

# VNA measurements of 6mm buttons in button block

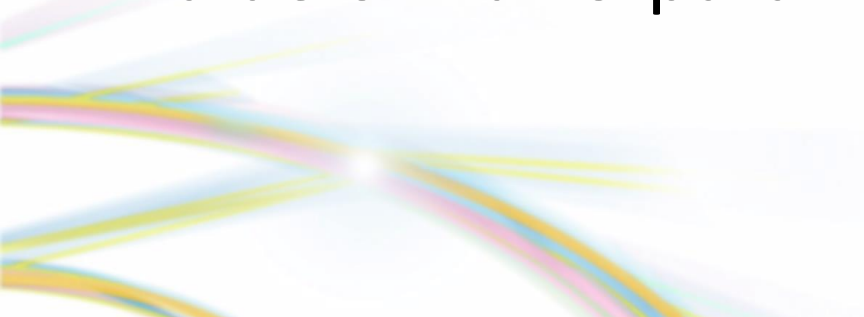
Guenther Rehm



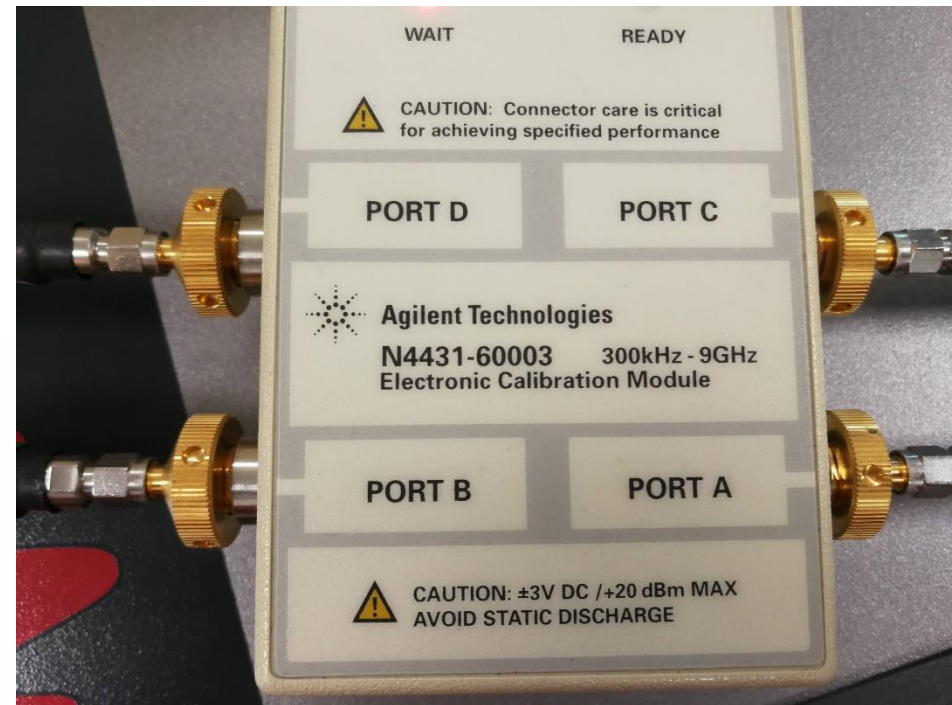
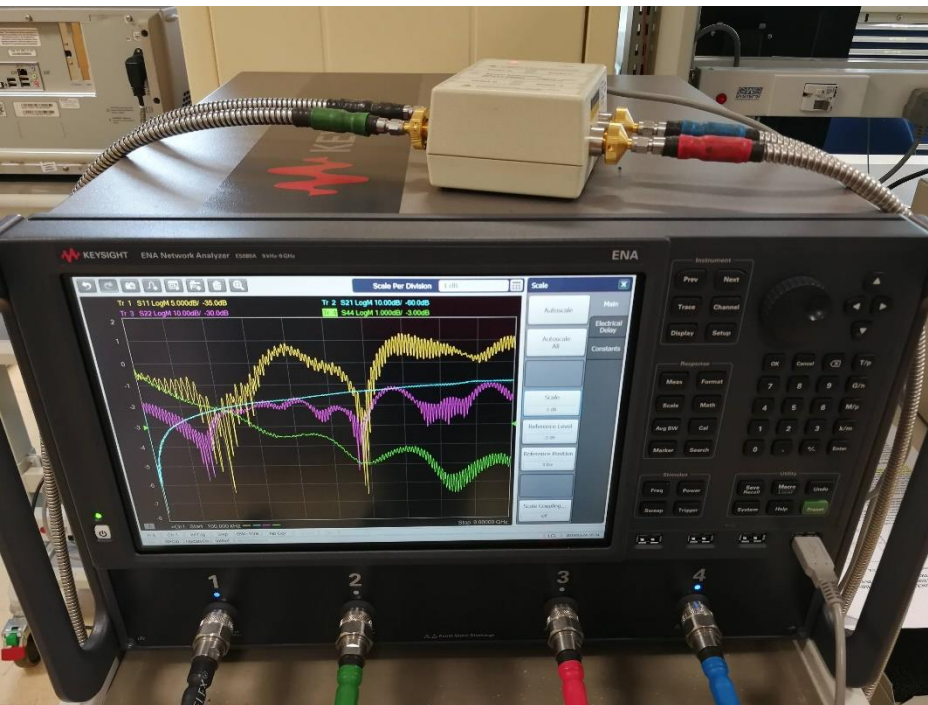
- Motivation
- Measurements
- Some initial statistics
- Conclusions



- Determine electrical centre of button block
- Goal is to use Lambertson method
- Choose classic tool: Vector Network Analyser
- How well can S params be measured @ -80dB?
  - Statistical errors
  - Systematic errors
  - Reproducibility
- Value of 'full S-parameter calibration'

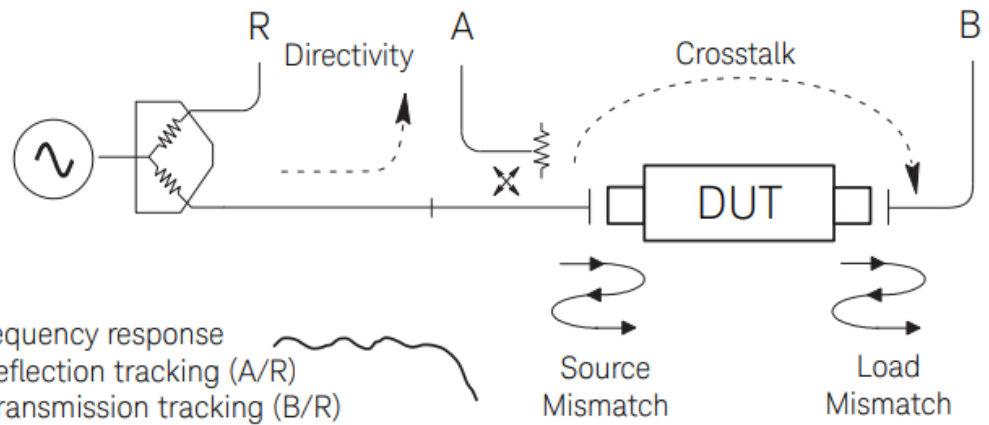


- Keysight E5080A 9kHz-9GHz 4-port VNA
  - Sweep 100kHz-9GHz
  - Power +15dBm
- N4431-60003 4 port electronic calibration unit



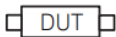
- Applying Error Correction to VNA Measurements

<http://literature.cdn.keysight.com/litweb/pdf/5965-7709E.pdf>



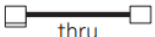
Frequency response  
 - reflection tracking (A/R)  
 - transmission tracking (B/R)

**UNCORRECTED**



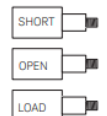
- Convenient  
 - Generally not accurate  
 - No errors removed

**RESPONSE**



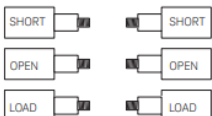
- Easy to perform  
 - Use when highest accuracy is not required  
 - Removes frequency response error

**ONE-PORT**



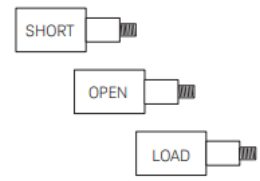
- For reflection measurements  
 - Need good termination for high accuracy with two-port devices  
 - Removes these errors:  
 Directivity  
 Source match  
 Reflection tracking

**FULL TWO-PORT**



- Highest accuracy  
 - Removes these errors:  
 Directivity  
 Source, load match  
 Reflection tracking  
 Transmission tracking  
 Crosstalk

Reflection	Test Set (cal type)	
	T/R (one-port)	S-parameter (two-port)
- Reflection tracking	✓	✓
- Directivity	✓	✓
- Source match	✓	✓
- Load match	✗	✓



✓ error can be corrected  
 ✗ error cannot be corrected

TRANSMISSION	Test Set (cal type)	
	T/R (response, isolation)	S-parameter (two-port)
- Transmission tracking	✓	✓
- Crosstalk	✓	✓
- Source match	✗	✓
- Load match	✗	✓

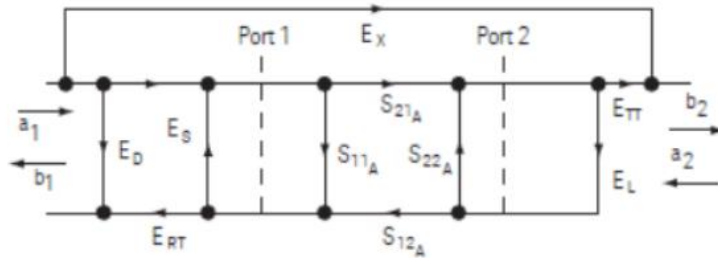
Other errors:  
 - Random (Noise, Repeatability)  
 - Drift

**ENHANCED-RESPONSE**

- Combines response and 1-port  
 - Corrects source match for transmission measurements

# 12-term Calibration

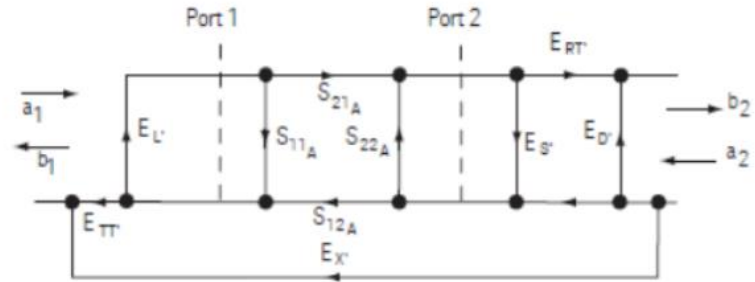
Forward model



- |                                     |                                       |
|-------------------------------------|---------------------------------------|
| $E_D$ = Fwd Directivity             | $E_L$ = Fwd Load Match                |
| $E_S$ = Fwd Source Match            | $E_{TT}$ = Fwd Transmission Tracking  |
| $E_{RT}$ = Fwd Reflection Tracking  | $E_X$ = Fwd Isolation                 |
| $E_{D'}$ = Rev Directivity          | $E_{L'}$ = Rev Load Match             |
| $E_{S'}$ = Rev Source Match         | $E_{TT'}$ = Rev Transmission Tracking |
| $E_{RT'}$ = Rev Reflection Tracking | $E_{X'}$ = Rev Isolation              |

- Notice that each actual S-parameter is a function of all four measured S-parameters
- Analyzer must make forward and reverse sweep to update any one S-parameter

Reverse model



$$S_{11a} = \frac{\left(\frac{S_{11m} - E_D}{E_{RT}}\right) \left(1 + \frac{S_{22m} - E_{D'}}{E_{RT'}} E_{S'}\right) - E_L \left(\frac{S_{21m} - E_X}{E_{TT}}\right) \left(\frac{S_{12m} - E_{X'}}{E_{TT'}}\right)}{\left(1 - \frac{S_{11m} - E_D}{E_{RT}} E_S\right) \left(1 + \frac{S_{22m} - E_{D'}}{E_{RT'}} E_{S'}\right) - E_L' E_L \left(\frac{S_{21m} - E_X}{E_{TT}}\right) \left(\frac{S_{12m} - E_{X'}}{E_{TT'}}\right)}$$

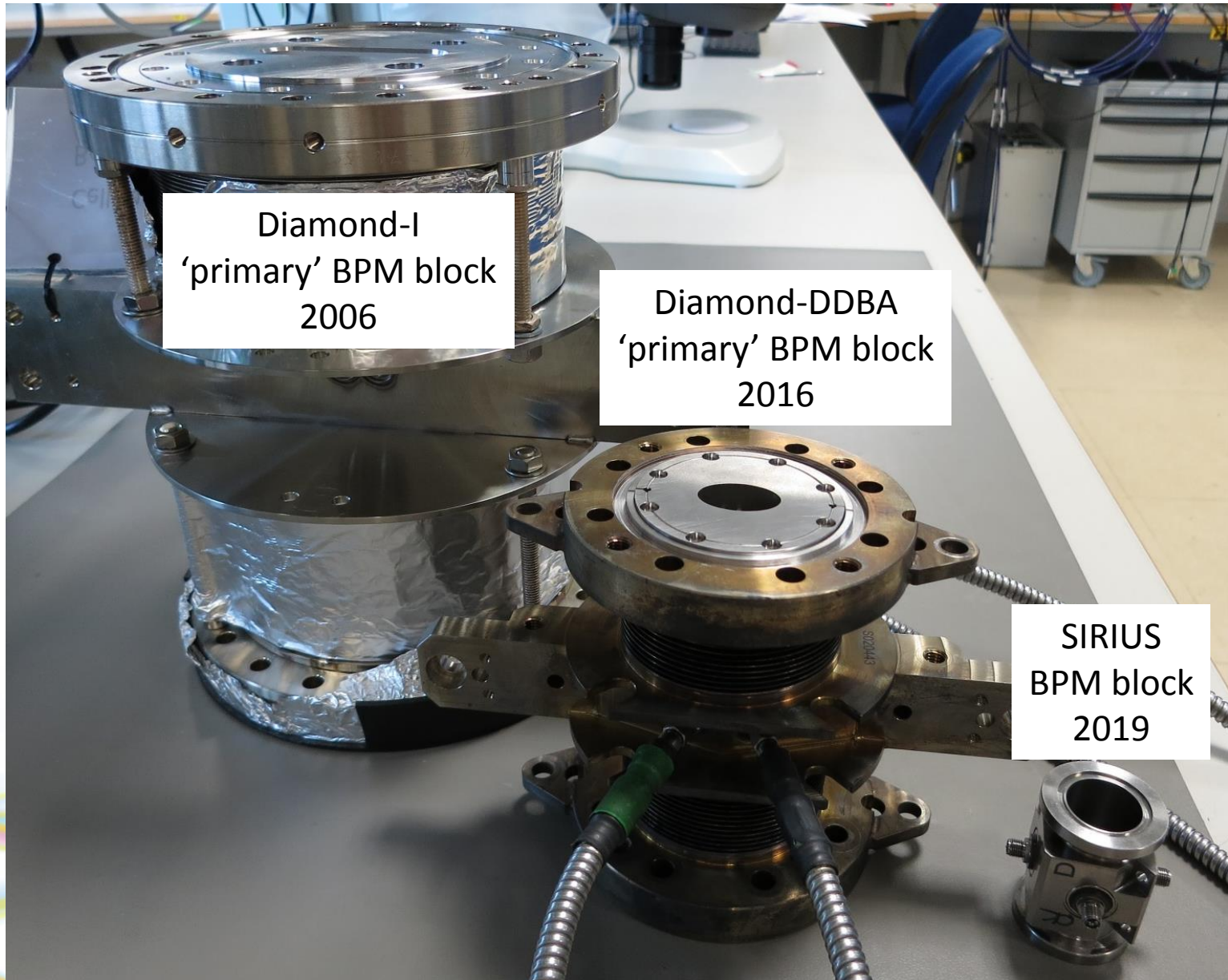
$$S_{21a} = \frac{\left(\frac{S_{21m} - E_X}{E_{TT}}\right) \left(1 + \frac{S_{22m} - E_{D'}}{E_{RT'}} (E_{S'} - E_L)\right)}{\left(1 - \frac{S_{11m} - E_D}{E_{RT}} E_S\right) \left(1 + \frac{S_{22m} - E_{D'}}{E_{RT'}} E_{S'}\right) - E_L' E_L \left(\frac{S_{21m} - E_X}{E_{TT}}\right) \left(\frac{S_{12m} - E_{X'}}{E_{TT'}}\right)}$$

$$S_{12a} = \frac{\left(\frac{S_{12m} - E_{X'}}{E_{TT'}}\right) \left(1 + \frac{S_{11m} - E_D}{E_{RT}} (E_S - E_L)\right)}{\left(1 - \frac{S_{11m} - E_D}{E_{RT}} E_S\right) \left(1 + \frac{S_{22m} - E_{D'}}{E_{RT'}} E_{S'}\right) - E_L' E_L \left(\frac{S_{21m} - E_X}{E_{TT}}\right) \left(\frac{S_{12m} - E_{X'}}{E_{TT'}}\right)}$$

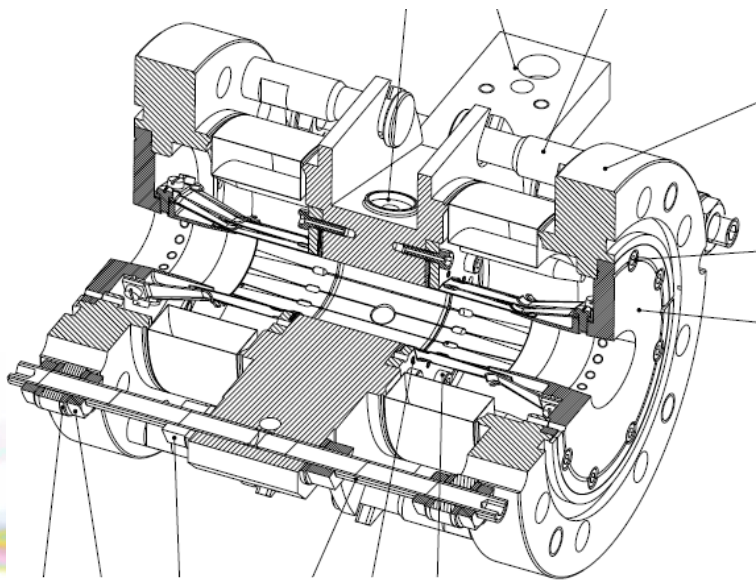
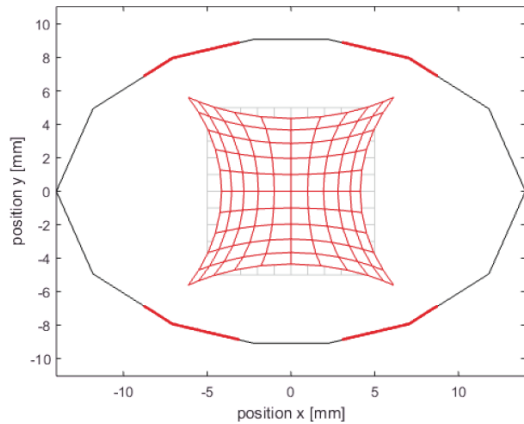
$$S_{22a} = \frac{\left(\frac{S_{22m} - E_{D'}}{E_{RT'}}\right) \left(1 + \frac{S_{11m} - E_D}{E_{RT}} E_S\right) - E_L' \left(\frac{S_{21m} - E_X}{E_{TT}}\right) \left(\frac{S_{12m} - E_{X'}}{E_{TT'}}\right)}{\left(1 - \frac{S_{11m} - E_D}{E_{RT}} E_S\right) \left(1 + \frac{S_{22m} - E_{D'}}{E_{RT'}} E_{S'}\right) - E_L' E_L \left(\frac{S_{21m} - E_X}{E_{TT}}\right) \left(\frac{S_{12m} - E_{X'}}{E_{TT'}}\right)}$$

This is just for two ports, with four ports this get even more complicated!

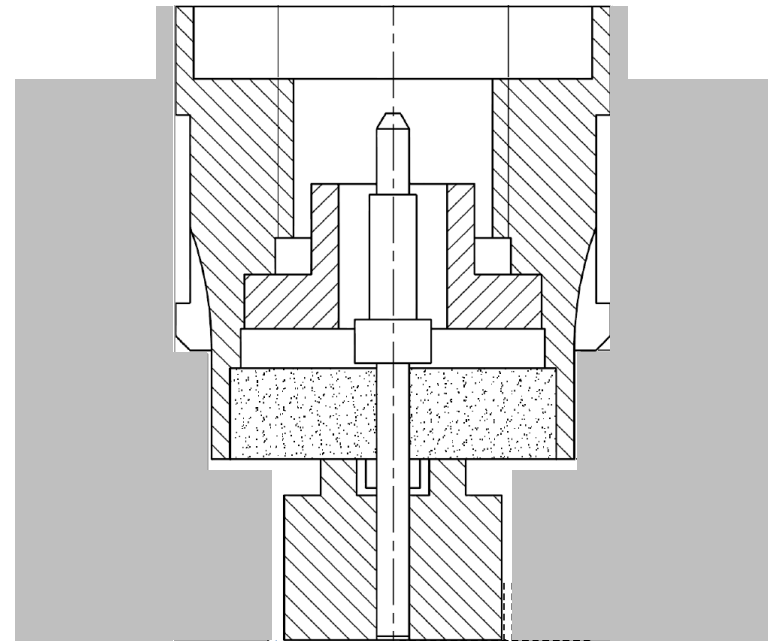




26mm wide, 18mm high



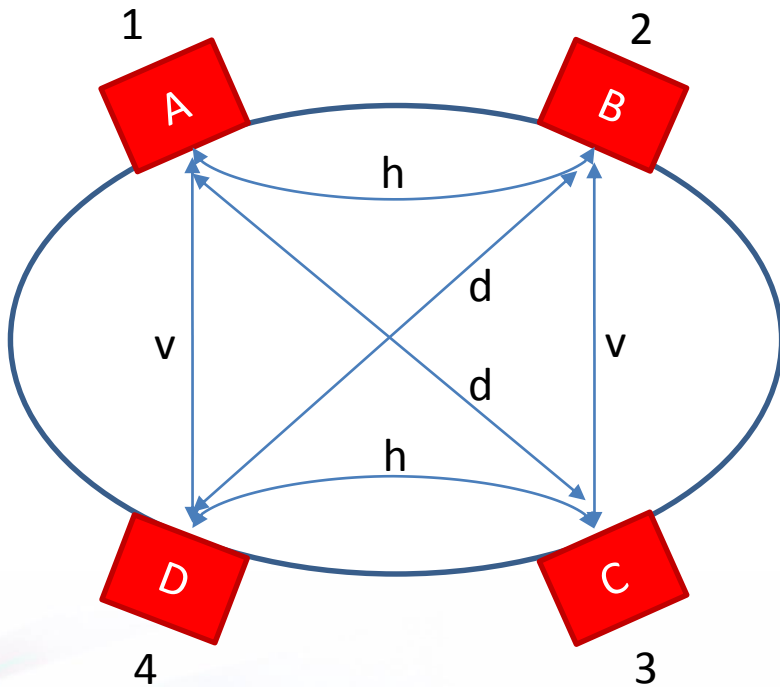
DDBA button is equivalent to  
ESRF-EBS 6mm button  
(but with Moly button not 316LN)



0.3mm gap between  
button and hole

*Drawing courtesy FMB Berlin*





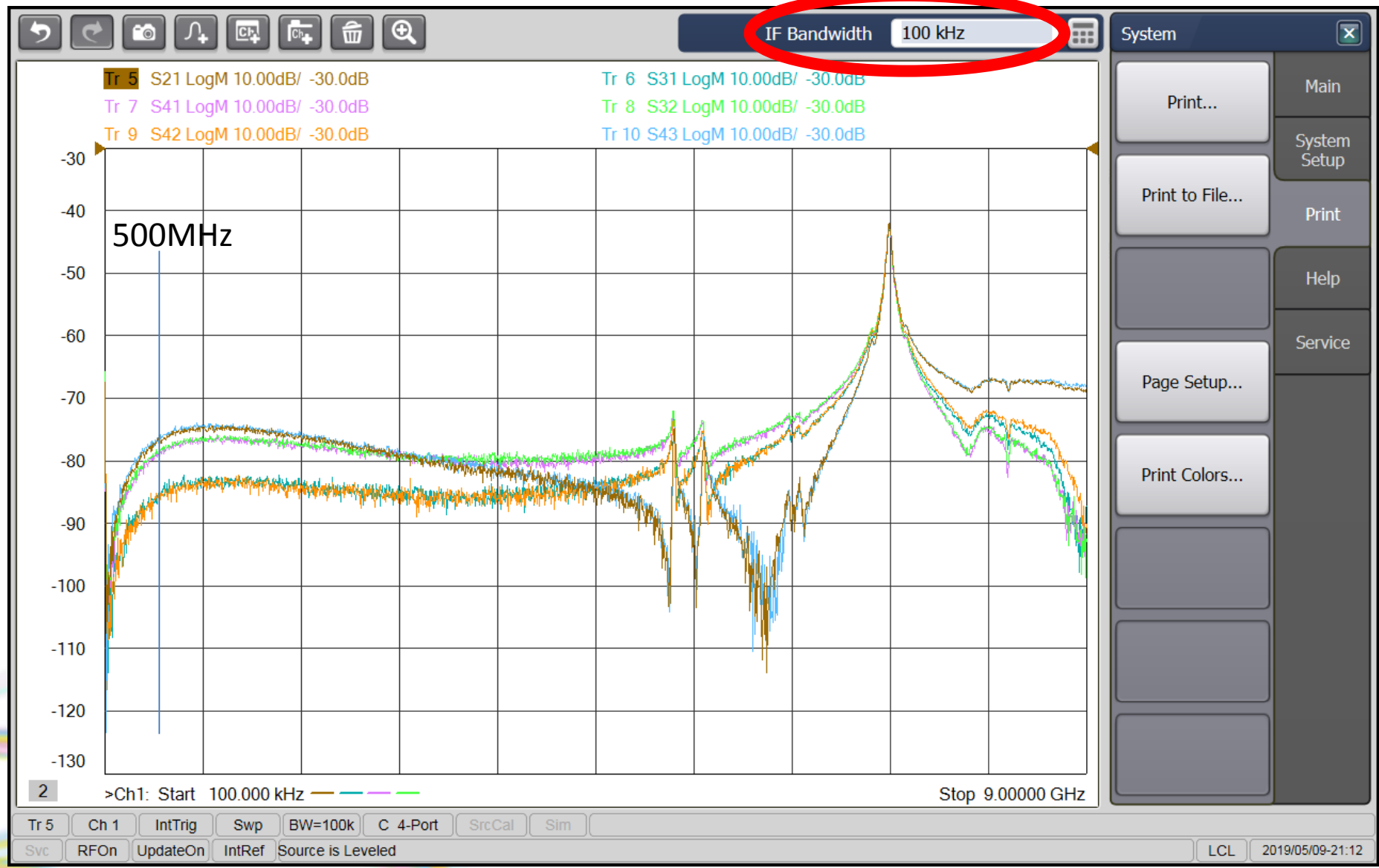
$$S_{21} = AhB$$

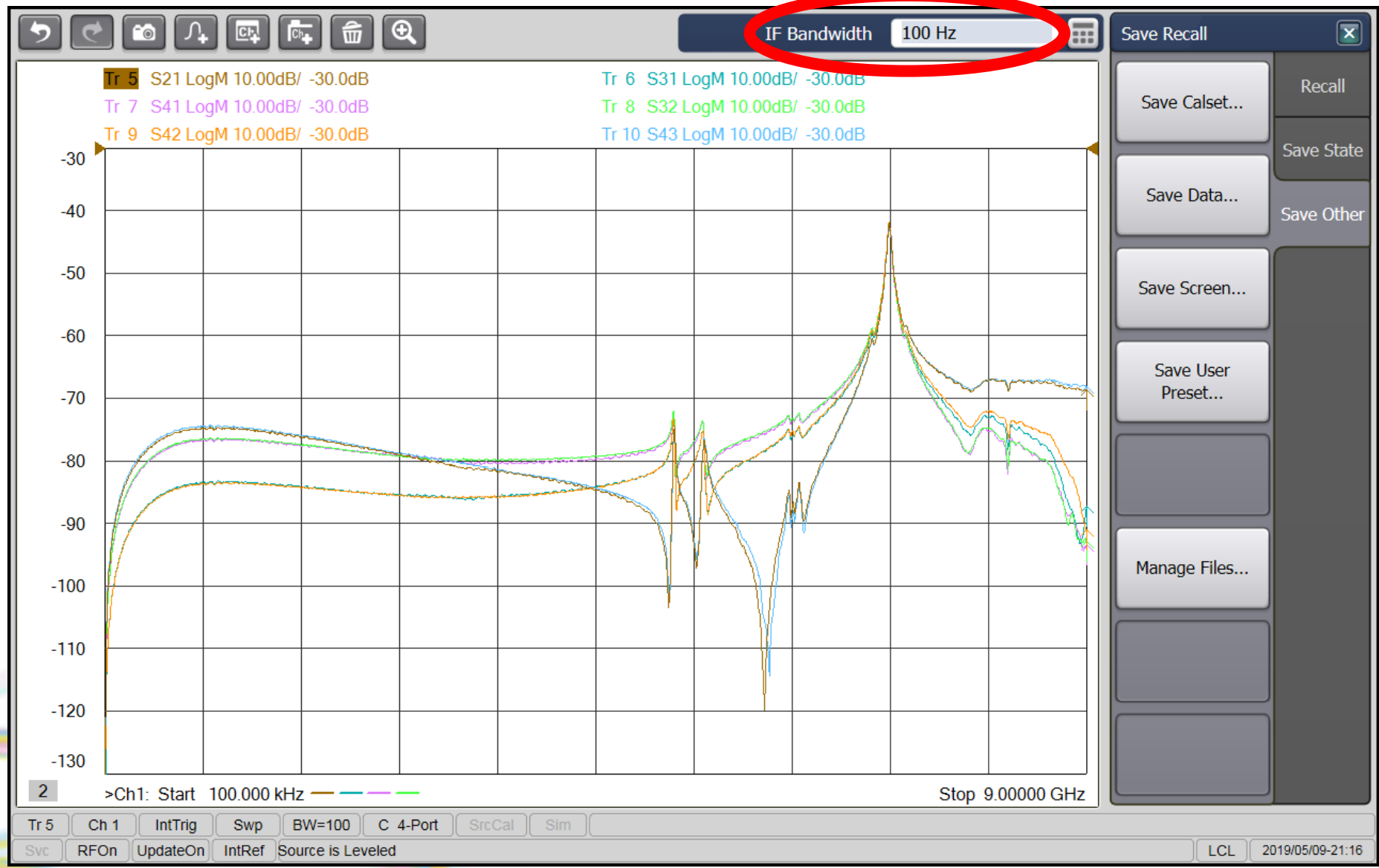
$$S_{42} = BdD$$

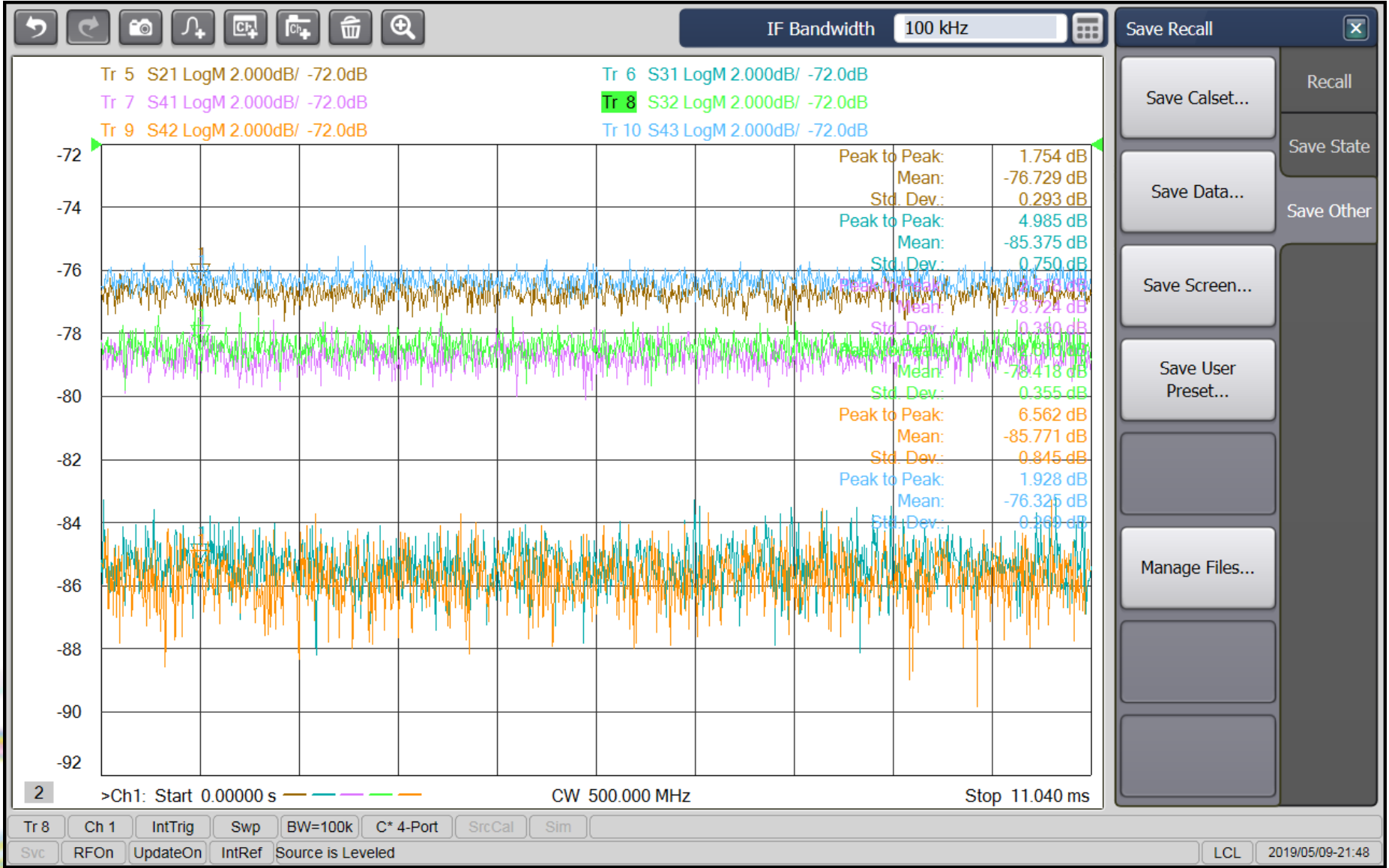
$$S_{14} = DvA$$

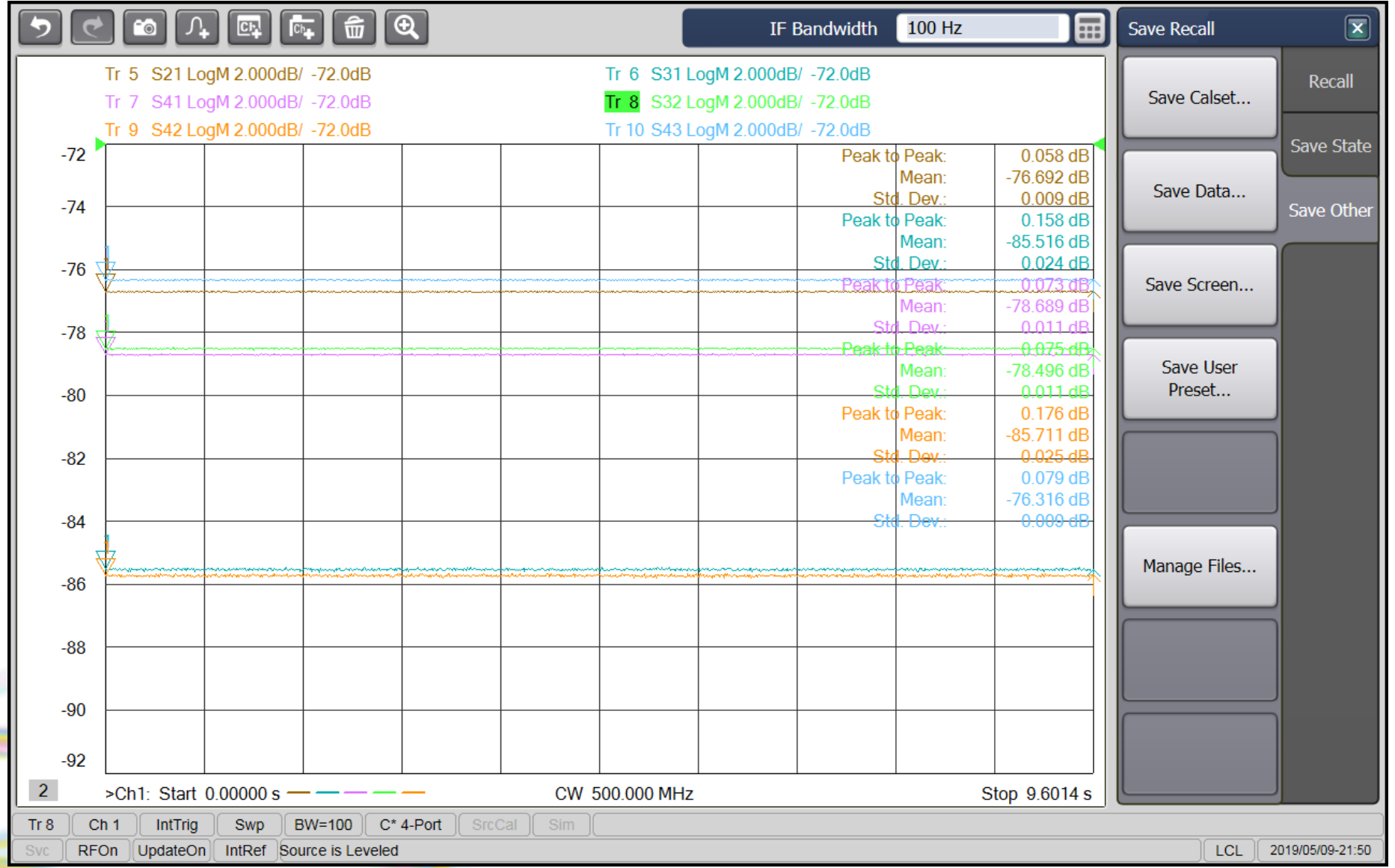
$$\frac{S_{21}S_{14}}{S_{42}} = \frac{AB * DA hv}{BD d} = A^2 * c_1$$

- Repeat for other buttons
- Repeat with other equations for other Lambertson types

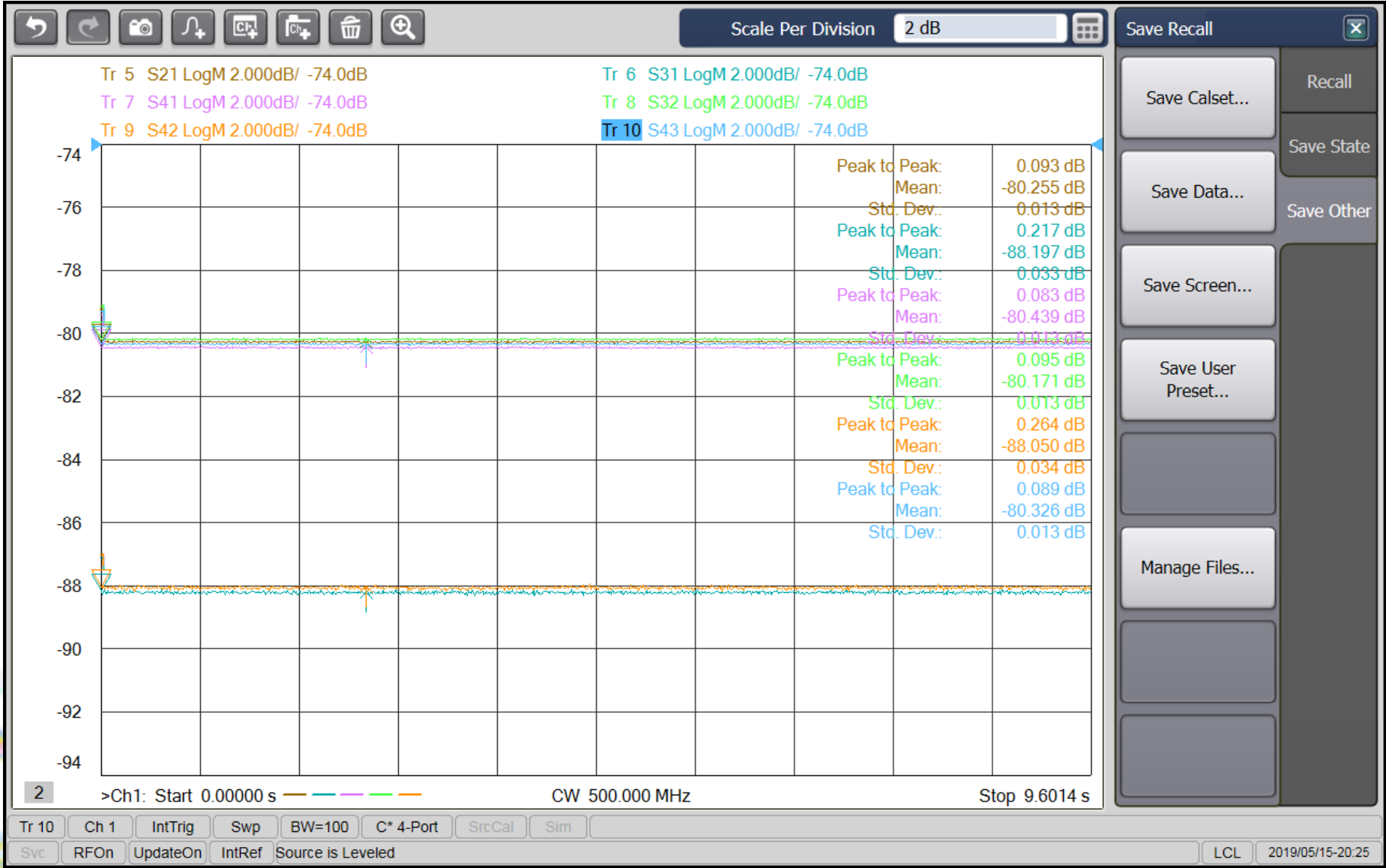












- Convert S-parameters to linear gains and XY offsets in matlab:

```
S = abs(sparameters(filename).Parameters);  
gains = sqrt(squeeze([S(2,1,:).*S(1,4,:)./S(4,2,:)...  
    S(2,1,:).*S(3,2,:)./S(3,1,:)...  
    S(3,2,:).*S(4,3,:)./S(4,2,:)...  
    S(1,4,:).*S(4,3,:)./S(3,1,:)]));  
xy = 7000*([-1 1 1 -1;1 1 -1 -1]*gains)./ repmat(sum(gains),2,1);
```

- Calculate statistics for all three cases
- Compare
  - measurement
  - measurement one day later (not disconnected)
  - three back-to-back measurements
  - disconnect and re-connect

All offset calculated for scale factor 7mm and displayed in  $\mu\text{m}$

	Day1	Day2-1 <sup>st</sup>	Day2-2 <sup>nd</sup>	Day2-3 <sup>rd</sup>	Day2-remade
X1 $\pm$ 1 $\sigma$	42.4 +/- 3.1	42.8 +/- 3.1	42.8 +/- 3.1	42.8 +/- 3.1	40.5 +/- 3.1
Y1 $\pm$ 1 $\sigma$	-67.7 +/- 2.4	-67.4 +/- 2.3	-67.3 +/- 2.5	-67.5 +/- 2.5	-79.6 +/- 2.5
X2 $\pm$ 1 $\sigma$	41.5 +/- 3.4	42.7 +/- 3.3	42.8 +/- 3.3	42.7 +/- 3.3	40.5 +/- 3.4
Y2 $\pm$ 1 $\sigma$	-66.8 +/- 2.1	-67.3 +/- 2.0	-67.2 +/- 2.2	-67.3 +/- 2.1	-79.5 +/- 2.2
X3 $\pm$ 1 $\sigma$	41.8 +/- 2.7	42.8 +/- 2.7	42.8 +/- 2.7	42.9 +/- 2.7	40.4 +/- 2.7
Y3 $\pm$ 1 $\sigma$	-67.1 +/- 2.8	-67.4 +/- 2.8	-67.2 +/- 3.0	-67.5 +/- 3.0	-79.5 +/- 3.0



- VNA:
  - Can measure with sufficient resolution
  - Reproducibility excellent
  - Reconnections produce larger deviations
- Lambertson:
  - Anybody who has the original paper, please forward
  - Presumably it requires symmetry in the geometry
  - Do the different types tell us something about symmetry?
- Real BPM:
  - Not well matched ports will read differently
  - Cables and connectors will change readings again
- Bluesky:
  - Could we add Lambertson like test into BPM?
  - Is there value in determining the button capacitance from time domain transformed  $S_{nn}$  –sweep, would that give comparable button gain?