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REFERENCE

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Note: When approved, an Engineering Change Request becomes an Engineering Change Order. This document is uncontrolled when printed. Check the EDMS to verify that this is the correct version before use. ENGINEERING CHANGE REQUEST **Installation of the 11 T Dipole Full Assembly in LHC P7 (HL-LHC WP11)** BRIEF DESCRIPTION OF THE PROPOSED CHANGE(S): It is foreseen to substitute in the DS region at point 7 two 14.3 m long 8.33 T standard LHC main dipoles (MB) each with a cryo-assembly composed by a pair of 5.5 m-long 11 T dipoles with in the middle a 3.3 m long bypass cryostat, in which is hosted a TCLD collimator. Thanks to this change the design losses can be sustained without quench. DOCUMENT PREPARED BY: DOCUMENT TO BE CHECKED BY: DOCUMENT TO BE APPROVED: D. Schoerling et al. **HiLumi-WP11-Integration** C. Adorisio, G. Arduini, V. Baglin, M. Barberan, I. Bejar Alonso, N. Bellegarde, M. Bernardini, C. Bertone, C. Boccard, L. Bottura, G. Bregliozzi, M. Brugger, J.P. Burnet, S. Bustamante, S. Chemli, F. Cerutti, P. Chiggiato, J. P. Corso, D. Delikaris, B. Delille, R. Denz, A. Devred, R. de Maria, S. Evrard, P. Fessia, R. Folch, A. Foussat, J.- F. Fuchs, C. Gaignant, M. Giovannozzi, G. Girardot, J.-L. Grenard, M. Lamont, S. Le Naour, M. Martino, D. Missiaen, M. Modena, V. Montabonnet, Y. Muttoni, M. Nonis, T. Otto, E. Page, S. Redaelli, D. Ricci, I. Romera Ramirez, B. Salvant, F. Savary, J. Sestak, A. Siemko, R. Steerenberg, L. Tavian, M. Tavlet, C. Vollinger, J. Wenninger, M. Zerlauth, A. Lechner, C. Bahamonde Castro, C. Zamantos. P. Collier (on behalf of LMC) L. Rossi (on behalf of the HL-LHC project) DOCUMENT SENT FOR INFORMATION TO: ATS Group Leaders SUMMARY OF THE ACTIONS TO BE UNDERTAKEN: Following drawings and documents need to be updated, once the change is being performed: -Survey reference drawings to be created (D. Missiaen) -LHCLSD7_0002, LHCLSD7_0004, LHCEY___7001, and LHCEY___7008 (P. Orlandi (responsible) and M. Zerlauth) -LHCLSQR_0032 and LHCLSQR_0033 (R. van Weelderen) -LHCLSVI_0020 and LHCLSVI_0031 (P. Cruikshank) -LHCQQ_IG0033 and LHC-LI-ES-0017 (JP. Tock) -LHC-LBA-ES-0011, LHC-LI-ES-0001, LHC-LE-ES-0001, and LHC-LE-ES-0002 (D. Duarte) -LHCLSSH_0013 and LHCLSSH_0014 (M. Amparo Gonzalez De La Aleja Cabana) -LHCLJ_7U0085 (C9.L7) and LHCLJ_7U0087 (C9.R7) (J. Oliveira)

1. INTRODUCTION

This ECR describes all necessary actions and required changes for the substitution of two 14.3 m long 8.33 T standard LHC main dipoles (MB) each with an assembly consisting out of a pair of 5.5 m-long 11 T dipoles surrounding the bypass cryostat and the Target Collimator Long Dispersion suppressor (TCLD) [1], where the latter is treated in a separate ECR by WP5 (HL Collimation) [2].

The present state of the areas concerned is shown in Figures 1 and 2.

Figure 1 — Picture of area under change, cell 9.L7 at R72 – present MB.B8L7 (18/02/2019)

Figure 2 — Picture of area under change, 9R7 at R78 – present MB.A9R7 (18/02/2019)

2. REASON FOR THE CHANGE

The increased intensities of the proton and heavy-ion beams in the High-Luminosity (HL) LHC configuration require the installation of collimators in the cold DS region of the IR7 cleaning insertion to protect the downstream dipoles. Beam lifetime drops to 0.2 h may occur and cause energy depositions close or above the quench limit in the DS dipoles for the nominal HL-LHC beam parameters planned for Run IV (Table 1) and for a 7 TeV beam energy [3, 4]. Heavy-ion beams are expected to reach full intensity already after LS2 and potentially producing losses well beyond the quench limit for 0.2h BLT. Therefore, the HL-LHC project, with the approval of the CERN management, has included the installation of the 11 T dipoles with TCLDs already in LS2 as a critical item in its baseline. This choice was taken as there is no room left for the installation of TCLDs without replacing two 14.3 m long 8.33 T standard LHC main dipoles (MB) each with an assembly consisting out of a pair of 5.5 m-long 11 T dipoles making room for a central bypass cryostat (length 3.3 m) hosting the TCLD collimator (length 1 m).

Table 1: Nominal HL-LHC beam parameters, Run IV

This baseline was decided in 2016, after a re-baselining took place, at which the second 11 T dipoles in cell 10 was removed from the initial HL-LHC baseline. This re-baselining was followed by a massive simulation campaign to explore the optimum position of the remaining TCLD collimators (see for example [5, 6]). Two positions (MB.B8 or MB.A9) were identified as good candidate positions. Tables 2 and 3 present the uniform power densities in the most exposed magnets and the total power deposition in the cryogenic half-cells for these two positions and compares the results to no TCLD collimator installed (no change). The calculation method for the uniform power density is specified in [7] (called in this publication minimum quench power density). Please note that the presented peak power densities provided in Tables 2 and 3 are averaged over the cable radial width and are multiplied by the empiric factor of 3 to take into account uncertainties between energy deposition simulations of the multi-turn collimation cleaning process and the LHC measurements during previous beam-based quench tests.

The minimum power density to induce a MB quench was found to be 15-20 mW/cm³ in the BFPP (bound-free pair production) quench test, which took place at 6.37 TeV [8]. This quench limit value was reconstructed by performing particle shower simulations based on the experimental conditions achieved in this test (20 second steady state losses). The value is however affected with some uncertainty as aperture imperfections in the beam screen could not be fully recreated in the simulations. Other quench tests were carried out with collimation losses using both proton and Pb beams [9]. In the later test a dipole quench at about 25-30 mW/cm³ (values reconstructed in simulations). The losses exhibited different time profiles in the different tests, which affected the minimum power density needed to induce a quench. According to electro-thermal simulations, the minimum quench power density in $mW/cm³$ can be a factor of two or more higher if the losses are rising (like in the collimation tests) than if the losses are constant in time (like in the BFPP quench test). This can possibly explain why the maximum power density was found to be somewhat higher for the Pb collimation quench

test than for the BFPP test. It should nevertheless be stressed that a certain error margin needs to be taken into account when interpreting the power densities reconstructed in the simulations, considering the complex simulation setup needed. At the nominal LHC beam energy of 7 TeV these values are around 20% lower.

The <u>expected</u> 11 T dipole quench limit for a uniform power density is 70 mW/cm³ (as relevant for comparison with Table 2) [10]. Please note that contrary to the quench limits of the MBs, which are based on beam based measurements under real conditions in the LHC, the values for the 11 T are based on (1) measurements of cable stack samples, (2) on short magnet models tests (not exactly of the same type as the 11 T) and on (3) calculations; as reviewed and summarized in [10]. Based on this review and the point of view of operating margin and stability, the 11 T dipole meets the requested resilience to heat load for both installation locations presented in Tables 2 and 3.

The cryogenic cooling capacity allows to extract \sim 200 W per 2-cells (Q7 to Q11); for a short time much higher heat loads can be sustained by using the heat capacity of the stored helium and extracting the heat once the heat load is again reduced. Taking into account the heat deposition as function of time, in all cases for protons and ions the magnets' temperature excursion can be contained below T_{λ} [11]; so as well both locations presented in Tables 2 and 3 fulfil the requested resilience.

From these tables, one concludes that the margin to quench improve for the downstream MBs and MQs (Nb-Ti magnets), in particular for ion runs, if the TCLD is installed in MB.A9 compared to MB.B8, allowing beam lifetimes of 0.2 h (but at the cost of higher losses for the 11 T dipoles [48 mW/cm³ (proton runs, MB.A9) compared to 21 mW/cm³ (ion runs, MB.B8)]. If the TCLD would be installed at MB.A8 beam lifetimes of 0.2 h could require a beam dump to not quench the Nb-Ti magnets for ion runs, or the use of other techniques like crystal collimation [12].

In view of the overall optimization goal to maximize the integrated luminosity, taking all information and the uncertainties into account, the HL-LHC management decided to install the 11 T dipole at MB.A9 [13].

Table 2: Uniform power density in SC coils in mW/cm³ for 0.2 h and 1 h beam lifetime for different scenarios (no TCLD, TCLD installed at MB.B8 or MB.A9) [3]

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Table 3: Total power in cryogenic cells in W for 0.2 h and 1 h beam lifetime for different scenarios (no TCLD, TCLD installed at MB.B8 or MB.A9) [3]

3. DETAILED DESCRIPTION

It is foreseen to exchange the following two MBs:

- **MB.A9L7** (LBBRB.9L7)
- **MB.A9R7** (LBARA.9R7)

The cryo-magnets (LB) are installed at the following positions (virtual interconnect plane, upstream B1):

- **MB.A9L7** (LBBRB.9L7): distance from IP7: -323.629 m, distance from IP1 (DCUM): 19670.5334 m, half-cell 9.L7, called following **P7 left side**
- **MB.A9R7** (LBARA.9R7): distance from IP7: 307.969 m, distance from IP1 (DCUM): 20302.1314 m, half-cell 9.L7, called following **P7 right side**

In detail, the changes comprise the following:

P7 left side

- Removal of the present main dipole **MB.A9L7** (LBBRB.9L7, circuit RB.A67)
- Installation of the 11 T dipole full assembly at the MB place in type cold-mass type B configuration (only MCS corrector connected). The assembly is composed of two dipoles of equal bending strength and shorter magnetic length (Cryoassembly A and B) and a bypass cryostat in the middle, providing cryogenic and electrical continuity between them.
- After that, installation of a new TCLD collimator between the two magnets, on the beam line 2 (internal beam, or passage side) will follow.

P7 right side

- Removal of the present main dipole **MB.A9R7** (LBARA.9R7, circuit RB.A78)
- Installation of the 11 T dipole full assembly at the MB place in type cold-mass type A configuration (both MCDO and MCS corrector connected): Cryo-assembly A and B, and a bypass cryostat in between.
- After that, installation of a new TCLD collimator between the two magnets, on the beam line 1 (external beam, or QRL side) will follow.

Layout drawings LHCLSS_0029/LHCLSS_0030 (LHC layout for the DS region at point 7) show the present situation in LHC. LHCLSSH_0013/LHCLSSH_0014 (HL-LHC layout for the same zones) show the situation after the installation of the TCLD

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collimator and the two short 11 T dipoles and replace the before mentioned drawings after LS2. Figures 3 and 4 show the section of the LHC layout for P7 left before and after the change. Detailed layouts are presented in [13].

The components to be installed (Table 1), to be kept (Table 2), to be displaced (Table 3) or to be removed (Table 4) are listed below.

Figure 3 - Section of LHC layout for P7 left (from LHCLSS__0029, top) and P7 right (from LHCLSS__0030, bottom) – Replaced magnet.

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3.2 BEAM DYNAMICS

The bending angle of the beam is kept the same thanks to the same integrated field generated by the pair of 5.5 m-long 11 T dipoles as by a standard main dipole magnet (MB). The same integrated field is achieved by powering the 11 T dipole pair in series with the MBs and by using a trim power supply, so no orbit distortions will be generated

due to differences in transfer function of the main and the 11 T dipoles during the energy ramp.

The field stability is similar, as the 11 T dipoles are connected in series with the MBs, so the main current in all magnets is identical during standard operation. The trim power converters have a marginal impact. Flux jumps are too slow for having a negative impact on the emittance and the orbit [16, 17].

The field quality is worse than for that of the MBs, in particular the sextupole component b₃ is larger. The latest field quality table of the 11 T dipoles can be found in [15]. Beam dynamics studies [18] have shown that the expected field quality is such to leave dynamic aperture essentially unaffected, both at injection and collision energy, given the limited number of magnets which will be installed.

The same type and number of spool pieces as currently installed in the MBs will be installed in the 11 T dipoles (LBBRB.9L7: MCS, for symmetry reason a MCDO will be installed but not connected to the circuit to mimic the type B dipole; LBARA.9R7: MCS and MCDO).

Unlike the main dipoles, the 11 T magnets are straight. The exact installation positon taking into account the sagitta is currently being assessed in the WG alignment [19].

3.3 VACUUM MODIFICATIONS

In order to provide beam vacuum continuity of the 11 T full assembly, the continuous beam line of the replaced dipole magnet must be segmented and adapted to accommodate the functioning of the TCLD collimator and the 11 T magnets. The installation of the TCLD collimator, operating at room temperature, imposes a new sectorization of the vacuum lines and new transitions between cold and warm vacuum lines. The improved pumping strategy for these new vacuum sectors is proposed in [20]. All changes of the vacuum layout are defined in [21].

Inside the 11 T magnets (LBH type) the standard LHC-type beam screens will be installed for both beam lines (cold bore inner diameter 50mm). Regarding the bypass cryostat (LEN type) there are two different configurations, one for each beam line, depending if it is the collimated or the non-collimated line.

For the collimated line, there will be one bellow to ease its mounting/dismounting and one sector valve installed on each side of the TCLD. The sector valves are then connected to the cold-warm transitions (short and long versions, located upstream and downstream respectively) and followed by the standard Plug-in-Module (PIM). The collimator itself will represent an added vacuum sector, described in detail within the TCLD ECR [2] after ongoing tests. A vacuum port (LHCVSTB_0010 – position5) is integrated in the cold/warm transition, between the sector valves and the continuous cryostat, to allow the RF ball tests.

For the non-collimated line, a new concept of conduction cooled copper cold bore has been developed to reduce the equipment needed on this line of the bypass cryostat. It will be thermalized at both of extremities by two hoses routed from the M3 line, feeding superfluid helium at 1.3 bar to the collars brazed around the line. The copper cold line is linked to the PIMs at the extremities. A standard LHC-type beam screen is inserted in the cold line. To accommodate all the described equipment within the existing space, special

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short beam screen bellows had to be design and manufactured. The additional cryogenic instrumentation is described in section 3.4.

The insulation vacuum continuity is ensured by the LEN cryostat.

3.4 CRYOGENICS MODIFICATIONS

The bypass cryostat placed between two 11 T dipole cryostats causes a significant increase of the longitudinal hydraulic impedance in the insulation vacuum-space compared to today's installation. In case of a 30 kg/s cold helium flow from the cold mass into the insulation vacuum space, as identified as Maximum Credible Incident (MCI) in [22], a sufficient number of safety valves are installed to limit the cryostat pressure to 1.5 bar. The present scheme, implemented after the incident of 19th September 2008 and revised in LS1 is summarized in [23, 24]. An investigation whether this MCI-discharge flow occurring on one side of the cryogenic bypass can be at least partly shared with the other side, without introducing an excessive pressure drop, showed that such sharing is insufficient [25]. Therefore, each side of the cryogenic bypass is to be considered as an individual hydraulic sector with respect to MCIs and it must be possible for the full flow to be discharged by safety valves on either side of the bypass.

In addition, to avoid multiple helium clouds in case of an incident when personnel access is allowed in the tunnel (during low current powering, so-called "phase I" [23]), one SV per vacuum subsector opens at a low pressure (so-called unsprung SV), allowing evacuation of up to 1 kg/s of helium via a single port. The additional hydraulic impedance of the bypass cryostat increases the maximum internal pressure for such a 1 kg/s discharge. An investigation whether this MCI-discharge flow occurring in the dispersion suppressor cryostat equipped with bypass cryostat showed that the internal pressure slightly exceeds the 80 mbar opening pressure of the sprung loaded DN200 SV in the hydraulic sector opposite to the location of the unsprung SV [25]. A simple solution to increase the opening pressure of the DN200 SV by applying a second spring has been verified [26]. Furthermore, the two DN90 SV with opening pressure of 67 mbar shall be removed from the vacuum subsector.

The cold mass complies to the functional requirements provided in [27]

The insulation vacuum protection scheme at LHC IR 7 DS vacuum sector before and after LS2 is summarized in Tables 8-11. The change concerns two 11 T dipole magnets (MBH), one by-pass cryostat (LEN), one additional DN200 SV to install on the MB between Q7 and Q8, removal of the DN90 SV at Q7 and Q9, doubling of DN200 springs in the zone Q11 to LEN. The valve without spring is displaced from cell 10 to cell 7.

Table 8: LHC IR7 LEFT Insulation vacuum protection scheme in sector 6-7 as installed on 31st of January 2019

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*no spring loading, **double spring loaded

Table 9: LHC IR7 LEFT Insulation vacuum protection scheme in sector 6-7 as after installation of the 11 T dipole (MBH)

*no spring loading, **double spring loaded

Table 10: LHC IR7 RIGHT Insulation vacuum protection scheme in sector 7-8 as installed on 31st of January 2019

*no spring loading, **double spring loaded

Table 11: LHC IR7 RIGHT Insulation vacuum protection scheme in sector 7-8 as after installation of the 11 T dipole (MBH)

*no spring loading, **double spring loaded

Additional cryogenic instrumentation will be implemented during LS2. A total of seven temperatures sensors (CERNOX) and two flowmeters (Coriolis) will be installed at P7 right side after having installed the 11 T dipole magnet [28]. No additional instrumentation at P7 left side will be installed. This choice was taken because the beam screen heat load on the right side is larger. Figure 5 shows the instrumentation in this half-cell.

Figure 5 – Instrumentation for the 11 T dipole, P7 right side [28].

3.5 GEOMETRY AND ALIGNMENT MODIFICATIONS

The installation of the 11 T dipole full assembly requires the alignment of two 11 T dipoles, the bypass cryostat and the TCLD collimator compared to previously only one MB magnet. In detail, the following operations have to be performed:

- 1. The marking on the floor of the beam points, jacks heads position of the nonstandard 11 T dipoles but also the beam points and component axis of the bypass cryostat and of the new TCLD collimator is required. A specific care will be brought to the jack configuration of the dipoles, as not standard.
- 2. 12 jacks per 11 T dipole full assembly will be installed.
- 3. EN-SMM-ASG will align the jacks' heads at their nominal position, prior to the installation of any component.
- 4. The 11 T dipole magnets will be installed.
- 5. An initial alignment of the dipoles will be carried out with respect to the adjacent cryo-magnets.
- 6. The bypass cryostat will be installed and the TCLD collimator will be inserted as last component to be installed.
- 7. The alignment of the TCLD and cryo-bypass will be carried out from the both 11T adjacent dipoles. Please note that during the smoothing activities of the cryo-magnets in the LHC (end of LS2), if one of the 11T magnets is re-aligned (vertical or radial), the components between the both 11T magnets (TCLD and cryo-bypass) may also need to be re-aligned.
- 8. After this pre-alignment, the 11 T dipole full assembly smoothing w.r.t. the adjacent components will be performed once all interconnections are closed, and the sector has been cooled down during the regular arc smoothing activity.
- 9. Roll measurements can only be performed by adding an inclinometer on a specific cylinder interface located on the plate that supports the survey socket on the tunnel transport side and on the double jack side.

To do all alignment operations described above, the MAD-X survey file providing the beam positions of the components must be available at least two months before any survey activity in the LHC tunnel, this will be possible only if the LHC layout database will be updated with the needed information at least a month in advance the deadline for the delivery of the MAD-X survey file. Drawings giving the positions of the jacks heads with respect to the component beam points must be available at least two weeks before the jack marking in the LHC tunnel.

3.6 MAIN DIPOLE CHAIN AND TRIM CIRCUIT

The modified circuit layout of RB.A67 (with trim circuit **RTB9.L7**) and RB.A78 (with trim circuit **RTB9.R7)** is shown in Figures 5 and 6. A detailed description of the circuits is provided in [29, 30], Section 2.1-2.7. The RB circuit characteristics before and after the change are summarized in Table 12. For the circuit RB.A78 the 11 T dipole full assembly

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Figure 6 - Main dipole circuit RB.A78 configuration for the HL-LHC with the 11 T trim power converter.

Table 12 - RB circuit characteristics in the current LHC configuration and after the introduction of 11 T dipole full assembly for circuits RB.A67 and RB.A78, updated from [\[1\]](#page-25-0).

3.7 POWER CONVERTERS AND SERVICES

For the operation of the 11 T dipole magnets the trim di-polar circuit power converters $(\pm 250 \text{ A})$ have to be added. The current profile of the trim power converters is presented in [30].

3.7.1 RB power converter

No modifications are applied to the RB power converters, except setting the expected circuit inductance in the regulation to the slightly higher value: 15.734 mH vs 15.708 mH.

3.7.2 Hardware requirements

Two additional HCRPMBE (R2E-HL-LHC600A-10V) power converters will be added to the service galleries RR73 to power RTB9.L7 and RR77 to power RTB9.R7. A detailed description of the power converter functional requirements is detailed in [31]. The power converters racks will replace the RYSA01 in both RR73 and RR77.

3.7.3 Power converters control

The 11 T trim power converters will be controlled by FGCLite. They will be connected to the already existing WorldFIP network in RR73 and in RR77. For 11 T trim power converters, one agent will be added to the CFC-SR7-RL7A network in RR73 and another agent will be added to CFC-SR7-RR7C network in RR77. The required performance in terms of precision and stability is defined in [29].

3.7.4 Power converters services

The power converters will require the following services as indicated in Section [4.2:](#page-19-0)

- AC cabling per converter: 3P+N 20 Arms from ERD with a terminal (model Schneider A9N15658) and 3P+N 2 Arms from EOD with a terminal (model Schneider A9N15656).
- DC cabling per converter: 2×50 mm² per polarity

 Demineralized water cooling: 4 l/min at 3.0 bar of differential pressure drop Two cables in parallel are used for the powering of the circuit, by means of 2 current leads of the 120 A LHC type per polarity (see section 3.12 for more details on PIC and section 3.13 for the DIC document number).

3.7.5 Power converter interface with PIC

The connection to the power converter will be done via a standard 12-pin female Burndy connector (the DIC number is reported in section 3.13).

3.8 Quench Detection System (QDS) modifications

For the protection of the 11 T dipoles, newly developed universal quench detection system (uQDS type) adapted to the specific properties of Nb₃Sn superconducting magnets (uQDS type) will be deployed. In addition, dedicated DAQ systems for the supervision of the quench heater circuits (DQHSU) will be provided.

3.8.1 Hardware

To assure the quench detection system, two crates are needed per IP side and will be installed in the service galleries RR73 (left side) and RR77 (right side). A detailed description of the integration of these racks is provided in [13].

The dipole quench detection crates DQLPU.A9L7 and DQLPU.A9R7, which are installed in protection racks DYPB.A9L7 and DYPB.A9R7, will be dismantled and removed from the LHC tunnel.

3.8.2 Location

The QDS for the protection of the 11 T dipoles and the associated quench heater circuit supervision unit (DQHSU) will be located in underground areas RR73/RR77 using the remaining free space in QPS protection racks DYPG01=RR73 and DYPG01=RR77.

3.8.3 Interlocks

This non-standard QDS will be integrated into the existing QPS internal current loop. While the connection to the powering interlock controller (PIC) will not change, it is foreseen to update the QPS quench loop controllers for circuits RB.A67 and RB.A78 in order to achieve a faster reaction time.

3.8.4 Controls

The physical layout of the QPS fieldbus needs to be slightly modified. This concerns segments CBW.IP7.DR7H, CBW.IP7.DL7J, CBW.IP7.DT7A and CBW.IP7.DT7F. The changes concerns only the number and position of field-bus clients; it does not affect any other active equipment like repeater or front-end computers.

The QPS software layer stack and the LHC circuit synoptic need to be updated to be able to interact correctly with the newly installed devices. In particular, this will require the implementation of several new application-programming interfaces (API) and the definition of the corresponding set of signals.

3.9 New Quench Protection System (nQPS) modifications

The DQLPU type S protection crates will not need any type of relocation since they are not affected for the new location of the 11T cryo-assemblies.

3.10 Changes to the racks containing the heater discharge units

For the protection of 11 T magnets, two non-standard QPS racks will be installed in the machine tunnel per IP side (underneath the cryostats). A new, non-standard design was established, to consider that the quench detectors will be located in the RRs (see Section [3.8\)](#page-13-0) and to accommodate the 16 quench heater power supplies per side instead of the previously installed 4 standard LHC MB quench heater power supplies. The quench heater power supply will accommodate redundancy in the powering of the F3 & F4 UPS distribution lines.

A detailed description of the integration of these racks is provided in [13].

3.10.1.1 DQHDS firing speed

The response time of the DQHDS units in firing is 2ms, which is considered sufficient.

3.10.1.2 Redundancy configurations

Since the full 11 T magnet cannot withstand the loss of more than two out of sixteen DQHDS units, powering redundancy must be incorporated. To ensure redundancy, each rack is powered with four F3 and four F4 AC inputs together with twice four circuit breakers per rack. In addition, each DQHDS unit will be modified in such a way that its trigger circuit will have a redundant powering from F3 and F4. However, the capacitors will still be energized by either F3 or F4. The powering requirements are addressed in the DIC.

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Monitoring of the proper connections of the quench heater discharge cables to the magnet IFS will be performed.

3.10.1.3 Rack containing the heater discharge units

A new rack type upgrading the current DYPB rack had to be designed to allow for installing 16 quench heater power supplies and allow maintenance during LHC operation. In addition to this, the DQHDS units must be upgraded to be compatible with the availability requested by the protection of the 11 T dipoles.

3.10.2 Location

The non-standard QPS racks will be placed at (see the grey boxes in Figure 7):

- \bullet L7: 1 rack under MB.B10L7 + 1 rack under MB.B9L7;
- R7: 1 rack under MB.A10R7 + 1 rack under MB.A8R7.

Four new racks will be installed in the machine. One spare unit will be manufactured.

Figure 7 - Location of the new DYPB for the 11 T dipoles.

3.11Powering Interlock System (PIC)

The Powering Interlock System (PIC) [31] is designed to ensure nominal conditions for circuit powering and provide the permission for powering the different electrical circuits with superconducting magnets installed around the LHC. For this, it interfaces power converters, quench detection systems, technical services (AUG, UPS, cryogenics, etc.)

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and is a client of the Beam Interlock System (BIS) in order to request a beam dump when necessary. The two new 11 T dipoles will be connected in series with the RB.67 and RB.78 main dipole circuits requiring a trim power converter each, which have to be connected to the PIC. The interlock requirements of the 11 T circuit and its trim are summarized in Table 13

¹The trim circuit will be considered as essential from the PIC side, which means unmaskeable at the BIC level.

3.11.1Hardware

The hardware interfaces of the PIC are standardized and are defined according to the type of electrical circuit. There are currently 5 different listed types (A, B1, B2, C, D) [32] grouped into 4 different patch panels (CIPPA, CIPPB, CIPPC, CIPPS). Since the configuration of a PIC is generic, there are some hardware interfaces that remain unused. For the two PIC in P7, the current interface configuration contains a free "B1 type" hardware interface on the CIPPS patch panel, which will be used to connect the new 11 T trim power converters. Moreover, the quench loop of the trim circuits will have the peculiarity of being connected to the QDS dedicated for the surveillance of the trim current leads (see Section 3.12, Protection of trim current leads)).

The proposed implementation will fulfil the requirements summarized in Table 6:

- If a quench in the RB circuit or an EE switch opening occurs, a general fast power abort action on both PICs on the odd and even side will be taken through the global protection mechanism.
- If a powering failure occurs, a slow power abort action will be taken only on the faulty circuit (RB or Trim).
- If a failure is detected on the current leads of the Trim circuits, a fast power abort of the trim circuits will be triggered.
- A cryo failure will cause a slow power abort of both RB and Trim circuit because the same status of the Cryo interlock is sent from a unique Cryo PLC to both arc PIC.
- For protection of the trim circuit bus-bars, the trim bus-bar supervision is added on the QDS of the 11 T, that means in case of a quench of the trim bus-bar the firing of the quench heaters of the 11 T dipole will be triggered and a fast power abort of the main dipole circuit will be performed [33].

As stated in Table 6 and confirmed in [34] the beam is dumped in all failure scenarios.

3.11.2 Configuration

The LHC main dipole circuits have the feature of being interfaced with the two adjacent PIC of the arcs (even and odd), sharing the same quench loop, and their power converters located on the even side. The new 11 T trim power converters will be located at the odd side of the arc (RR73 and RR77) and connected to the corresponding PIC as independent circuits.

3.12 Protection of trim current leads

The trim circuit (RTB8) for each of the 11 T dipoles will be powered through a set of 2 \times 2 resistive current leads. The protection of the four trim leads will require monitoring of the lead voltages and currents. These signals will be evaluated by a standard HL-LHC quench detection system (uQDS), which initiates the necessary action e.g. a fast power abort of the concerned trim circuit.

3.12.1 Hardware

The additional quench detection crates need to be installed inside RR73/RR77 (ground floor). There is not enough space to integrate these units in protection racks DYPG01=RR73 and DYPG01=RR77. For the additional space, the adjacent half rack DYPIB01 (shared with the PIC half rack CYCIP01) will be used.

For the measurement of the lead currents, current sensors of the Hall type and clamped to the power cables will be installed in RR73 and RR77.

3.12.2 Interlocks

The new QDS for the trim current leads needs to be integrated into the hardwired interlock loop for the trim circuits.

3.12.3 Controls

As for the changes above, the QPS software layer stack and the LHC circuit synoptic need to be updated accordingly. In this case, this concerns as well the configuration of the PIC.

3.13 Cabling

Detailed DICs (reference: RQF0908671 (instrumentation), RQF0888406 (PIC), and RFQ0981328 (powering)) have already been prepared and sent to EN-EL. Another WorldFIP fieldbus extension for the trim power converters is requested to BE-CO (RQF0809614). Accordingly, all the cabling concerning the new racks (discharge, monitoring, triggering, control, etc) needs to be installed.

The installation will require the respective set of instrumentation, signal, and hardware trigger and interlock cables. The default QPS interlock cabling traversing the 11 T assembly will need to be modified.

The nQPS instrumentation and interlock cabling need to be modified. All cables going through the 11 T assembly must be re-routed to one of the cables trays on the tunnel wall to not interfere with maintenance operations of the collimators.

Instrumentation cables linking the current lead feed through box with the quench detection crates have to be installed. In addition, there will be the signal cables for the current sensors and the interlock cables, which are local to RR73/RR77.

The nQPS crates below the dipoles located in A9 (both sides), will be moved to a position below A10 and various cables will be re-installed.

Moreover, there is today a DYPQ rack located under MB.A9L7 that will be moved under MB.B8L7. This requires consequently new cabling between the quadrupole cryostat and the new position of the rack (see Figure 7).

All cabling for other required equipment is summarized in the integration report [13] and the list of cables to be modified is summarized in [35].

3.14Organization of the work during LS2

During LS2 each equipment owner is in charge of the installation of their own equipment. DISMAC will be in charge of the installation and connection of the 11T dipoles full assembly. The detailed procedures for the installation and connection will be given to the DISMAC team. An onsite coordination for the whole activities related to the 11 T dipole will be guarantee by WP11 through the activity technical coordination of WP11 (Daniel Schoerling). The role description is provided in [36].

4. IMPACT

4.1 IMPACT ON ITEMS/SYSTEMS

The following drawings and documents have to be updated.

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5. IMPACT ON COST, SCHEDULE AND PERFORMANCE

5.1 IMPACT ON COST

5.2 IMPACT ON SCHEDULE

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5.3 IMPACT ON PERFORMANCE

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6. IMPACT ON OPERATIONAL SAFETY

6.1 ÉLÉMENT(S) IMPORTANT(S) DE SECURITÉ

6.2 OTHER OPERATIONAL SAFETY ASPECTS

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7. WORKSITE SAFETY

7.1 ORGANISATION

7.2 REGULATORY TESTS

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7.3 PARTICULAR RISKS

8. FOLLOW-UP OF ACTIONS BY THE TECHNICAL COORDINATION

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