is rotated by  $R(d\theta, d\phi, d\psi)$  and translated by  $T(dx, dy, ds)$ .

$$\mathbf{x}'_1 = R \mathbf{x}_1 + T$$

$$\mathbf{x}_1 = R^t (\mathbf{x}'_1 - T)$$

$$R = R_y(d\theta) \cdot R_x(-d\phi) \cdot R_z(d\psi)$$

$$R^t = R_z(-d\psi) \cdot R_x(d\phi) \cdot R_y(-d\theta) \quad (\text{inverse})$$

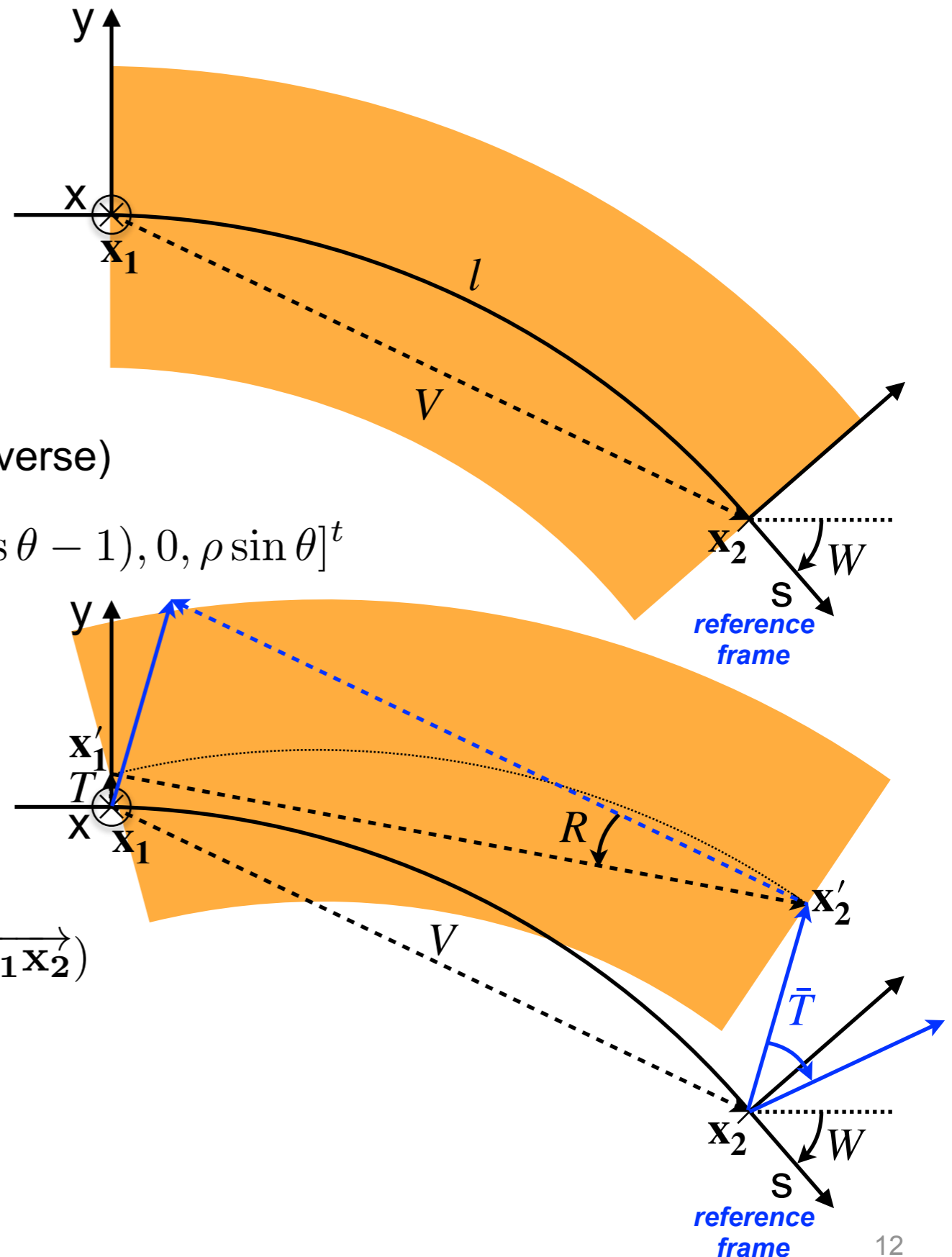
- At **exit**, using  $V = \overrightarrow{\mathbf{x}_1 \mathbf{x}_2} = R_z(\psi) \cdot [\rho(\cos \theta - 1), 0, \rho \sin \theta]^t$  and  $W = R_z(\psi) \cdot R_y(-\theta) \cdot R_z(-\psi)$  of an element with length  $l$ , angle  $\theta$  and tilt  $\psi$  (i.e.  $\rho = l/\theta$ ).

$$\mathbf{x}'_2 = \bar{R} \mathbf{x}_2 + \bar{T}$$

$$\mathbf{x}_2 = \bar{R}^t (\mathbf{x}'_2 - \bar{T})$$

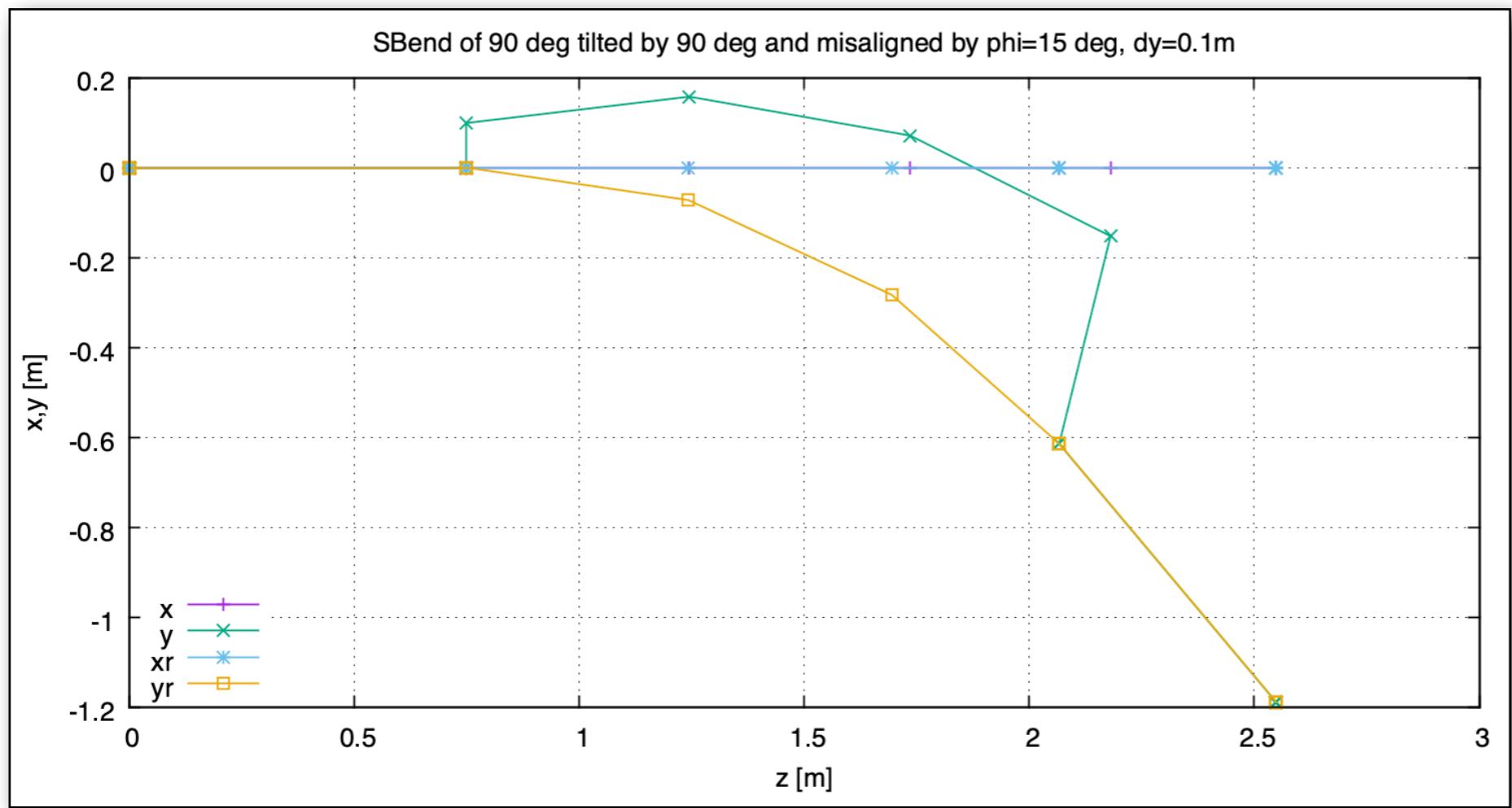
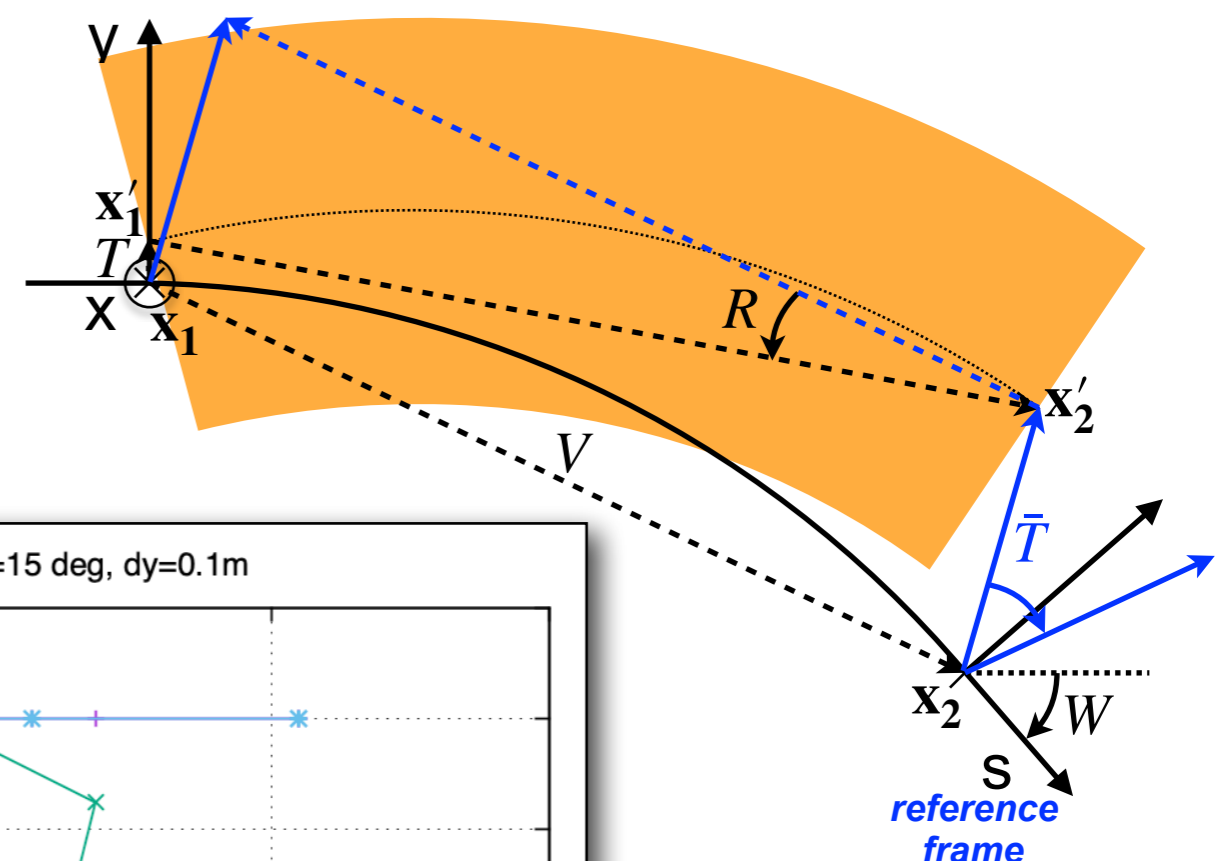
$$\bar{T} = W^t (R V + T - V) = W^t (\overrightarrow{\mathbf{x}_1 \mathbf{x}'_2} - \overrightarrow{\mathbf{x}_1 \mathbf{x}_2})$$

$$\bar{R} = W^t R W ; \bar{R}^t = W R^t W^t$$

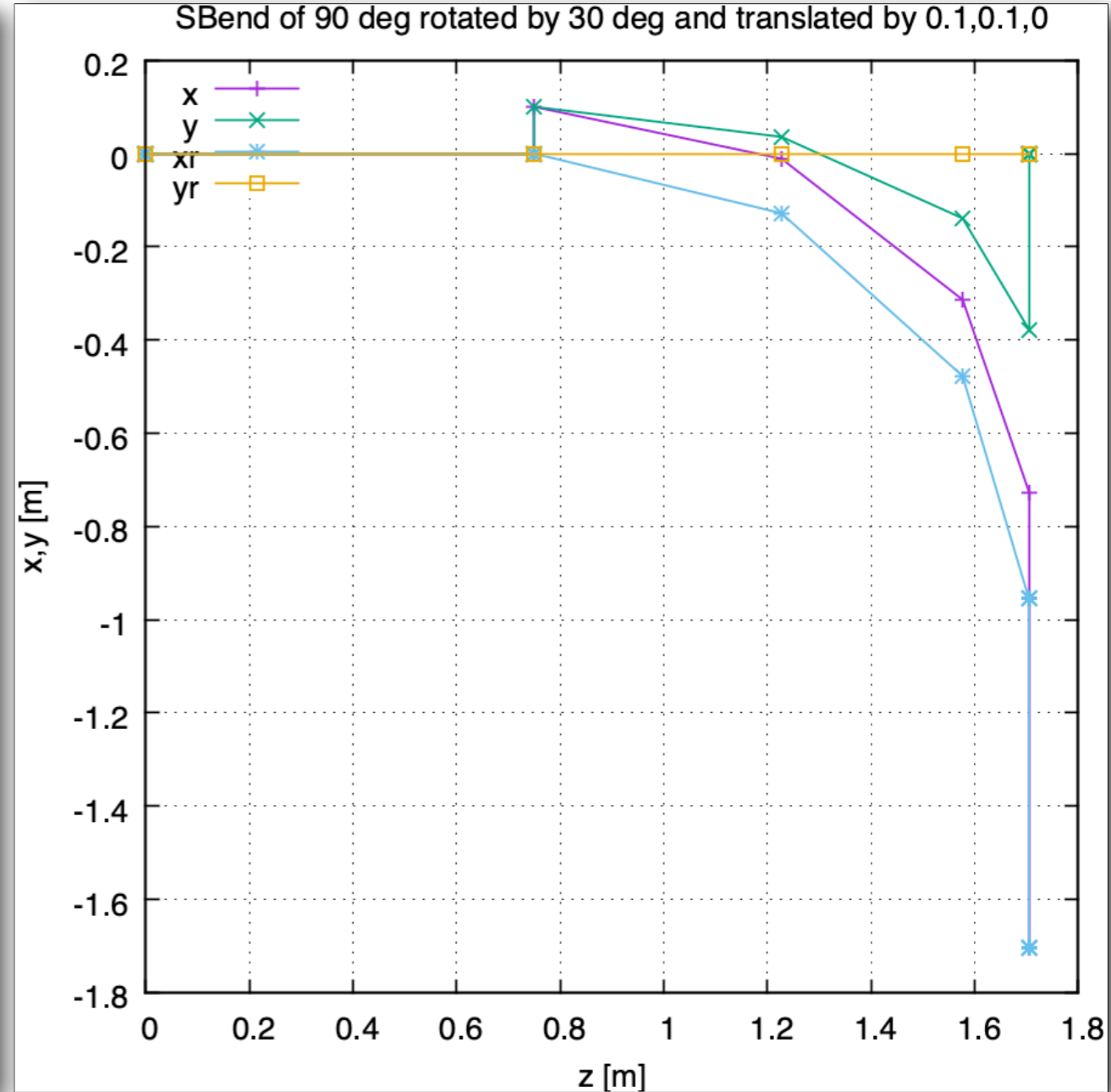
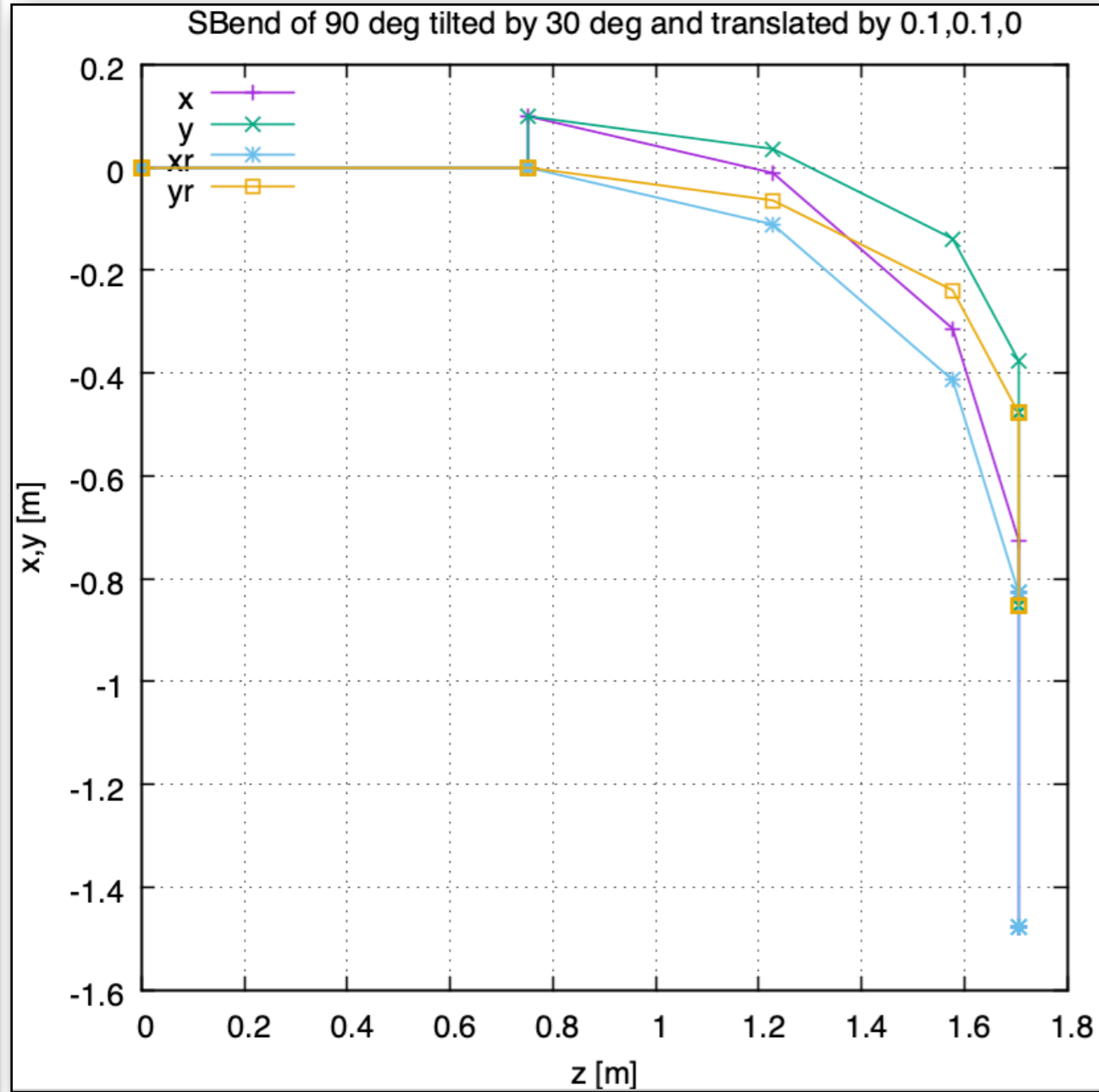


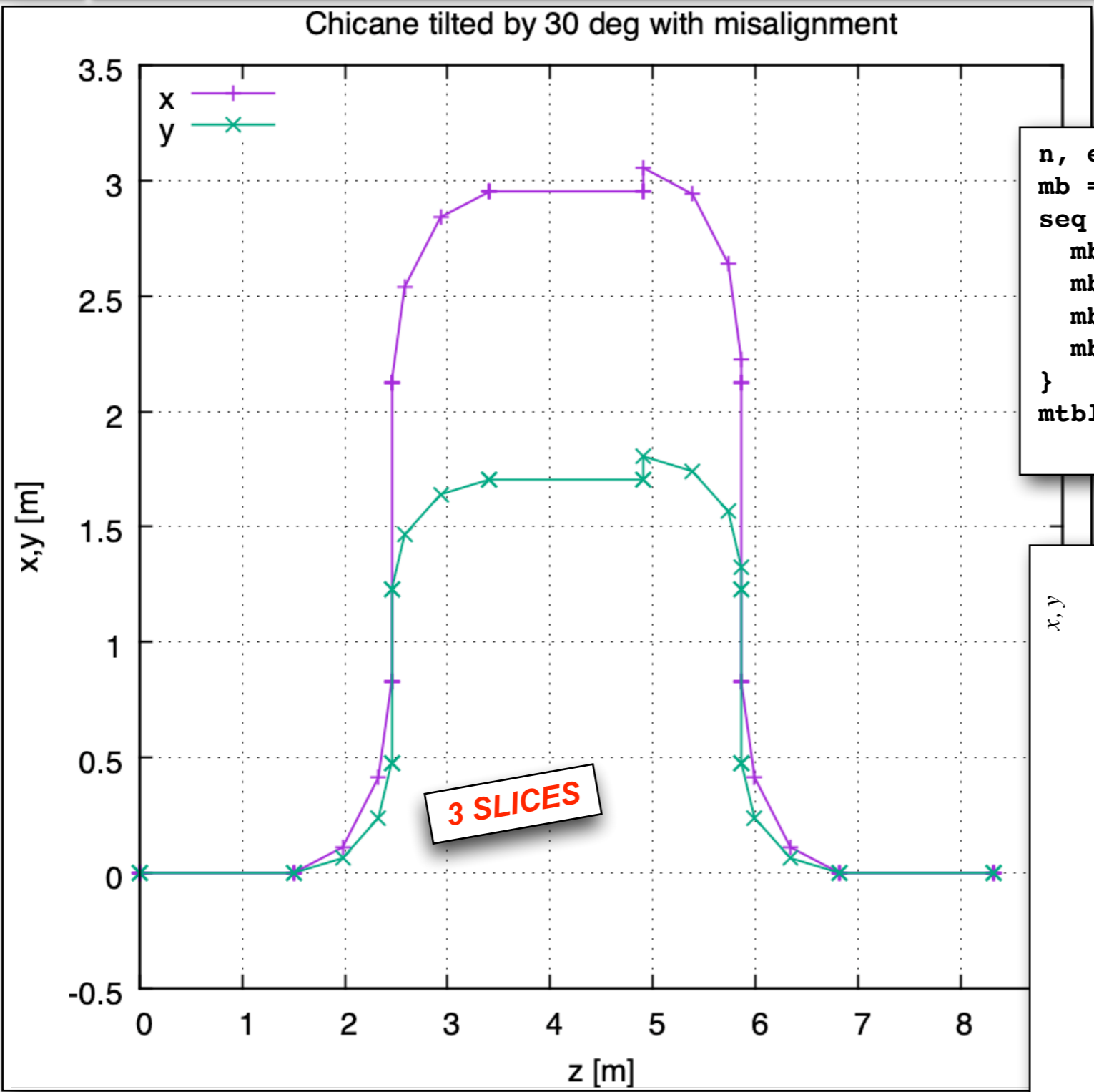
*x, y with misalignments, xr, yr reference frame without misalignment*

**SBEND angle is ~50 deg.**



*x, y with misalignments, xr, yr reference frame without misalignment*





```
n, e1, ang, tlt = 5, 1.5, pi/2, pi/6
mb = sbend 'm1' {l=e1, tilt=tlt},
seq = sequence 'seq' { l=(2*n-1)*e1,
  mb 'm1' {at=1.5*e1, angle=-ang},
  mb 'm2' {at=3.5*e1, angle= ang},
  mb 'm3' {at=5.5*e1, angle= ang, dx=0.1, dy=0.1},
  mb 'm4' {at=7.5*e1, angle=-ang},
}
mtbl = survey {sequence=seq,
  nslice=3, atslice=ftrue, misalign=true}
```

