

- What are AC-LGAD (RSD)
- Signal formation
- Laser study
- Reconstruction method
- Results

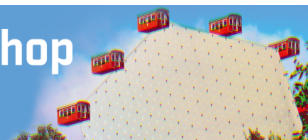
Nicolò Cartiglia

INFN - Italy

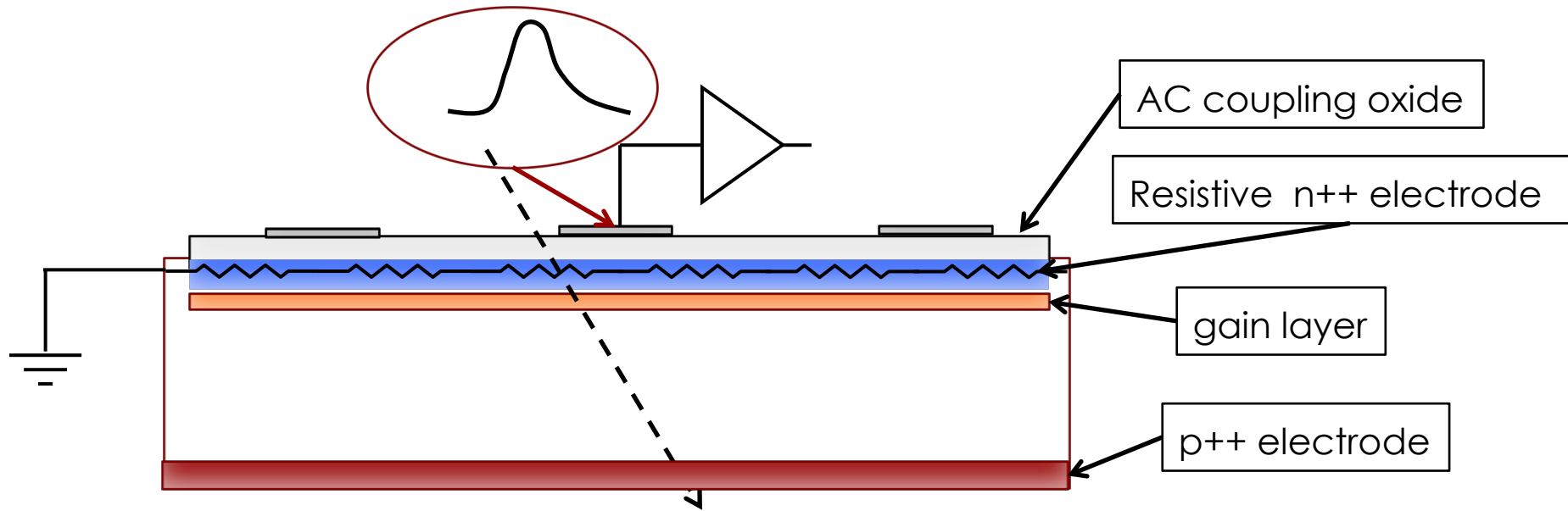
R. Arcidiacono^{ab}, G-F Dalla Betta^{ae}, G. Borghi^f, M. Boscardin^f, M. Costa^{ac}, F. Fausti^{ac}, F. Ficorella^f, M. Ferrero^{ab}, M. Mandurrino^a, J. Olave^a, L. Pancheri^{ae}, F. Siviero^a, V. Sola^a, M. Tornago^{ac}, G. Paternoster^f, H. Sadrozinski^d, A. Seiden^d, M. C. Vignale^f

^a INFN, ^b Università del Piemonte Orientale, ^c Università di Torino,

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AC – LGAD: Resistive Silicon Detectors (RSD)



AC-LGAD are a design evolution of LGAD detectors where the gain layer is not segmented, and the signal is read-out via AC coupling (see TREDI 2015 for details).

The **key technological feature** that makes this design work is the “**resistive n++ layer**”, necessary to produce the local AC coupling. For this reason, they are called “**Resistive Silicon Detector**”, **RSD**.

The sensors presented here are manufactured at FBK within the RSD project (INFN).

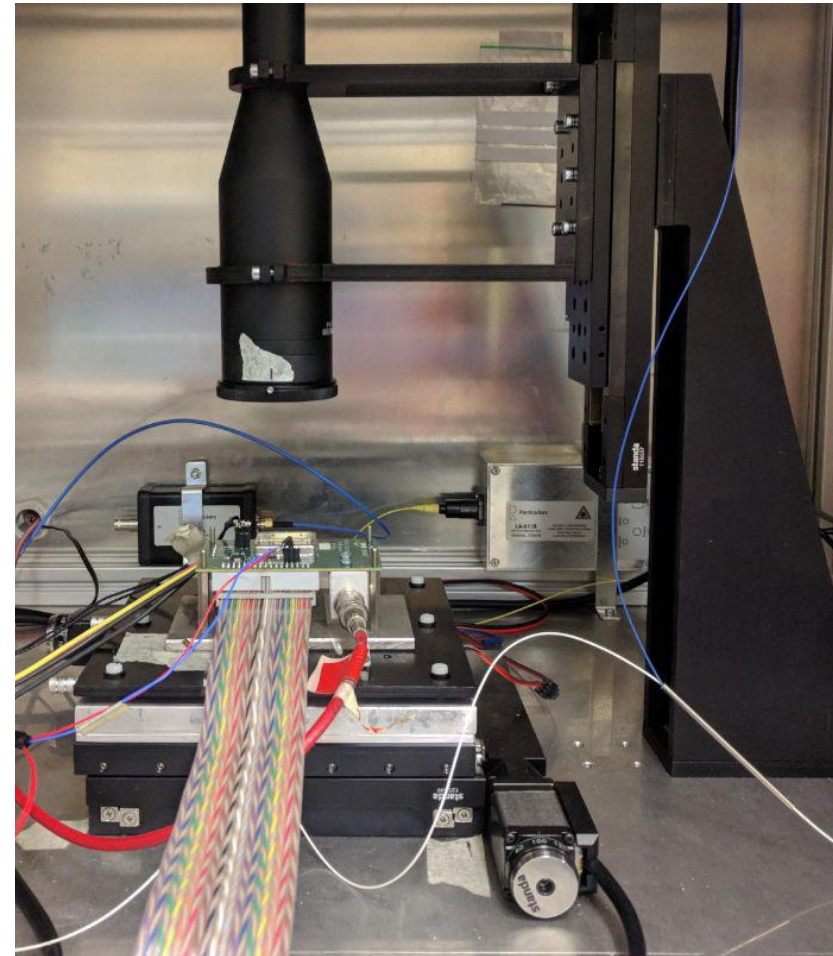
➔ CNM produced AC-LGAD sensors in 2017, Sadrozinski’s talk @ HSTD11, BNL in 2019.

Publications:

M. Mandurrino *et al.*, "Demonstration of 200-, 100-, and 50- μm Pitch Resistive AC-Coupled Silicon Detectors (RSD) With 100% Fill-Factor for 4D Particle Tracking," in *IEEE Electron Device Letters*, vol. 40, no. 11, pp. 1780-1783, Nov. 2019.

M. Mandurrino *et al.* "Analysis and numerical design of Resistive AC-Coupled Silicon Detectors (RSD) for 4D particle tracking" <https://doi.org/10.1016/j.nima.2020.163479>

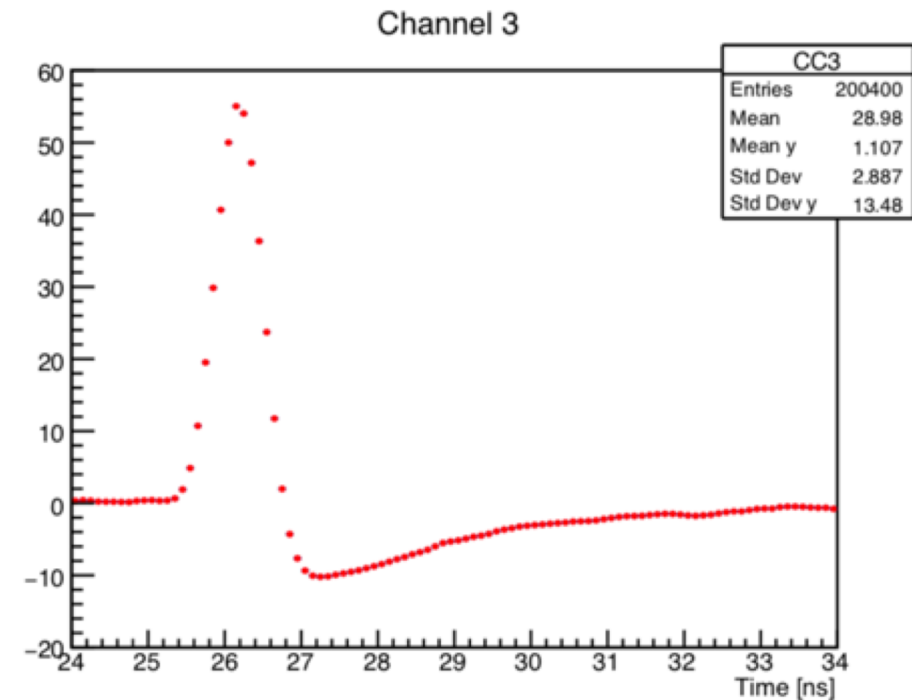
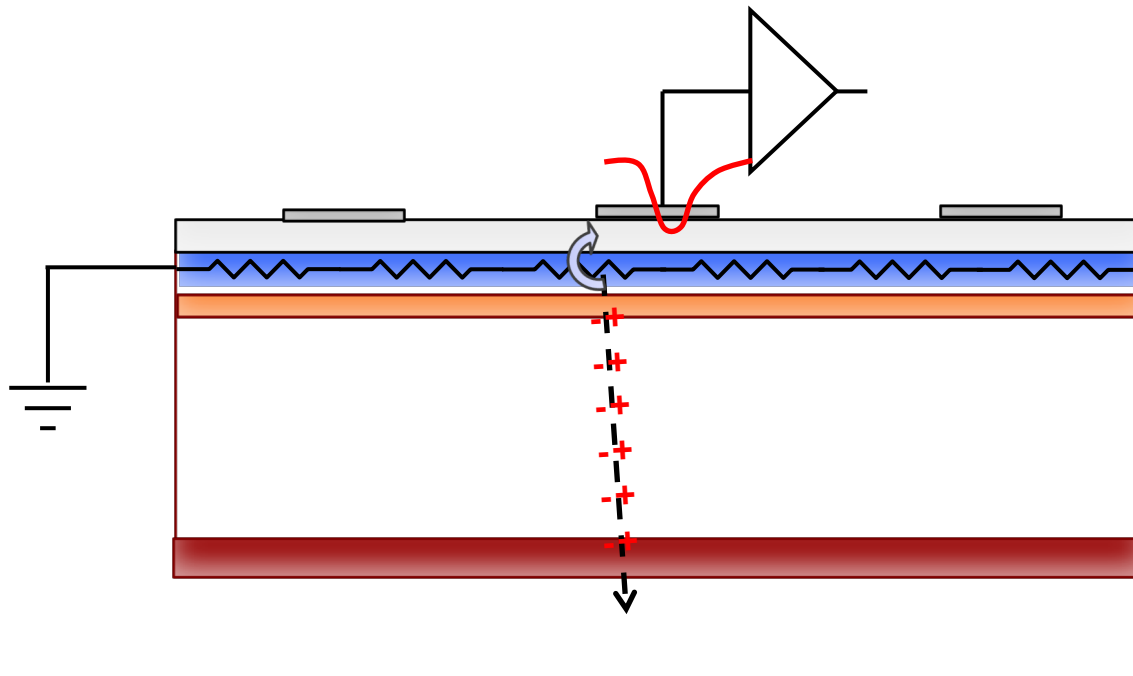
- The study presented here are obtained using a “Particular” laser TCT set-up
- Sensors are glued on a 16-channel read-out board.
- The signal of the 4 pads is recorded using an oscilloscope
- The laser is shot in various position via an x-y-z micrometric stage



RSD Signal formation - I

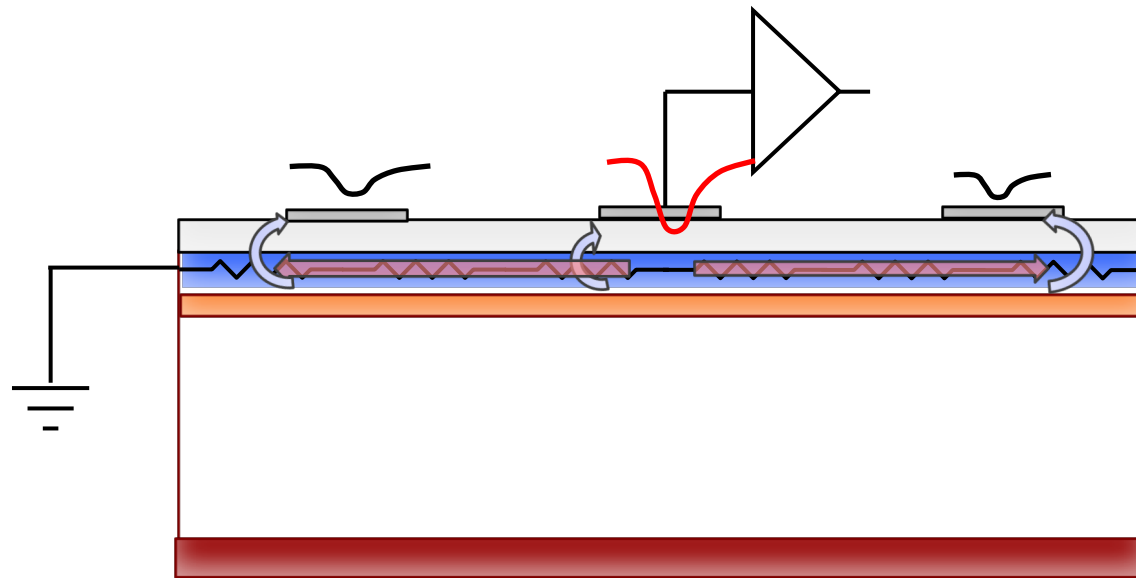
Act 1: the e/h are drifting and they produce a direct charge induction in the n++ layer (Ramo theorem)

1. The signal is immediately AC-coupled to the metal pad above (if there is one), its shape identical to an equivalent DC LGAD
2. Large signal (gain 10-20): 5 - 10 fC
3. Very fast collection (1 ns)
4. No lateral spread, very vertical E field and drift



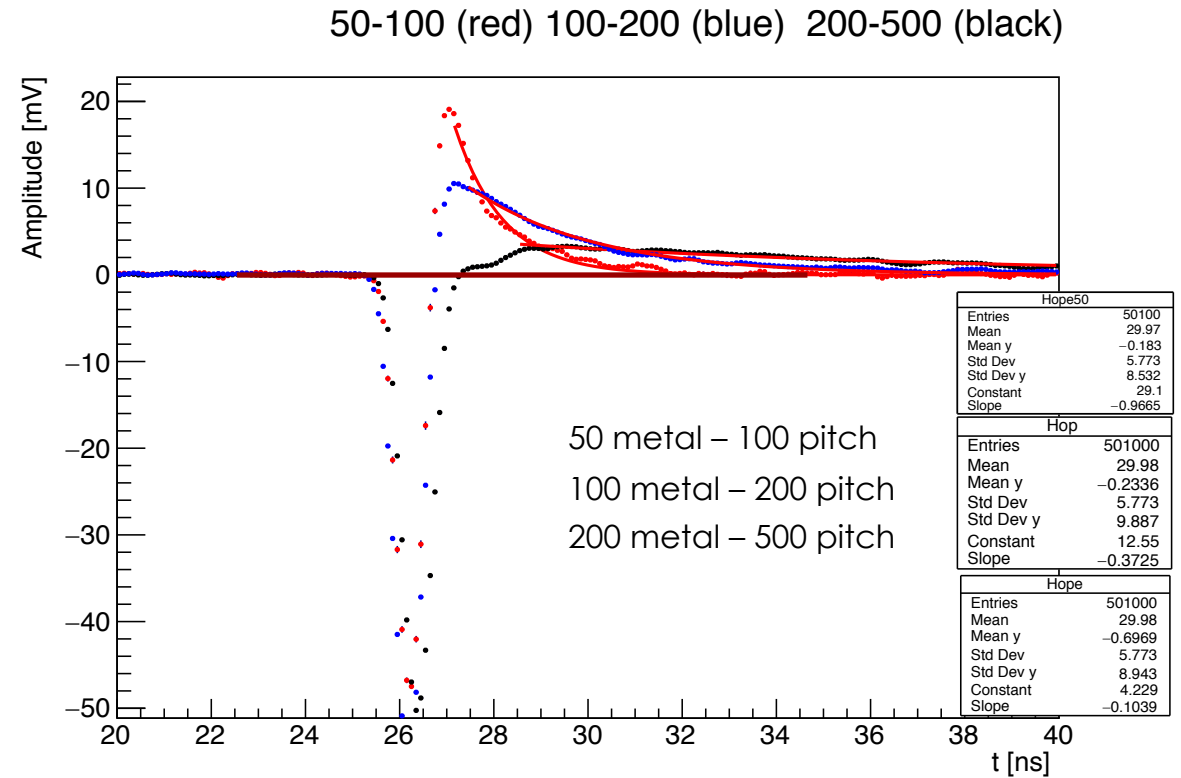
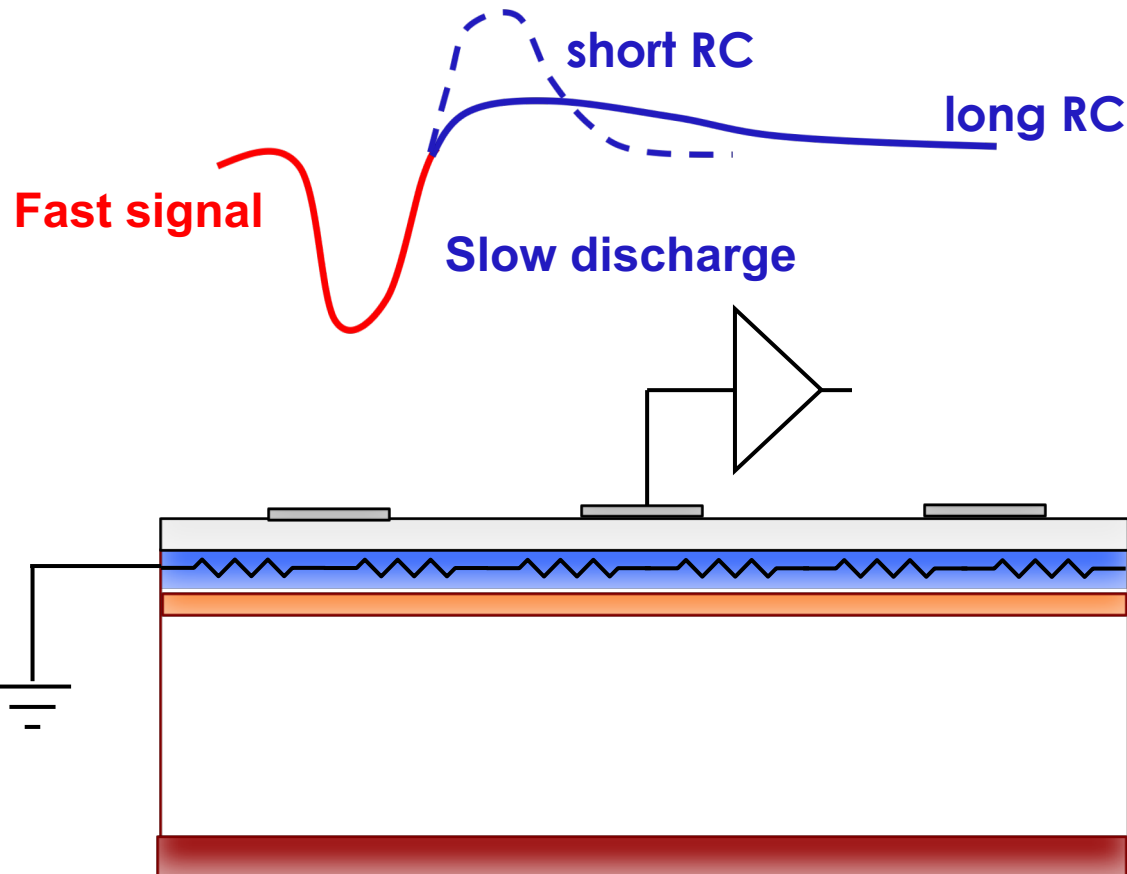
Act 2: the signal propagates on the n++, firing the near-by pads

1. The n++ is an almost ideal resistive divider
2. Lateral spread controlled by n++ resistivity, metal pad capacitance, pitch, system inductance.
3. The metal AC pads act as “pick-up” electrodes
4. Signal gets smaller and delayed with distance



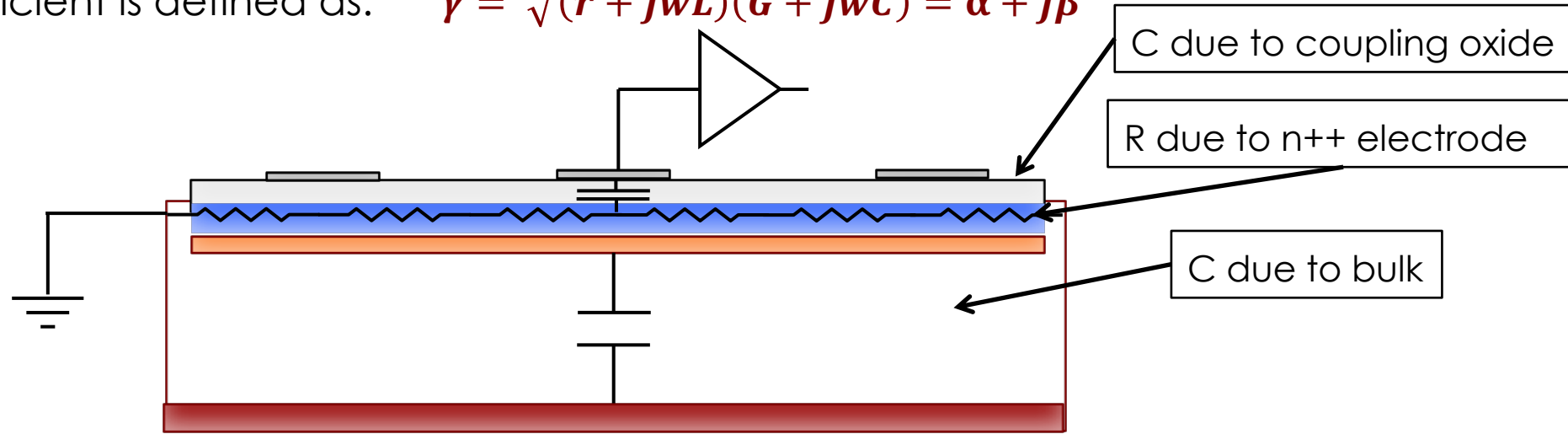
RSD Signal formation - III

Act 3: the signal discharges, according to the read-out RC. Small RC have larger and shorter positive lobes (need to discharge the same charge in a shorter time)

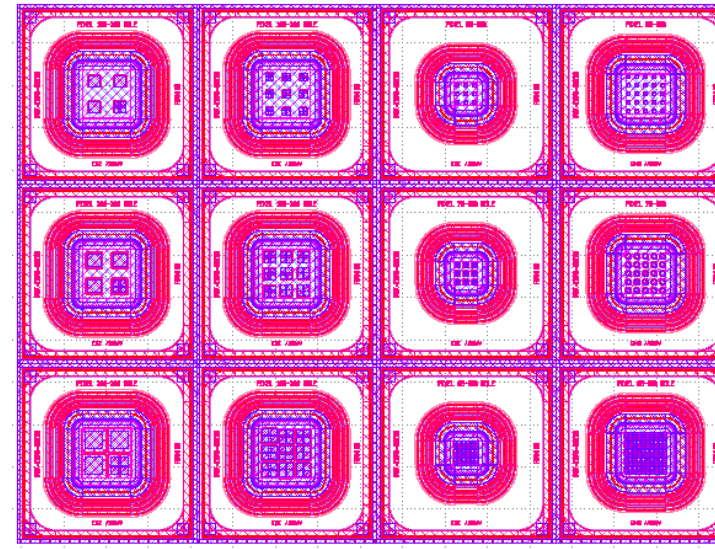


Effect of L,C,R on the signal propagation

The n++ layer of RSD is a lossy transmission line, with R,C and L components. The propagation coefficient is defined as: $\gamma = \sqrt{(r + j\omega L)(G + j\omega C)} = \alpha + j\beta$



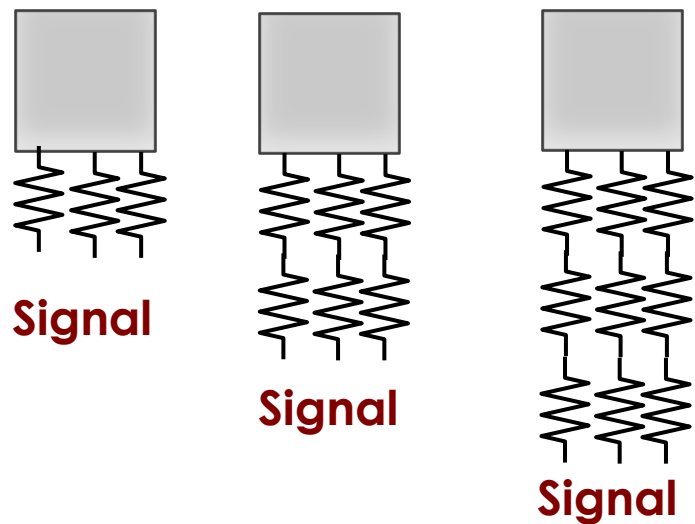
In order to study signal formation, propagation, and attenuation in RSD, sensors with many geometries have been produced (metal-pitch combinations), including strips and large matrices. For example: →



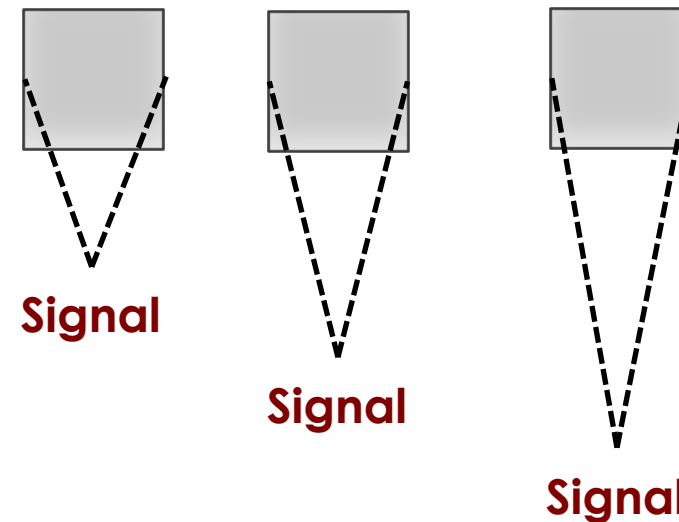
subset of the structures manufactured in the RSD project

Attenuation versus distance

How is the signal attenuated as a function of the distance from the pad?



The amplitude decreases linearly with **Increasing distance** due to the resistivity of the n++ layer



The amplitude decreases linearly with **decreasing angle** (angle of view)

Attenuation with distance: resistivity and angle

The 2 sources of attenuation with distance, $V(d)$, can be parametrized as follow:

1) Attenuation due to the resistivity:

$$V(d) = V(0) - \beta * d$$

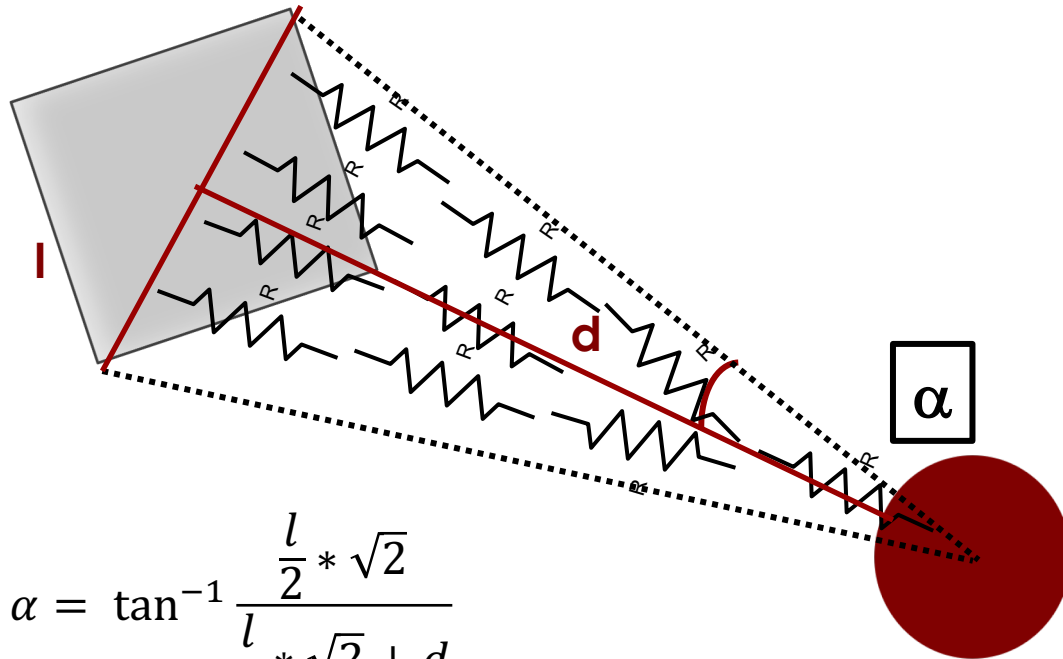
where

$V(0)$: amplitude at distance = 0

d : distance from metal

2) Attenuation due to the angle of view:

$$V(d) = V(0) \frac{\tan^{-1} \frac{\frac{l}{2} * \sqrt{2}}{\frac{l}{2} * \sqrt{2} + d}}{\tan^{-1} \frac{\frac{l}{2} * \sqrt{2}}{\frac{l}{2} * \sqrt{2}}}$$



$$\alpha = \tan^{-1} \frac{\frac{l}{2} * \sqrt{2}}{\frac{l}{2} * \sqrt{2} + d}$$

where

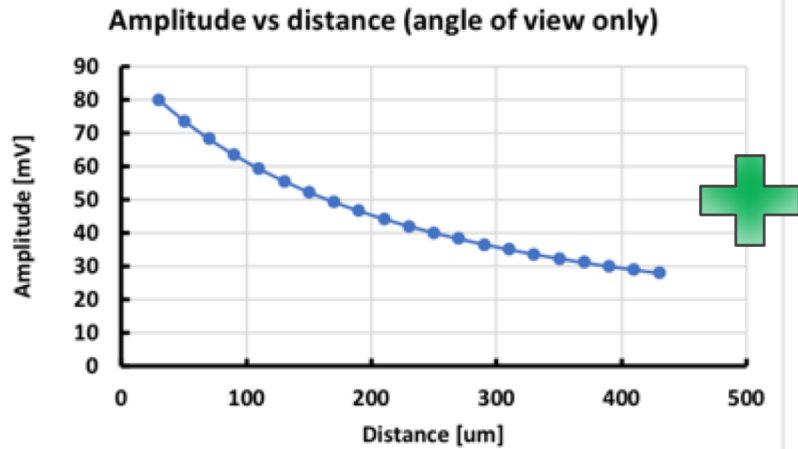
l : side of the pad

d : distance from metal

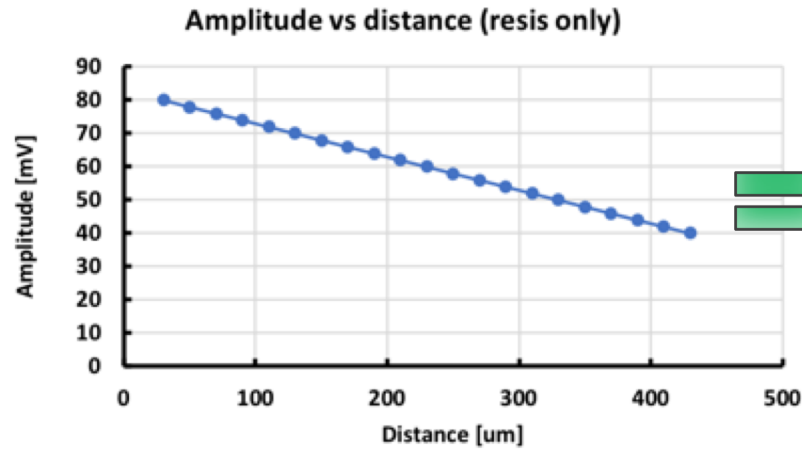
Model of signal attenuation

Using the equations in the previous page, we can make a model of the combination of the two type of attenuations

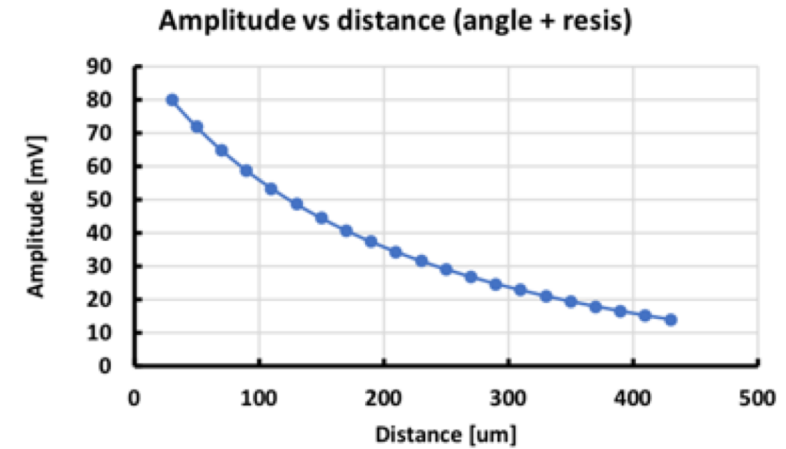
Effect of decreasing angle



Effect of increasing distance



Combined effects of decreasing angle and increasing distance



Fitting the data

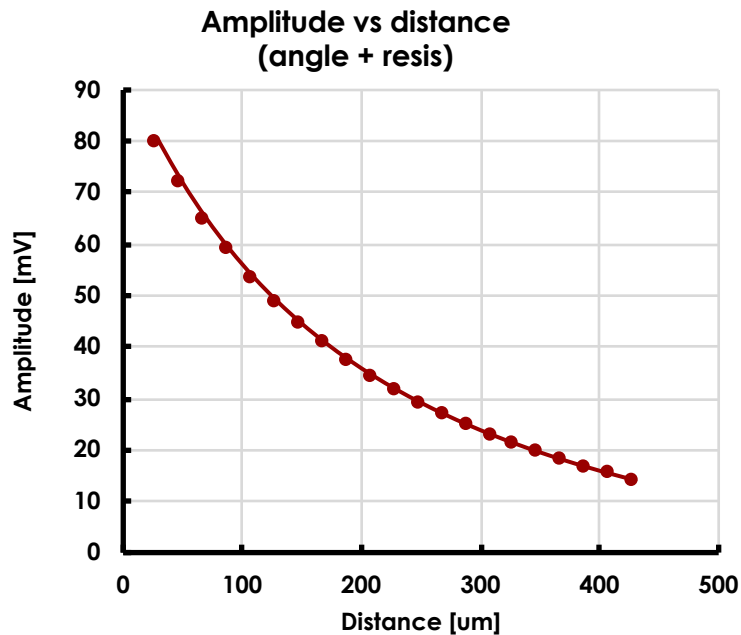
x = distance

[0] = amplitude

[1] = **resistive attenuation with distance**

[2] dimension of the pad, fixed to 1/sqrt(2)

$$([0] + [1] * x) * \left(\frac{\text{atan2}([2], [2] + x)}{\text{atan2}([2], [2])} \right)$$



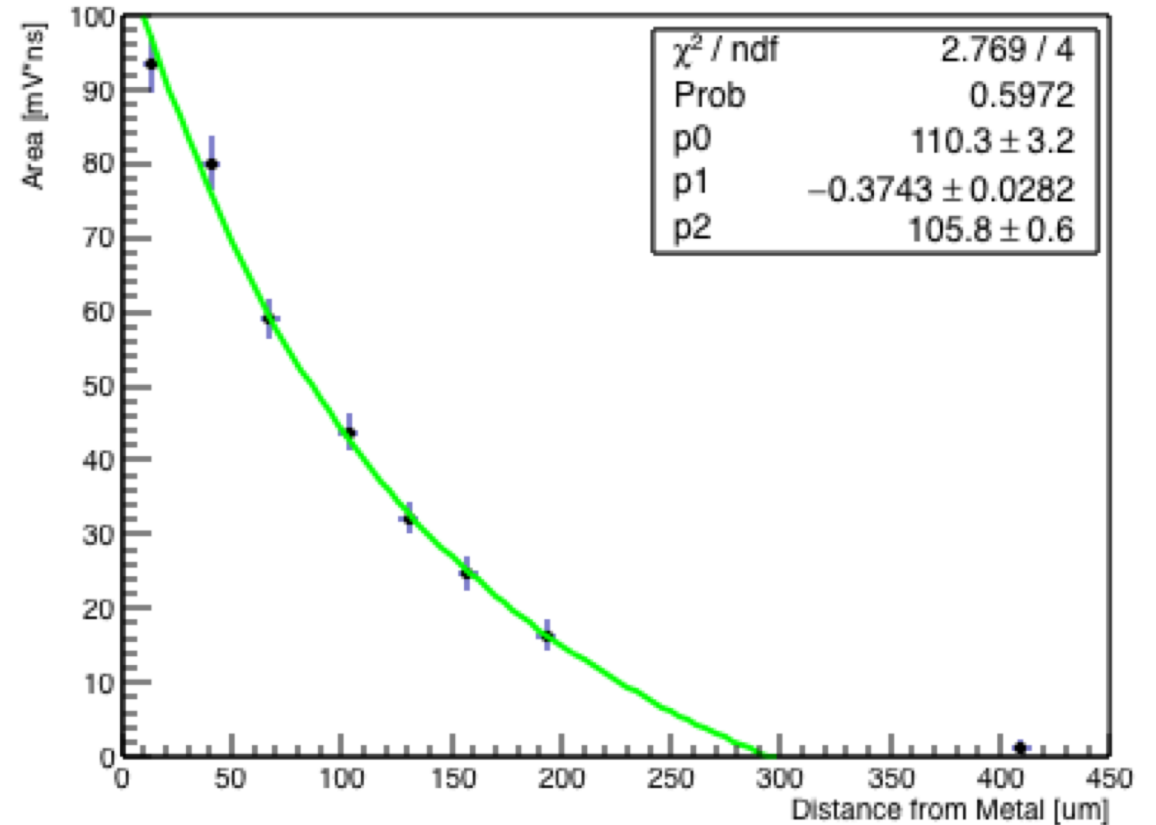
DATA



Model



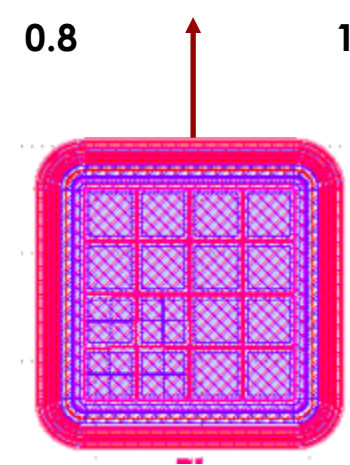
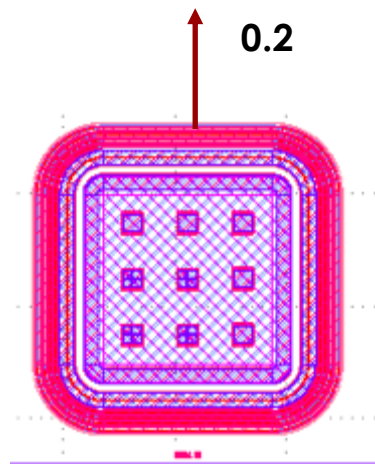
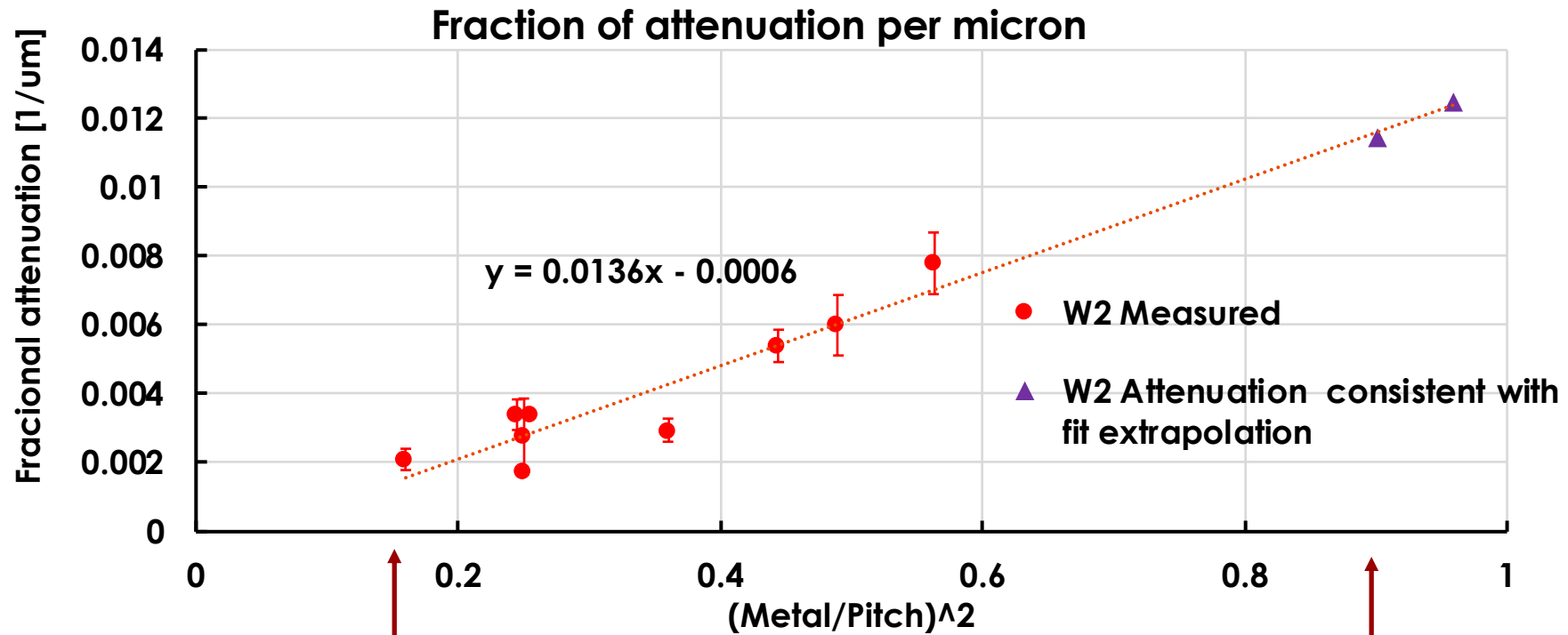
W2 Area vs Distance from Metal ch 0 150-300



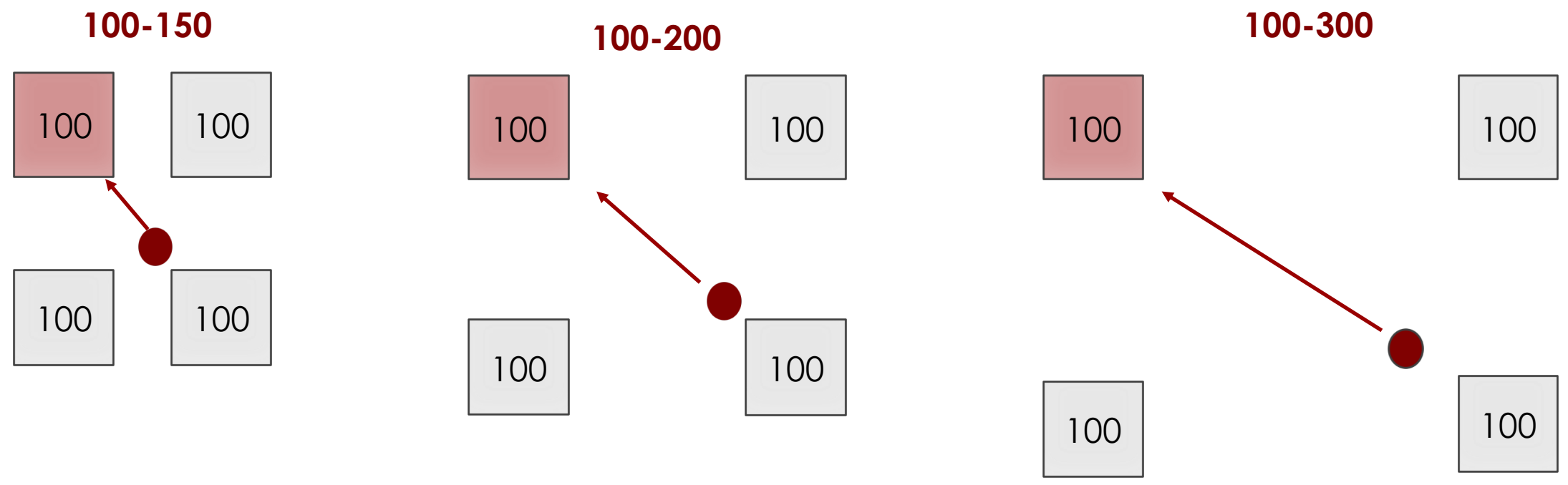
**Now we have an analytic model of signal attenuation
The only unknown is [1], the attenuation with distance**

Effect of geometry on attenuation

The attenuation factor was measured for many geometries. **It is dominated by the coupling capacitance: attenuation is higher for sensors where the metal pads cover a large fraction of the area**

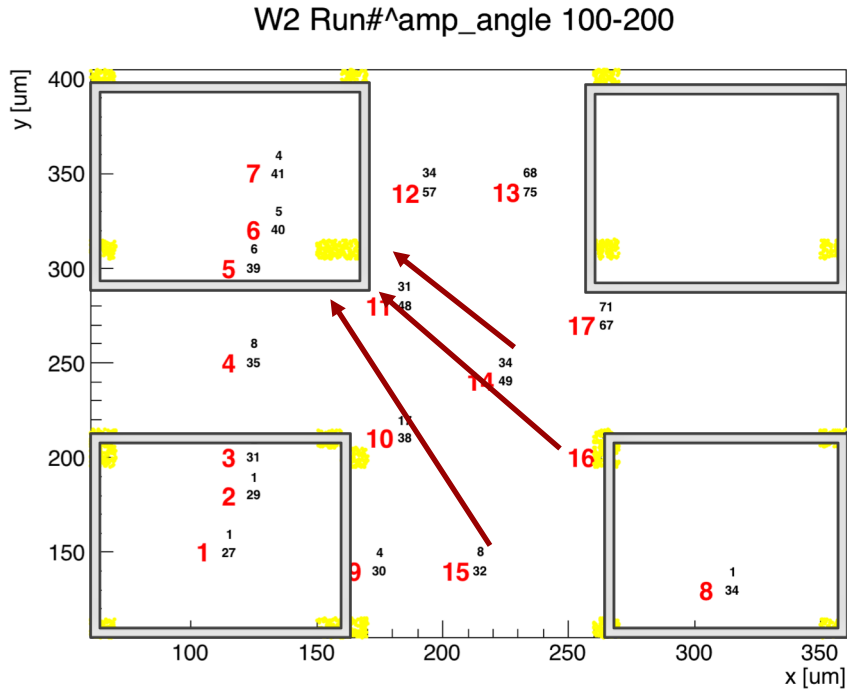


Signal delay

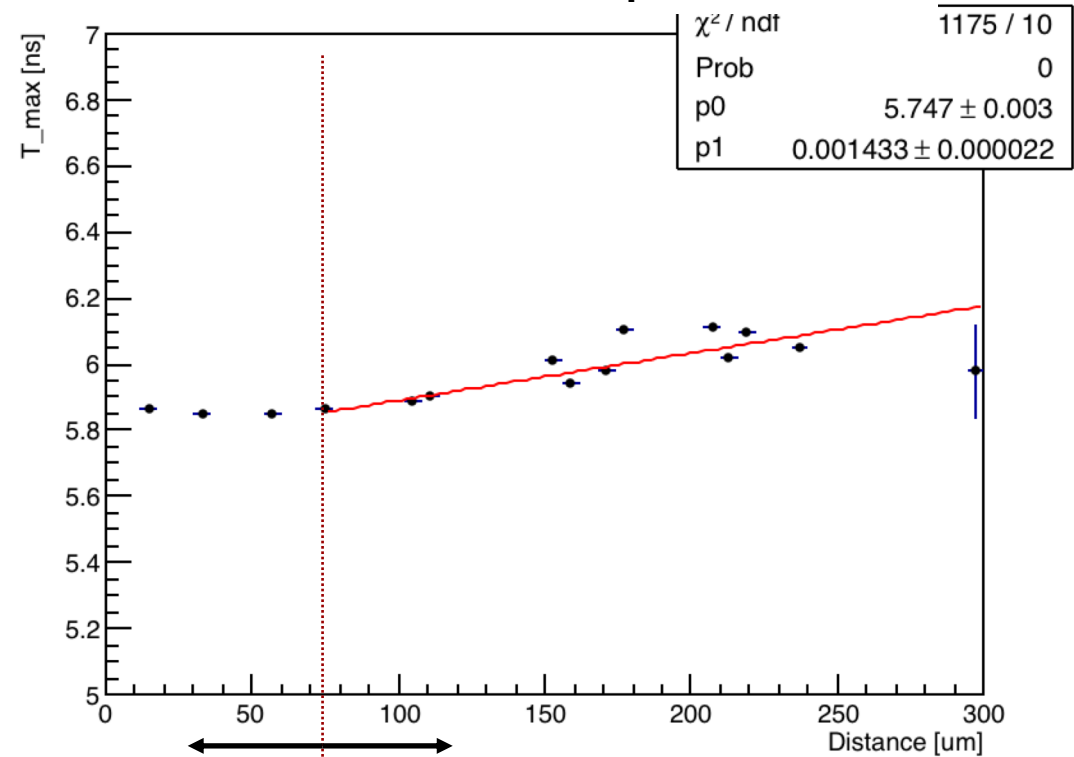


What is the signal delay as a function of distance?

Laser study: signal delay



Signal delay as a function of distance from the pad center



Propagation in metal:
no delay

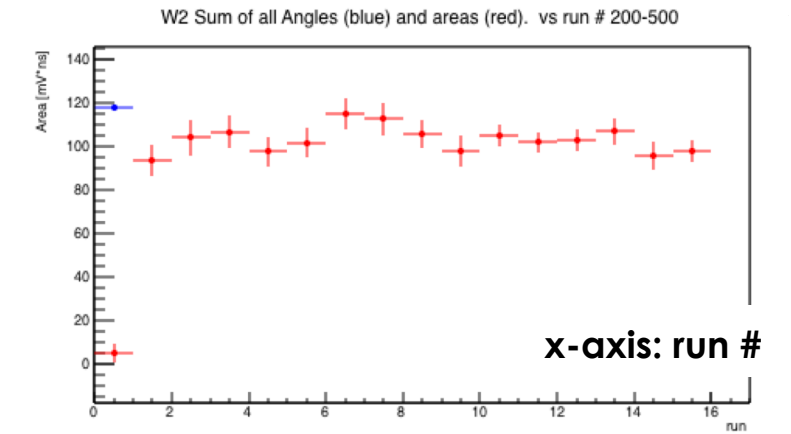
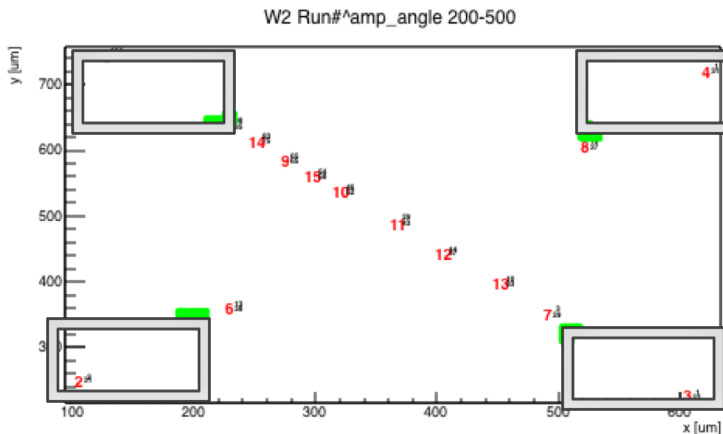
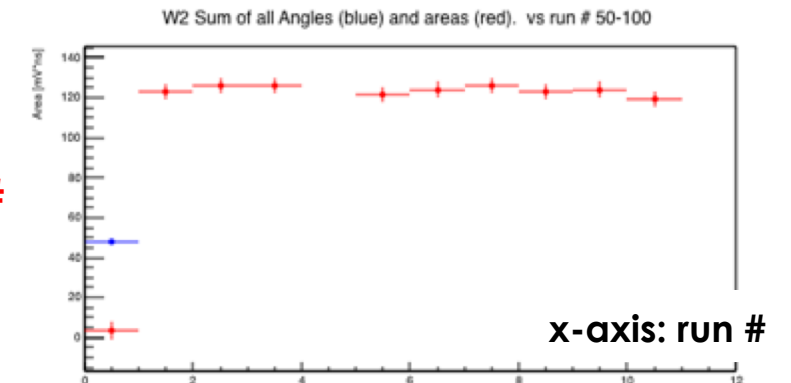
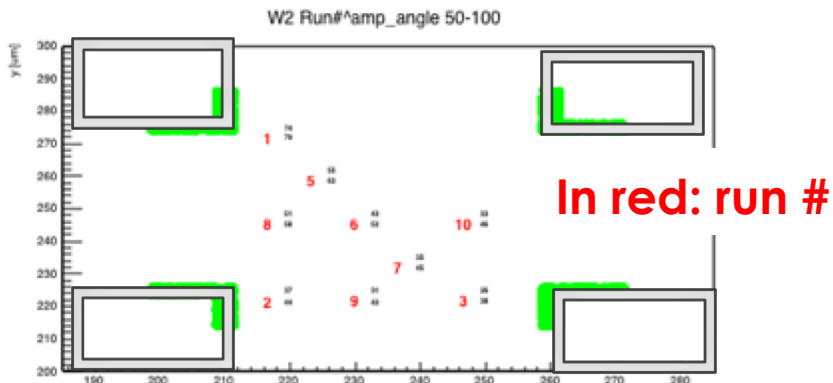
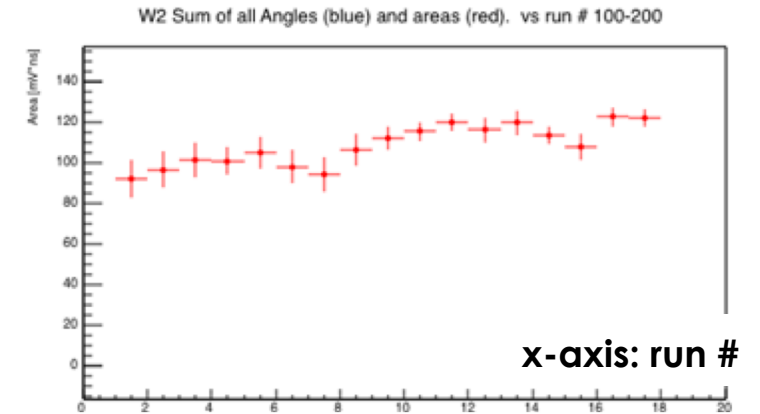
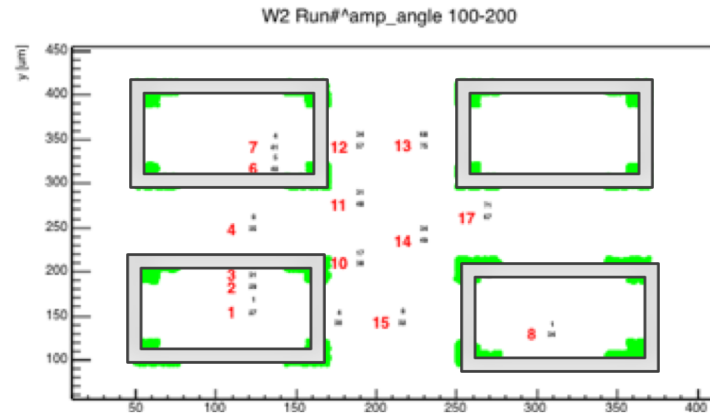
Propagation in n++
delay

The signal is delayed when it propagates in the n++ and not when it does in the metal

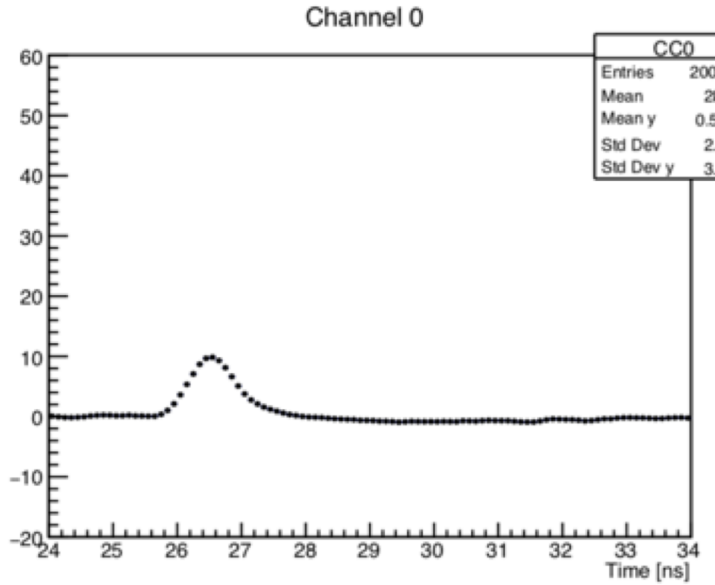
Laser study: total charge vs position

For all geometries, **the sum of the signals on the 4 pads is almost constant**, weakly dependent on the hit position

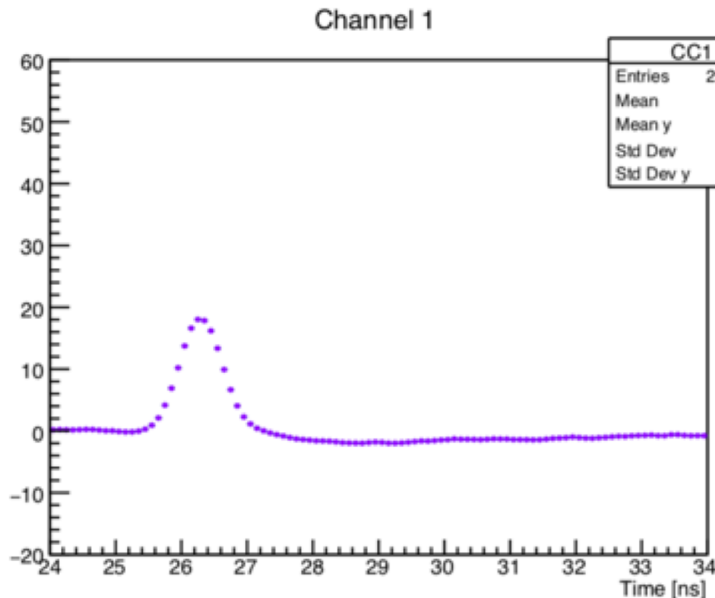
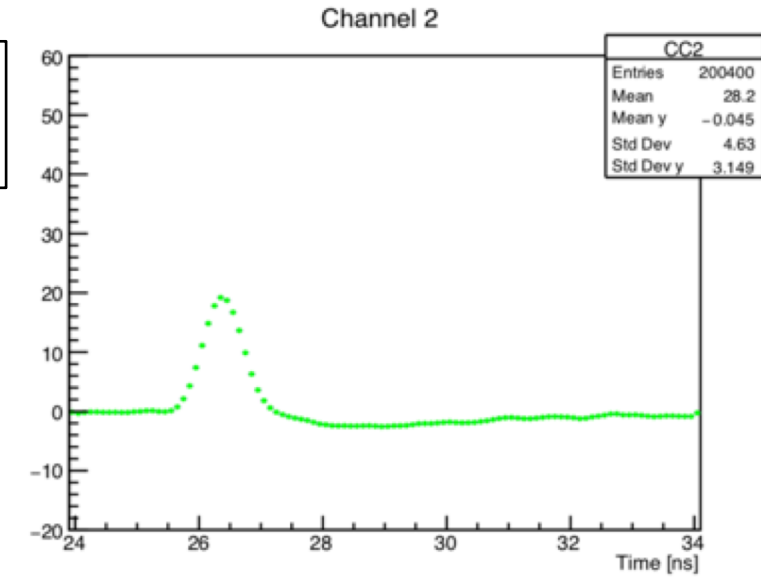
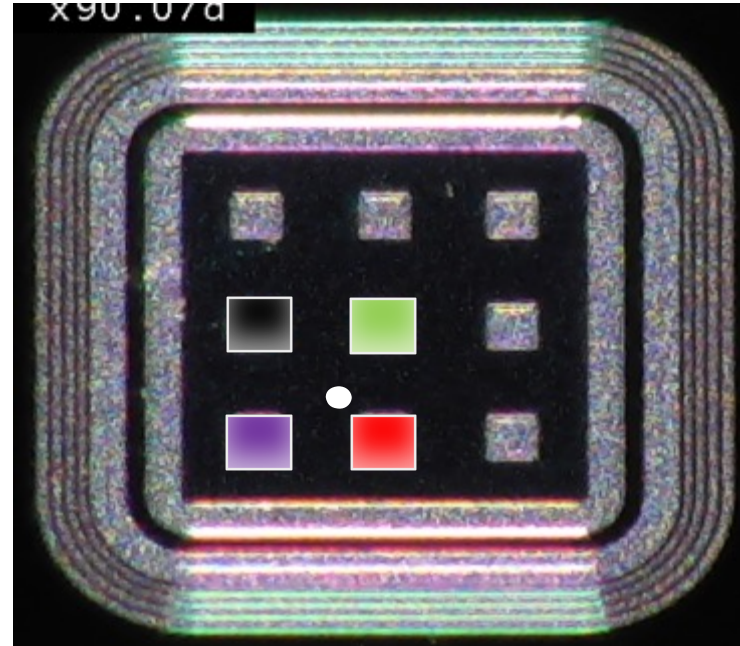
$$A_{tot} = \sum_1^n A[i] = const$$



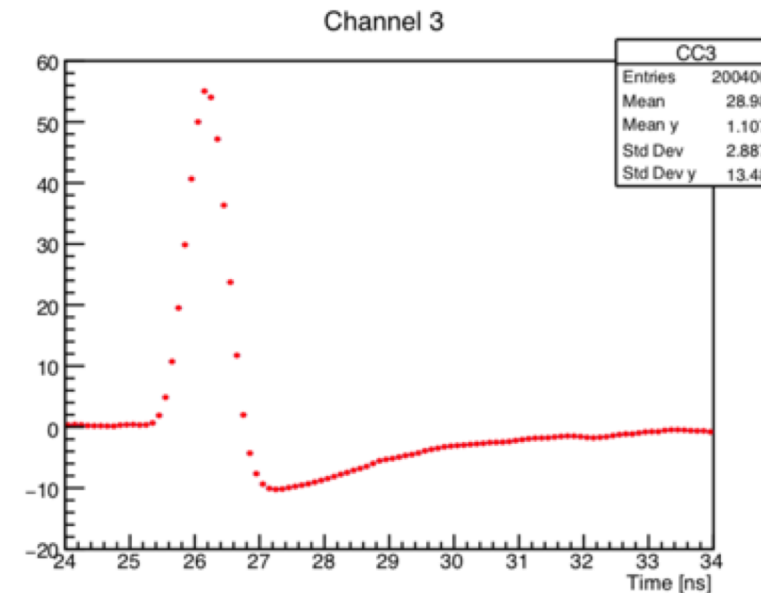
Position reconstruction method - I



Each hit position is characterized by a specific set of amplitudes in the pads

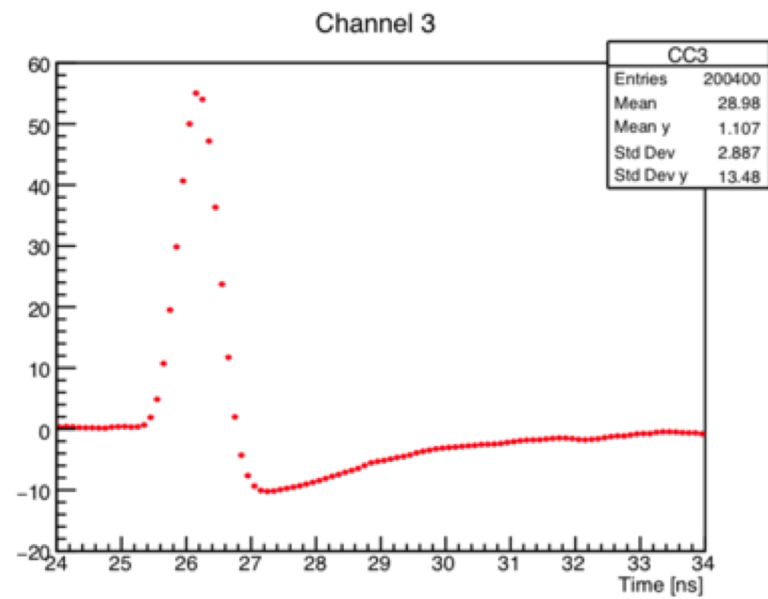
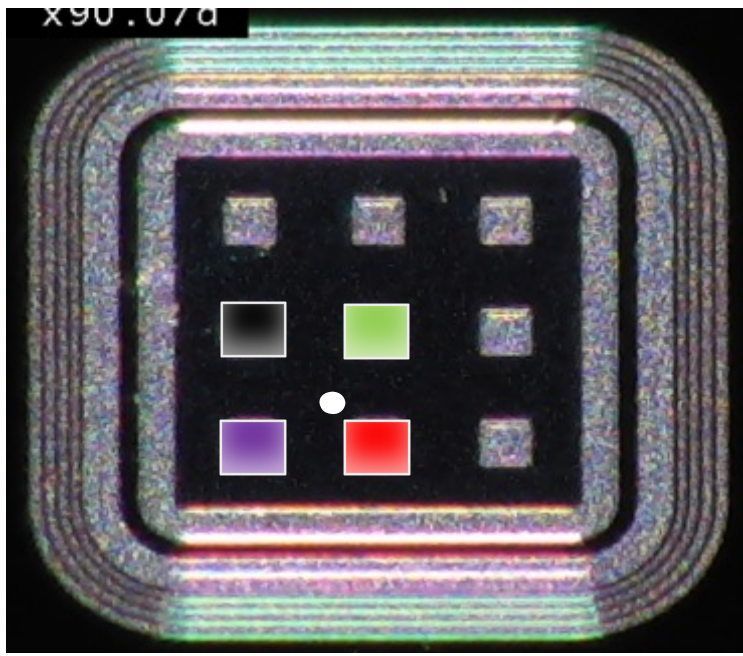
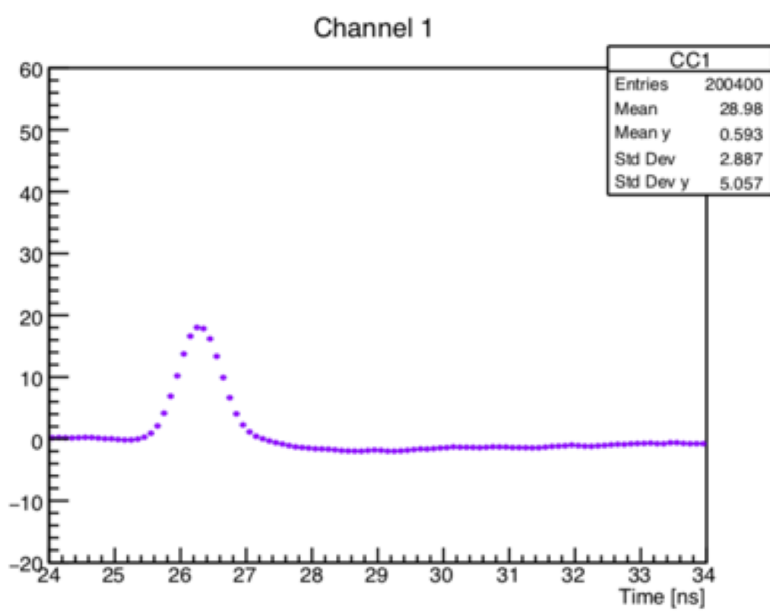
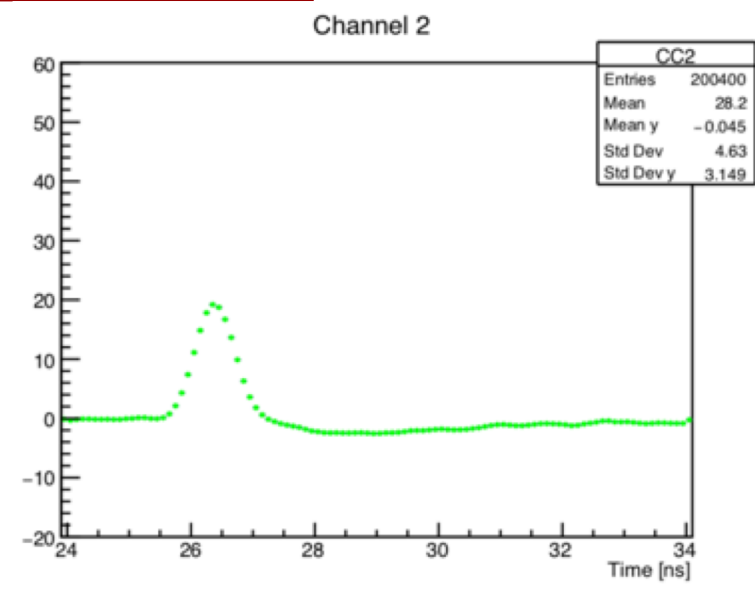
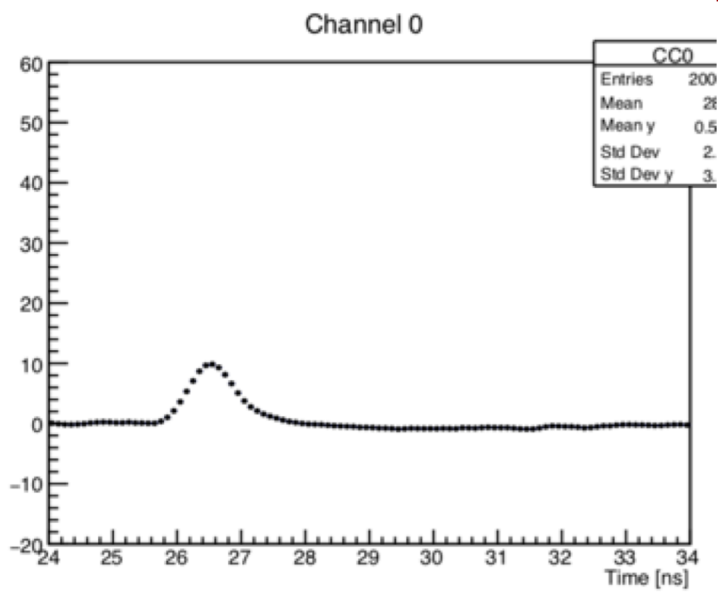


It is possible to associate to each x-y point the relative importance of the signal in each pad: $A[0]/A_{tot}$, $A[1]/A_{tot}$, $A[2]/A_{tot}$, $A[3]/A_{tot}$,
In this case (0.09, 0.18, 0.18, 0.55)



Position reconstruction method - I

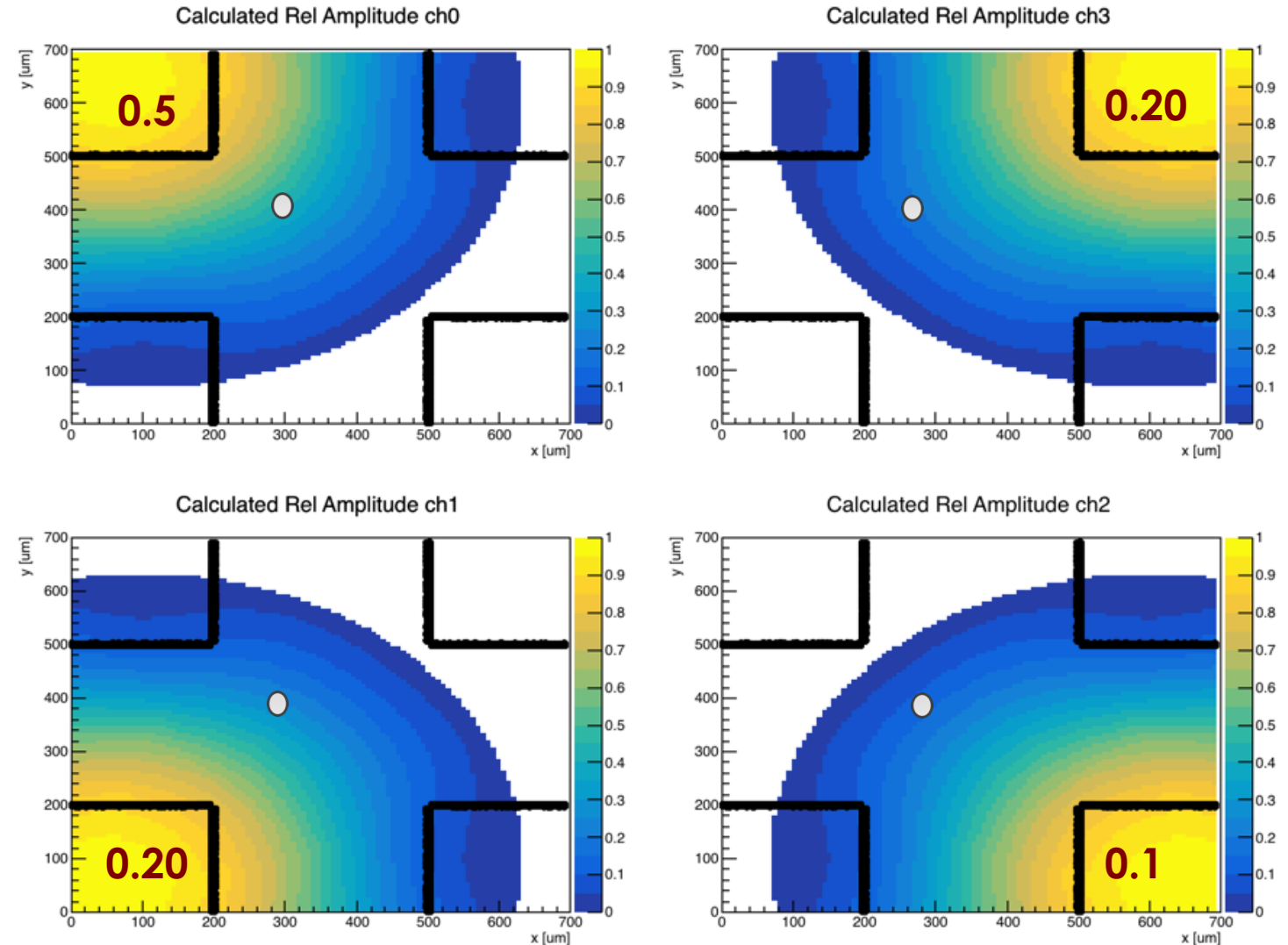
N. Cartiglia, INFN Torino, TREDI, Wien, 18/02/2020



Using the **attenuation model**, the fraction of the total amplitude seen in each pad for every x-y point can be calculated

In this example, 4 values:
(0.5,0.2,0.1,0.2) are associated to the x-y point

The analytic model allows computing a look-up table containing for each x-y point the relative signal amplitude of every pad.



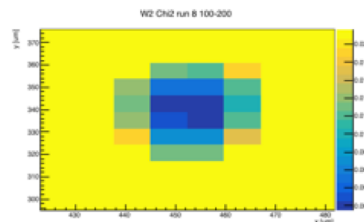
Position reconstruction method: the recipe

Recipe:

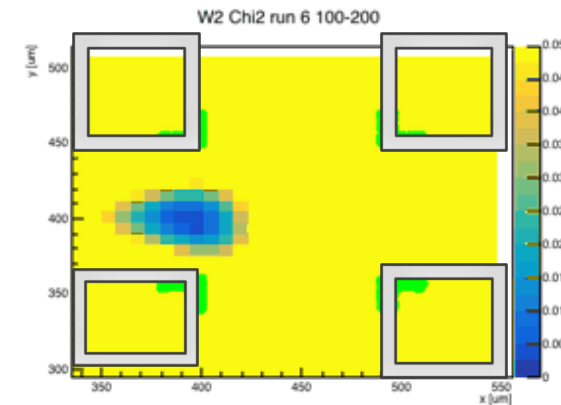
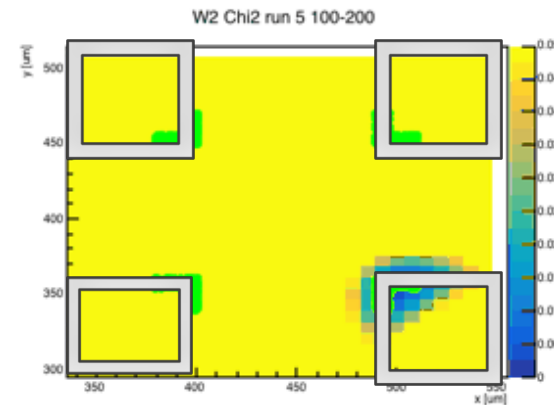
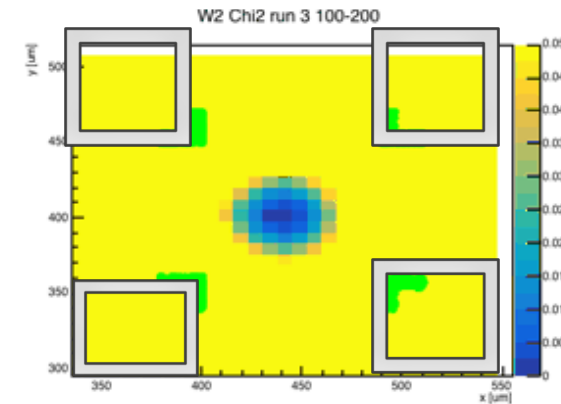
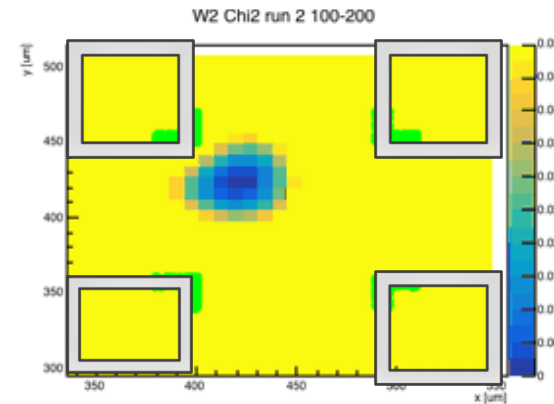
- For each hit, calculate the total amplitude summing all pads: $A_{tot} = \sum A[i]$
- Calculate the relative amplitudes $\left(\frac{A[i]}{A_{tot}}\right)_{Meas}$ seen in each pad.
- Use the look-up table to find which x-y bin minimize the quantity:

$$\chi^2 = \sum_1^4 \left[\left(\frac{A[i]}{A_{tot}}\right)_{Meas} - \left(\frac{A[i]}{A_{tot}}\right)_{Calc} \right]^2$$

- Perform a local interpolation around the minimum.



χ^2 values for 4 different laser shots
(sensor geometry: 100-metal 200-pitch)
The reconstructed position is the bin with the minimum χ^2 value



Laser study: position resolution

Shooting the laser in many positions, the “**single point precision**” and the “**overall precision**” can be evaluated.

This is done by comparing the position reconstructed using the look-up table to the known laser position.

Two examples:

Geometry:

Single point precision:

Global precision:

100 Metal, 200 pitch

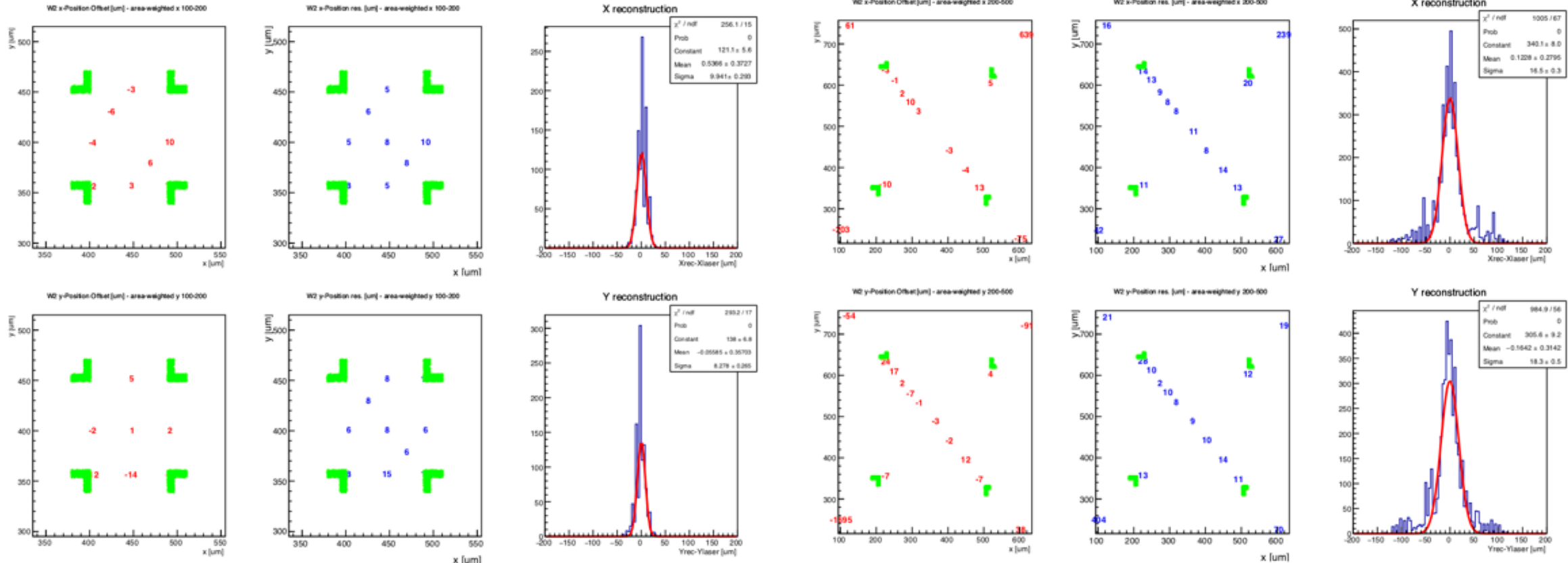
6 micron

10 micron

200 Metal, 500 pitch

10 micron

18 micron



Laser study: time resolution

An estimate of the RSD time resolution is obtained in the following way:

- 1) Determine the hit position using the look-up table
- 2) Correct for the propagation delay between the hit position and each pad
- 3) Compute the amplitude weighted time centroid (assume no jitter on the laser shot)

Geometry:

100 Metal, 200 pitch

200 Metal, 500 pitch

Single point precision:

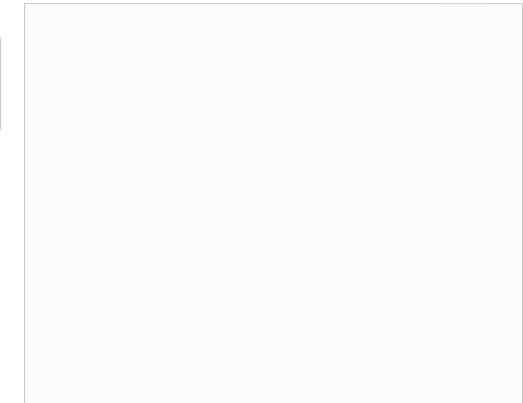
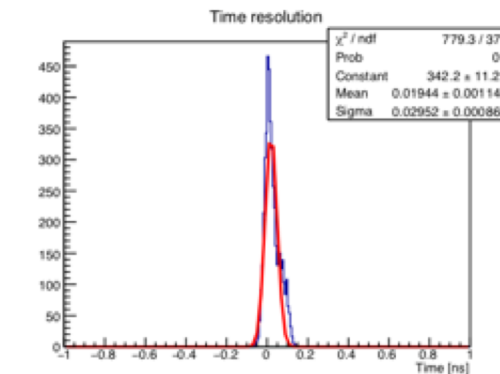
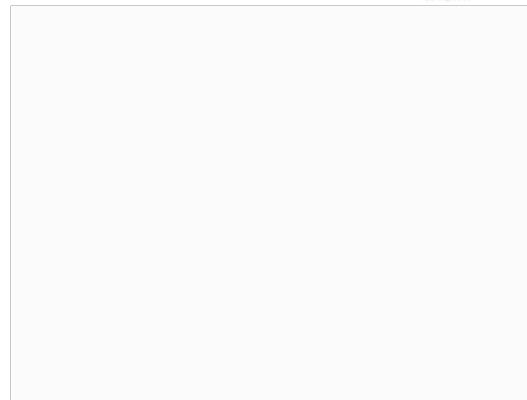
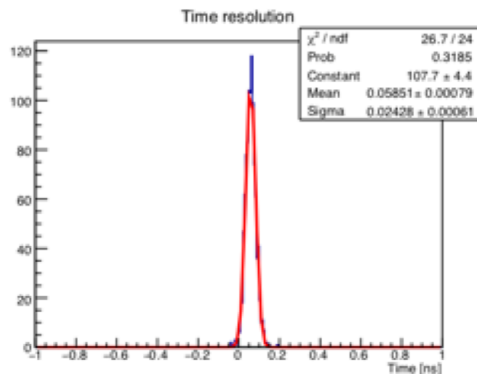
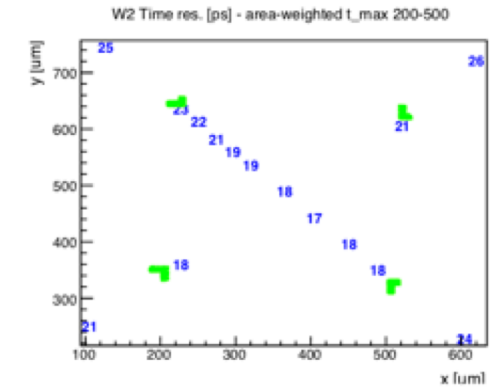
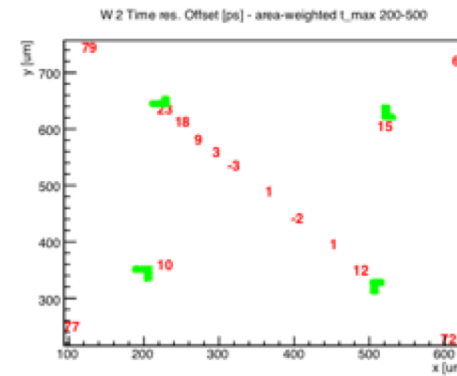
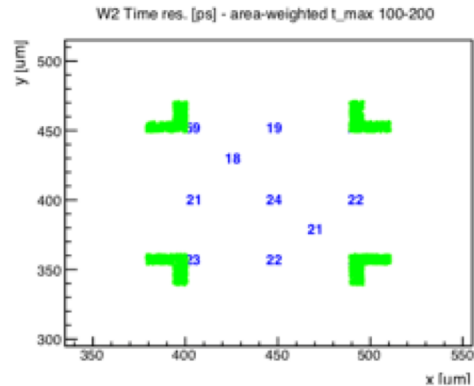
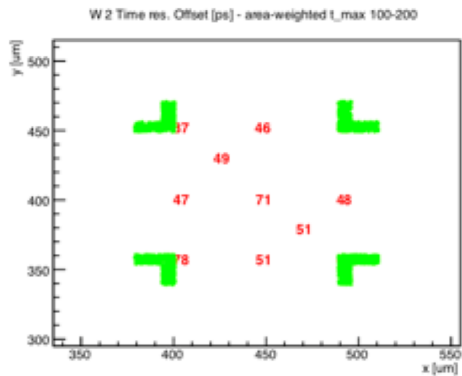
20 ps

20 ps

Global precision:

24 ps

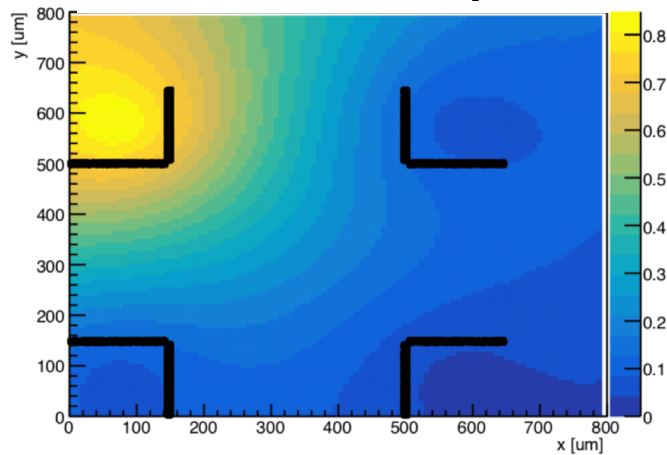
30 ps



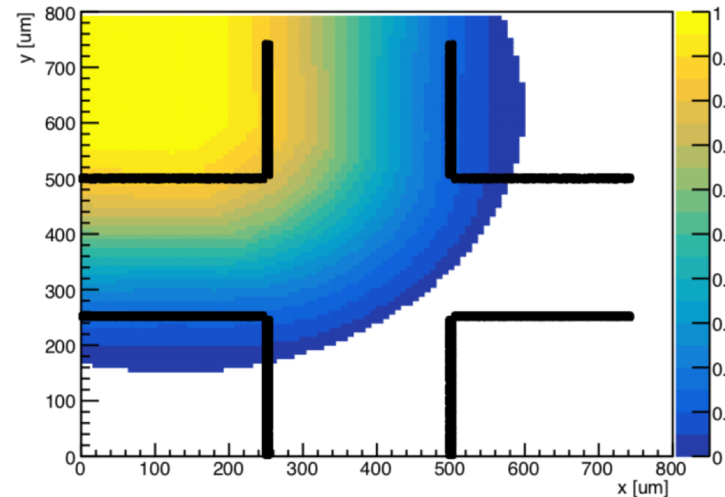
Design optimization

Position and time resolutions are optimized when several pads see a signal
 Let's examine signal sharing in 3 designs with equal pitch (500 micron)

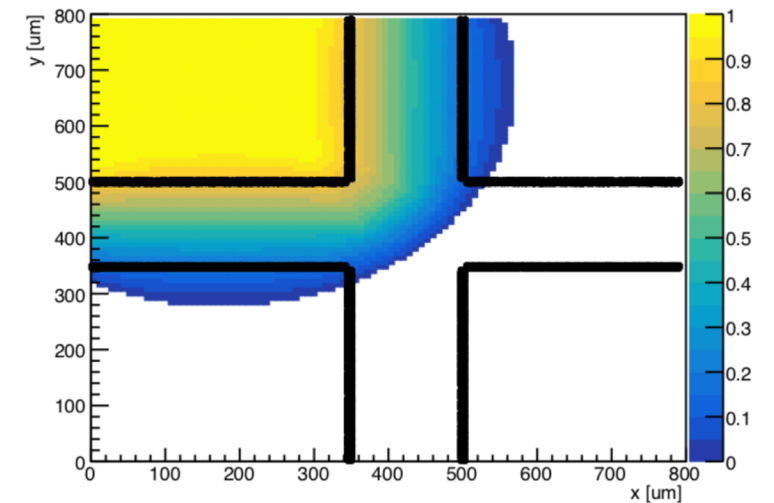
150 metal – 500 pitch



250 metal – 500 pitch



350 metal – 500 pitch



For small metal pads, the signal is shared among many pads, however the amplitude seen by each pad is small

For large metal pads, the signal is very attenuated and sharing is limited.

Best performance is obtained when at least 4 pads see an amplitude well above the noise level.

- AC-LGADs (RSD) are silicon sensors working on the principle of charge sharing
- Charge sharing is obtained using a delayline-like lossy system (and not drift lines)
- RSDs employ the LGAD mechanism for charge multiplication
- They have a uniform response, no dead area between pads. This design is well suited for very small pitch.
- Charge sharing allows reaching the same spatial precision of traditional silicon detector using a factor of 5-10 larger pitch (in bump-bonding design, this allows a lot of space for electronics):
 - $\sigma_{position} = 10 \mu m$ for 200-micron pitch, $\sigma_{position} = 20 \mu m$ for 500-micron pitch
- Time resolution, obtained using information from multiple pads, is at the level of (or better) traditional LGAD sensors: $\sigma_{time} = 25 - 30 ps$
- Signal delay happens only in n++, not in metal: for best results use round and not square metal pads
 - First ever polka dot detector



Next steps:

- More testing of other geometries, strips...
- Beam test
- Irradiated samples have been received last week, need to check the stability of the sensors' parameter

Acknowledgement

We kindly acknowledge the following funding agencies, collaborations:

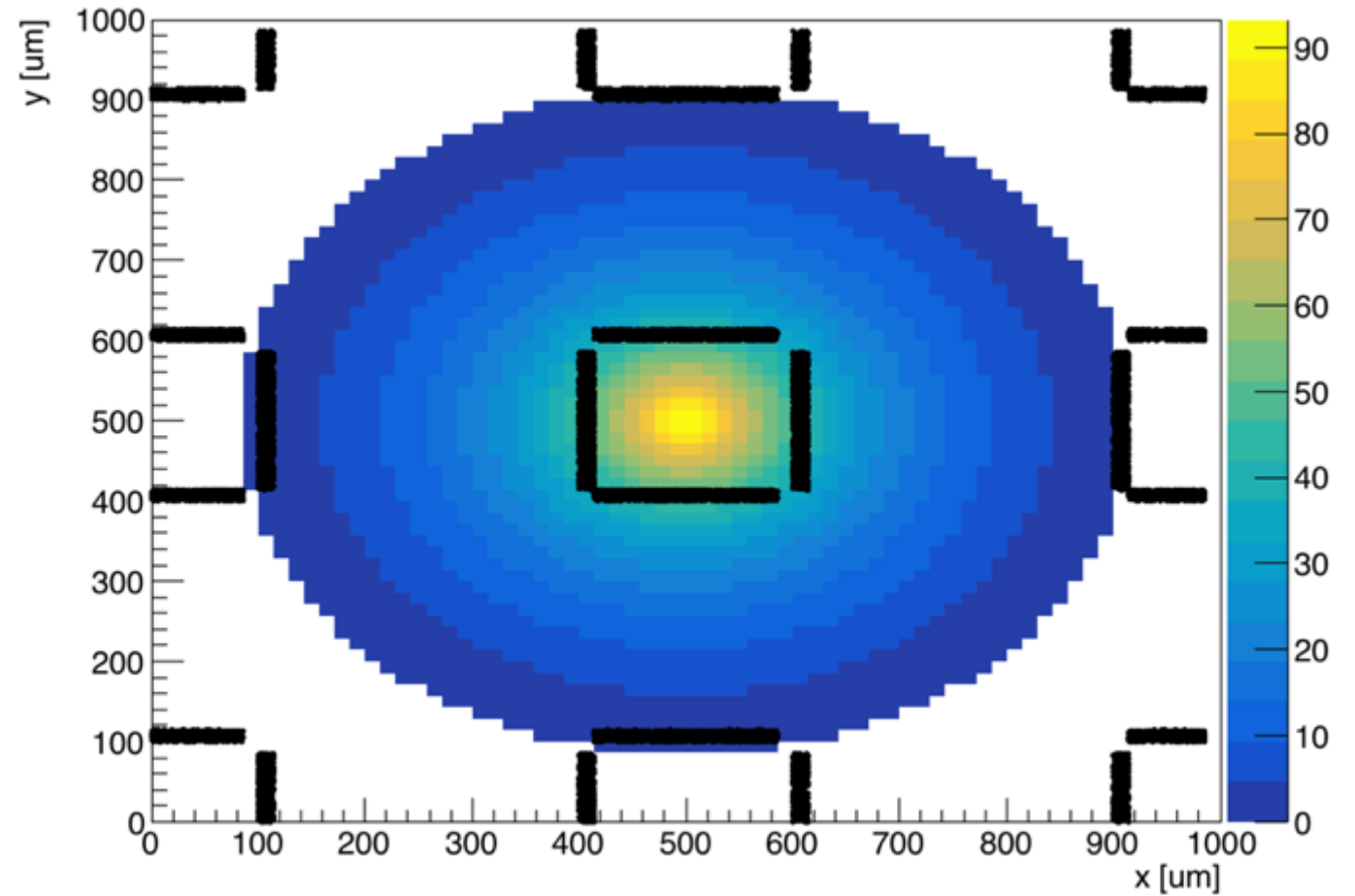
- INFN - Gruppo V
- Horizon 2020, grant UFSD669529
- Horizon 2020, grant no. 654168 (AIDA-2020)
- U.S. Department of Energy grant number DE-SC0010107
- Dipartimenti di Eccellenza, Univ. of Torino (ex L. 232/2016, art. 1, cc. 314, 337)
- Ministero della Ricerca, Italia , PRIN 2017, progetto 2017L2XKTJ – 4DinSiDe
- Ministero della Ricerca, Italia, FARE, R165xr8frt_fare



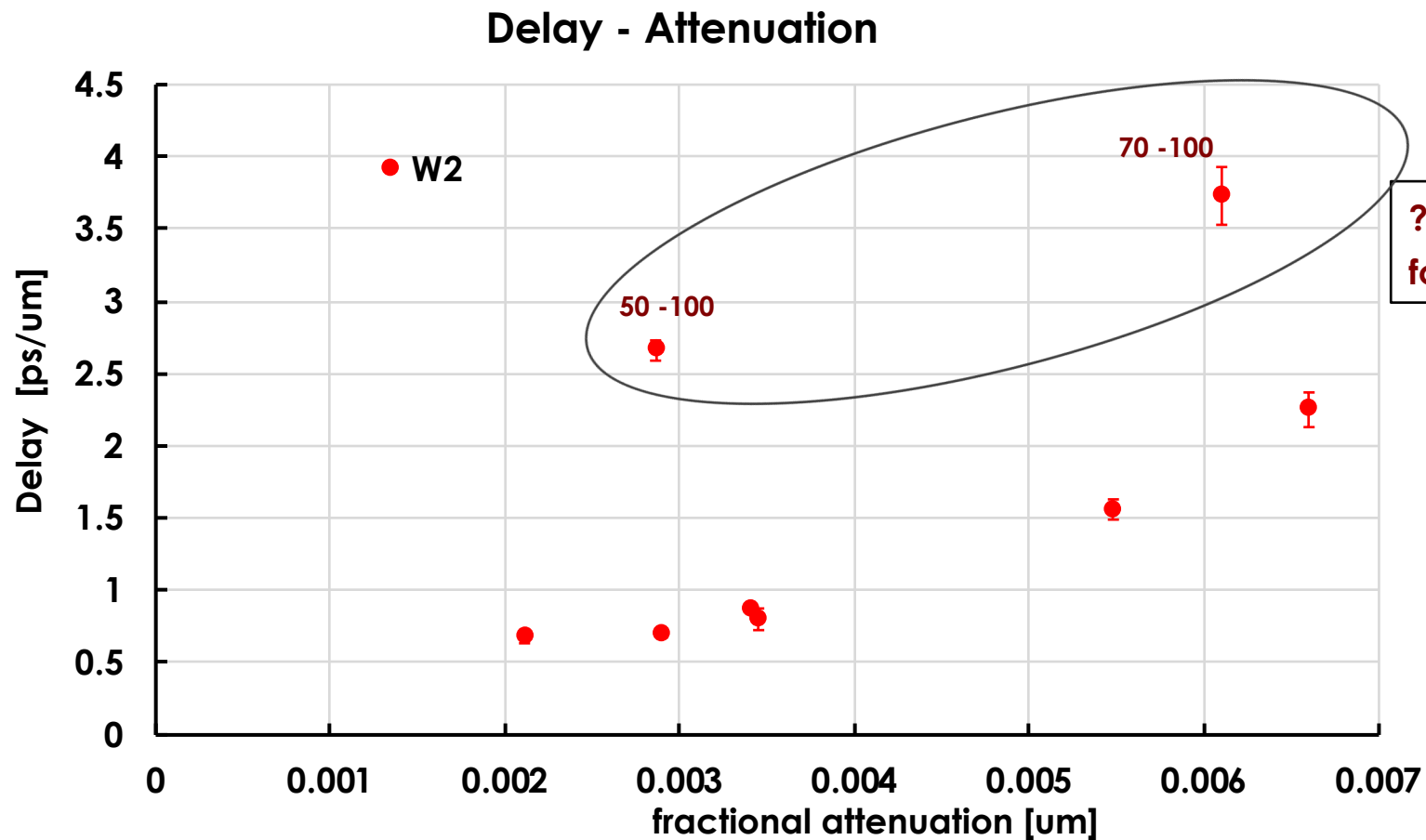
extra

$$A(d) = (A(0) - \beta * d) \frac{\tan^{-1} \frac{\frac{l}{2} * \sqrt{2}}{\frac{l}{2} * \sqrt{2} + d}}{\tan^{-1} \frac{\frac{l}{2} * \sqrt{2}}{\frac{l}{2} * \sqrt{2}}}}$$

W2 3x3 Amplitude Map 200-500



Attenuation vs delay



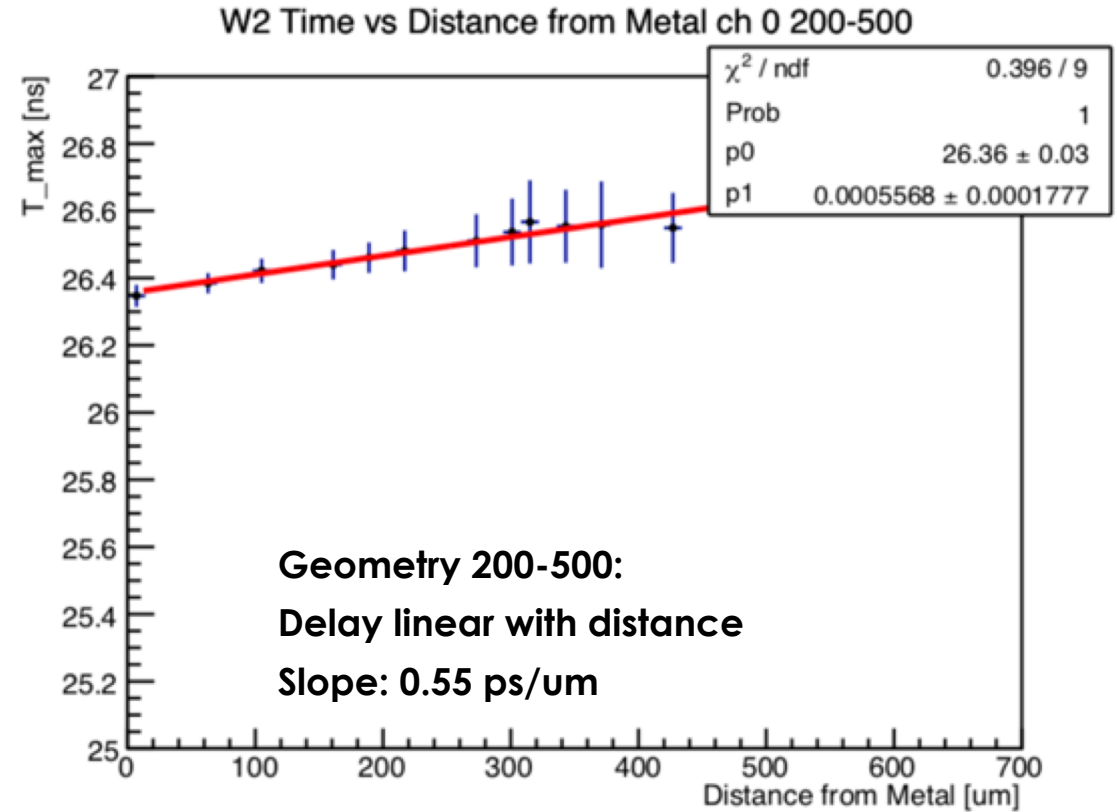
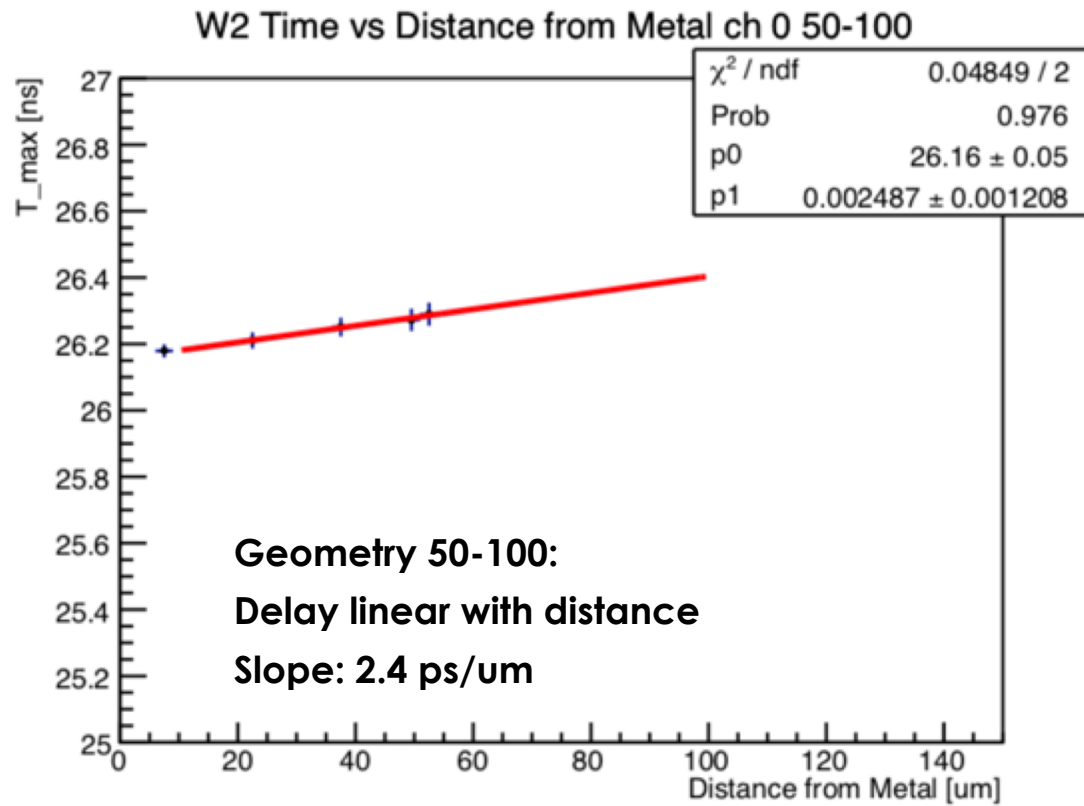
?? Why so much delay for small gaps?

Delay and attenuation are connected in the dispersion relationship:

higher attenuation is coupled to higher delay

→ The two smallest geometries are somewhat different.

Laser study: signal delay



The delay slope is computed for every geometry