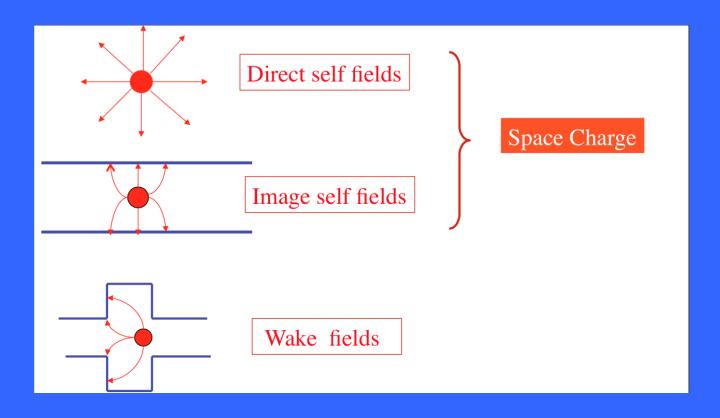
## **INSTABILITIES IN LINACS**

Massimo.Ferrario@LNF.INFN.IT







## OUTLINE

- Introduction and Heuristic model
- Basic Concepts
- Beam Break Up in Linear Accelerators
- BNS damping

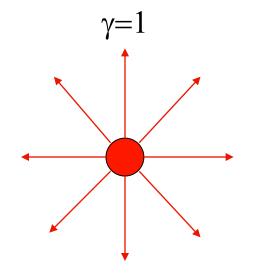
$$g = \frac{I}{\sqrt{I - b^2}}$$

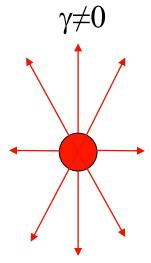
$$\vec{E} = \frac{q}{4\rho e_o} \frac{(1 - b^2)}{(1 - b^2 \sin^2 q)^{3/2}} \frac{\vec{r}}{r^3}$$

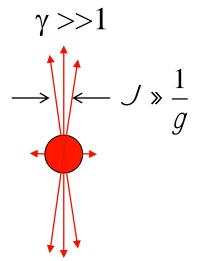
$$\beta = 0 \Rightarrow \vec{E} = \frac{q}{4\pi\varepsilon_o} \frac{\vec{r}}{r^3}$$

$$\theta = 0 \Rightarrow E_{//} = \frac{1}{\gamma^2} \frac{q}{4\pi\varepsilon_o} \frac{\vec{r}}{r^3} \xrightarrow{\gamma \to \infty} 0$$

$$\theta = \frac{\pi}{2} \Rightarrow E_{\perp} = \gamma \frac{q}{4\pi\varepsilon_o} \frac{\vec{r}}{r^3} \xrightarrow{\gamma \to \infty} \infty$$



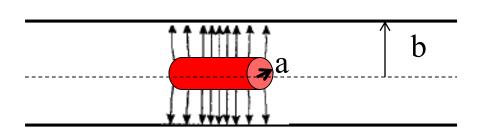




## **Bunched beam - Circular Perfectly Conducting Pipe**

## - Beam at Centre- Static Approximation $\gamma \rightarrow \infty$

$$r = \frac{I}{\rho a^2 v}$$



$$j(b) = 0$$

$$E_{r} = \frac{I}{2\rho e_{o} a^{2} v} r \quad \textbf{for} \quad r \in \mathbf{a}$$

$$E_{r} = \frac{I}{2\rho e_{o} v} \frac{1}{r} \quad \textbf{for} \quad r > \mathbf{a}$$

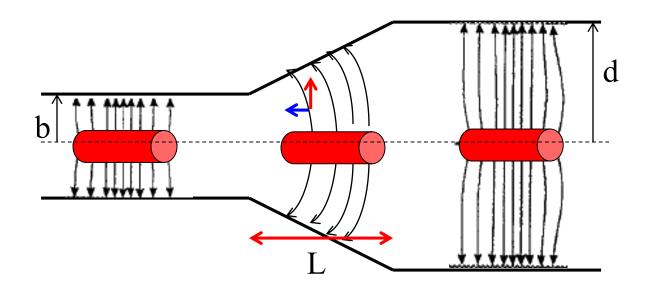
$$B_{\vartheta} = \frac{\beta}{c} E_{\eta}$$

$$\int_{r}^{b} (r) = \int_{r}^{b} E_{r}(r) dr$$

$$= \frac{I}{4\rho e_{o}v} \int_{e}^{a} I + 2 \ln \frac{b}{a} - \frac{r^{2} \ddot{0}}{a^{2} \dot{d}} \quad \text{for } r \in a$$

$$= \frac{I}{2\rho e_{o}v} \ln \frac{b}{r} \qquad \text{for } a \in r \in b$$

## **Circular Perfectly Conducting Pipe with Transition**



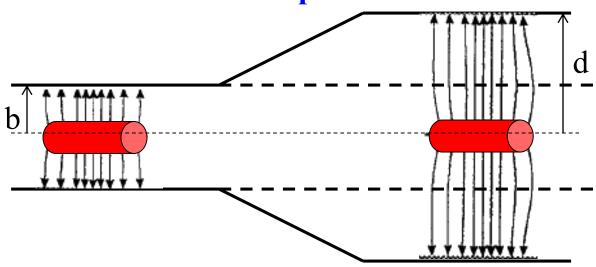
There is a longitudinal  $E_z(r,z)$  field in the transition and a test particle experience a voltage given by:

$$V = - \mathop{\circ}\limits_{0}^{L} E_{z}(r,z)dz = -\left(j(r,L) - j(r,0)\right) = -\frac{I}{2\rho e_{o}v} ln \frac{d}{b}$$

decelerating if d > b

$$P_b = VI = \frac{I^2}{2\rho e_o v} ln \frac{d}{b}$$
 Power lost by the beam

## For d > b the power is deposited to the energy of the fields: moving from left to right the beam induces the fields in the additional space available



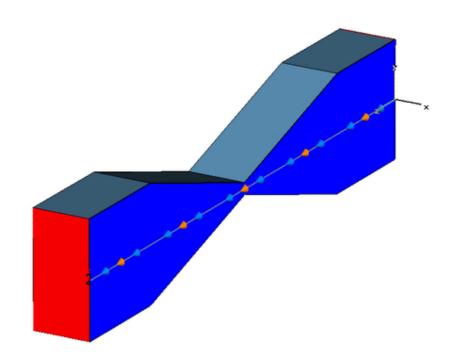
The additional power passing through the right part of the beam pipe is obtained by

integrating the Poynting vector throught the sourface  $\Delta S = \pi (d^2 - b^2)$ 

$$P_{em} = \int_{DS} \left( \frac{1}{m} \vec{E} \times \vec{B} \right) \cdot d\vec{S} = \int_{b}^{d} \frac{E_{r} B_{J}}{m} 2 \rho r dr = \frac{I^{2}}{2 \rho e_{o} v} \ln \frac{d}{b}$$

Notice that if d < b the beam gains energy. If  $d - > \infty$  the power goes to infinity, such an unphysical result is nevertheless consistent with the original assumption of an infinite energy beam  $(\gamma - > \infty)$ .

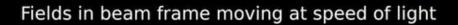
## **Reflected and Diffracted fiels**



CST MICROWAVE STUDIO®

# ILC cryomodule of 8 Superconducting RF cavities

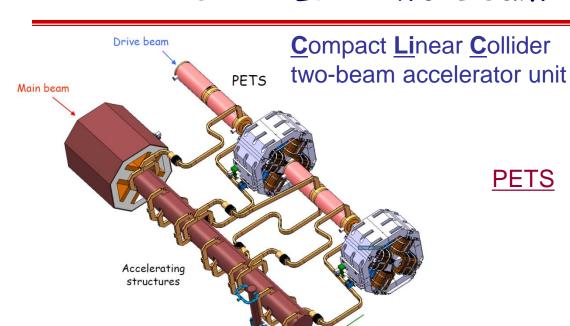
Expanded views of Input and HOM couplers



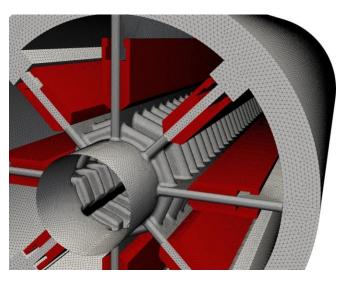


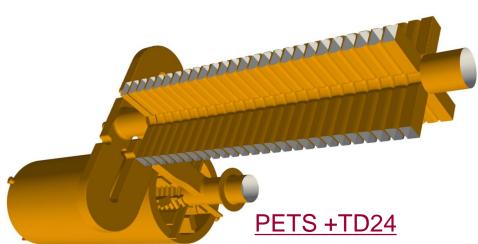


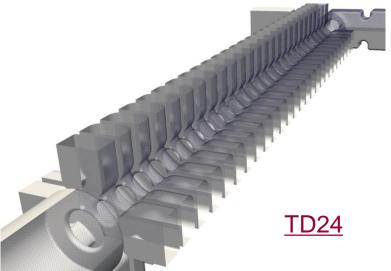
## T3P - CLIC Two-Beam Accelerator



RF power

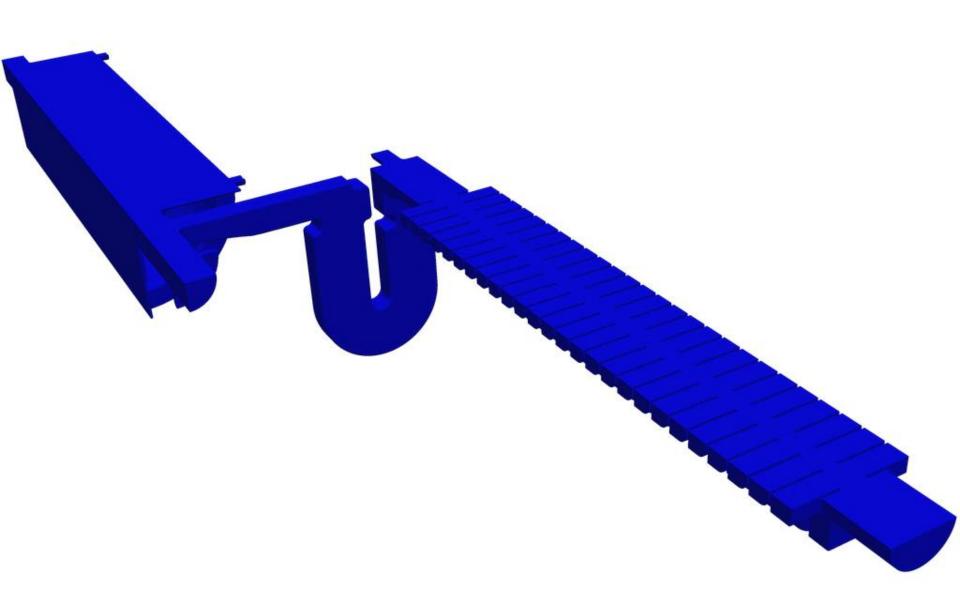








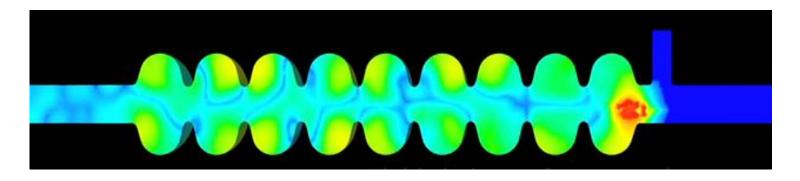




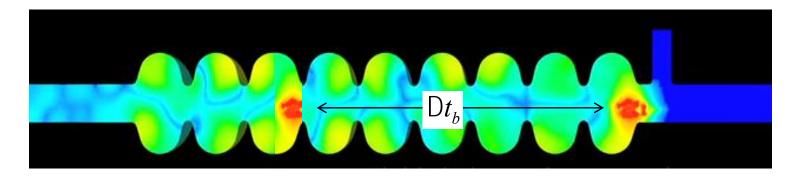




Short Range Wake Fields Effects → head tail effects



Long Range Wake Fields Effects → multibunch instabilities

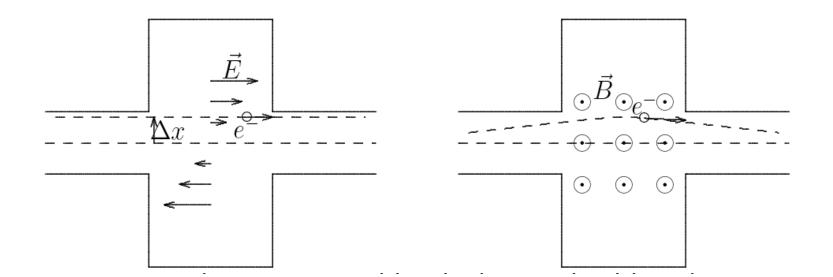


$$Dt_b \approx t = \frac{2Q}{W} \begin{cases} \approx ms \implies \text{Normal Conducting Cavities} \\ \approx ms \implies \text{Superconducting Cavities} \end{cases}$$

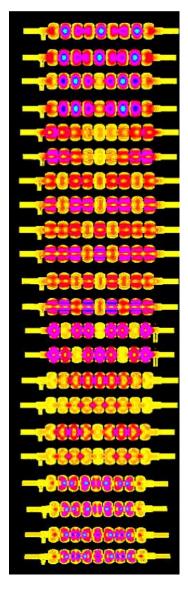
Table 3 Mode Patterns in Circular Waveguide.

| Wave Type                                                                                         | TM <sub>01</sub>              | TM <sub>02</sub>              | TM <sub>11</sub>                                      | TE <sub>01</sub>              | TE <sub>11</sub>                                      |
|---------------------------------------------------------------------------------------------------|-------------------------------|-------------------------------|-------------------------------------------------------|-------------------------------|-------------------------------------------------------|
| Field distributions<br>in cross-sectional<br>plane, at plane of<br>maximum trans-<br>verse fields |                               |                               | Distributions below along this plane                  |                               | Distributions below along this plane                  |
| Field distributions<br>along guide                                                                |                               |                               |                                                       |                               |                                                       |
| Field components present                                                                          | $E_Z$ , $E_r$ , $H_{\varphi}$ | $E_Z$ , $E_r$ , $H_{\varphi}$ | $E_Z$ , $E_r$ , $E_{\varphi}$ , $H_r$ , $H_{\varphi}$ | $H_Z$ , $H_r$ , $E_{\varphi}$ | $H_Z$ , $H_r$ , $H_{\varphi}$ , $E_r$ , $E_{\varphi}$ |

Energy exchange if: 
$$\frac{dg}{dt} = \frac{e}{mc} \vec{E} \times \vec{b} = \frac{e}{mc} (E_{//} b_{//} + E_{\wedge} b_{\wedge}) \stackrel{1}{=} 0$$

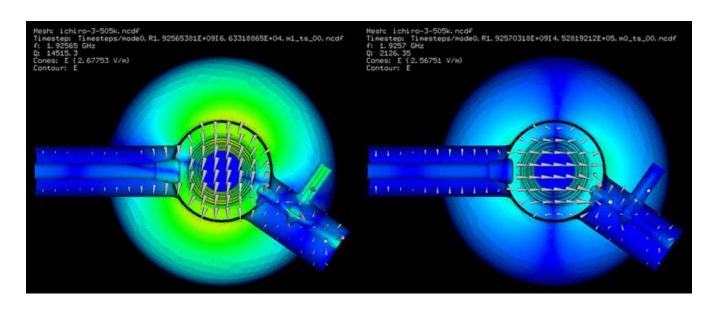


| Mode         | f<br>[MHz] | (R/Q)*<br>[Ω/cm <sup>n</sup> ] | $Q_{ext}$         |
|--------------|------------|--------------------------------|-------------------|
| M: TM010-9   | 1300.00    | 1161                           | 8·10 <sup>5</sup> |
| D: TE111-7a  | 1717.15    | 5.0                            | 4·10 <sup>4</sup> |
| D: TE111-7b  | 1717.21    | 5.0                            | 5.104             |
| D: TE111-8a  | 1738.12    | 3.0                            | 6.104             |
| D: TE111-8b  | 1738.15    | 3.0                            | 8.104             |
| D: TM110-2a  | 1882.15    | 3.4                            | 6.103             |
| D: TM110-2b  | 1882.47    | 3.4                            | 6.103             |
| D: TM110-4a  | 1912.04    | 4.6                            | 9.103             |
| D: TM110-4b  | 1912.21    | 4.6                            | 1.104             |
| D: TM110-5a  | 1927.10    | 15.6                           | 1.5.104           |
| D: TM110-5b  | 1927.16    | 15.6                           | 1.5.104           |
| D: TM110-6a  | 1940.25    | 12.1                           | 2.104             |
| D: TM110-6b  | 1940.27    | 12.1                           | 2.104             |
| M: TM011-6   | 2177.48    | 192                            | 104               |
| M: TM011-7   | 2182.81    | 199                            | 104               |
| D: 3-rd-1a   | 2451.07    | 31.6                           | 1.105             |
| D: 3-rd -1b  | 2451.15    | 31.6                           | 2.105             |
| D: 3-rd 1-2a | 2457.04    | 22.2                           | 5.104             |
| D: 3-rd 1-2b | 2457.09    | 22.2                           | 5.104             |
| D: 5-th - 7a | 3057.43    | 0.5                            | 3.105             |
| D: 5-th - 7b | 3057.45    | 0.5                            | 3.105             |
| D: 5-th - 8a | 3060.83    | 0.4                            | 8·10 <sup>5</sup> |
| D: 5-th - 8b | 3060.88    | 0.4                            | 9.105             |

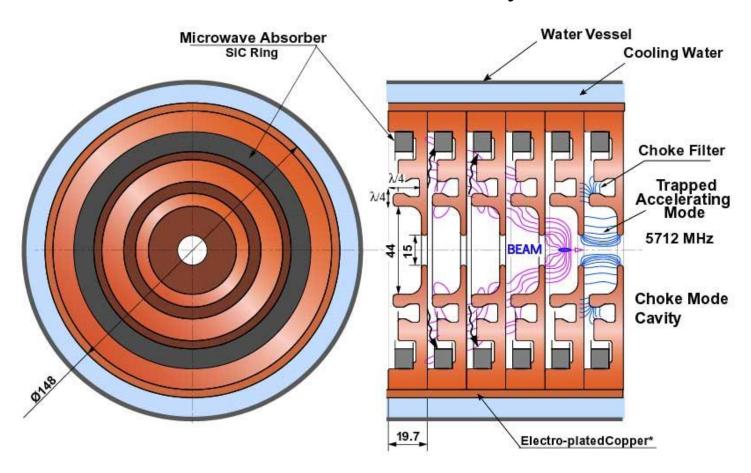




#### Example of two dipoles overlapping modeling in the TESLA cavity with Omega3P



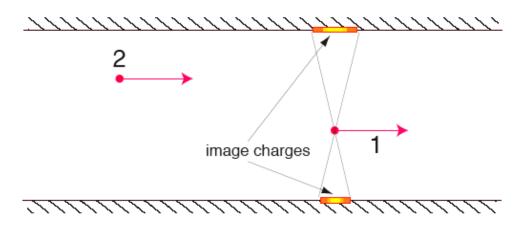
## "Choke Mode Cavity"



## Causality and the Catch-Up distance

The induced charges travel with the same particle velocity v.

Since both the particles and the image charges move on parallel paths, in the limit  $\mathbf{v} = \mathbf{c}$  they do not interact with each other, no matter how close to the wall the particles are.

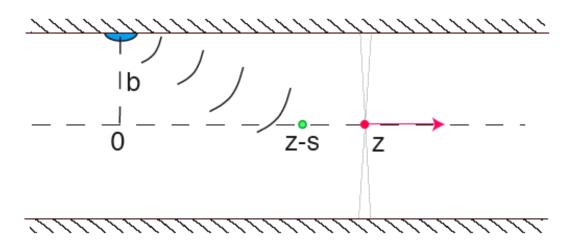


**FIGURE 2.** Particles traveling inside a perfectly conducting pipe of arbitrary cross section. Shown are the image charges on the wall generated by the leading charge.

If a particle moves along a straight line with the speed of light, the electromagnetic field of this particle scattered off the boundary discontinuities will not overtake it and, furthermore, will not affect the charges that travel ahead of it.

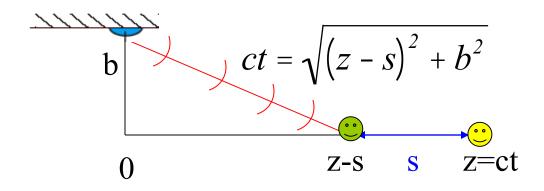
The field can interact only with the trailing charges in the beam that move behind it.

This constitutes the principle of causality in the theory of wake fields



**FIGURE 3.** A wall discontinuity located at z=0 scatters the electromagnetic field of an ultrarelativistic particle. When the particle moves to location z, the scattered field arrives to point z-s.

We can estimate the distance at which the electromagnetic field produced by a leading charge reaches a trailing particles traveling at a distance s behind.



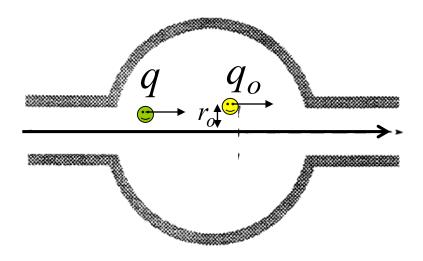
$$z^{2} = (z - s)^{2} + b^{2} = z_{catch-up} * \frac{b^{2}}{2s}$$
 for  $s << b$ 

Only after the leading charge has traveled  $\mathbf{z}_{\text{catch-up}}$  away from the discontinuity, can a particle at point **s** behind it feel the field generated by the discontinuity.

# OUTLINE

- Heuristic model
- Basic Concepts
- Beam Break Up in Linear Accelerators
- BNS damping

#### **Wake Potentials**



$$\boldsymbol{F} = q \left[ E_z \hat{z} + \left( E_x - v B_y \right) \hat{x} + \left( E_y + v B_x \right) \hat{y} \right] \circ \boldsymbol{F}_{\parallel} + \boldsymbol{F}_{\wedge}$$

there can be two effects on the **test charge**:

- 1) a longitudinal force which changes its energy,
- 2) a transverse force which deflects its trajectory.

If we consider a device of length L:

the Energy Gain is:

$$U = \bigcap_{0}^{L} F_{z} ds$$

the Transverse Deflecting Kick is:

$$\mathbf{M} = \mathbf{\hat{0}}_{0}^{L} \mathbf{F}_{\wedge} ds$$

These quantities, normalised to the charges, are called *wake-potentials* and are both function of the distance z.

Note that the integration is performed over a given path of the trajectory.

# Longitudinal wake potential [V/C]

$$w_{\parallel} = -\frac{U}{q_o q} = -\frac{V}{q_o}$$
 Energy Loss

# Transverse wake potential [V/Cm]

$$\boldsymbol{w}_{\wedge} = \frac{1}{r_o} \frac{\boldsymbol{M}}{q_o q}$$

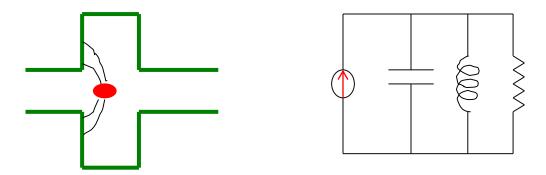
**Transverse Kick** 

The sign minus in the longitudinal wake-potential means that the test charge loses energy when the wake is positive.

Positive transverse wake means that the transverse force is defocusing.

## Longitudinal wake potential of a resonant HOM

When a charge crosses a resonant structure, it excites the fundamental mode and high order modes (HOM). Each mode can be treated as an electric RLC circuit loaded by an impulsive current.



Just after the charge passage, the capacitor is charged with a voltage  $V_o = q/C$  and the electric field is  $E_{so} = V_o/l_o$ .

The time evolution of the electric field is governed by the same differential equation of the voltage

$$\ddot{V} + \frac{1}{RC}\dot{V} + \frac{1}{LC}V = \frac{1}{C}\dot{I}$$

The passage of the impulsive current charges only the capacitor, which changes its potential by an amount  $V_c(0)$ .

This potential will oscillate and decay producing a current flow in the resistor and inductance.

For t > 0 the potential satisfy the following equation and initial conditions:

$$\ddot{V} + \frac{1}{RC}\dot{V} + \frac{1}{LC}V = 0$$

$$V(t = 0^+) = \frac{q}{C} \circ V_0$$

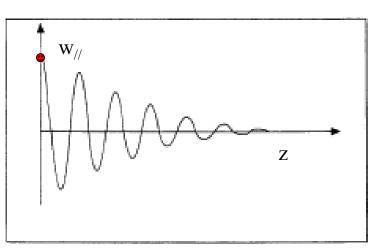
$$\dot{V}(t = 0^+) = \frac{\dot{q}}{C} = \frac{I(0^+)}{C} = \frac{V_0}{RC}$$

$$V(t) = V_0 e^{-gt} \stackrel{\text{\'e}}{\underset{\text{\'e}}{\text{\'e}}} cos(\overline{W}t) - \frac{g}{\overline{W}} sin(\overline{W}t) \stackrel{\text{\`u}}{\underset{\text{\'e}}{\text{\'e}}}$$

$$\overline{W}^2 = W_r^2 - g^2 \quad 2g = 1/RC \quad W_r^2 = 1/LC$$

putting z = -ct (z is negative behind the charge):

$$w_{//}(z) = \frac{V(z)}{q} = w_o e^{g z/c} \hat{\theta} \cos(\overline{W}z/c) + \frac{g}{\overline{W}} \sin(\overline{W}z/c) \hat{\psi}$$



...but what about the source charge?

It is also useful to define the *loss factor* as the normalised energy lost by the source charge q

$$k = -\frac{U(z=0)}{q_o^2}$$

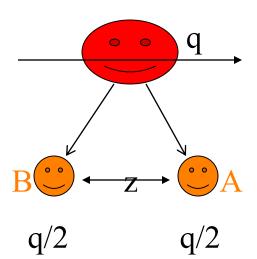
Although in general the loss factor is given by the longitudinal wake at z=0, for charges travelling with the light velocity the longitudinal wake potential is discontinuous at z=0

The exact relationship between k and w(z=0) is given by the **beam loading theorem:** 

$$k = \frac{w_{\parallel}(z \to 0)}{2}$$

Causality requires that the longitudinal wake potential of a charge travelling with the velocity of light is discontinuous at the origin.

$$U_o = -q^2 k$$



$$U_A = -q_A^2 k = -\frac{q^2}{4} k$$

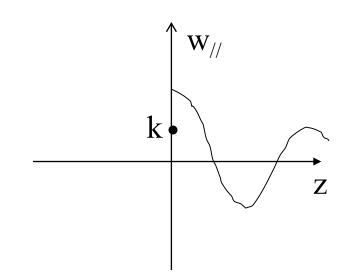
$$U_{B} = -q_{B}^{2}k - q_{A}q_{B}w_{//}(z)$$
$$= -\frac{q^{2}}{4}k - \frac{q^{2}}{4}w_{//}(z)$$

$$U_{A} + U_{B} = -\frac{q^{2}}{2}k - \frac{q^{2}}{4}w_{//}(z)$$

$$z \rightarrow 0$$
  $U_o = U_A + U_B$ 

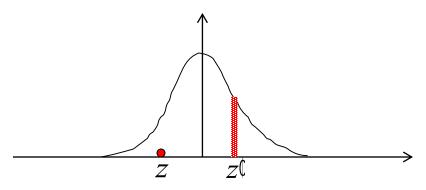
$$q^2k = \frac{q^2}{2}k + \frac{q^2}{4}w_{//}(0)$$

$$k = \frac{w_{//}(0)}{2}$$



### Wake potentials and energy loss of a bunched distribution

When we have a bunch with density  $\lambda(z)$ , we may wander what is the amount of energy lost or gained by a single charge e in the beam



To this end we calculate the effect on the charge from the whole bunch by means of the convolution integral:

$$U(z) = -e \int_{-\infty}^{\infty} w_{//}(z'-z)\lambda(z')dz'$$

Which allows to define the wake potential of a distribution

$$W_{//}(z) = -\frac{U(z)}{qe} = \frac{1}{q} \int_{-\infty}^{\infty} w_{//}(z'-z)\lambda(z')dz'$$

The total energy lost by the bunch is computed summing up the loss of all particles:

$$U_{bunch} = \frac{1}{e} \int_{-\infty}^{\infty} U(z) \lambda(z) dz = -q \int_{-\infty}^{\infty} W_{||}(z) \lambda(z) dz$$

#### Example: Energy spread and loss for a finite uniform beam due to a HOM

$$W_{//}(z) \approx W_0 \cos\left(\frac{\omega_r}{c}z\right) H(-z)$$

$$U(z) = -e \int_{-\infty}^{+\infty} w_{//}(z - z') \lambda(z') dz'$$

$$U(z) = -\frac{eqw_0}{l_0} \int_{z}^{\infty} \cos \left[ \frac{\omega_r}{c} (z - z') \right] dz'$$

$$z - z' = x$$

$$\frac{1}{\lambda(z)} = q/l_0$$

$$\frac{-l_0}{2} \quad \mathbf{Z} \quad \mathbf{Z}, \quad \frac{l_0}{2}$$

$$U(z) = \frac{eqw_0}{l_0} \int_0^{(z-l_0/2)} \cos\left(\frac{\omega_r}{c}x\right) dx = \frac{eqw_0}{l_0} \left| \frac{\sin\left(\frac{\omega_r}{c}x\right)}{\left(\frac{\omega_r}{c}\right)} \right|_0^{(z-l_0/2)}$$

$$U(z) = -\frac{eqw_0}{2} \left| \frac{\sin \left[ \frac{\omega_r}{c} \left( \frac{l_0}{2} - z \right) \right]}{\left( \frac{\omega_r}{c} \frac{l_0}{2} \right)} \right|$$

Wake potential? Energy spread  $(U_{max}-U_{min})$ ?

## **Energy loss**

$$U_{bunch} = \frac{1}{e} \int_{-\infty}^{+\infty} U(z) / (z) dz \approx \frac{-q^2 w_0}{2l_0 \left(\frac{W_r}{c} \frac{l_0}{2}\right)} \int_{-\frac{l_0}{2}}^{\frac{l_0}{2}} \sin \left[\frac{W_r}{c} \left(\frac{l_0}{2} - z\right)\right] dz$$

$$U_{bunch} = \frac{-q^2 w_0 c}{W_r l_0^2} \left| \frac{-\cos\left[\frac{W_r}{c}\left(\frac{l_0}{2} - z\right)\right]^{\frac{l_0}{2}}}{-\frac{W_r}{c}} \right|^{\frac{l_0}{2}}$$

$$U_{bunch} = -\frac{q^2 w_0 c^2}{W_r^2 l_0^2} \left[ 1 - \cos\left(\frac{W_r l_0}{c}\right) \right] = -\frac{2q^2 w_0 c^2}{W_r^2 l_0^2} \sin^2\left(\frac{W_r l_0}{2c}\right)$$

$$U_{bunch} = -\frac{q^2 w_0}{2} \frac{\sin^2\left(\frac{W_r l_0}{2c}\right)}{\left(\frac{W_r l_0}{2c}\right)^2}$$

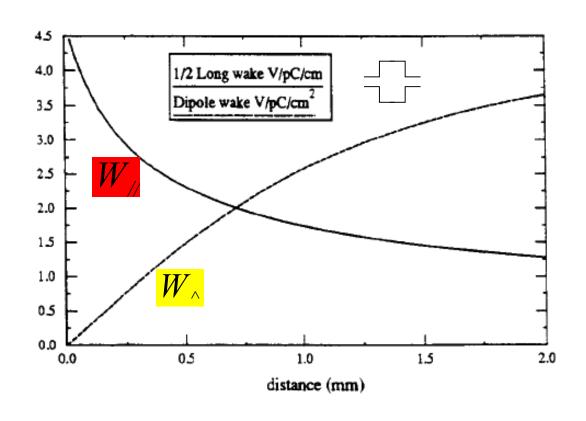
$$\lim_{l_0 \to 0} \left(U_{bunch}\right) = -\frac{q^2 w_0}{2}$$

$$\lim_{l_0 \to 0} \left( U_{bunch} \right) = -\frac{q^2 w_0}{2}$$

# Relationship between transverse and longitudinal forces: "Panofsky-Wenzel theorem".

$$\nabla_{\perp} F_{\parallel} = \frac{\partial}{\partial z} F_{\perp}$$

$$\nabla_{\perp} w_{\parallel} = \frac{\partial}{\partial z} w_{\perp}$$



## **Coupling Impedance**

The wake potentials are used for to study the beam dynamics in the time domain (s=vt). If we take the equation of motion in the frequency domain, we need the Fourier transform of the wake potentials. Since these quantities have Ohms units are called *coupling impedances*:

Longitudinal impedance ( \subseteq \subseteq

$$Z_{//}(w) = \frac{1}{v} \mathop{\grave{0}}_{-¥}^{¥} w_{//}(z) e^{-i\frac{wz}{v}} dz$$

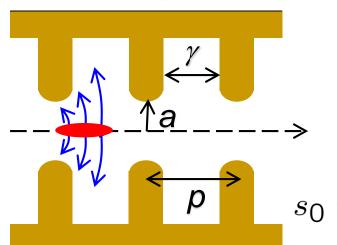
*Transverse impedance*  $(\Box \Box m)$ 

$$\mathbf{Z} \wedge (\mathbf{W}) = \frac{i}{v} \mathop{\grave{0}}_{-\frac{1}{2}}^{\frac{1}{2}} \mathbf{w} \wedge (z) e^{-i\frac{\mathbf{W}z}{v}} dz$$

 $Z_R$  is responsible for the energy losses

 $Z_i$  defines the phase between the beam response & exciting wake potential

# Longitudinal Wakefields of RF Structures



SLAC S-band:

*a* □ 11.6 mm

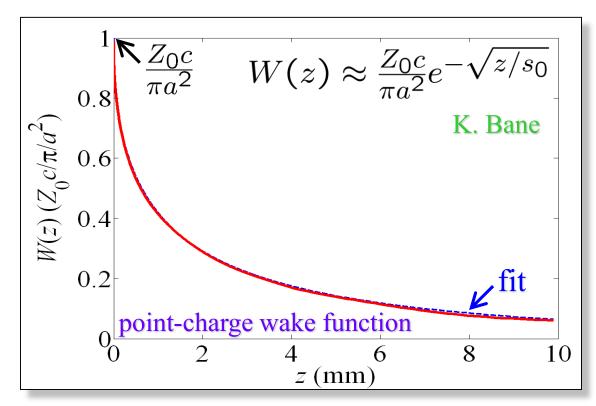
*γ* □ 29.2 mm

*p* □ 35.0 mm

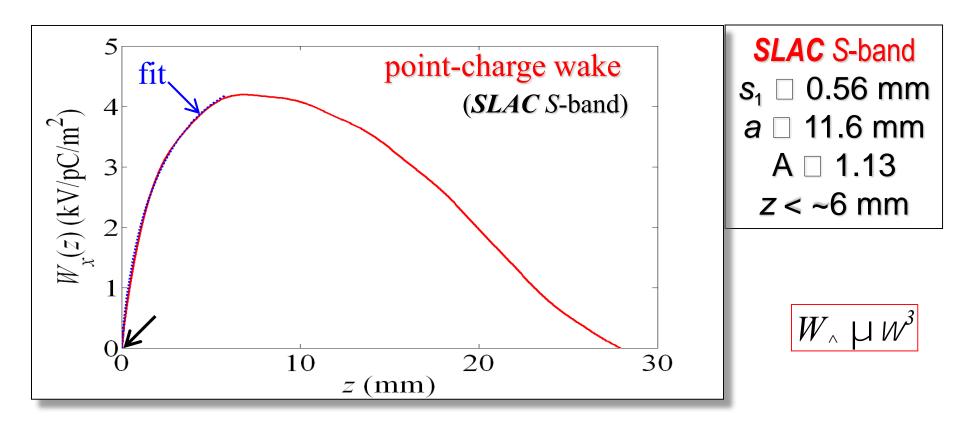
$$s_0 \approx 0.41 \frac{a^{1.8}g^{1.6}}{p^{2.4}}$$







## Transverse Wakefields



transverse point-charge wakefield function and short-range fit:

$$W_x(z) \approx A \frac{4Z_0 c s_1}{\pi a^4} \left[ 1 - (1 + \sqrt{z/s_1}) e^{-\sqrt{z/s_1}} \right], z < 6 \text{ mm}$$

# Energy spread compensation

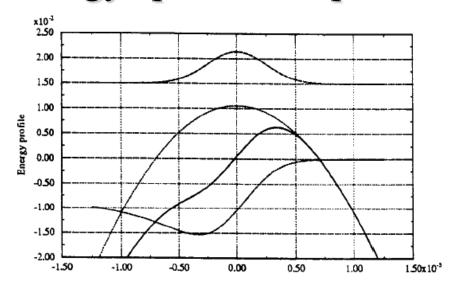


Fig. 5 Energy profile within the bunch sitting on the crest of the rf wave

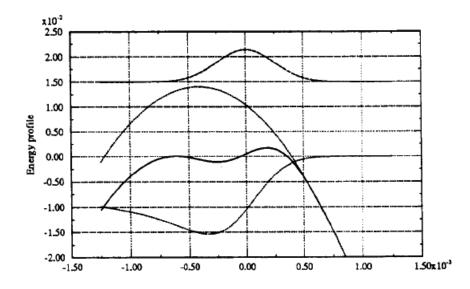


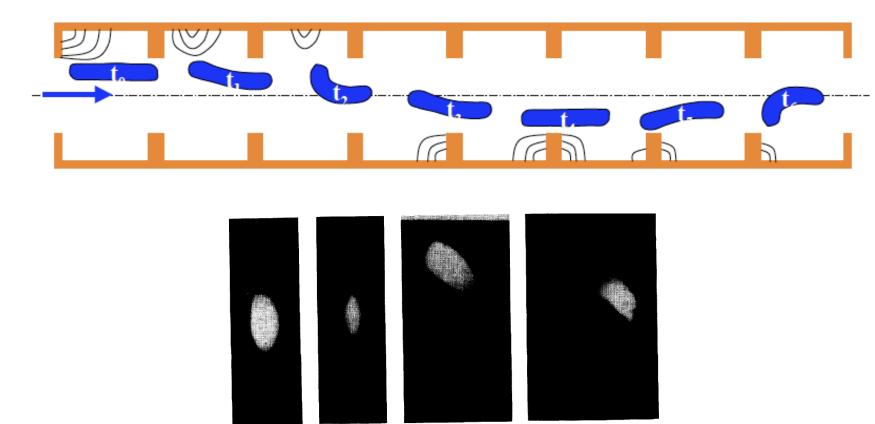
Fig. 6 Energy profile within the bunch after optimization of the rf phase

## OUTLINE

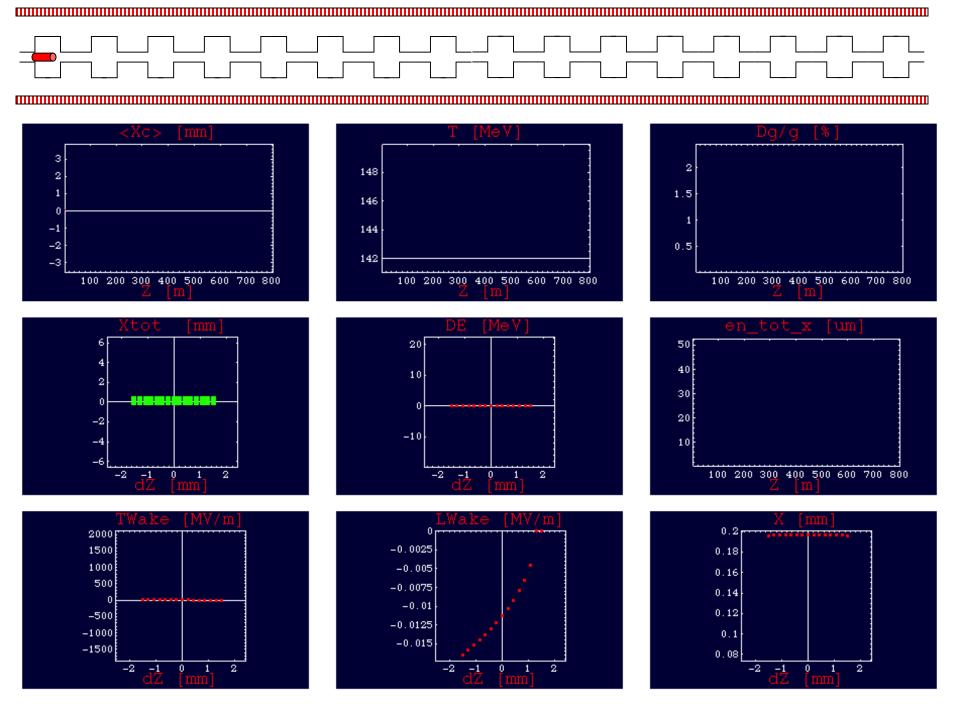
- Heuristic model
- Basic Concepts
- Beam Break Up in Linear Accelerators
- BNS damping

## Beam Break Up

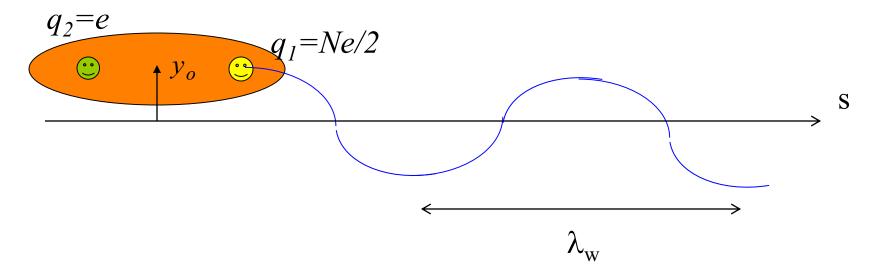
A beam injected off-center in a LINAC, because of the focusing quadrupoles, execute betatron oscillations. The displacement produces a transverse wake field in all the devices crossed during the flight, which deflects the trailing charges.



**Figure 3.4.** Four transverse beam profiles observed at the end of the SLAC linac are shown when the beam was carefully injected and injected with 0.2, 0.5, and 1 mm offsets. The beam sizes  $\sigma_{\nu}$  and  $\sigma_{\nu}$  are about 120  $\mu$ m. (Courtesy John Seeman, 1991.)



In order to understand the effect, we consider a simple model with only two charges  $q_1=Ne/2$  (leading = half bunch) and  $q_2=e$  (trailing = single charge).



the leading charge executes free betatron oscillations:

$$y_1(s) = \hat{y}_1 \cos \frac{\partial w_y}{\partial c} = \frac{\partial w_y}{\partial c} = \frac{\partial w_y}{\partial c} = \frac{\partial p}{\partial c}$$

the test charge, at a distance z behind, over a length  $L_w$  experiences a deflecting force proportional to the displacement  $y_1$ , and dependent on the

distance z:  

$$M(r_0,z) = \int_0^{L_w} F_{\perp} ds = \langle F_{\perp}(r_0,z) \rangle L_w \implies \langle F_{\perp}(z,y_1) \rangle = \frac{Ne^2}{2L_w} w_{\perp}(z) y_1(s)$$

This force drives the motion of the test charge:

betatron equation of motion with coherent force

$$y_2'' + \left(\frac{\omega_y}{c}\right)^2 y_2 = \frac{1}{\beta^2 E_o} \left\langle F_\perp(z, y_1) \right\rangle = \frac{Ne^2 w_\perp(z)}{2\beta^2 E_o L_w} \hat{y}_1 \cos\left(\frac{\omega_y}{c}s\right)$$

This is the typical equation of an harmonic oscillator driven at the resonant frequency. The solution is given by the superposition of the "free" oscillation and a "driven" oscillation which, being driven at the resonant frequency, grows linearly with *s*.

$$y_{2}(s) = \hat{y}_{2} \cos \frac{\Re W_{y}}{c} \stackrel{\ddot{0}}{s} \div y_{2}^{driven}$$

$$y_{2}^{driven} = \frac{cNe^{2}w_{\wedge}(z)}{4W_{y}E_{o}L_{w}} s\hat{y}_{1} \sin \frac{\Re W_{y}}{c} \stackrel{\ddot{0}}{s} \div$$

$$continuos growth$$

At the end of the LINAC of length  $L_L$ , the oscillation amplitude is grown by :

$$\left(\frac{D\hat{y}_2}{\hat{y}_2}\right)_{\text{max}} = \frac{cNe^2w_{\wedge}(z)L_L}{4W_yE_oL_w}$$

## OUTLINE

- Heuristic model
- Basic Concepts
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## Balakin-Novokhatsky-Smirnov Damping

The BBU instability is quite harmful and hard to take under control even at high energy with a strong focusing, and after a careful injection and steering.

A simple method to cure it has been proposed observing that the strong oscillation amplitude of the bunch tail is mainly due to the "resonant" driving.

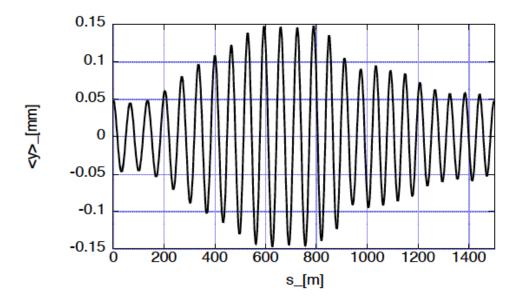
If the tail and the head move with a different frequency, this effect can be significantly removed.

Let us assume that the tail oscillates with a frequency  $\omega_y + \Delta \omega_y$ , the equation of motion reads:

$$y_2'' + \left(\frac{W_y + DW_y}{c}\right)^2 y_2 = \frac{Ne^2 w_{\wedge}(z)}{2b^2 E_o L_w} \hat{y}_1 \cos\left(\frac{W_y}{c}s\right)$$

## the solution of which is:

$$y_2(s) = \hat{y}_2 \cos\left(\frac{\omega_y + \Delta\omega_y}{c}s\right) + \frac{c^2 N e^2 w_\perp(z)}{4\omega_y \Delta\omega_y E_o L_w} \hat{y}_1 \left[\cos\left(\frac{\omega_y}{c}s\right) - \cos\left(\frac{\omega_y + \Delta\omega_y}{c}s\right)\right]$$



$$y_2(s) = \hat{y}_2 \cos\left(\frac{\omega_y + \Delta \omega_y}{c}s\right) + \frac{c^2 x^2}{4\omega_y \omega_y \omega_y \omega_z} \hat{y}_1 \left[\cos\left(\frac{\omega_y}{c}s\right) - \cos\left(\frac{\omega_y + \Delta \omega_y}{c}s\right)\right]$$

by a suitable choice of  $\Delta \omega_y$ , it is possible to fully depress the oscillations of the tail.

$$\hat{y}_2 = \hat{y}_1 \qquad \frac{c^2 N e^2 w_{\perp}(z)}{4 \omega_y \Delta \omega_y E_o L_w} = 1 \qquad \qquad y_2(s) = \hat{y}_1 \cos\left(\frac{\omega_y}{c}s\right) = y_1(s)$$

$$\Delta\omega_y = \frac{c^2 N e^2 w_{\perp}(z)}{4\omega_y E_o L_w}$$

The extra focusing at the tail can be obtained by:

- Using an RFQ, where head and tail see a different focusing strength.
- Creating a correlated energy distribution along the bunch which, because of the chromaticity, induces a spread in the betatron frequencies. An energy spread correlated with the longitudinal position is attainable with the external accelerating voltage, or with the wake fields.  $Dw_v$  DE

More general model including charge distribution and acceleration

$$\frac{\partial}{\partial s} \left[ \gamma(s) \frac{\partial y(z,s)}{\partial s} \right] + k_y^2(s) \gamma(s) y(z,s) = -\frac{e^2 N_p}{m_0 c^2 L_w} \int_z^\infty y(s,z') w_\perp(z'-z) \lambda(z') dz'$$

$$y(L_L) = y_m \sqrt{\frac{\gamma_i}{6\pi\gamma_f}} \eta^{-1/6} \exp\left[\frac{3\sqrt{3}}{4} \eta^{1/3}\right] \cos\left[k_y L_L - \frac{3}{4} \eta^{1/3} + \frac{\pi}{12}\right]$$

$$\eta = \frac{e^2 N_p}{k_y (dE_0 / ds)} \frac{w_{\perp 0}}{L_w} ln \left(\frac{\gamma_f}{\gamma_i}\right)$$

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Thomas P. Wangler



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