

Magnet quench tests of the shielded HL-LHC beam screen

M. Morrone, C. Garion,

With contributions and materials from: O. Sacristan, M. Guinchard, L. Fiscarelli

WP3 Meeting

TE-VSC-DLM

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Outline

- Magnet quench test
- Physics of the problem
- Instrumentation
- Results and comparison with simulations
- Conclusions and next steps



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Test plan

Start date of the test in SM18: 10th October 2018

End date of the test in SM18: 18th October 2018

Time required at cold

- HV, transfer function at 80 K
- HV, transfer function at 1.9 K
- Beam screen & training verification
- Protection studies
- HV, transfer function at 1.9 K
- Other tests?

Total



54 quenches

(CLIQ, quench heater, training, extraction, high quench integral, ramp rate)



4

EDMS: 2024740

Aim of the test

- Training verification of the MQXFS4b at 1.9 K.
- Flux jump effect on the current studies, both during other tests' ramps and during dedicated exponential cycles;
- Magnet protection studies, including CLIQ discharges in different configurations, QH delay and performance and QH-only discharges;
- Effect of CLIQ on the beam screen studied with over 20 runs dedicated to that measurement;
- Measurement of the magnetic field during CLIQ and quench heater discharge by means of dedicated pickup coils in the beam screen;



Test conditions

- Q1 beam screen version compatible with the CLIQ discharge (pins and W block geometry modified);
- Beam screen immersed in the 1.9 K helium bath;
- Temperature: 1.9 K (significant change of the electrical resistivity of Cu due to temperature and magneto-resistivity
 → reduced thickness of Cu inner layer for the prototype, from 75 µm to 25 µm);
- Magnetic field decay representative of the HL-LHC conditions, including the CLIQ system;
- Vertical position of the beam screen within the cryostat.



BS quench test prototype -Q1 type-

Û

2 m

15150

an tol

S. Martin

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Physics of the problem



Therefore, opposite forces are expected in the same component.





Numerical results at 17.8 kA

Integrated forces induced in the W block



Region 1: Most critical!!

component	Q1		
	Torque [N m/W block]	Tangential force [N/W block]	
Cold bore	253	3400	
Heat absorber	280	4200	
Octagonal pipe	81.5	1600	

Assumption of the numerical model

- No magnet coil modelled;
- The electro-dynamic of the magnet is not considered (No IFCC, ISCC);
- Magneto-resistivity of copper considered;
- Heat load affecting the electrical properties considered;
- Measured magnetic field assigned as input for the comparison of the experimental results with the simulations in this presentation.



Animations



* For visual purposes only as the W blocks are not welded.



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Instrumentation

EDMS 1762736

<u>42 Strain gauges</u> distributed in 3 sections along 4 diametrally opposed faces of the beams screen in axial and transversal directions



<u>3 custom made displacement measuring</u> <u>heads</u> inside the beam screen to measure:

- Beam screen expansion
- W block tilt
- Magnetic field

<u>4 lines of fibers</u> installed in 4 diametrally opposed generatrixes of the cold bore: 12 biaxial strain measurement points







Strain gauges

EDMS 1762736

<u>42 Strain gauges</u> distributed in 3 sections along 4 diametrally opposed faces of the beam screen in axial and transversal directions.





Measuring probe

EDMS 1762736

<u>3 custom made displacement measuring heads inside the beam screen to measure:</u>

- Beam screen expansion
- W block tilt





Measuring probe

EDMS 1762736

<u>3 custom made displacement measuring heads inside the beam screen to measure:</u>

- Beam screen expansion
- W block tilt
- Magnetic field



Before the quench test

After the quench test



Cold bore fibers

EDMS 1762736

<u>4 lines of fibers</u> installed in 4 diametrally opposed generatrixes of the cold bore: 12 biaxial strain measurement points.







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General overview of all the strain gauges





General overview of all the strain gauges



The behaviour observed at the points located at M_F2 can be explained by the extra thickness induced by a slight surplus of the adhesive used for the bonding of the strain gages which entered in contact with the tungsten block. It can be seen in the red frame on the picture above on the left. It is also noticeable that a strain gauge got detached (picture on the right).



Results at 8.2 kA (Strain gauges, measuring probe)





8 kA Face Center (P2) Transversal Strains U_F1_P2_T 200 M_F1_P2_T M_F3_P2_T Strain [um/m] 0 simulation X -200 -400 -600 0.2 0.6 0.4 0.8 0 Time [s] 60 dB/dt*B [T^2/s] 40 p. 1-3 20 — p. 2-3 0 -20 -40 -60 B measured at r =75 mm in front of each pole. 0.2 0.4 0.6 0.8 0 Time [s]



8 kA Beam Screen Expansion





8 kA CLIQ Discharge Induced Tilt





Results at 18.2 kA (Strain gauges, measuring probe)





18.2 kA Face Center (P2) Transversal Strains





18.2 kA Beam Screen Expansion





Cold bore (optical fibers)

















Thermal link (17.8 kA)

Time=0.05 s Streamline: Induced current density Arrow Surface: Lorentz force contribution











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Conclusions

- The mechanical integrity of a Q1 beam screen prototype has been demonstrated. The behaviour of the beam screen remains elastic after 54 quenches up to 18.2 kA of current (ultimate current 17.8 kA);
- The thermal links, the elastic rings and the centring pins have been inspected after the quench test and no damage nor unexpected deformation has been observed;
- The beam screen behaves as expected during a quench:
 - The torque induced during the first phase of CLIQ has been observed;
 - The beam screen goes in contact with the cold bore;
- The mechanical response of the beam screen is directly correlated with the magnetic field measurements.
- A good agreement with simulation has been found;



Next steps

- Test of a Q2 type beam screen with the correct material (P506 instead of 316 L) and aC coating:
 - Magnetic field quality measurements;
 - Quench test.



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Thank you



Back up slides



13 kA CLIQ Discharge Induced Tilt



16 kA CLIQ Discharge Induced Tilt



Numerical results: baseline (17.8 kA)

CLIQ phase 1



	material	Elastic limit	Q1		
component			F _{y max} [N/mm] -per eight-	σ _{max} [MPa]	δ _{max} [mm]
Cold bore	Ss 316 LN	860 MPa (at 4 K)	12.3	624	1.51
Heat absorber	Inermet	1284 (at 77K)	22	> 1284 (loc.)	-
Octagonal pipe+ Cu layer	Ss P506	1350 MPa (at 50 K)	5.3	> 1350 (loc.)	-
Pin	Ss P506	1350 MPa (at 50 K)	-	> 1350 (loc.)	-



Numerical results: baseline (17.8 kA)





signal of the compensator probe at 8.2 kA



Cold bore and beam screen instrumentation layout



