



# Nb<sub>3</sub>Sn RRP 108 Wire Beam Impact Damage Study

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Supervisor: Andreas Will

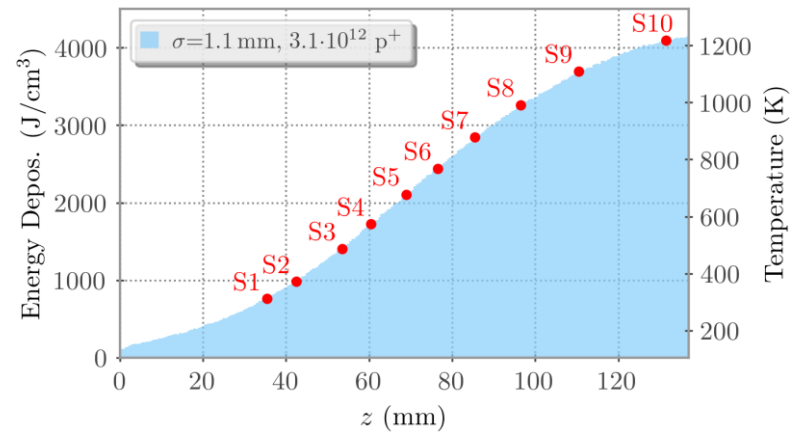
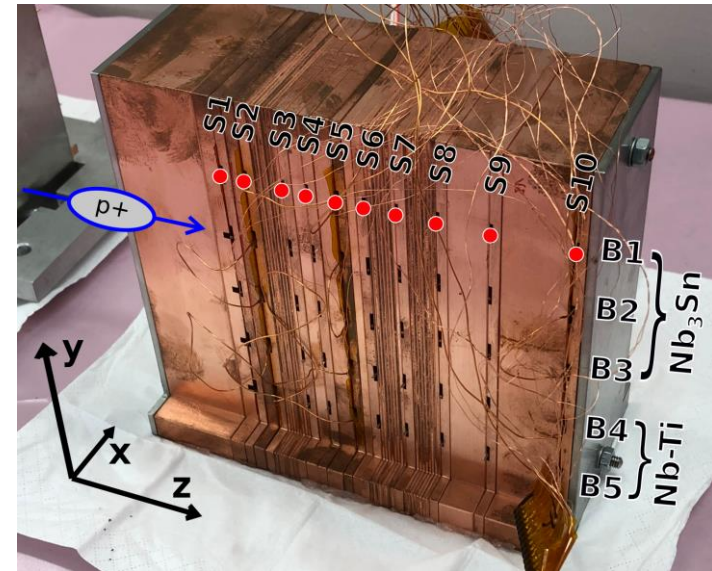
Daniel Wollmann

# What I want to talk about

- A brief reminder of what we work on
- Simulation Workflow
- Results
- Summary

# A brief reminder of what we work on

## Beam Impact studies on Superconductor Strands at 4K

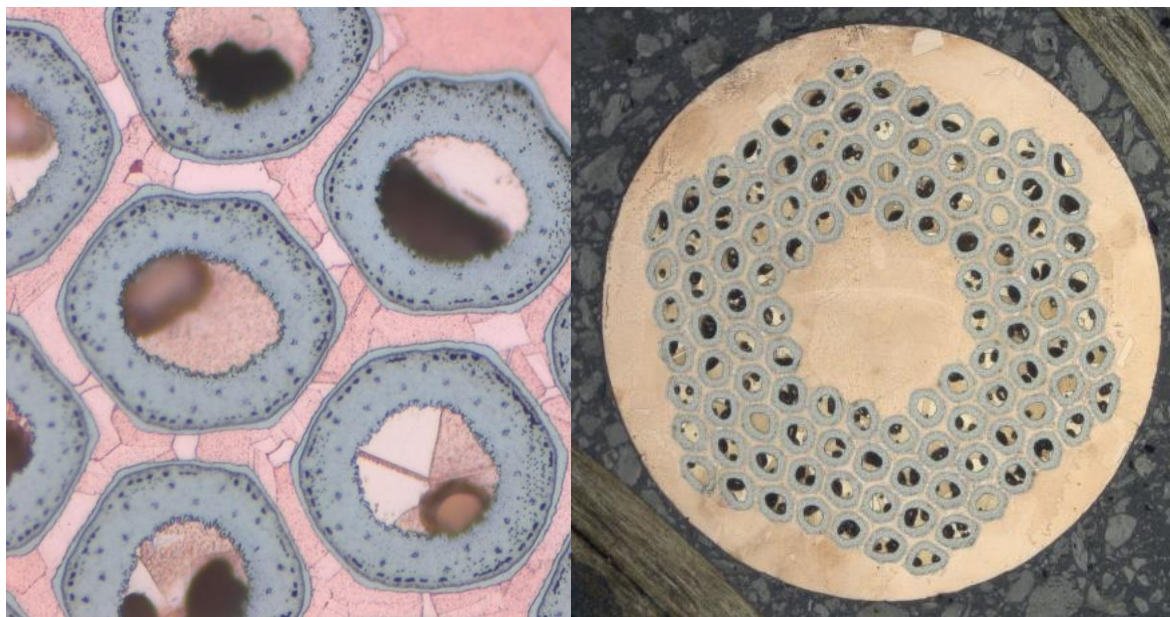


# A brief reminder of what we work on

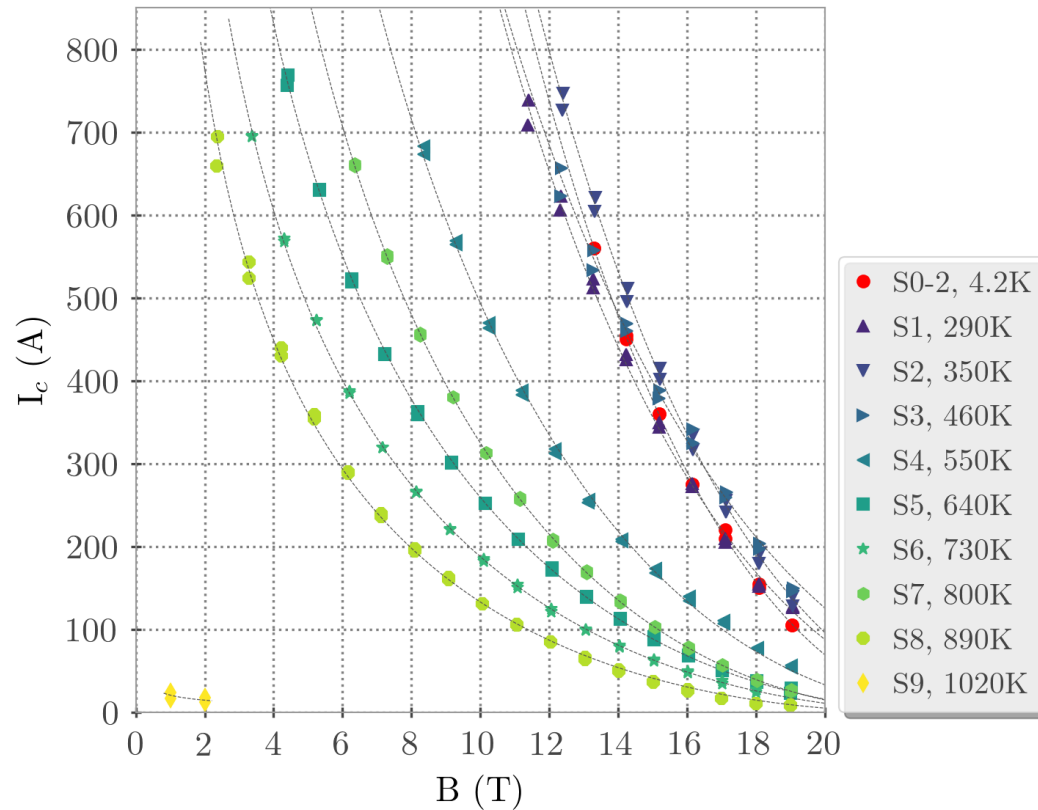
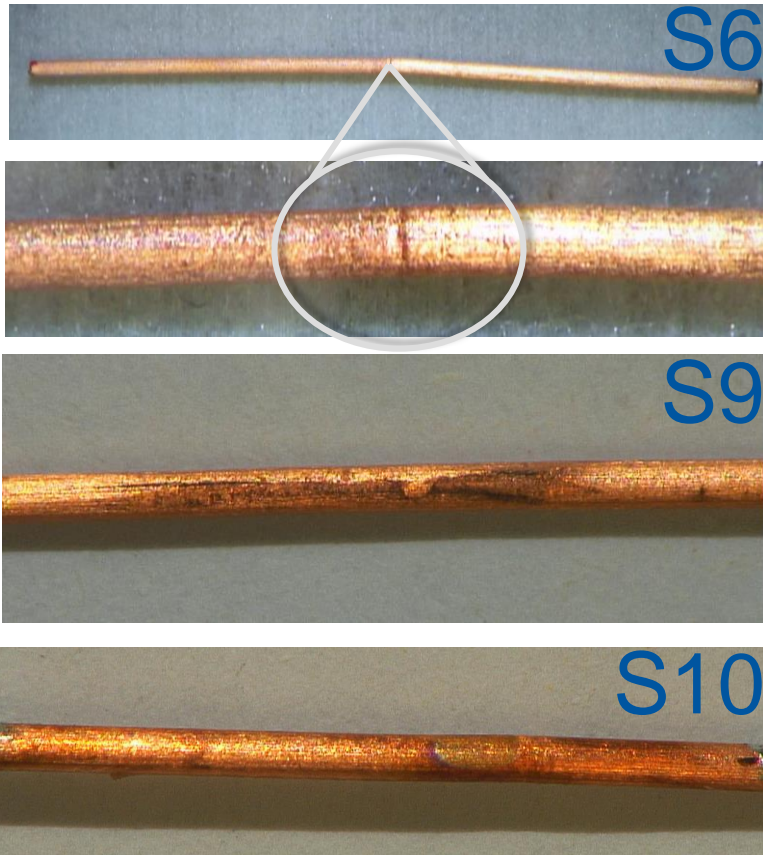
My work focused on:

$\text{Nb}_3\text{Sn}$  strand (HL-LHC)

50 mm,  $\varnothing$  0.85 mm



# A brief reminder of what we work on



# Simulating the Impact



# The general idea / workflow pipe



Energy Deposition



Thermal Evolution



Mechanical response



Theory based Evaluation

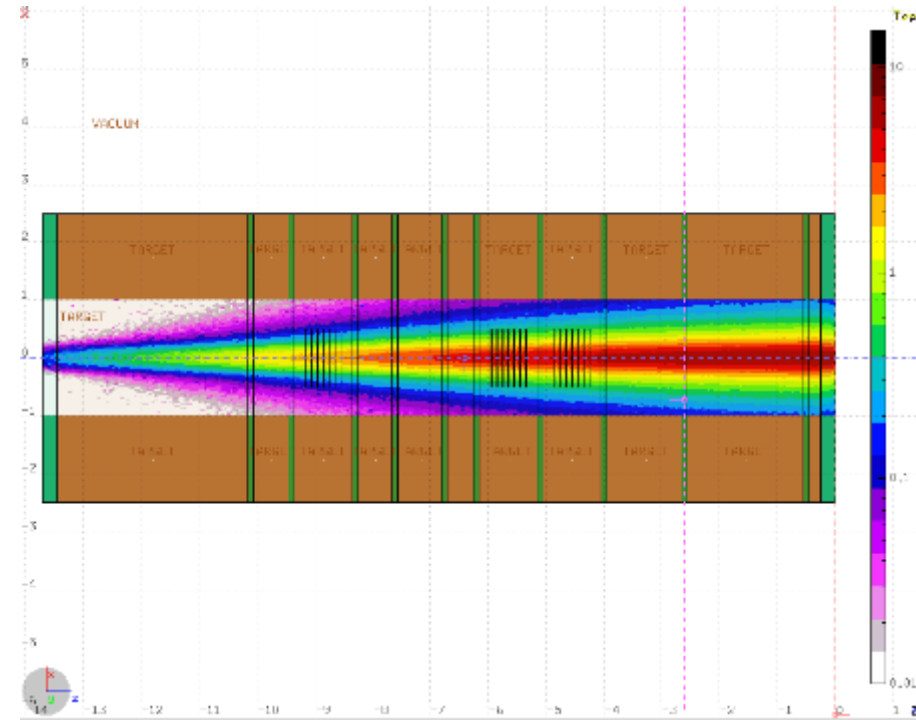


# Energy Deposition

Generating a probabilistic  
Energy Deposition Map  
per Primary Particle

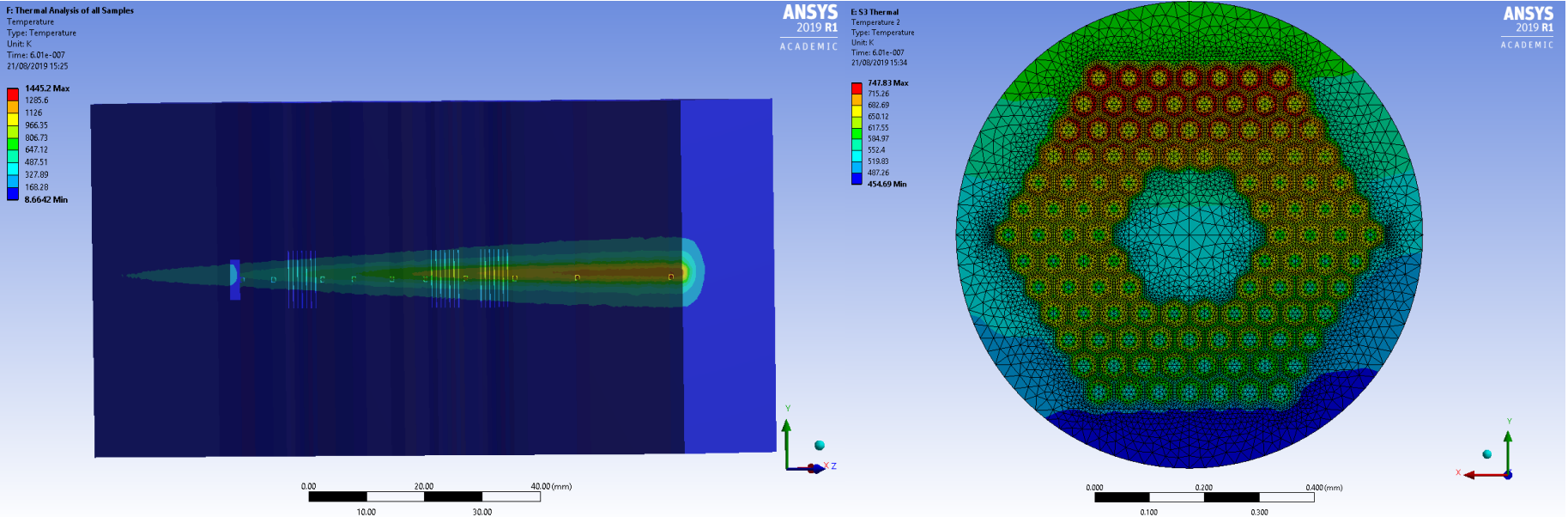


Scaling the Energy with the  
Beam Signature to get an  
on/off heating Rate



FLUKA Model

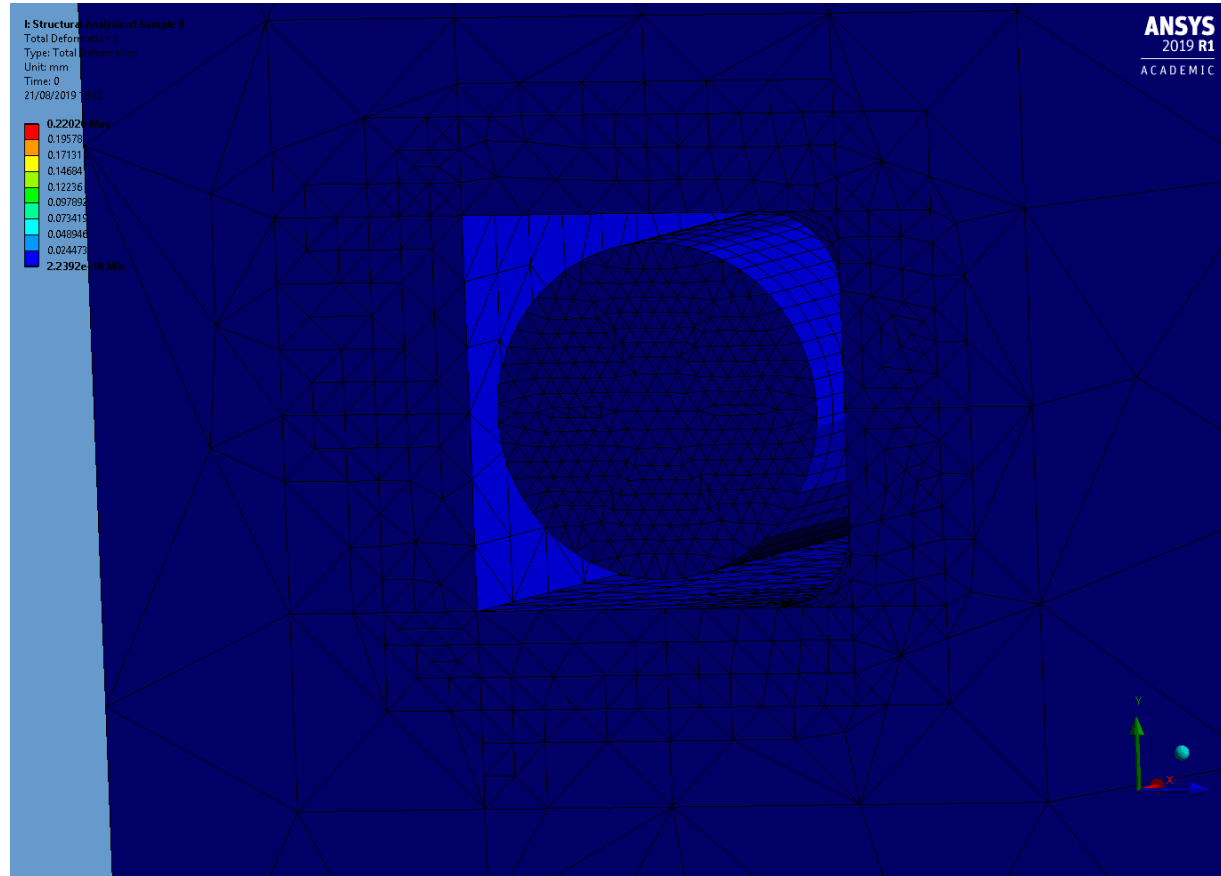
# Thermal Evolution



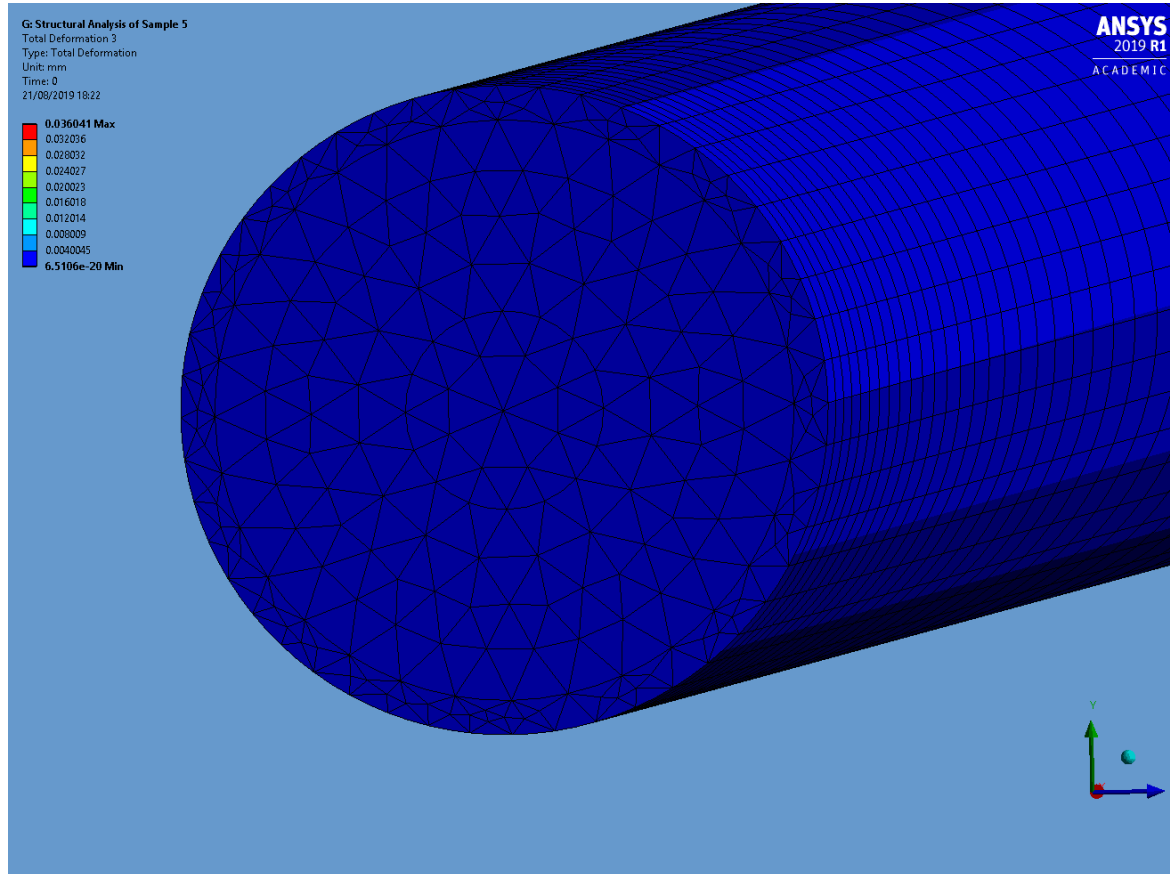
Temperature Distribution in  
Sample Holder  
right after Beam Impact

Temperature Distribution in  
Detailed Strand  
right after Beam Impact

# Mechanical Response



# Mechanical Response

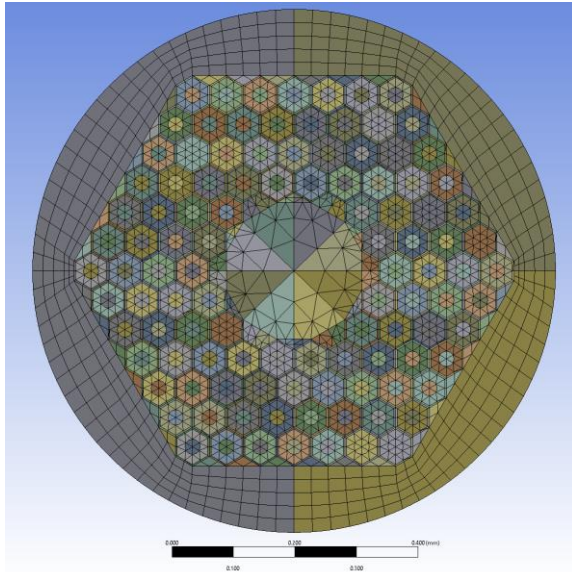


# Mechanical Response

Allowed for quantitative results such as:

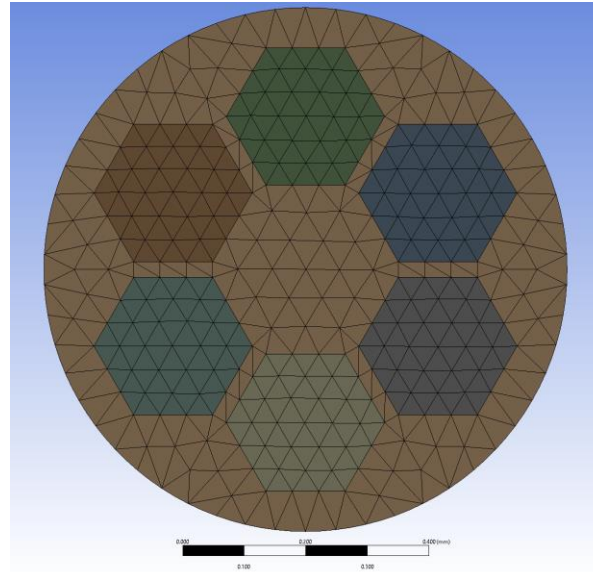
- Importance of placement in the Strandholder
- Strain induced bending of the Strands and their movement during the Reaction

# Different Models



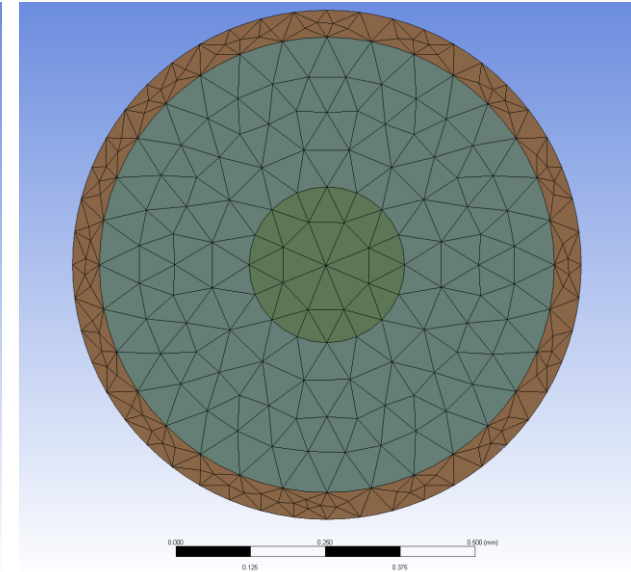
Maximum Detail Model:

- Fully elastic Nb<sub>3</sub>Sn
- Plastic fully annealed Cu



Nb<sub>3</sub>Sn Cluster Model:

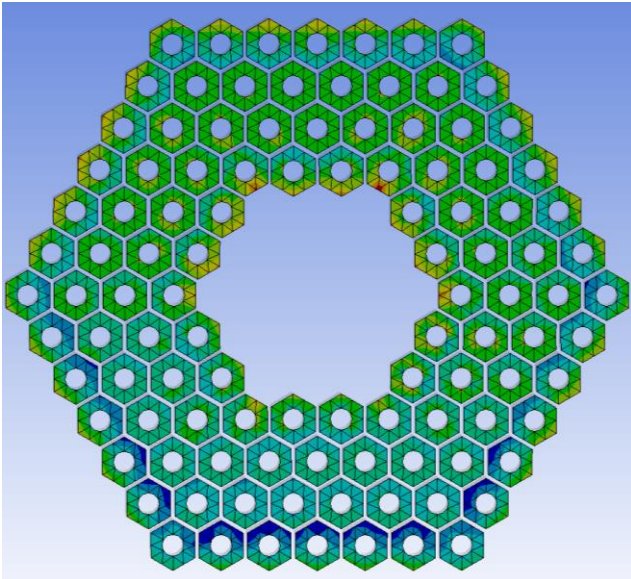
- Absolute area of Nb<sub>3</sub>Sn preserved
- Plastic behavior for Nb<sub>3</sub>Sn
- Plastic fully annealed Cu



Cylindrical Shell Model:

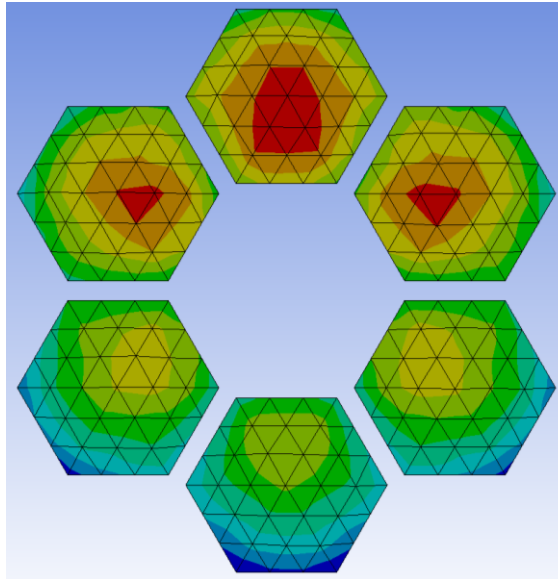
- Plastic composite Material of Nb<sub>3</sub>Sn and fully annealed Cu
- Plastic fully annealed Cu

# Mechanical Response



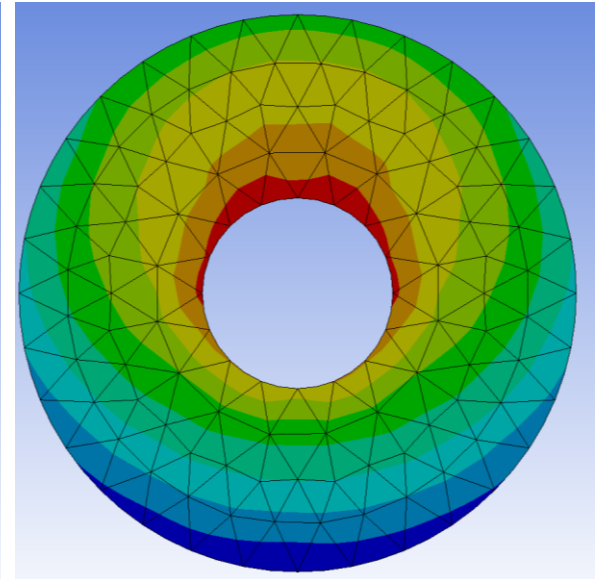
Maximum Detail Model:

- Fully elastic  $\text{Nb}_3\text{Sn}$
- Plastic fully annealed Cu



$\text{Nb}_3\text{Sn}$  Cluster Model:

- Absolute area of  $\text{Nb}_3\text{Sn}$  preserved
- Plastic behavior for  $\text{Nb}_3\text{Sn}$
- Plastic fully annealed Cu



Cylindrical Shell Model:

- Plastic composite Material of  $\text{Nb}_3\text{Sn}$  and fully annealed Cu
- Plastic fully annealed Cu



# Theory based Evaluation

# Strain Dependency

$$J_c(B, T, \varepsilon) = C_1 (1 - t^2) b^{-0.5} (1 - b)^2,$$

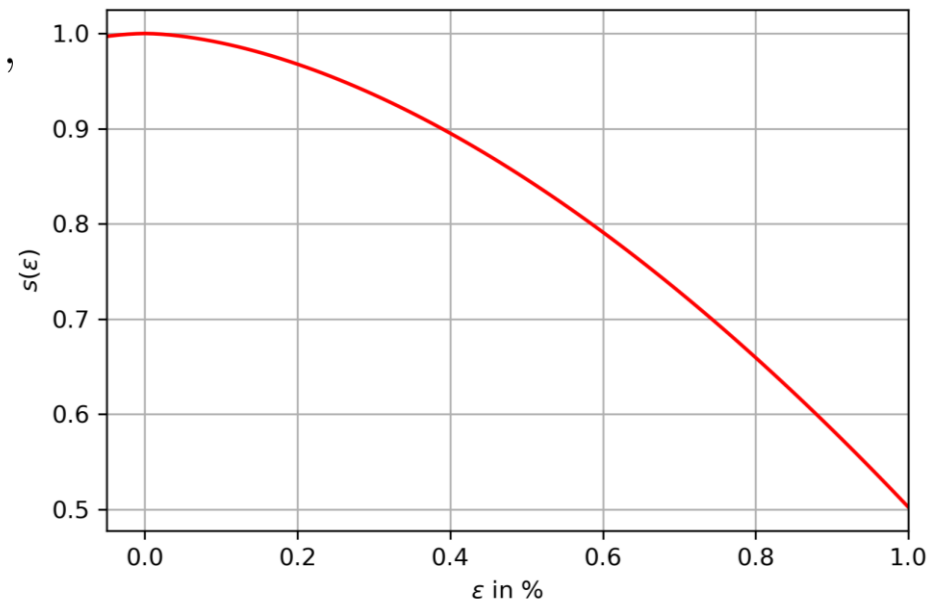
$$t = \frac{T}{T_c \cdot s(\varepsilon)^{\frac{1}{3}}},$$

$$b = \frac{B}{B_{c2}(T, \varepsilon)},$$

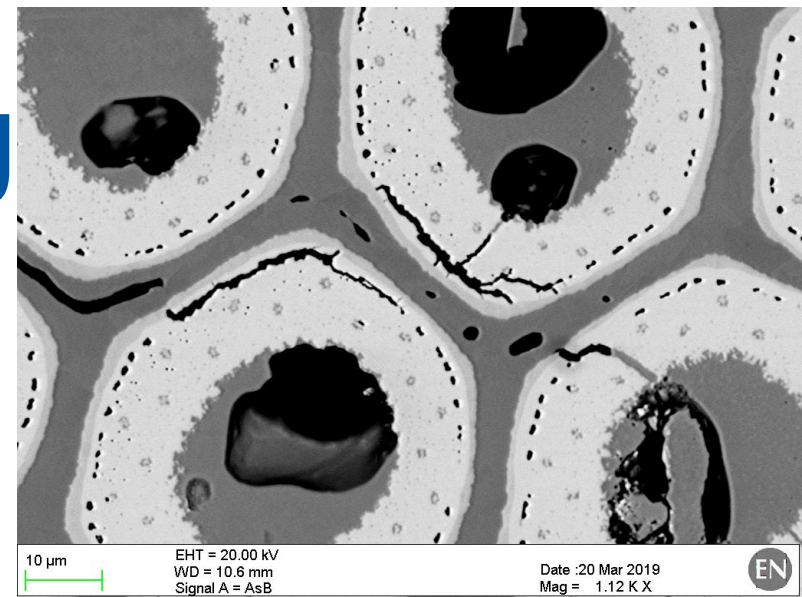
$$B_{c2}(T, \varepsilon) = B_{c2,0} \cdot (1 - t^{1.5}) \cdot s(\varepsilon)$$

MAG - Scaling Law

Power Law strain dependence



# Filament Cracking



- Highly dependent on the local composition
- Is a filament dead when it has cracks?

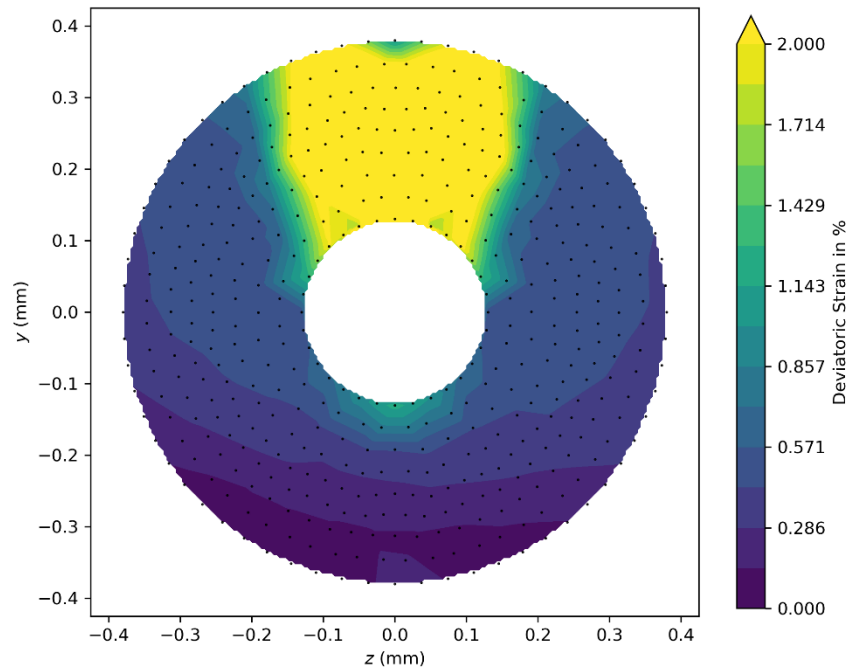
-> Irreversibility Cliff

-> rather than a strict limit

Fundamental Difference to Strain Scaling Law

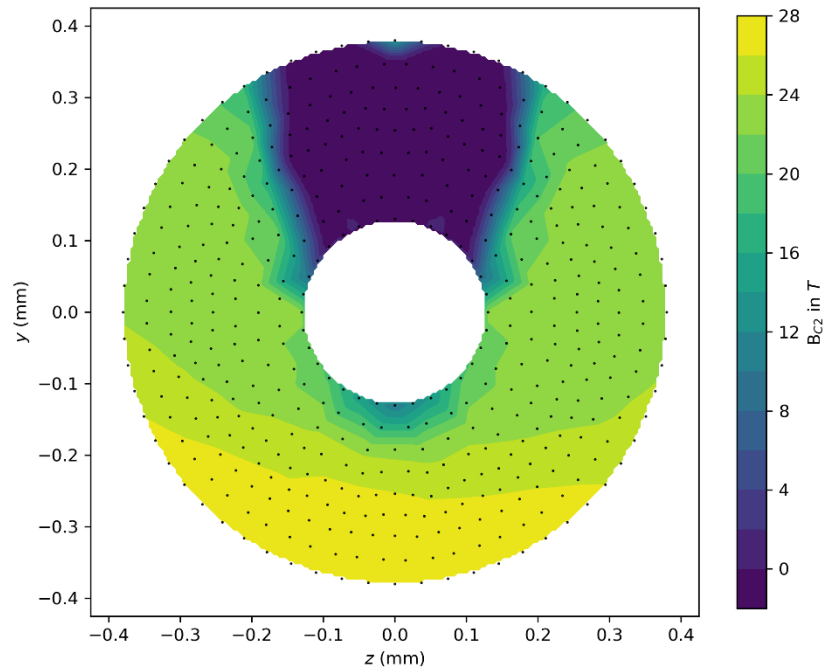
# Post Processing

3D Residual Deviatoric Strain  
Central Cross Section of Sample 5 after reaction in centre



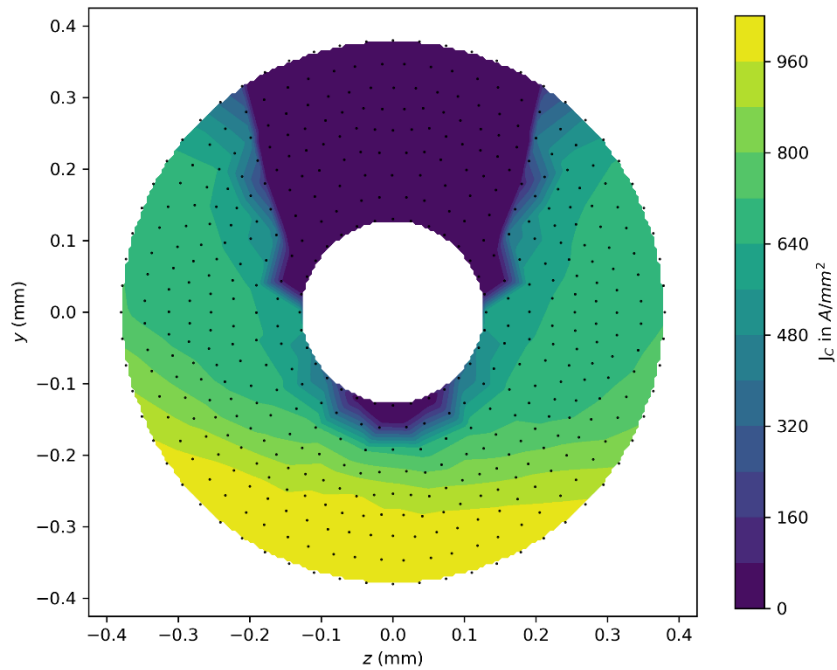
# Post Processing

Local  $B_{C2}$  after reaction  
Central Cross Section of Sample 5 after reaction in centre



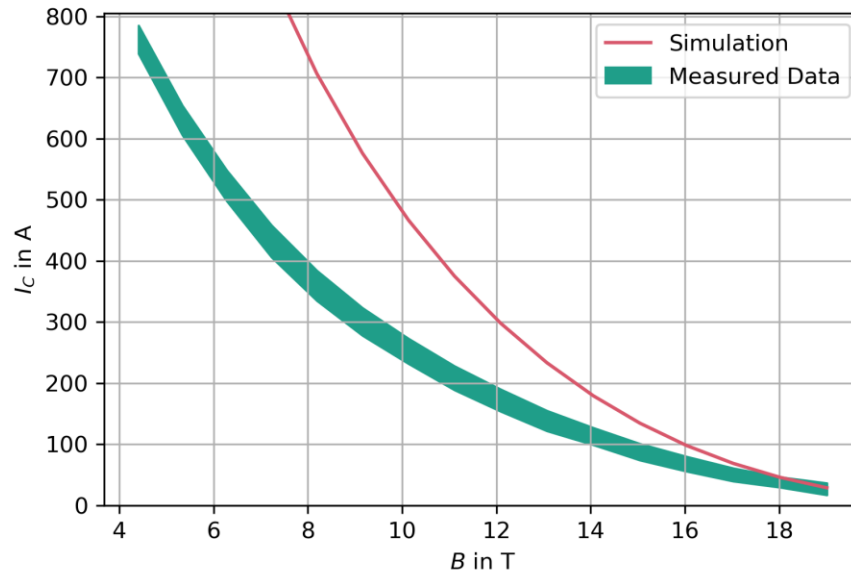
# Post Processing

Local  $J_c$  @ B = 10.13465825 after reaction  
Central Cross Section of Sample 5 after reaction in centre



# Post Processing

Comparison of  $I_C$  Values for Sample 5

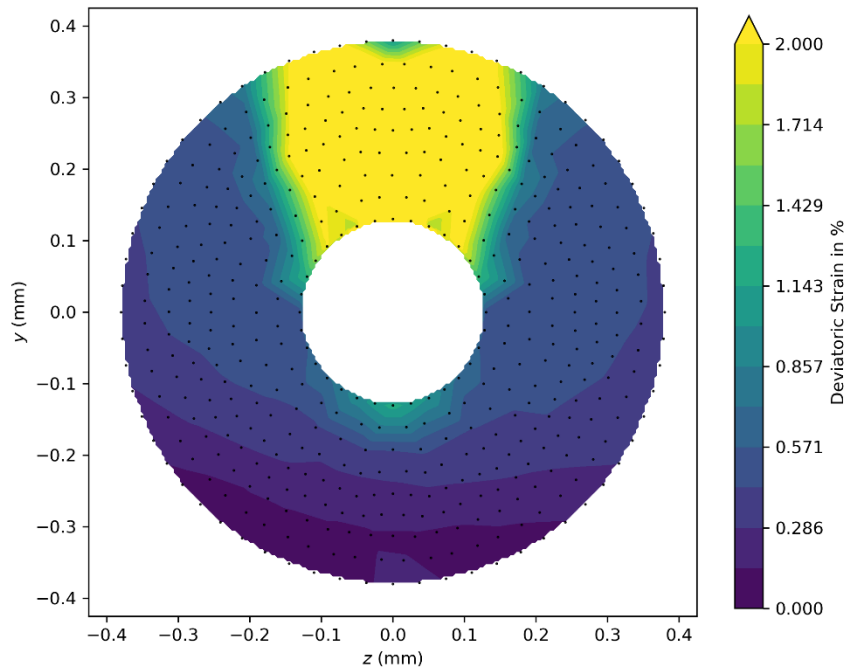


Now Let's introduce Filament Cracking



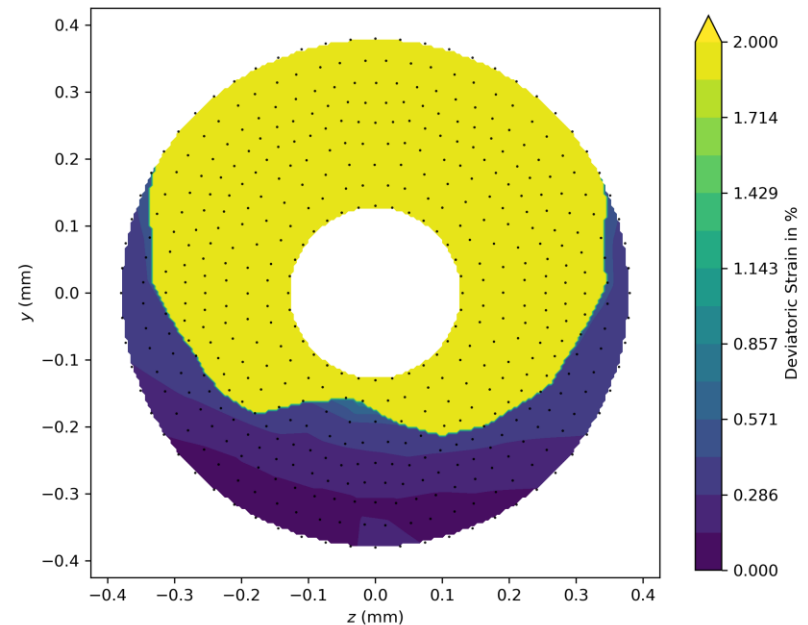
# Post Processing

3D Residual Deviatoric Strain  
Central Cross Section of Sample 5 after reaction in centre



Cracking Disregarded

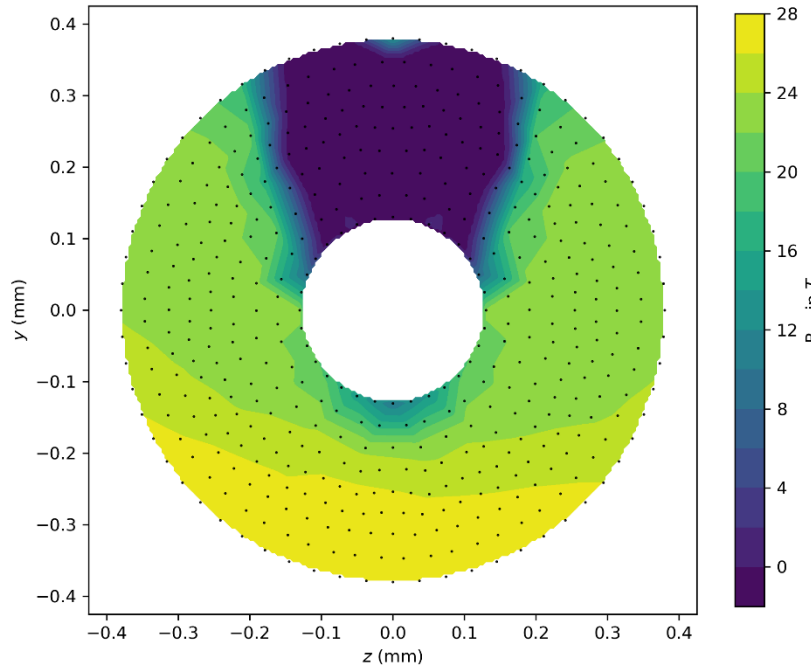
3D Residual Deviatoric Strain  
Central Cross Section of Sample 5 after reaction in centre



Cracking from .26%

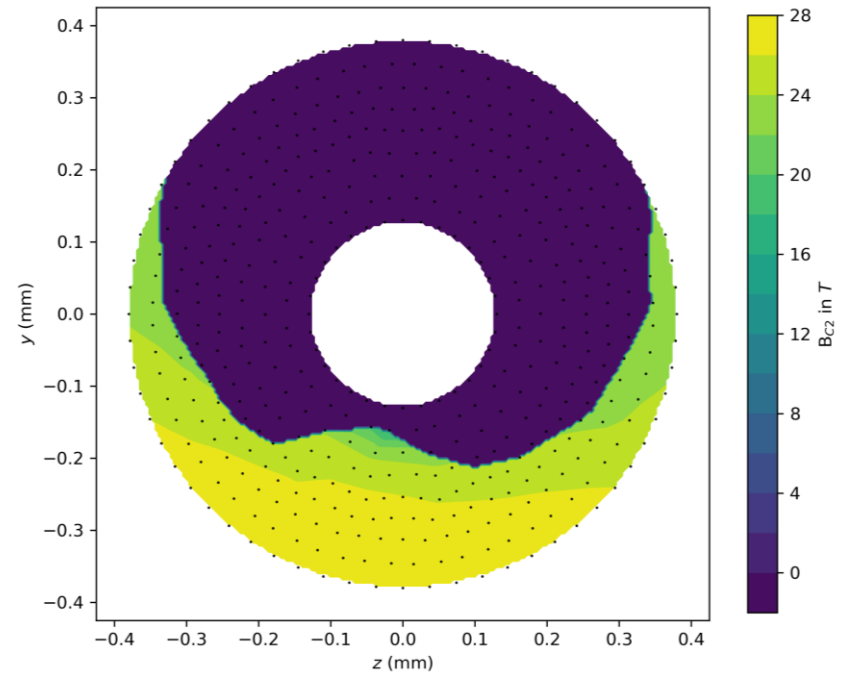
# Post Processing

Local  $B_{C2}$  after reaction  
Central Cross Section of Sample 5 after reaction in centre



Cracking Disregarded

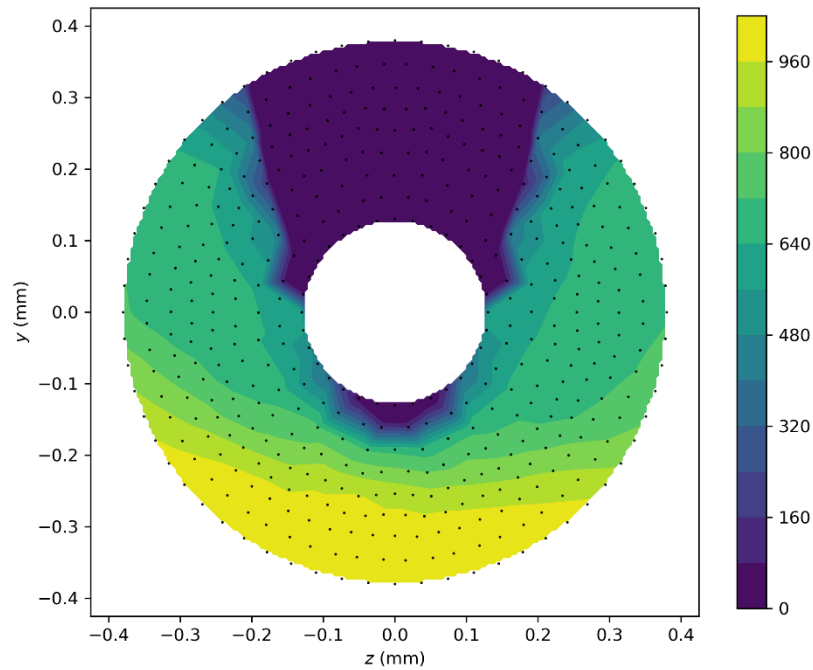
Local  $B_{C2}$  after reaction  
Central Cross Section of Sample 5 after reaction in centre



Cracking from .26%

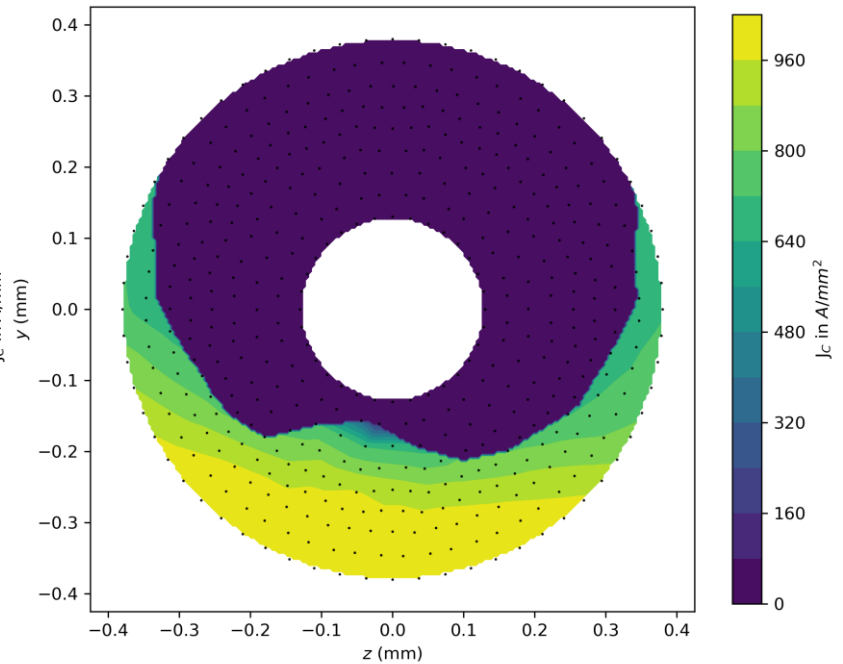
# Post Processing

Local  $J_C$  @ B = 10.13465825 after reaction  
Central Cross Section of Sample 5 after reaction in centre



Cracking Disregarded

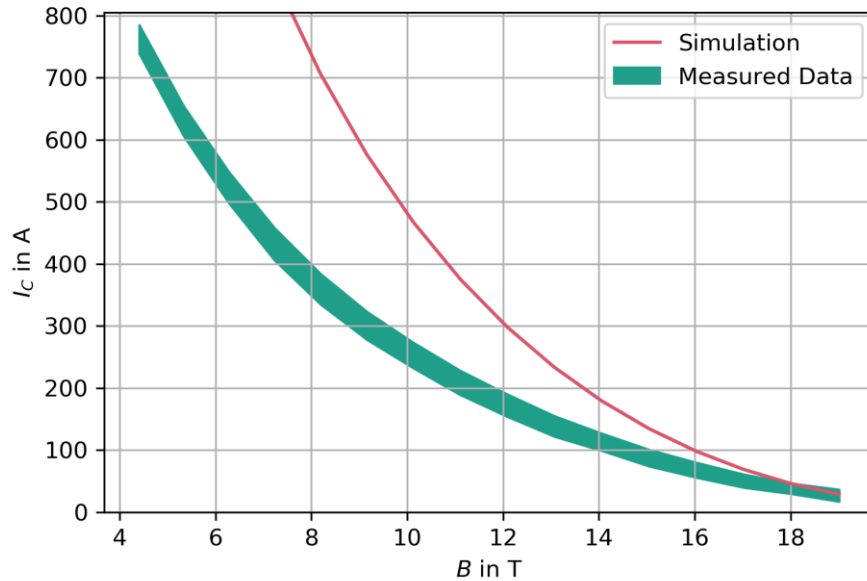
Local  $J_C$  @ B = 10.13465825 after reaction  
Central Cross Section of Sample 5 after reaction in centre



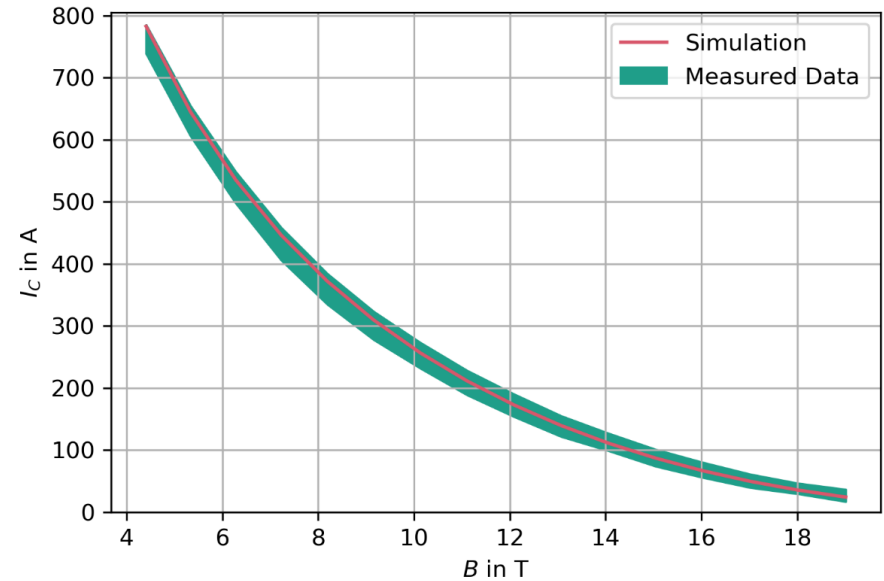
Cracking from .26%

# Post Processing

Comparison of  $I_C$  Values for Sample 5



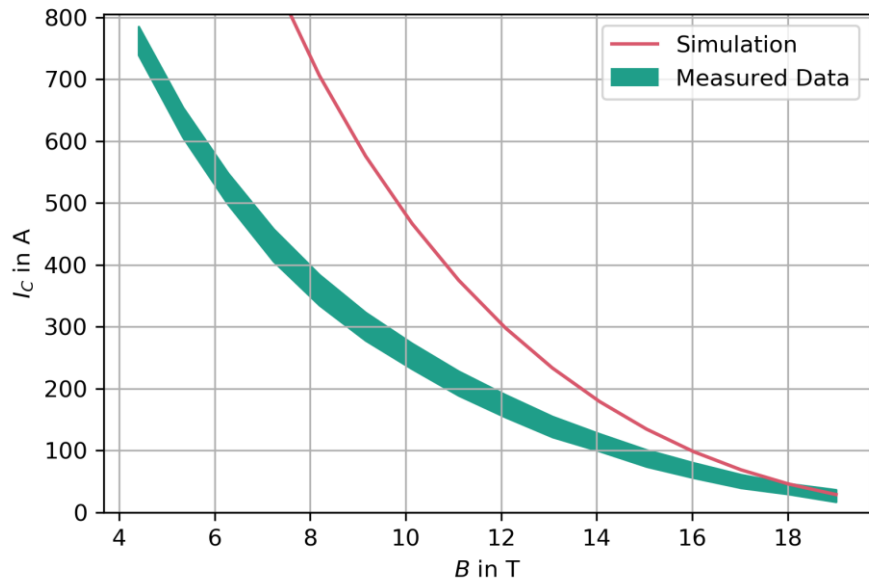
Comparison of  $I_C$  Values for Sample 5 and  $\epsilon_{ultimate} = 0.26$



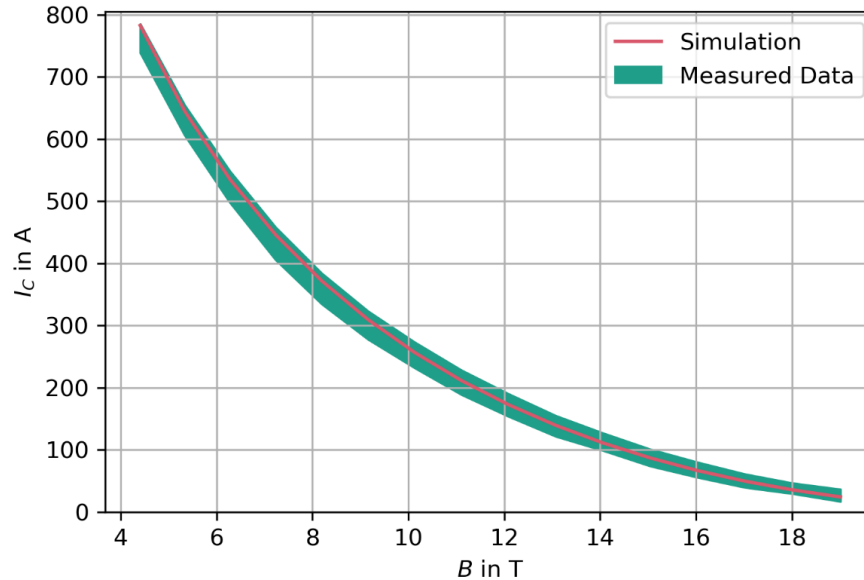
Cracking Disregarded

Cracking from .26%

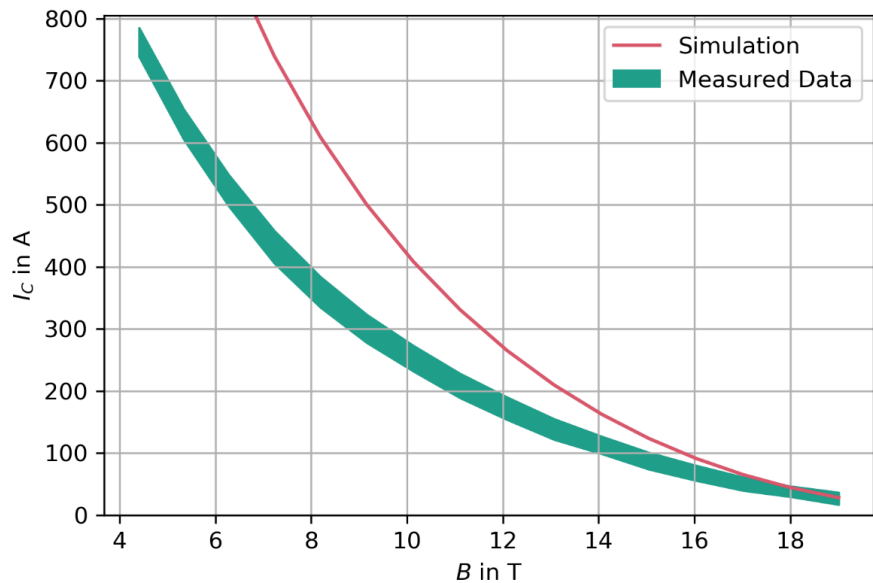
Comparison of  $I_C$  Values for Sample 5



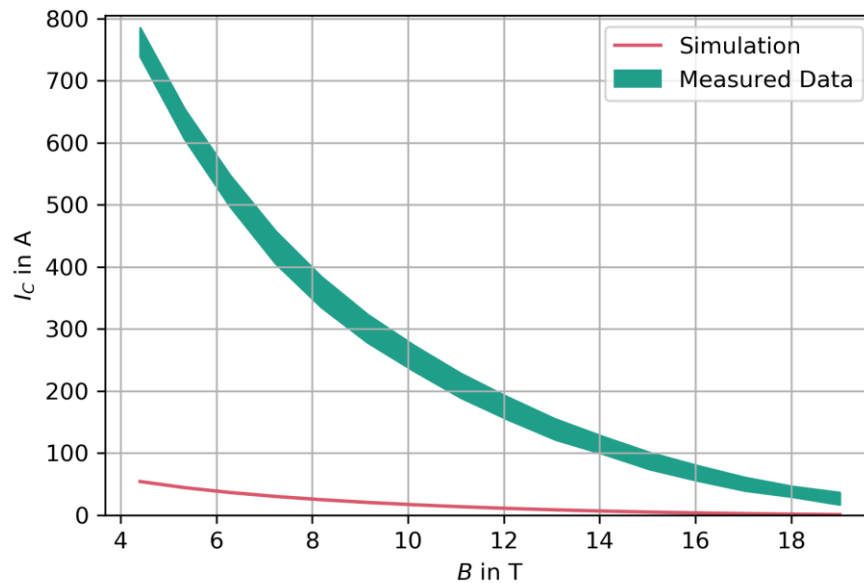
Comparison of  $I_C$  Values for Sample 5 and  $\epsilon_{ultimate} = 0.26$



Comparison of  $I_C$  Values for Sample 5 and  $\epsilon_{ultimate} = 0.3$

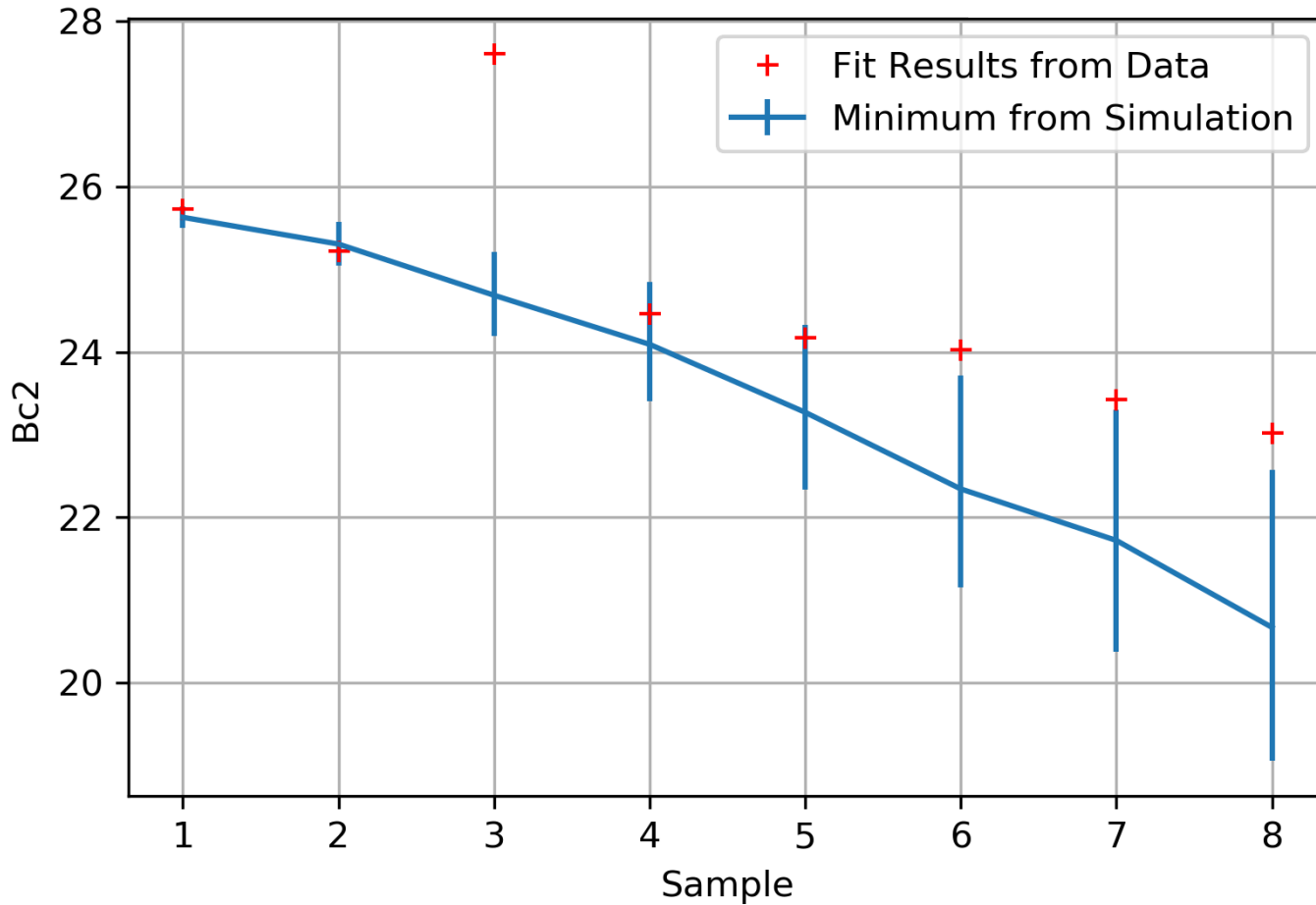
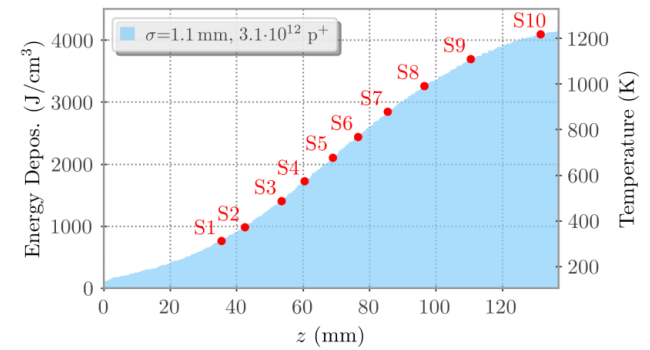


Comparison of  $I_C$  Values for Sample 5 and  $\epsilon_{ultimate} = 0.2$



# Results

## B<sub>C2</sub> degradation



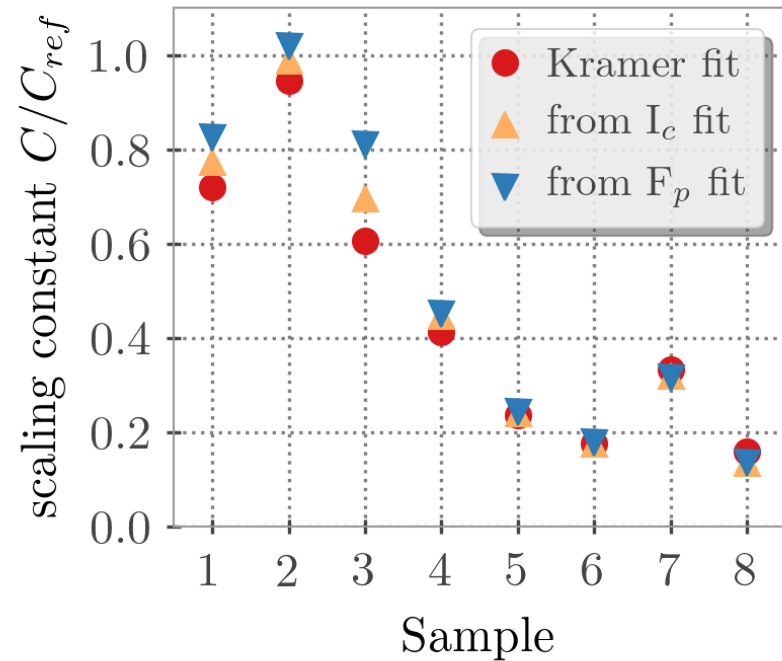
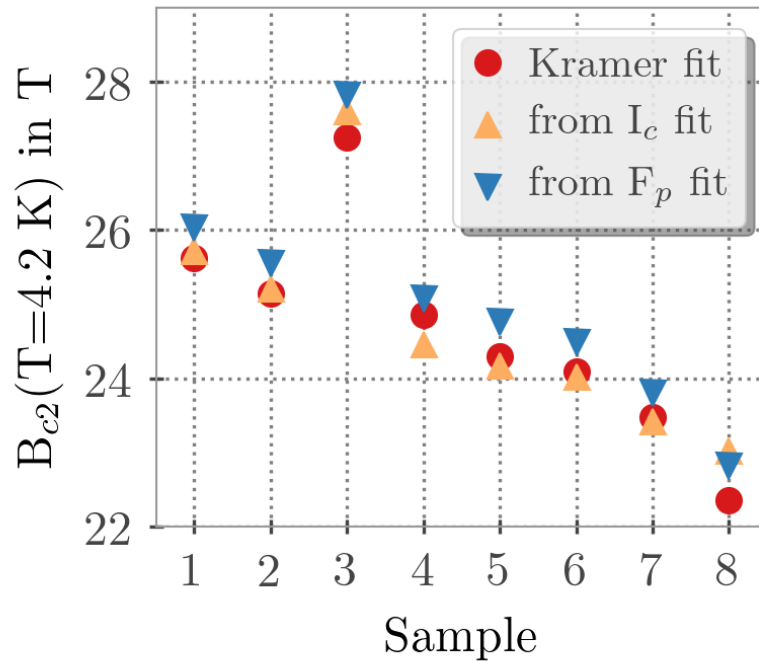
# Results

We were able to qualitatively explain:

- The bending and marking of the Strands
- The nonlinear influences of the Sample Holder
- difference between  $I_C$  and  $B_{C2}$  degradation
- Inconsistencies in  $I_C$  degradation for high Sample numbers



# Results



Fits on Measurement Data

# Results

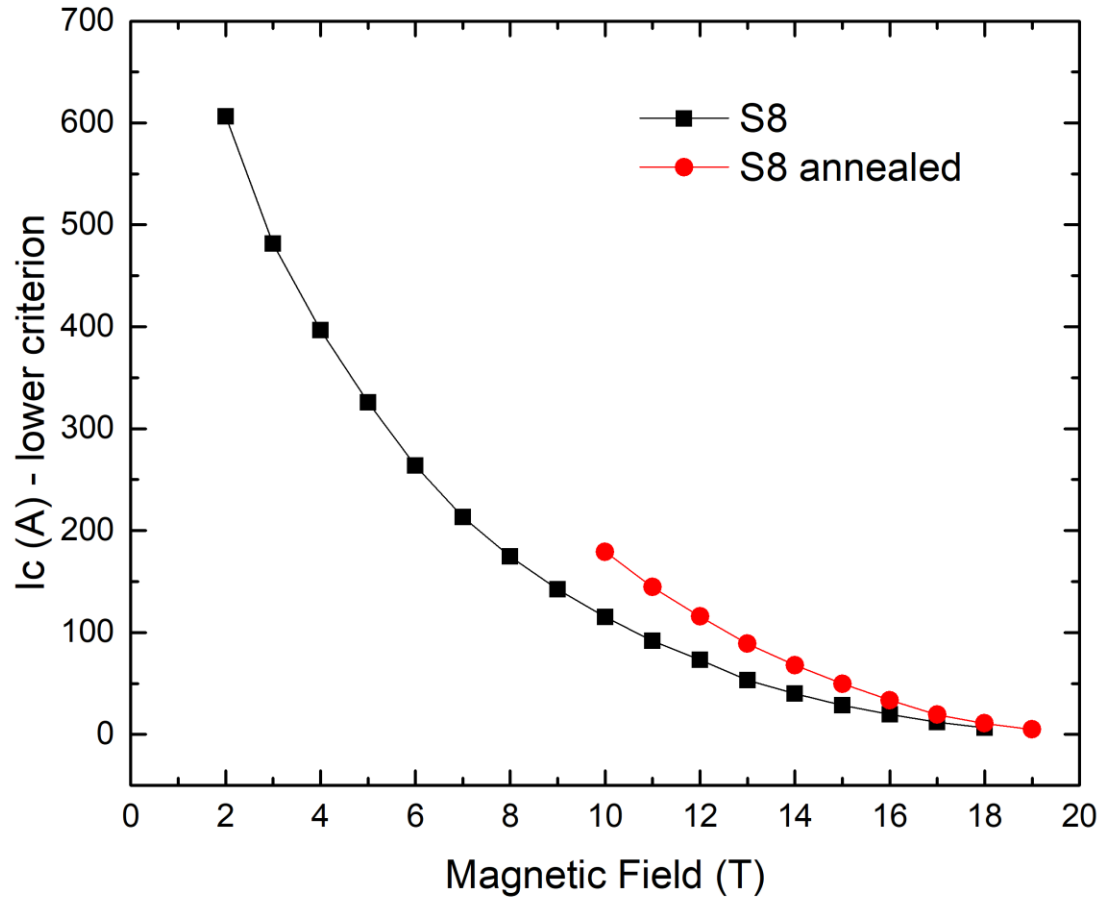
It was not possible to:

- Provide an Analysis tool to accurately predict the  $I_C$  degradation in areas of Large thermal gradients

We were able to predict:

- $B_{C2}$  degradation tendencies of the Samples

# Results



UNIGE Annealing Measurements

# Conclusion

- We have modeled the experimental Set up
- We were able to identify the two main sources of degradation
- This was verified by the annealing experiment
- Still Model Based Predictions for future experiments remain a big challenge

Thank you for your attention.



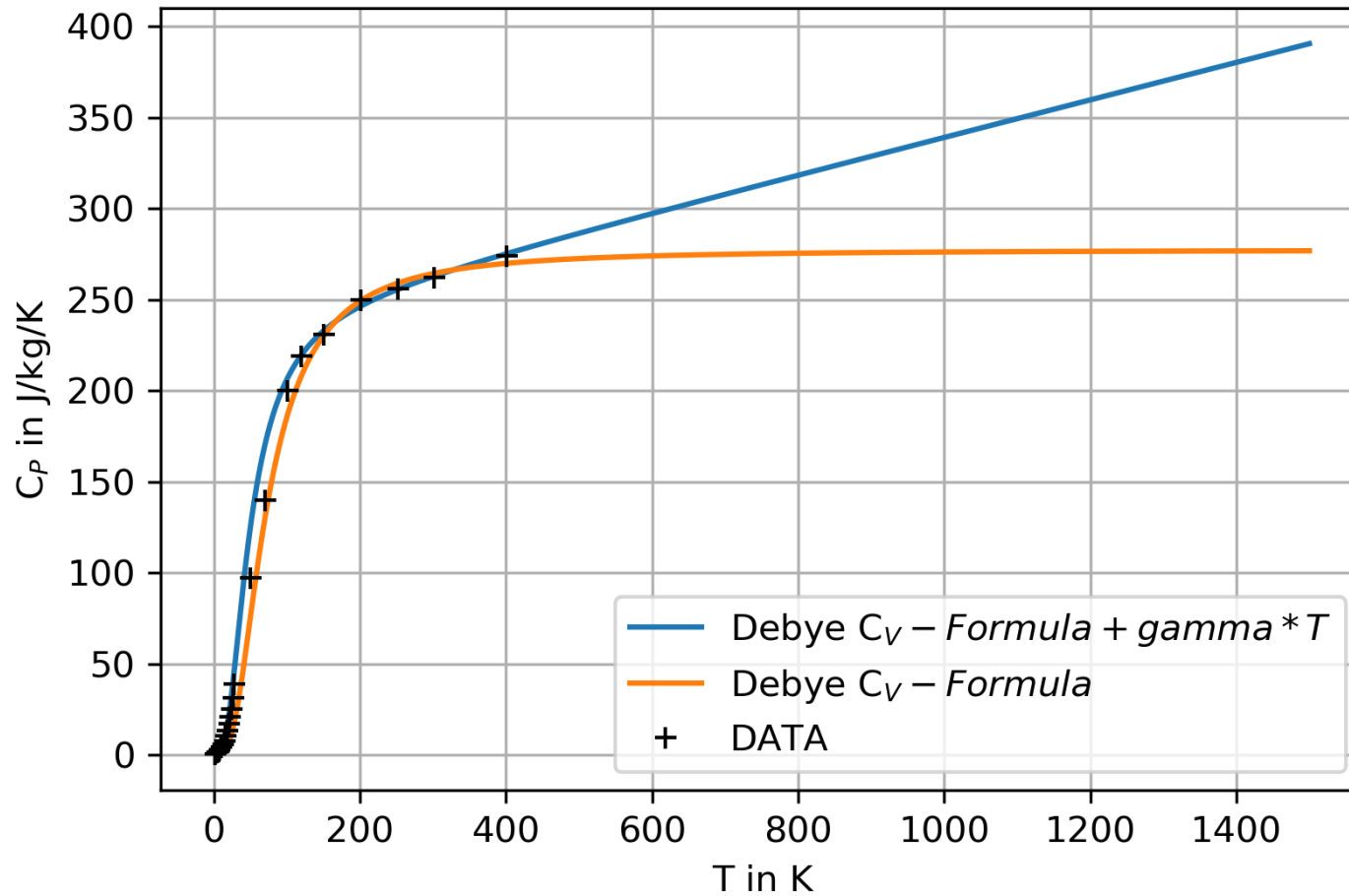
# Backup Slides



# Discussion

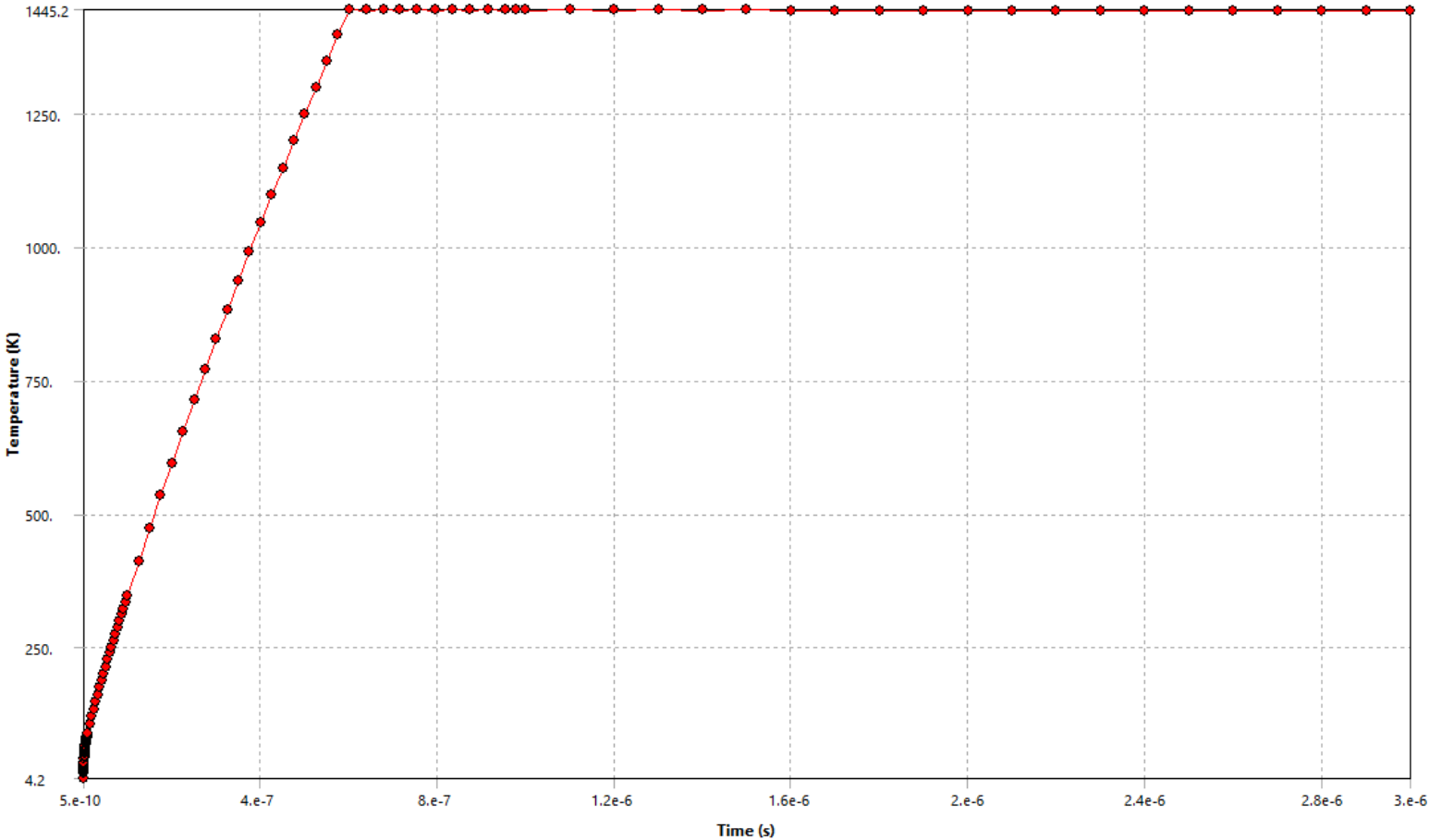
- $\epsilon_{\text{ultimate}}$  as a fit parameter cannot be found consistently for all samples, but with individual fits we can fit the measurements very well.
- The individual  $\epsilon_{\text{ultimate}}$  lie within a reasonable range of literature values and show a linear growth with Hotspot Temperature.
- Either this is physically relevant or a systematic error within the Analysis Model (see  $B_{C2}$  Degradation Maybe Material Data for extreme temperatures?).

# Nb<sub>3</sub>Sn C<sub>P</sub>

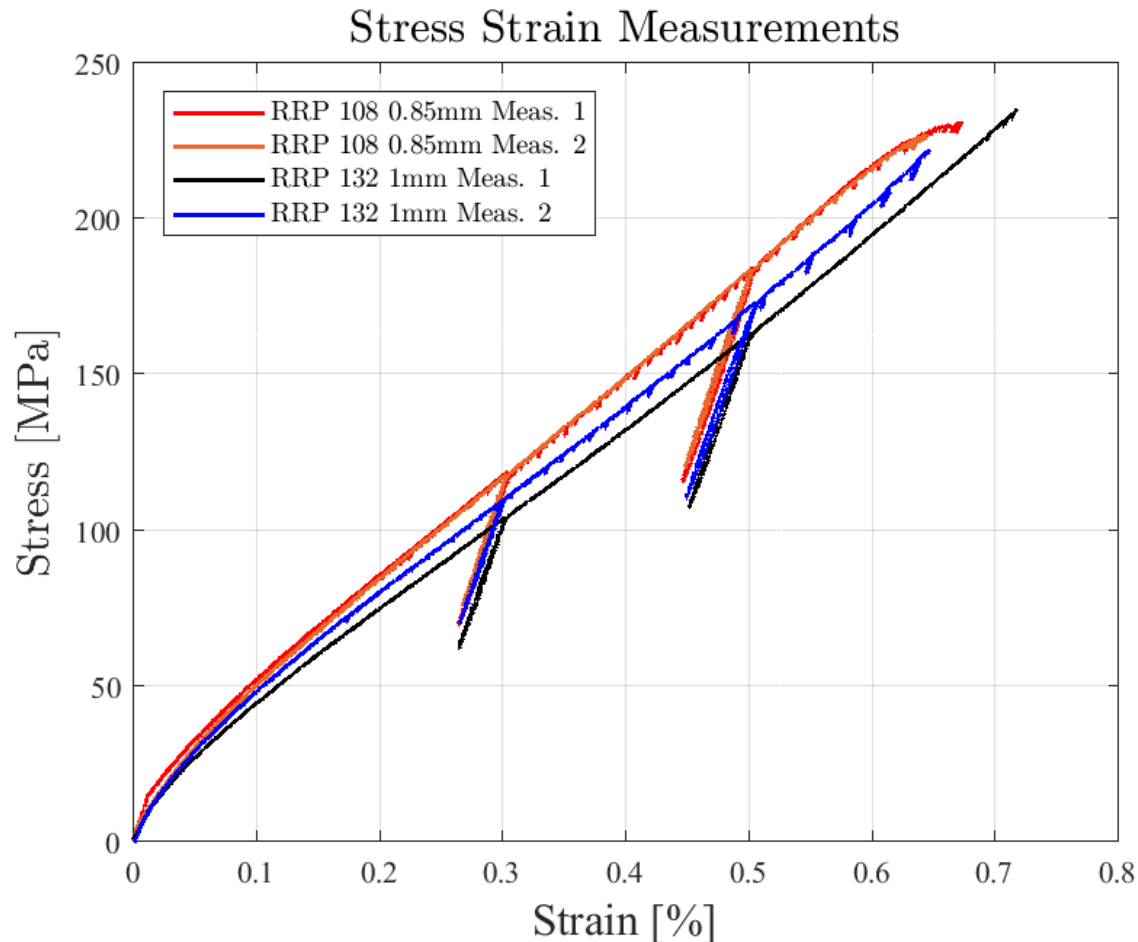


# Temperature Evolution

Temperature - Global Maximum



# RRP Stress-Strain Curve



*José FERRADAS – Paris Nb3Sn Workshop*