



Considerations for Magnets for a Muon Collider

Gijs de Rijk
CERN

10th April 2019



Magnet types: field

- 1.5 - 2T resistive (Cu or Al coils, steel yoke, all warm), ramp rates 10 th T/s, ~40kCHF/m
- 2 - 3 T Superferric (Superconducting, Nb-Ti coil, warm or cold steel yoke) ramp rates 10 th T/s
 - Multi turn coil in cryostat, H or C warm yoke, 2T, few T/s (FCM CERN)
 - Window frame, internally cooled cables, 2-3 T, ~4T/s, (JINR Nuclotron)
 - Transmission line: pipetron type, 2T, few T/s, <10 kCHF/m
- 3 - 8.5 T Superconducting, Nb-Ti , ramp rates from 0.1 to 4 T/s, ~65kCHF/m
- 9 - 12 T Superconducting, Nb₃Sn , ramp rates from < 0.1 T/s, ~85kCHF/m
- 12 - 16 T Superconducting, Nb₃Sn , ramp rates from < 0.1 T/s, ~100kCHF/m
- > 16 T Superconducting, HTS

■ = existing type used in accelerators

■ = prototypes exists

■ = under development, models in 5 years

■ = developed just started, at least 5 years before basic demonstration



solenoids

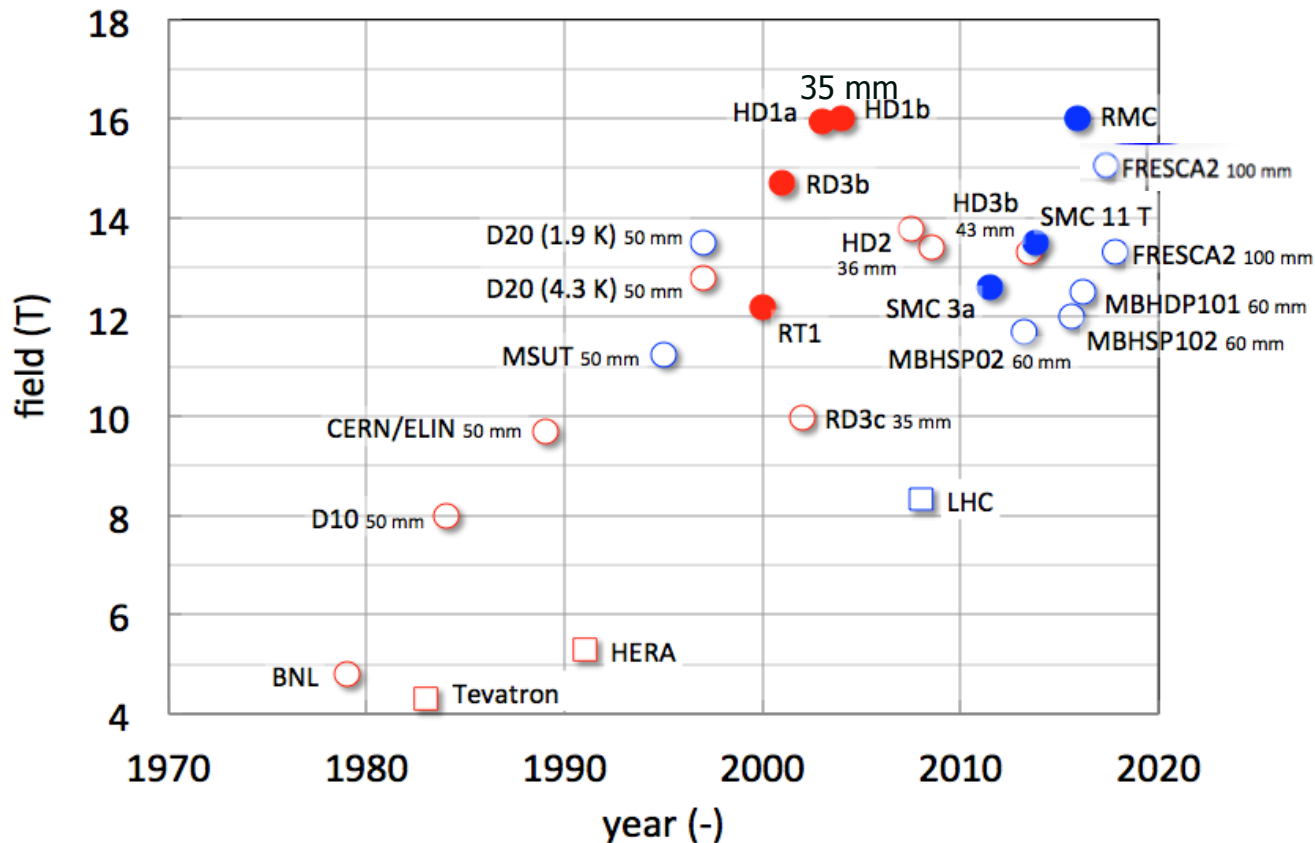
- up to 1.5T resistive (Cu or Al coils, steel yoke, all warm) (MRI)
- 1.5 T-10 T , superconducting Nb-Ti (MRI)
- 10 T - 20 T, superconducting Nb₃Sn (MRI)
- > 20T superconducting HTS

- Issue: Rad hardness ! not the same game as MRI



Superconducting accelerators magnets; the state of the art

- Maximum attainable field slowly approaches 16 T
 - 20% margin needed (80% on the load line):
for a 16 T nominal field we need to design for 20 T





Magnet types: rad hardness

- Up to few MGy
All HEP machine magnets are at least this standard
- Up to 30 MGy
HL-LHC triplet magnets, Nb₃Sn and epoxy were rad tested
- > 50 MGy
 - Fusion: ITER both Nb₃Sn, Nb-Ti and special impregnation were rad tested (Cyanite ester-epoxy mix)
 - magnets in target areas: SPS north area (concrete insulation), spallation sources (mineral insulation)



Magnet stored energy

- Stored Energy and Power

$$E = \frac{1}{2\mu_0} \int B^2 dV. \quad P = \frac{dE}{dt}$$

- Example 1 :

A volume of 1 m³ with a 2 T field has a stored energy of 1.6 MJ
ramped in 30 ms requires a power of 53 MW purely to “feed the field”

- Example 2 :

Ring : C= 22 km, dipole filling factor 80%, fast pulsed dipole 89%,
Fast pulsed dipole field B = ±2 T,
ramp -2 T to +2 T in 3.8 ms., (I take 0-2 T in 3.8 ms)
magnet aperture H x V = 100 x 50 mm² →

$$V_{\text{field}} = 78 \text{ m}^3.$$

$$E_{\text{stored}}(2\text{T}) = 125 \text{ MJ}$$

$$P_{\text{mag}} = 33 \text{ GW}$$

- Comparison SPS

$$E_{\text{stored}}(2\text{T}) = 36 \text{ MJ}, \text{ ramp in 3 s, } P_{\text{mag}} = 12 \text{ MW.}$$

(with a power convertor $P_{\text{peak}} = 120 \text{ MW}$)



some remarks

- Magnet system conceptual design
 - to make a realistic cost and feasibility estimate we need a parameter table:
 - B , L_{mag} , aperture $H \times V$, ramp rate
 - In general we always iterate over the parameter table to get to something feasible
- Development cycles for magnets are long (e.g. ~8 years for 1 new type model)
 - typically per new magnet type: 6 FTE and 2 MCHF per year
 - “het is een dure tak van sport”
- Pulsed magnets are an effort of magnet and powering groups together
- Radiation flux on components need to be looked at early on: Radiation damage and heat load



www.cern.ch