

# $^3\text{He}$ - $^4\text{He}$ Dilution Refrigeration in Space

cooling detectors to study the universe ...

Gerard Vermeulen

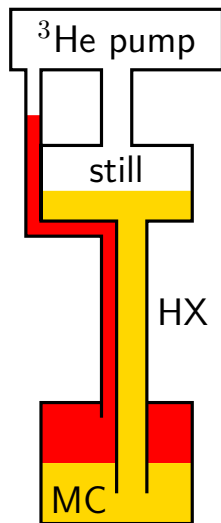
Néel Institute (CNRS)

EASISCHOOL, Grenoble, 2019-10-03

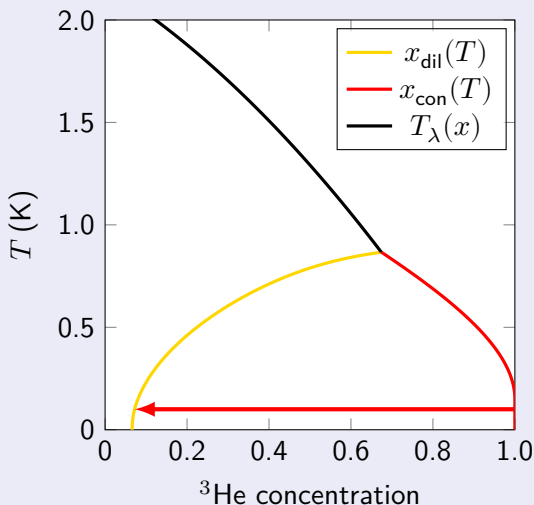
# Outline

- 1 Introduction: dilution refrigeration and gravity
- 2 1st Idea: Open Cycle Dilution Refrigerator for Space
- 3 2nd Idea: Closed Cycle Dilution Refrigerator for Space
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- 5 LiteBIRD: Cooling Chain Integration Example
- 6 Status and concluding remarks

# Gravity and dilution refrigeration on earth



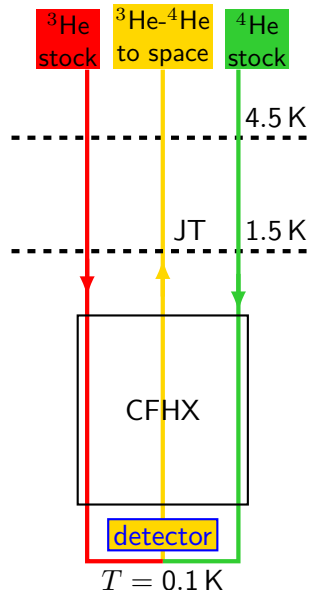
## Normal $^3\text{He}$ - $^4\text{He}$ dilution refrigeration



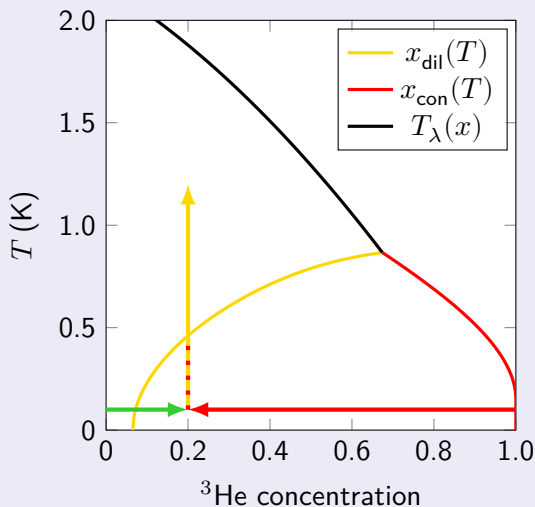
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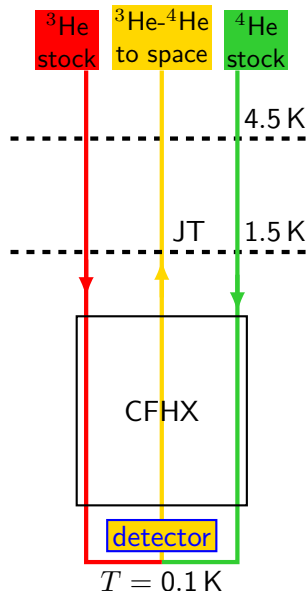
# Open cycle dilution refrigerator for space?



## Planck's OCDR



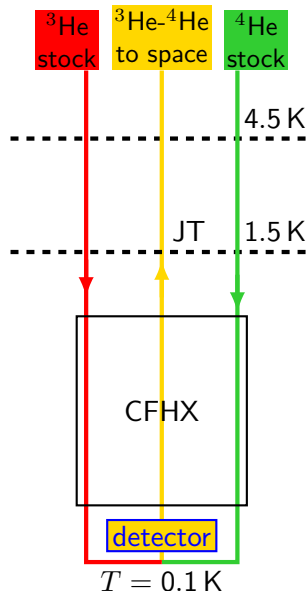
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## Planck's OCFR

- pre-cooler heat lift specs 10 mW @ 4.5 K
- $^3\text{He}$  and  $^4\text{He}$  stocked on satellite
- space plays role of pump
- capillary forces play role of gravity
  - ingeniously simple solution to zero gravity problems in space
- intrinsic 1.5 K Joule-Thompson cooler
- 100% duty cycle

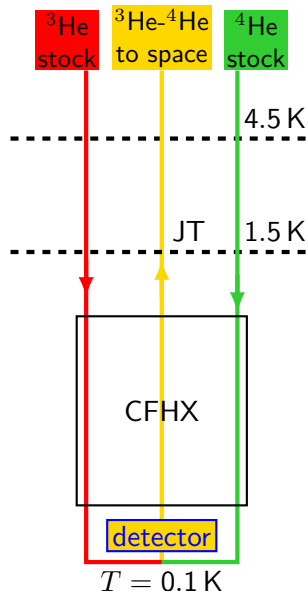
# Open cycle dilution refrigerator for space?



## Planck's OCDR

- cooling power:  $0.2\text{ }\mu\text{W}$  @  $0.1\text{ K}$
- lifetime: 2.5 years
- helium flowrates:
  - $^3\text{He}$   $6\text{ }\mu\text{mol s}^{-1}$
  - $^4\text{He}$   $18\text{ }\mu\text{mol s}^{-1}$
- high pressure storage on satellite:
  - $^3\text{He}$   $12\text{ m}^3$  STP or 9 M\$ now
  - $^4\text{He}$   $36\text{ m}^3$  STP

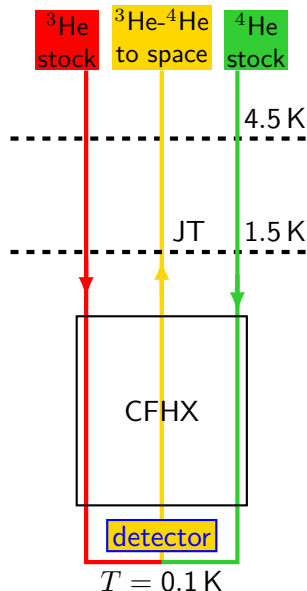
# Open cycle dilution refrigerator for space?



## 2020–2025: future missions

- cooling power:  $1\ \mu\text{W}$  @ 50 mK
  - X-IFU:  $0.8\ \mu\text{W}$  @ 50 mK
- lifetime: 5 years
- helium flowrates:
  - $^3\text{He}$   $18\ \mu\text{mol s}^{-1}$
  - $^4\text{He}$   $360\ \mu\text{mol s}^{-1}$
- high pressure storage on satellite:
  - $^3\text{He}$   $90\ \text{m}^3$  STP or 70 M\$ now
  - $^4\text{He}$   $1800\ \text{m}^3$  STP

# Open cycle dilution refrigerator for space?



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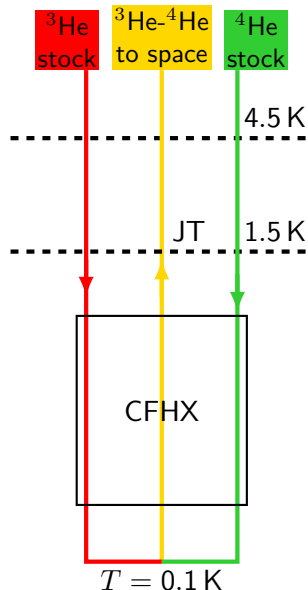
Too heavy and too costly ...

- $\Rightarrow$  closed cycle is required

# Outline

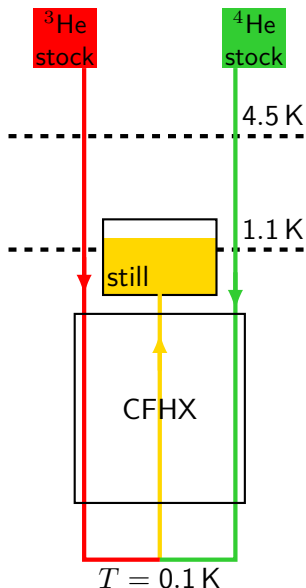
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# Closed cycle dilution refrigerator for space?



OCDR  $\Rightarrow$  CCDR  $\Rightarrow$  zero gravity on earth?

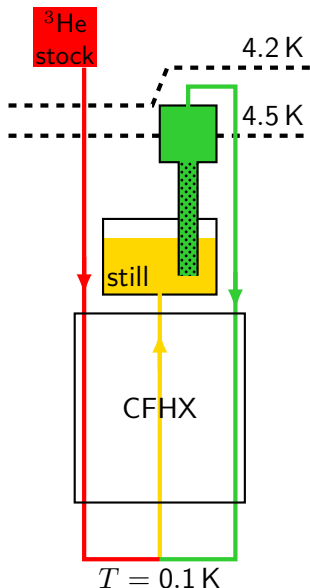
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  - liquid-vapor interface in zero gravity?

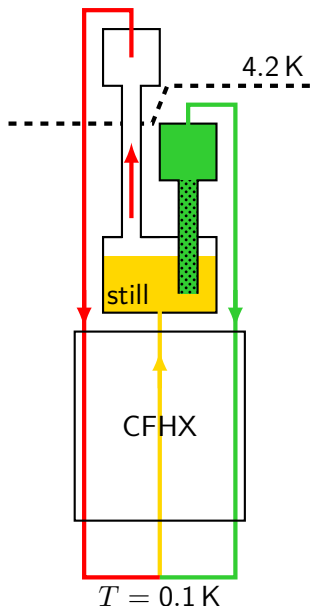
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  - ②  $^4\text{He}$  circulation: fountain pump
    - $3.5 \text{ mW @ } 2.1 \text{ K} \Rightarrow (0.1 - 0.4) \text{ mmol s}^{-1}$
- very well understood
  - tune  $^4\text{He}$  flow rate by a factor 0.5–2

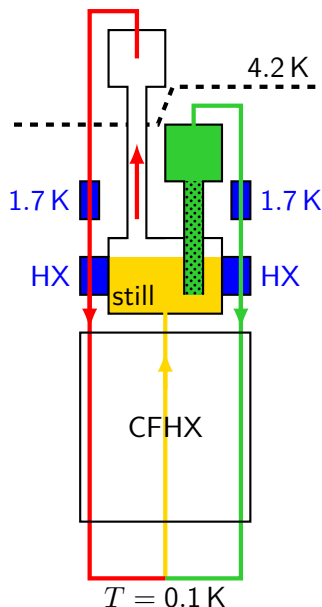
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  - ③  $^3\text{He}$  circulation: pump development
    - $\dot{n}_3 = (20 - 60) \mu\text{mol s}^{-1}$  at  $p_{\text{still}} = (0.3 - 15) \text{ mbar}$
    - determine  $^3\text{He}$  pump specs
- trade-off between 2 and 3
  - collaboration with JAXA for pump: discussion since 2009 and test with JAXA pump in 2015

# Closed cycle dilution refrigerator for space?

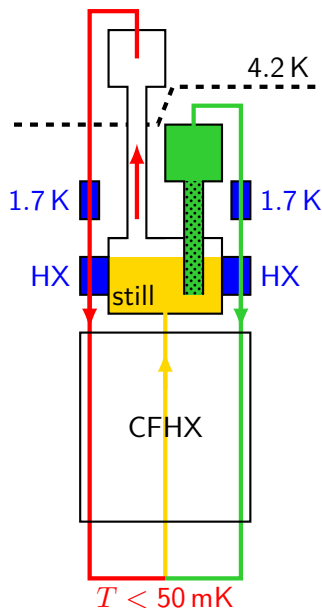


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- ④ pre-cooling (JAXA SPICA compatible)
  - heat load  $\approx 5\text{ mW}$  at  $T = 1.7\text{ K}$

- JAXA pre-cooler is most suitable available
- lower  $T$  is better for 1, 2, 3

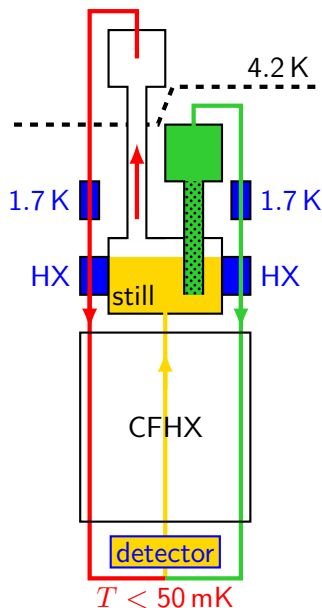
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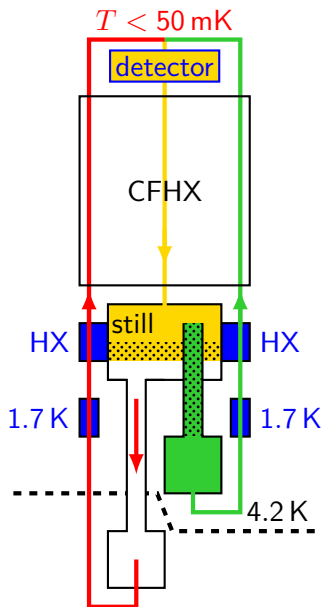
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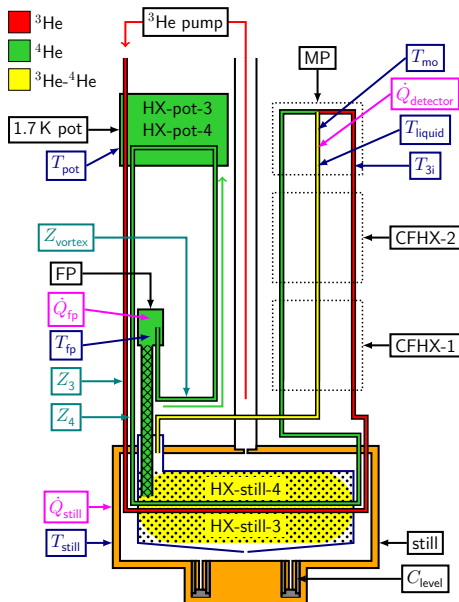
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- ⑥ optimize detector simulator
- ⑦ no zero gravity on earth
  - upside-down or negative gravity

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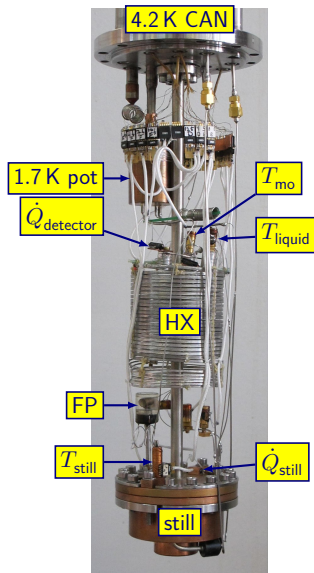
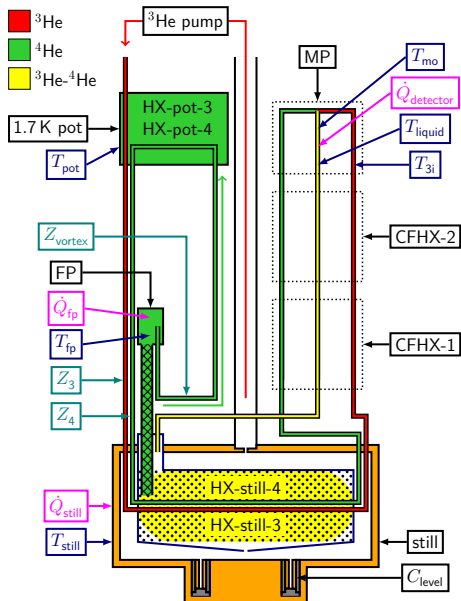
## Negative (not Zero) Gravity CCDR (NG-CCDR)



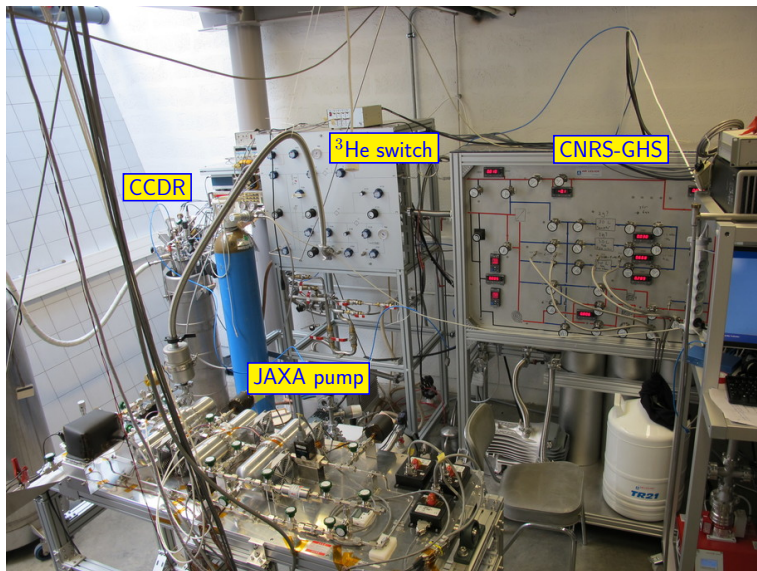
## Upside-down CCDR setup

- sponge confines liquid in still
- capacitance liquid level gauge to detect leaking liquid
- $^3\text{He}$  pump circulates  $^3\text{He}$  gas from sponge to 1.7 K pot (e.g. SPICA) and MP
- fountain pump circulates  $^4\text{He}$  liquid from sponge to 1.7 K pot and MP
- $^3\text{He}$ - $^4\text{He}$  mixture returns from MP to still

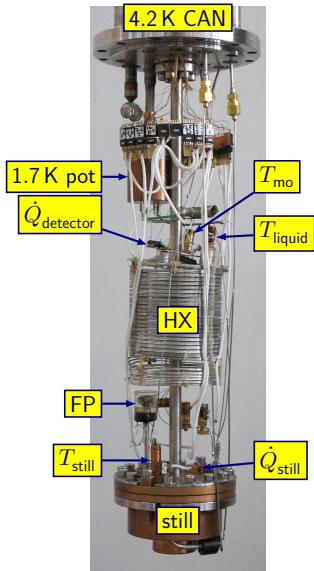
# Negative (not Zero) Gravity CCDDR (NG-CCDDR)



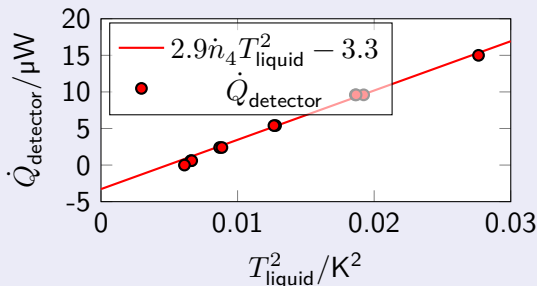
# Upside-down CCDR with JAXA $^3\text{He}$ circulator



# Upside-down CCDR with JAXA $^3\text{He}$ circulation pump



## Cooling power result



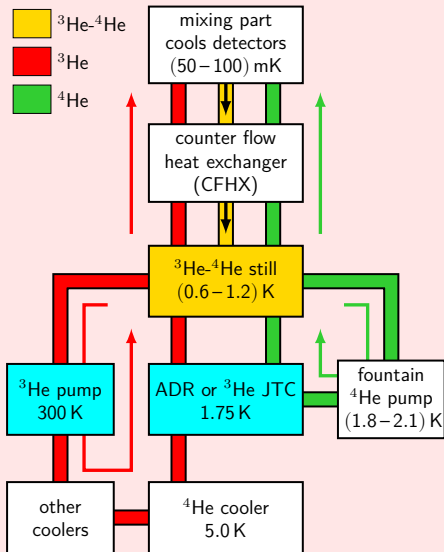
- $\dot{Q}_{\text{detector}} = A \dot{n}_4 T_{\text{liquid}}^2 - \dot{Q}_{\text{leak}}$ 
  - $\dot{n}_4 = 235 \mu\text{mol s}^{-1}$  fountain pump physics
  - $A = 2.9 \text{ J mol}^{-1} \text{ K}^2$  OK with “theory”
- conclusion
  - $3.5 \mu\text{W}$  @  $0.1 \text{ K}$  with  $\dot{Q}_{\text{leak}} = 3.3 \mu\text{W}$
  - if  $\dot{Q}_{\text{leak}} \approx 1 \mu\text{W}$ : OK for today missions

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# Closed cycle dilution refrigerator in simplified cooling chain

## cooling power budget

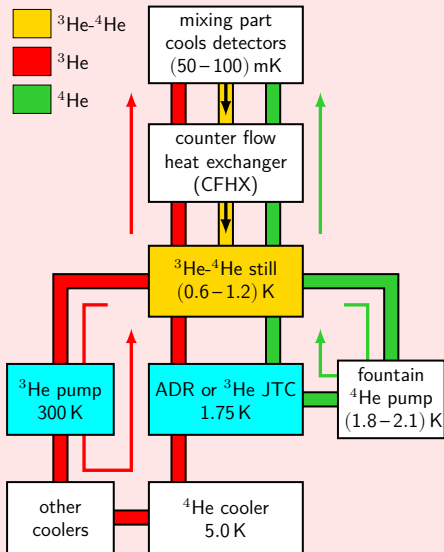


## thermal-mechanical design issues

- CFHX and mixing part tuning
  - $\dot{Q}_{\text{lift}} \propto ^4\text{He}$  and  $^3\text{He}$  circulation rates  $\dot{n}_4$  and  $\dot{n}_3$
- direct CCDD interfaces:
  - $^3\text{He}$  circulation pump
  - $^3\text{He}$  Joule-Thompson (JTC)
- $^4\text{He}$  circulation  $\dot{Q}_{\text{load}}$  on
  - ADR or  $^3\text{He}$  JTC
  - lower  $T_{\text{still}}$  implies lower  $\dot{Q}_{\text{load}}$
- $^3\text{He}$  circulation  $\dot{Q}_{\text{load}}$  on
  - other coolers
  - $^4\text{He}$  cooler
  - ADR or  $^3\text{He}$  JTC
- CCDD support struts and links to focal plane (launch)

# Closed cycle dilution refrigerator in simplified cooling chain

## cooling power budget



## model CFHX and mixing part

- 1 flows of enthalpy
  - $^3\text{He}$  and  $^3\text{He}$ - $^4\text{He}$  thermo
- 2 heat exchange (Kapitza)
- 3 laminar + turbulent heating
- 4 heat loads
  - instrument (focal plane)
  - CCDR support structure

## model $^3\text{He}$ - $^4\text{He}$ still

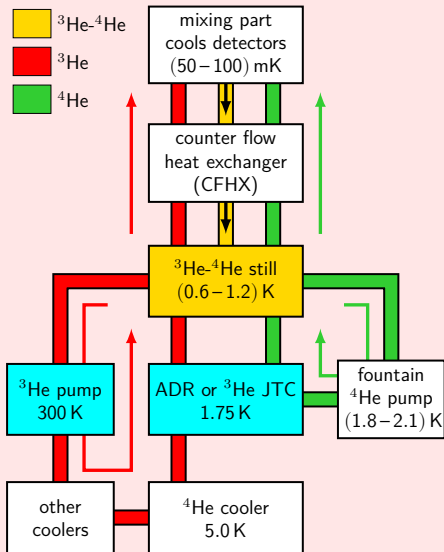
- 1 flows of enthalpy including
  - $^4\text{He}$  demixing heat  $< 0$
  - $^3\text{He}$  evaporation heat  $> 0$

## model fountain pump

- 1 depends on  $T_{\text{still}}$  or  $p_{\text{still}}$

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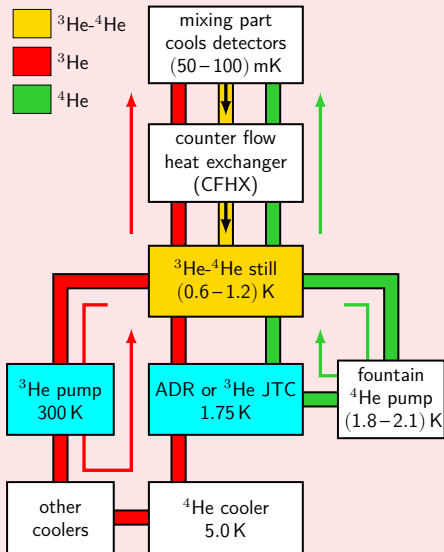


## LiteBIRD context

- ✓ tuning of CFHX and mixer part:  
 $\dot{n}_4 = 210 \mu\text{mol s}^{-1}$  &  
 $\dot{n}_3 = 30 \mu\text{mol s}^{-1}$  give  
 $40.0 \mu\text{W @ 0.3 K}$  &  
 $4.0 \mu\text{W @ 0.1 K}$  or  $7.0 \mu\text{W}$  with  
new tested mixing chamber
- ✓ within JAXA  $^3\text{He}$  pump specs
- ✓ 1.56 mW load on 5.0 K
- 👉 2.40 mW load on 1.75 K
  - 2.5× too high for ADR
- ✗ so far no way without 1.75 K

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- 👉 2.40 mW load on 1.75 K
  - $2.5\times$  too high for ADR
- ✗ so far no way without 1.75 K

## but, due to JAXA budget cuts

- no JAXA  $^3\text{He}$  JTC
- no JAXA  $^3\text{He}$  circulation pump

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# Status and conclusion

## Status

- we work on a DM (demonstration model) and with the IAS on an EM (engineering model)
- we want an European or French mechanical  $^3\text{He}$  circulation pump

## Comparing ADR and CCDR ...

- ideal ADR cycle is a Carnot cycle and a CCDR is less efficient
  - CCDR heat load on 1.75 K is  $2.5\times$  higher than that of LiteBIRD's continuous ADR
- LiteBIRD's continuous ADR weighs  $\approx 20$  kg, CCDR DM  $\approx 6$  kg, and CCDR EM  $\approx 3$  kg (IAS, design goal)
  - weight below 4 K has a much bigger negative system impact than weight at 300 K, since stronger implies more conductive heat loads
- TRL of ADR is higher than of CCDR

# Thank you and thanks to

Ariel Haziot (post-doc), Sébastien Triqueneaux (Air Liquide, CNRS), Pierre-Frédéric Sibeud (CNRS), Alain Benoit (CNRS), Philippe Camus (CNRS), Angela Volpe (Ph. D.), Gunaranjan Chaudhry (post-doc), Florian Martin (Ph. D.), Yan Pennec (Air Liquide), Sylvain Martin (Air Liquide, CEA), Thierry Tirolien (CNES, ESA), Jérôme André (CNES), Stéphane d'Escrivan (CNES), **Keisuke Shinozaki (JAXA)**, **Kenichiro Sawada (JAXA)**, **Institute d'Astrophysique Spatiale**, Néel Institute technical services