

Complementary solutions to improve the beam vacuum protection and to protect sensitive equipments (RF, kickers, experiments,...)



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Main Topics



- Review of the beam vacuum failure modes
- Pending issues
- Mitigation solutions
- Closing remarks



Introduction MCI definition





Courtesy L. Tavian





Accidental beam loss making a hole on the beam pipe

Short on the cryomagnet coil or lira creating a hole in the cold bore

Expected consequences depend on the type of beam vacuum

- Experimental beam vacuum (min. 6 months for repair)
 - Opening of the Detectors, beam pipe exchange, detector repair...
- Beam vacuum at cryogenic temperature e.g. arcs, triplets and SAMs (min. 12 weeks for repair)
 - Warm-up, magnet exchange, in situ cleaning, cool down...
- Beam vacuum operated at ambient temperature (min. 3 weeks for repair)
 - Mechanical intervention, bake out and NEG activation

The seam vacuum depends on the type of damages (ranking)

- Contamination by dust, MLI or soot
 - Dust and MLI could be cleaned in-situ, soot implies the removal of contaminated components
- Internal pressurization of the beam vacuum
 - Could lead to buckling of the bellows and require the exchange of cryomagnets...
- Venting to air or to dry helium
 - Venting to dry helium does not require the warm-up of cryomagnets...





• Beam pipe pressurization resulting from an injection of cold helium

- Expected consequences depend on the type of beam vacuum
 - Beam vacuum operated at ambient temperature (LSS and Experimental areas)
 - Mechanical intervention, bake out and NEG activation
 - Experimental beam vacuum
 - Opening of the Detectors, beam pipe exchange...
 - Beam vacuum at cryogenic temperature (arcs, triplets and SAMs)
 - Warm-up, magnet exchange, in situ cleaning, cool down...
- Impact onto the beam vacuum depends on the efficiency of compensatory measures decided after the incident of sector 3-4
 - Reinforcement of the supports of the cryomagnets with vacuum barriers
 - Limits the risk of mechanical displacement and damaging of the Plug-in modules (PIMs) and nested bellows
 - Additional pressure relief valves (or unclamped flanges)
 - Limit the pressurization level of the insulation vacuum
 - By-pass at the vacuum barriers (on pumping stations)
 - Limit the pressurization level of the insulation vacuum





- Reinforcement of the supports of the cryomagnets with vacuum barriers
 - Limits the risk of mechanical displacement and damaging of the Plug-in modules (PIMs) and nested bellows
 - The Preventing the injection of cold helium and contamination into the beam vacuum





Review of the beam vacuum failure modes Beam Vacuum damaged by collateral effects (3/4)



• DN200/160/100 pressure relief valves and/or declamped flanges to limit the pressurization of the insulation vacuum

- Limit the pressurization level of the insulation vacuum



Without DN200 (declamping of existing flanges)



DN200 "declamped" configuration



DN200 "spring" configuration



DN100 "declamped" configuration



DN100 "spring" configuration





- By-pass at the vacuum barriers (on pumping stations)
 - Limit the pressurization level of the insulation vacuum
 - Implemented on sectors not yet consolidated with DN200 pressure relief valves
 - Proposal being prepared to extend this configuration to all arcs (2012)







Pending Issues RF cavities, kickers and Experimental areas (1/4)



• Vacuum failure without pressurization

- Venting with dry helium without contamination should not be a major issue
 - Commissioning: several days will be required
- Venting with air without contamination will required a bake out for the kickers and a warming up of the SC RF cavities
 - Bake out/venting followed by commissioning: several weeks
- Venting with contamination will impact significantly the performances of these equipments
 - Removal from the tunnel to be considered
 - Not enough spare available

• Vacuum failure with pressurization

- Critical in most of these equipments
 - Supports in the Experimental areas are not design to stand induced forces
 - Ceramics, bellows could fail in presence of an internal pressurization

None of these vacuum sectors is equipped with rupture disks



Pending Issues

RF cavities, kickers and Experimental areas (2/4)



- Configuration around and on between the kickers does not favor optimum solution
 - 0.5 m between kickers
 - Cannot protect one kicker against its neighbor...
 - 2 m between kickers and Q4D2/Q5 cryomagnets
 - Cannot protect one kicker against its neighboring cryomagnet...
 - Can protect kickers from the arc
 - Not obvious that absolutely required, "damping" effect of NEG coatings and Q6/Q5 cryomagnets





Pending Issues

RF cavities, kickers and Experimental areas (3/4)



- Configuration around and on between the cavities does not favor optimum solution
 - 0.5 m between cavity 2 and 3
 - Cannot protect one cavity against its neighbor...
 - [©] Can protect cavity 1 and 4...
 - >30 m between kickers and D3 cryomagnets
 - Can protect the cavities against their neighboring cryomagnets...
 - Can protect cavities from the arc
 - Not obvious that it is absolutely required, "damping" effect of NEG coatings and Q6/Q5/D4/D3 cryomagnets





Pending Issues

RF cavities, kickers and Experimental areas (4/4)



- Configuration around and on the Experimental areas does not favor optimum solution
 - Few meters between the "central" beam vacuum sector and Q1 cryomagnets
 - Cannot protect the Experimental beam vacuum from the triplets...
 - >50 m between the Experimental beam vacuum and the D2Q4 cryomagnets,
 - Can protect the Experiments against D2Q4 cryomagnets...
 - Can protect the Experimental beam vacuum from the arc
 - Not obvious that absolutely required, "damping" effect NEG coatings and cryomagnets





Mitigation solutions Pressure relief valves



• New design of DN200/160/100 valves

- Opens in case of a slight overpressure an then "recloses" at equilibrium (internal/external)
- "Self" positioning to improve tightness reliability
- Limits contamination /condensation of huge quantities of air
 - Water (MLI) and Oxygen (explosion risk) are the most delicate
- To be applied to all "declamped" positions (DN100/160/200)
 - Proposal being studied for all positions (2012)











Mitigation solutions Rupture disks (1/4)



- New design of rupture disks
 - Opens in case of pressurization and then closes off when pressures are at equilibrium
 - Limits the contamination /condensation of huge quantities of air
 - Water (MLI) and Oxygen (explosion risk) are the most delicate
 - Self protected in case of a failure of the disk
 - Accidental venting is avoided by the viton sealed cap
 - Less critical design, more adapted to an extended use in the arcs
 - Limits the buckling of the bellows (PIMs and nested) in case of an internal pressurisation







Mitigation solutions Rupture disks (2/4)

Accidental rupture of the disk







Technology Department

Vacuum Surfaces...

Coatings





Distance from incident (m)



Distance from incident (m)



Mitigation solutions Rupture disks (4/4)



• External pressurization should no longer be a problem

- 1.5 bar for consolidated sectors, for an MCI (40 kg/s)
- 3.5 bars for the non-consolidated sectors, for an MCI (40 kg/s)
- PIMs and Nested bellows have a higher buckling pressure, 3.5 and 5 bars respectively

• Internal pressurization is a major issue

- If an impact of the beam onto the beam screen / cold bore can not be excluded
- The Recommends to install additional rupture disks. In case of an MCI,
 - 200 m of machine could have buckled bellows if each SSS is equipped
 - 400 m of machine could have buckled bellows if each 1 SSS over 2 is equipped
 - 600 m of machine could have buckled bellows if each 1 SSS over 3 is equipped
 - Etc.



Mitigation solutions Fast shutters (1/2)



• Prerequisites

- Shall not be necessarily leak tight
- Shall limit the propagation of the contamination
- Shall close within 20-50 ms
- Shall not be dangerous for the machine in case beams intercept the sealing plate
- The sealing plate The sealing
 - Transparent to the beam
 - Faster since lighter
 - Spring or pyrotechnic actuator (adapt commercially available actuators)
- ⇒ Requires reliable interlock signals
 - Beam loss monitors
 - Pressure gauges or nQPS in the absence of circulating beams
- Needs a complete development and validation tests
- Being studied in the TE-VSC group
 - Conceptual design expected by end 2010
 - Tinstallation foreseen for 2012



Mitigation solutions Fast shutters (2/2)



- Vacuum failure without pressurization
 - Propagation of the contamination is an issue since the arc is not sectorised
 - No space left in an interconnection to install a fast shutter...



Still looking for ideas...



Mitigation solutions Half-shells



• Two half-shells in Vetronite or equivalent

- Shall protect the bellows (PIMs and nested) in the interconnections
 - Increase resistance to plasma discharge (high temperature resistance)
 - Avoid damages induced by the projections of melted metal
 - Limit the injection of MLI in the Beam Vacuum
 - Slightly increase the buckling pressure by a "guiding effect"
- Shall use insulating material to repulse the plasma/arcing risk
- Easy to retrofit during the consolidation of the splices







Closing Remarks



• Prerequisites and required time to implement

- Half-shells are easy to install and will be coupled with the consolidation of the splices (2012)
- Additional rupture disks sounds a good idea
 - Installed at all extremities of the 4 Experimental areas ⇒ Needs a venting to dry Neon to equip the central vacuum sector
 - Will allow to put back into operation, the sector valves...
 - In the arcs \Rightarrow Needs a warm up and can be coupled with the consolidation of the splices
 - Proposal will be presented to LMC by Automn'10
- Reliability and limitation of collateral damages in case of a membrane failure is being considered (see new design)
- Fast-closing valves need a technical development and validation
 - On going studies, first proposal (conceptual) by end 2010
 - Implementation in 2012
- Timplementation in the arcs seems difficult





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