



A Ferroelectric
Fast Reactive
Tuner

N. Shipman

The issue

What can we
do?

Reactive
Tuners

Ferroelectric
Material

Prototype
Tuner

Experimental
Results

Case Studies

Conclusion

A FerroElectric Fast Reactive Tuner(FE-FRT) for ERLs

Reducing power consumption by microphonics
compensation

N. Shipman¹, J. Bastard¹, M. Coly¹, F. Gerigk¹, A.
Macpherson¹, N. Stapley¹, I. Ben-Zvi², C. Jing³, A.
Kanareykin³, G. Burt⁴, A. Castilla⁴, E. Nenasheva⁶

¹CERN, ²Brookhaven National Laboratory, ³Euclid Techlabs LLC,
⁴Lancaster University, ⁶Ceramics Ltd.

Electrons in the LHC, October 2019



How much RF power do we need per cavity in PERLE?

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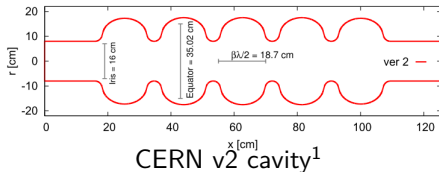


Table: PERLE Cavity Parameters

Parameter	Value
Q_0	2×10^{10}
R/Q	393Ω
V_c	18.7 MV

¹R. Calaga, "A design for an 802 MHz ERL

Cavity", CERN-ACC-NOTE-2015-0015, May 2015.



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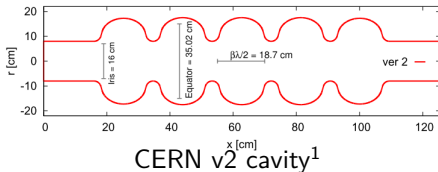
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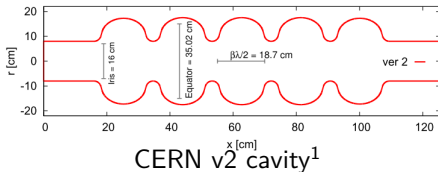
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- How much power do we "need"?
- No beam loading.

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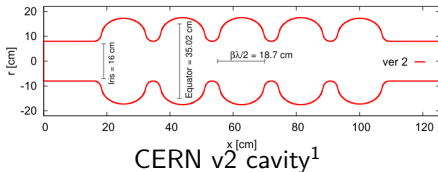
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- $P_0 = \frac{V^2}{R/Q Q_0}$

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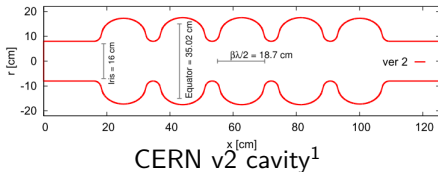
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- How much power do we "need"?

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- $P_0 = \frac{V^2}{R/Q Q_0}$
- $P_0 \approx \mathbf{44 \text{ W}}$

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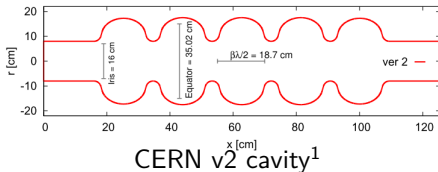
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- How much power do we "need"?

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- $P_0 = \frac{V^2}{R/Q Q_0}$
- $P_0 \approx 44 \text{ W}$

- How much power is budgeted?

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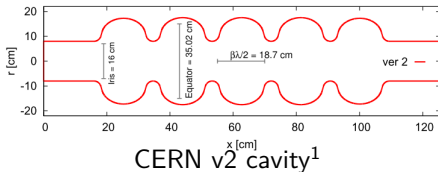
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- $P_0 = \frac{V^2}{R/Q Q_0}$

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- How much power is budgeted?

- $P_{RF}^{avg} \approx 23 \text{ kW}$

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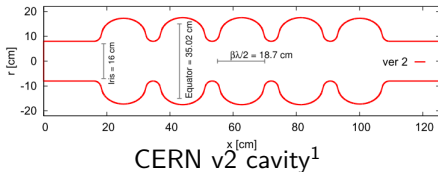
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- $P_0 = \frac{V^2}{R/Q Q_0}$
- $P_0 \approx 44 \text{ W}$

- How much power is budgeted?

- $P_{RF}^{avg} \approx 23 \text{ kW}$
- $P_{RF}^{peak} \approx 45 \text{ kW}$

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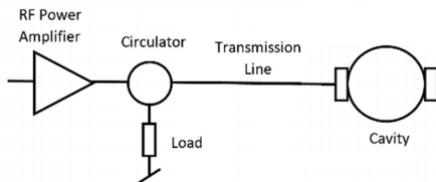
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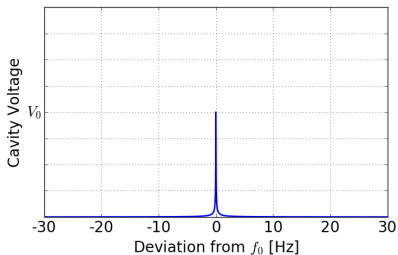
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■ Microphonics!





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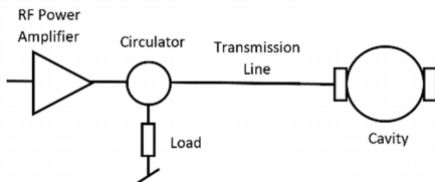
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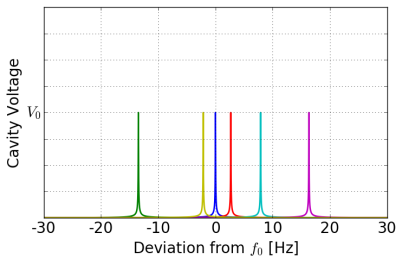
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- Microphonics!
- Detuning \gg natural cavity bandwidth.





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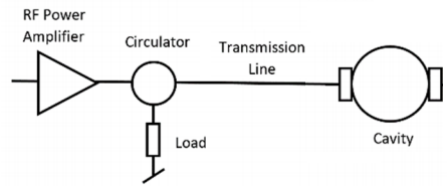
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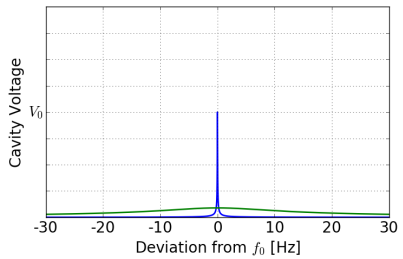
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- $Q_e \ll Q_0$





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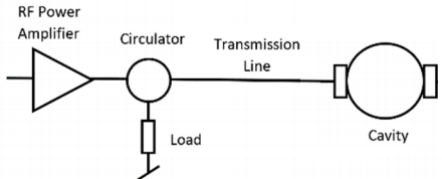
Ferroelectric Material

Prototype Tuner

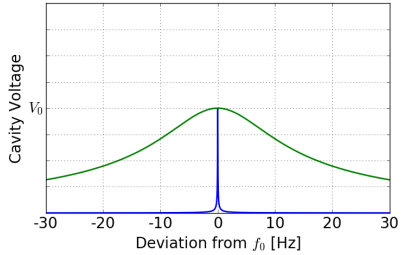
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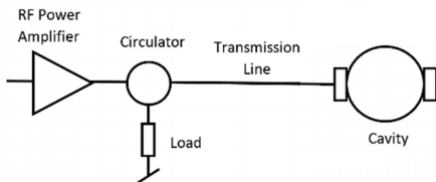
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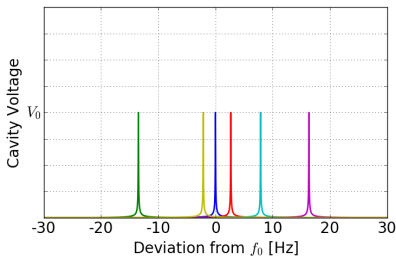
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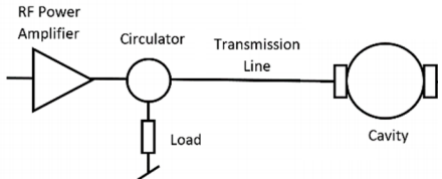
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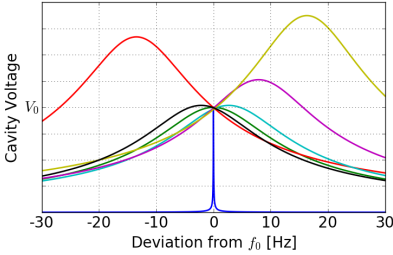
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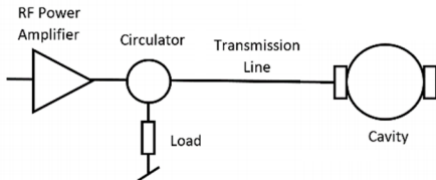
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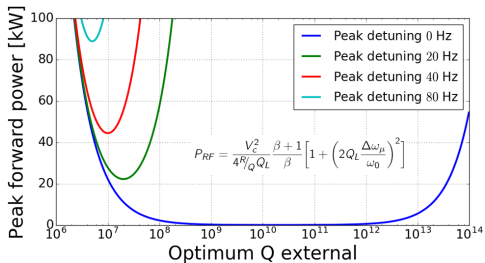
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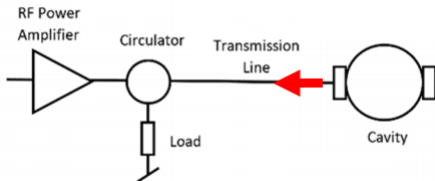
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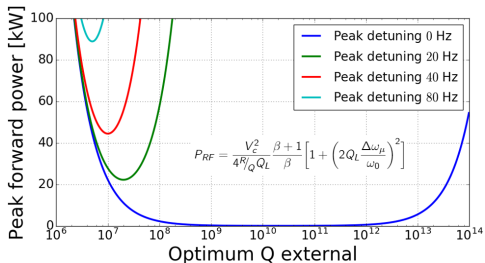
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- Microphonics!
- Detuning \gg natural cavity bandwidth.
- $Q_e \ll Q_0$
- $\approx 99.8\%$ of power is reflected and





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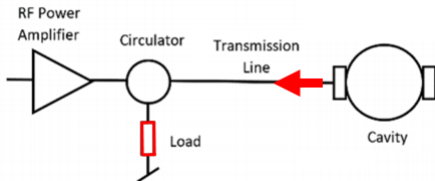
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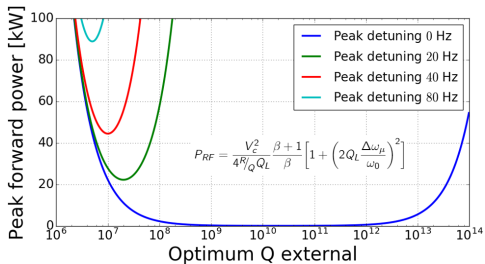
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- Microphonics!
- Detuning \gg natural cavity bandwidth.
- $Q_e \ll Q_0$
- $\approx 99.8\%$ of power is reflected and
- Dissipated in load.





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Conclusion

- What we already do.
 - Design stiff cavities/cryomodules
 - Reduce noise sources.
 - Use over-coupled power couplers

²N. Banerjee *et al.*, *Physical Review Accelerators and Beams*, vol. 22, pp. 052002-17, Jan. 2019.



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- What we already do.

- Design stiff cavities/cryomodules
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- Use over-coupled power couplers

- What we've just started doing.

- Actively compensate microphonics with fast piezo tuners.²

²N. Banerjee *et al.*, *Physical Review Accelerators and Beams*, vol. 22, pp. 052002-17, Jan. 2019.



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- What we already do.
 - Design stiff cavities/cryomodules
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 - Use over-coupled power couplers
- What we've just started doing.
 - Actively compensate microphonics with fast piezo tuners.²
- What we are proposing.
 - Actively compensate microphonics with FerroElectric Fast Reactive Tuner **FE-FRT!**

²N. Banerjee *et al.*, *Physical Review Accelerators and Beams*, vol. 22, pp. 052002-17, Jan. 2019.



How does it work?

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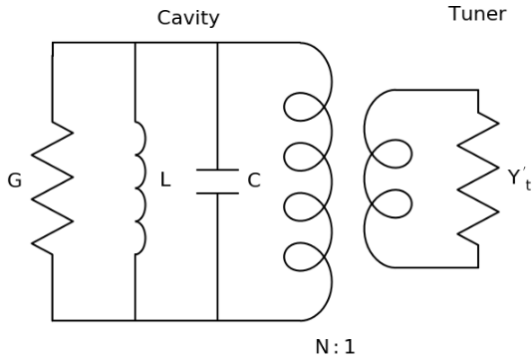
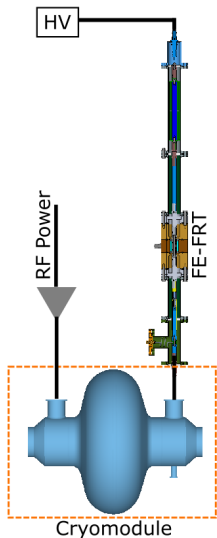
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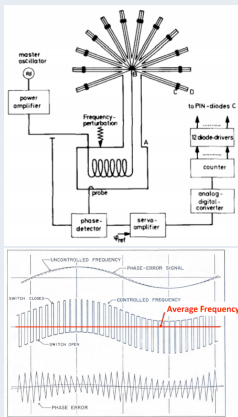
Conclusion



$$\Delta\omega_{12} = \frac{-\omega_0 \Delta B'_{t12} \sqrt{L_c/C_c}}{2N^2}$$

$$\Delta BW_n = \frac{G'_{tn}}{N^2 C_c}$$

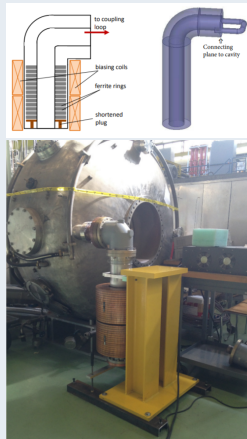
Pin Diode Tuners



O. Despe, K. Johnson and T. Khoe, *IEEE Trans. Nucl. Sci.*, vol. 20 (3), p. 71, Jun. 1973.

D. Schulze *et al.*, in *Proc. 1972 Proton Linear Accelerator Conference*, Los Alamos, NM, USA, October 1972, G01, pp. 156–162.

Ferrite Tuners



C. Vollinger and F. Caspers, "Ferrite-tuner Development for 80 MHz Single-Cell RF-Cavity Using Orthogonally Biased Garnets", in *Proc. IPAC'15*, Richmond, VA, USA, May 2015.



Why use an FE-FRT?

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- No moving parts



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- No moving parts
- Outside cryomodule



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- No moving parts
- Outside cryomodule
- Continuous tuning range



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- Intrinsic speed $< 10 \text{ ns}^3$

³S. Kazakov *et al.*, "Fast Ferroelectric L-band Tuner", in *Proceedings of the 12th AAC Workshop*, Lake Geneva, WI, USA, Jul. 2006, AIP Conf.Proc. (877), pp. 331–338.



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³S. Kazakov *et al.*, "Fast Ferroelectric L-band Tuner", in *Proceedings of the 12th AAC Workshop*, Lake Geneva, WI, USA, Jul. 2006, AIP Conf.Proc. (877), pp. 331–338.



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- Low losses/small increased bandwidth
- So why hasn't this been done before?

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Newly Developed Ferroelectric

- Suitable material only recently developed.⁴

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⁴E. Nenasheva *et al.*, *Journal of European Ceramic Society*, vol. 30, pp. 395–400, Jan. 2010.



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- Suitable material only recently developed.⁴
 - BaTiO₃ - SrTiO₃ solid solution (BST)

⁴E. Nenasheva *et al.*, *Journal of European Ceramic Society*, vol. 30, pp. 395–400, Jan. 2010.



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- Suitable material only recently developed.⁴
 - BaTiO₃ - SrTiO₃ solid solution (BST)
 - Added linear (non-tunable) Mg-based ceramic component⁵

⁴E. Nenasheva *et al.*, *Journal of European Ceramic Society*, vol. 30, pp. 395–400, Jan. 2010.

⁵A. Kozyrev *et al.*, *Appl.Phys. Lett.*, vol. 95, pp. 1–5, Jul. 2009.



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 - Enhanced tunability with low losses

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Table: Material Properties at ≈ 800 MHz

Parameter	Value
Max. ϵ_r	140
Min. ϵ_r	131.6
$\tan \delta$	9.1×10^{-4}
$\frac{\Delta \epsilon_r}{E}$	$0.6 \text{ kV}^{-1} \text{ cm}$
τ	$< 10 \text{ ns}$

⁴E. Nenasheva *et al.*, *Journal of European Ceramic Society*, vol. 30, pp. 395–400, Jan. 2010.

⁵A. Kozyrev *et al.*, *Appl. Phys. Lett.*, vol. 95, pp. 1–5, Jul. 2009.



Prototype Tuner

A Ferroelectric Fast Reactive Tuner

N. Shipman

The issue

What can we do?

Reactive Tuners

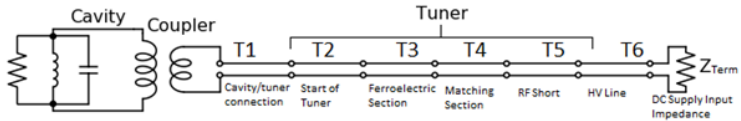
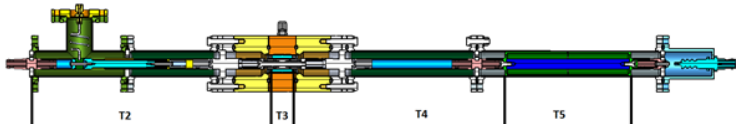
Ferroelectric Material

Prototype Tuner

Experimental Results

Case Studies

Conclusion



Prototype Tuner, 3D model and transmission line model.



Experimental Setup

A Ferroelectric
Fast Reactive
Tuner

N. Shipman

The issue

What can we
do?

Reactive
Tuners

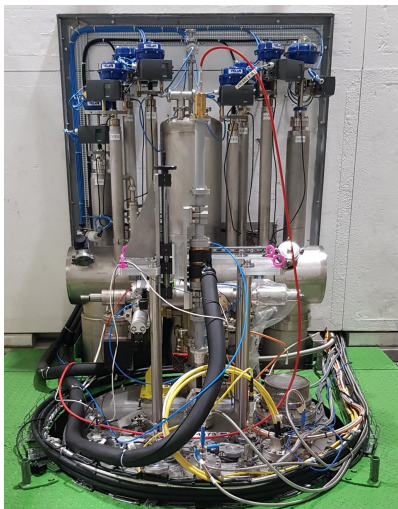
Ferroelectric
Material

Prototype
Tuner

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FE-FRT mounted on cryostat.



Cryostat insert.

Demonstration of Frequency Tuning

A Ferroelectric
Fast Reactive
Tuner

N. Shipman

The issue

What can we
do?

Reactive
Tuners

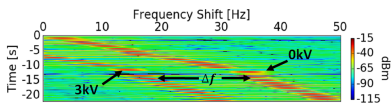
Ferroelectric
Material

Prototype
Tuner

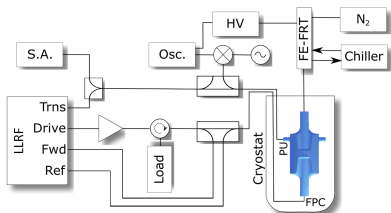
Experimental
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Signal analyser measurement.



Experimental Setup.

Demonstration of Frequency Tuning

A Ferroelectric
Fast Reactive
Tuner

N. Shipman

The issue

What can we
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Reactive
Tuners

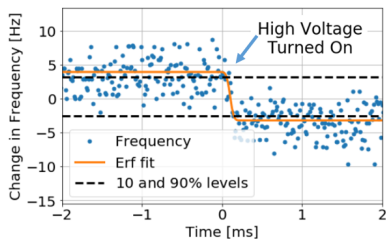
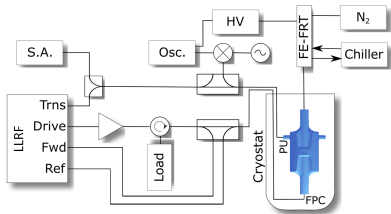
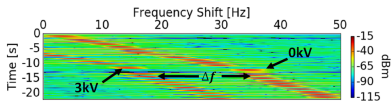
Ferroelectric
Material

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Tuner

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Frequency calculated from I and Q measurements.



Timescale of Frequency Shift

A Ferroelectric
Fast Reactive
Tuner

N. Shipman

The issue

What can we
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Reactive
Tuners

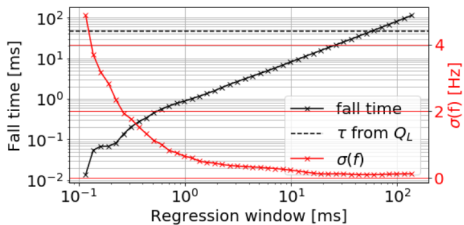
Ferroelectric
Material

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Tuner

Experimental
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Fall time and $\text{std}(f)$ vs. regression window length.



Timescale of Frequency Shift

A Ferroelectric
Fast Reactive
Tuner

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What can we
do?

Reactive
Tuners

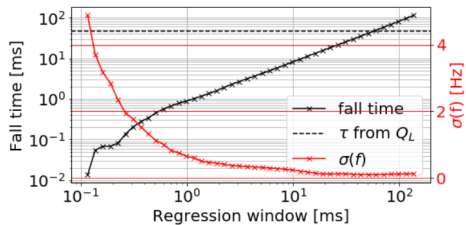
Ferroelectric
Material

Prototype
Tuner

Experimental
Results

Case Studies

Conclusion



- Cavity response to tuner $< 50 \mu\text{s}$

Fall time and $\text{std}(f)$ vs. regression window length.



Timescale of Frequency Shift

A Ferroelectric
Fast Reactive
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N. Shipman

The issue

What can we
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Reactive
Tuners

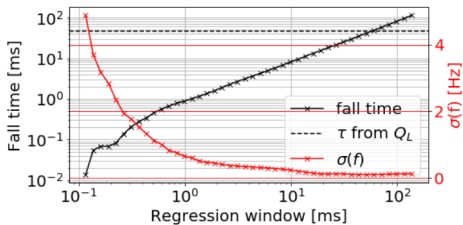
Ferroelectric
Material

Prototype
Tuner

Experimental
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Conclusion



Fall time and $\text{std}(f)$ vs. regression window length.

- Cavity response to tuner $< 50 \mu\text{s}$
- Cavity time constant $\tau_L = \frac{Q_L}{\omega_0} \approx 46 \text{ ms}$



Timescale of Frequency Shift

A Ferroelectric
Fast Reactive
Tuner

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What can we
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Reactive
Tuners

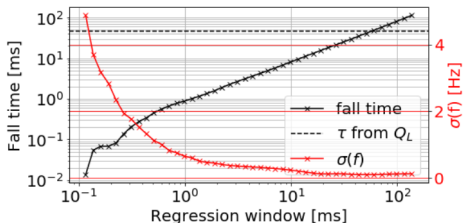
Ferroelectric
Material

Prototype
Tuner

Experimental
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Case Studies

Conclusion



Fall time and $\text{std}(f)$ vs. regression window length.

- Cavity response to tuner $< 50 \mu\text{s}$
- Cavity time constant $\tau_L = \frac{Q_L}{\omega_0} \approx 46 \text{ ms}$
- Cavity responds faster to FE-FRT than τ_L .



FoM and Frequency Dependence

A Ferroelectric
Fast Reactive
Tuner

N. Shipman

The issue

What can we
do?

Reactive
Tuners

Ferroelectric
Material

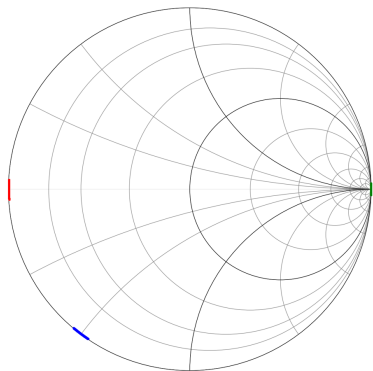
Prototype
Tuner

Experimental
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Conclusion

$$\text{FoM} \approx \frac{2 \left| \sin \frac{\Delta\theta_{12}}{2} \right|}{\sqrt{(1 - |\Gamma_1|^2)(1 - |\Gamma_2|^2)}}$$





FoM and Frequency Dependence

A Ferroelectric
Fast Reactive
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The issue

What can we
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Reactive
Tuners

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Material

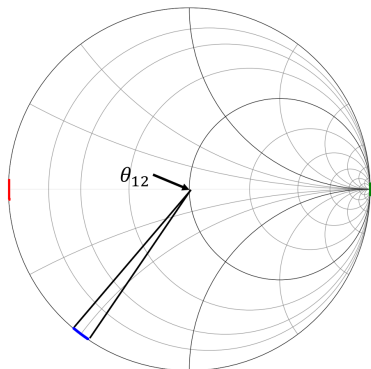
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FoM and Frequency Dependence

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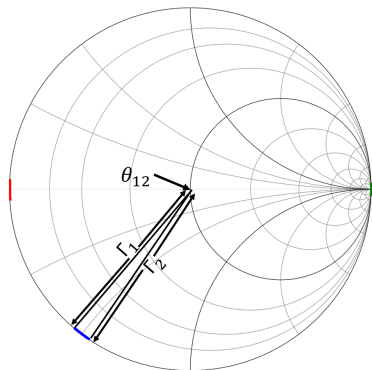
Prototype
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Experimental
Results

Case Studies

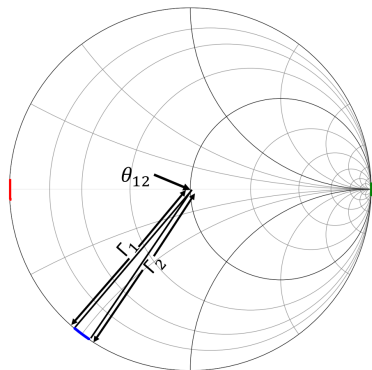
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$$\text{FoM} \approx \frac{2 \left| \sin \frac{\Delta\theta_{12}}{2} \right|}{\sqrt{(1 - |\Gamma_1|^2)(1 - |\Gamma_2|^2)}}$$

- FoM larger for:
 - lower losses





FoM and Frequency Dependence

A Ferroelectric
Fast Reactive
Tuner

N. Shipman

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What can we
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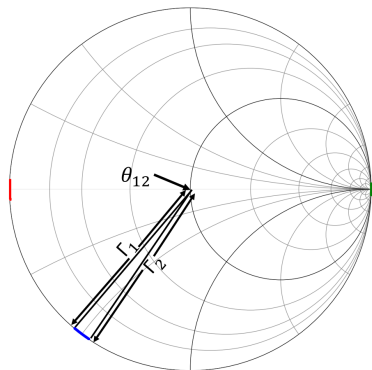
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- FoM larger for:
 - lower losses
 - greater phase change





FoM and Frequency Dependence

A Ferroelectric
Fast Reactive
Tuner

N. Shipman

The issue

What can we
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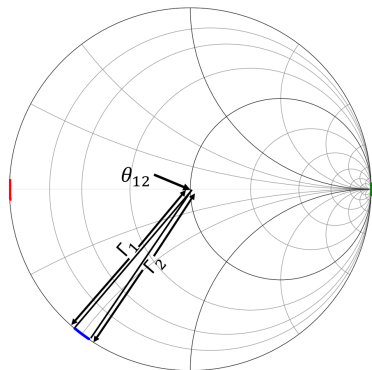
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- FoM larger for:
 - lower losses
 - greater phase change
- Larger FoM gives:





FoM and Frequency Dependence

A Ferroelectric
Fast Reactive
Tuner

N. Shipman

The issue

What can we
do?

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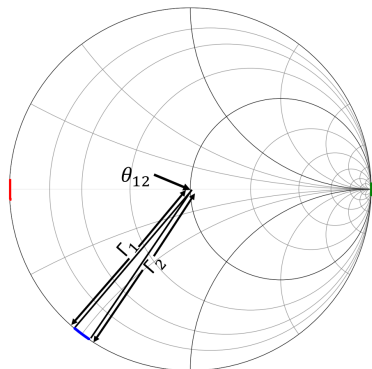
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- FoM larger for:
 - lower losses
 - greater phase change
- Larger FoM gives:
 - Increased tuning range





FoM and Frequency Dependence

A Ferroelectric
Fast Reactive
Tuner

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The issue

What can we
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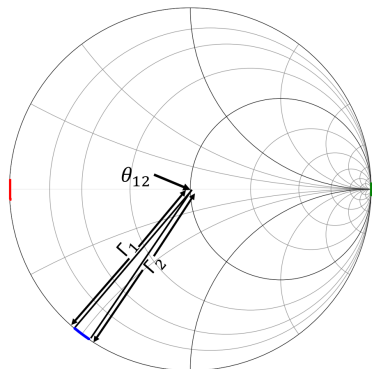
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- FoM larger for:
 - lower losses
 - greater phase change
- Larger FoM gives:
 - Increased tuning range
 - Decreased bandwidth





FoM and Frequency Dependence

A Ferroelectric
Fast Reactive
Tuner

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The issue

What can we
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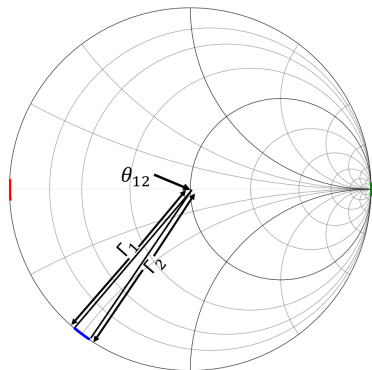
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- FoM larger for:
 - lower losses
 - greater phase change
- Larger FoM gives:
 - Increased tuning range
 - Decreased bandwidth
 - Decreased forward power





FoM and Frequency Dependence

A Ferroelectric
Fast Reactive
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What can we
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Tuner

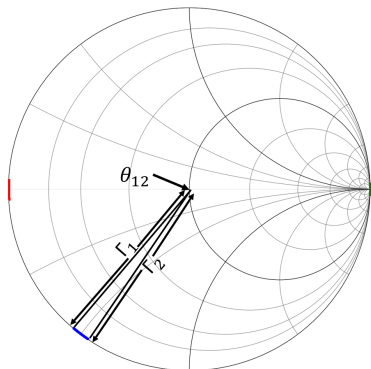
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- FoM larger for:
 - lower losses
 - greater phase change
- Larger FoM gives:
 - Increased tuning range
 - Decreased bandwidth
 - Decreased forward power
- P_{RF}^{avg} reduced by $\frac{\text{FoM}}{4}$



$$\text{FoM} \approx \frac{2 \left| \sin \frac{\Delta\theta_{12}}{2} \right|}{\sqrt{(1 - |\Gamma_1|^2)(1 - |\Gamma_2|^2)}}$$

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- P_{RF}^{avg} reduced by $\frac{\text{FoM}}{4}$
- P_{RF}^{peak} reduced by $\frac{\text{FoM}}{2}$

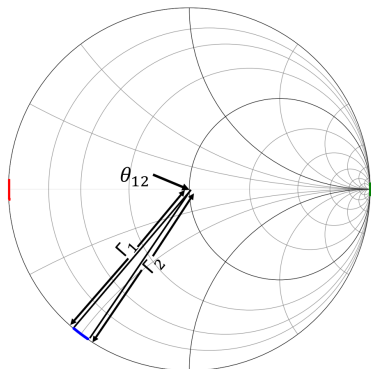




Figure of Merit (FoM) and Frequency Dependence

A Ferroelectric
Fast Reactive
Tuner

N. Shipman

The issue

What can we
do?

Reactive
Tuners

Ferroelectric
Material

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Experimental
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Conclusion

- P_{RF}^{avg} reduced by $\frac{\text{FoM}}{4}$
- P_{RF}^{peak} reduced by $\frac{\text{FoM}}{2}$

- $\alpha_c = 2.98 \cdot 10^{-7} \sqrt{f} \frac{1}{b} \left(1 + \frac{b}{a}\right) \frac{\epsilon}{\ln \frac{b}{a}} \text{ dB/m}$



Figure of Merit (FoM) and Frequency Dependence

A Ferroelectric
Fast Reactive
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N. Shipman

The issue

What can we
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- $\alpha_d = 9.11 \cdot 10^{-8} f \sqrt{\epsilon_r} \tan \delta \text{ dB/m}$



Figure of Merit (FoM) and Frequency Dependence

A Ferroelectric
Fast Reactive
Tuner

N. Shipman

The issue

What can we
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Reactive
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Ferroelectric
Material

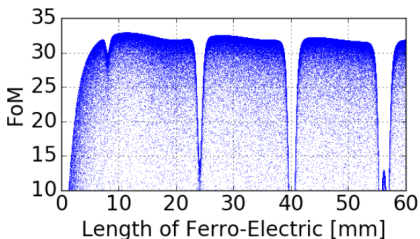
Prototype
Tuner

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- Monte Carlo, transmission line model



Figure of Merit (FoM) and Frequency Dependence

A Ferroelectric
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N. Shipman

The issue

What can we
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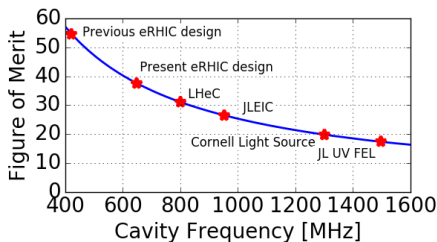
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- P_{RF}^{avg} reduced by $\frac{FoM}{4}$
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- Monte Carlo, transmission line model

- FoM frequency dependence



Figure of Merit (FoM) and Frequency Dependence

A Ferroelectric
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Tuner

N. Shipman

The issue

What can we
do?

Reactive
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Ferroelectric
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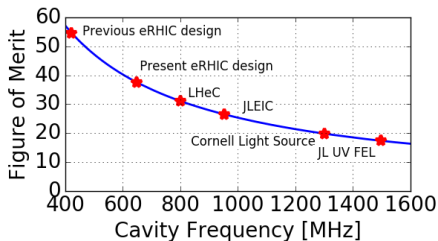
Prototype
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- Monte Carlo, transmission line model

- FoM frequency dependence

- Cross-checked with CST simulations



Figure of Merit (FoM) and Frequency Dependence

A Ferroelectric
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The issue

What can we
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Ferroelectric
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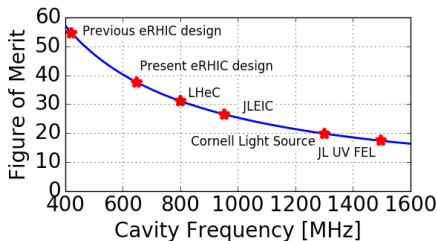
Prototype
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- P_{RF}^{avg} reduced by $\frac{FoM}{4}$
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- Monte Carlo, transmission line model

- FoM frequency dependence

- Cross-checked with CST simulations

- Better for lower frequencies



Case Studies

A Ferroelectric
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N. Shipman

The issue

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Parameter	eRHIC	PERLE	LHeC	Cornell
Frequency	647.4 MHz	801.58 MHz	801.58 MHz	1.3 GHz
Cavity Voltage – V_c	26.88 MV	18.7 MV	18.7 MV	13.1 MV
External Q-Factor of FPC – Q_e	1.60 × 10 ⁷	1.00 × 10 ⁷	1.56 × 10 ⁷	6.5 × 10 ⁷
Intrinsic Q-Factor – Q_0	2.00 × 10 ¹⁰	2.00 × 10 ¹⁰	2.00 × 10 ¹⁰	2.00 × 10 ¹⁰
R/Q	502 Ω	393 Ω	393 Ω	387 Ω
Peak Detuning – $\Delta\omega_{\mu peak}$	20.0 Hz	40.0 Hz	26.2 Hz	20.0 Hz
RMS Detuning – $\sigma(\Delta\omega_{\mu})$	3.33 Hz	6.67 Hz	4.36 Hz	3.33 Hz
Accelerating Gradient – E_{acc}	16 MV/m	20 MV/m	20 MV/m	16.2 MV/m
Cavity Length	1.68 m	0.935 m	0.935 m	0.81 m
Final Beam Energy	20 GeV	0.9 GeV	60 GeV	5 GeV
ERL Passes	12	3	3	1
Number of Cavities	62	16	1069	384
Grid to RF conversion efficiency	≈ 70%	≈ 50%	≈ 70%	≈ 50%
Total Electrical Power for microphonics control	1.37 MW	732 kW	22.2 MW	734 kW

- Black: From a reference
- Orange: Calculated from a referenced value
- Red: Estimated



Case Studies

A Ferroelectric
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- Black: From a reference
- Orange: Calculated from a referenced value
- Red: Estimated
- Every effort was made to ensure consistency.
- No guarantee that these are the latest accepted values.



Case Studies - PERLE

A Ferroelectric
Fast Reactive
Tuner

N. Shipman

The issue

What can we
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Ferroelectric
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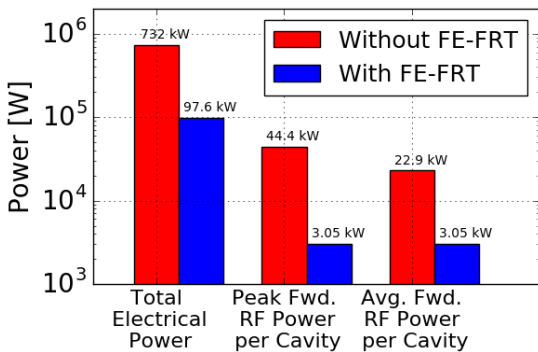
Prototype
Tuner

Experimental
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Conclusion

$$P_{RF} = \frac{V_c^2}{4R/QQL} \frac{\beta + 1}{\beta} \left[1 + \left(2QL \frac{\Delta\omega\mu}{\omega_0} \right)^2 \right]$$





Case Studies - PERLE

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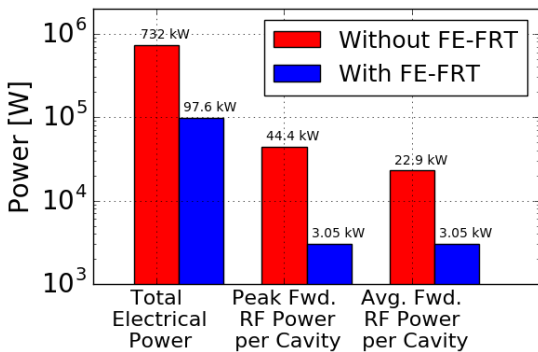
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- Peak power per cavity 44.4 kW → 3.05 kW



Case Studies - PERLE

A Ferroelectric
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What can we
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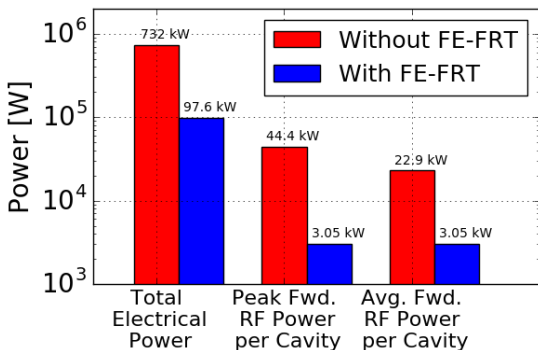
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$$P_{RF} = \frac{V_c^2}{4R/QQL} \frac{\beta + 1}{\beta} \left[1 + \left(2QL \frac{\Delta\omega\mu}{\omega_0} \right)^2 \right]$$



- Peak power per cavity 44.4 kW → 3.05 kW
- Total Electrical Power 732 kW → 97.6 kW



Case Studies - LHeC

A Ferroelectric
Fast Reactive
Tuner

N. Shipman

The issue

What can we
do?

Reactive
Tuners

Ferroelectric
Material

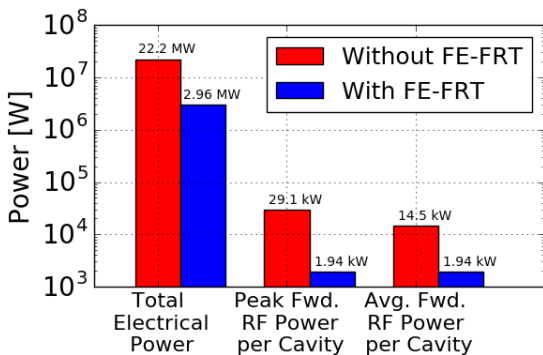
Prototype
Tuner

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Conclusion

$$P_{RF} = \frac{V_c^2}{4R/Q Q_L} \frac{\beta + 1}{\beta} \left[1 + \left(2Q_L \frac{\Delta\omega_\mu}{\omega_0} \right)^2 \right]$$





Case Studies - LHeC

A Ferroelectric
Fast Reactive
Tuner

N. Shipman

The issue

What can we
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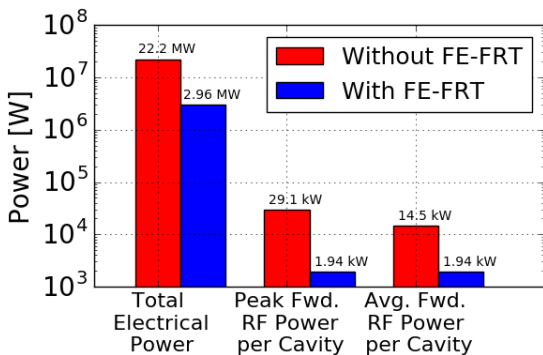
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- Peak power per cavity 29.1 kW → 1.94 kW



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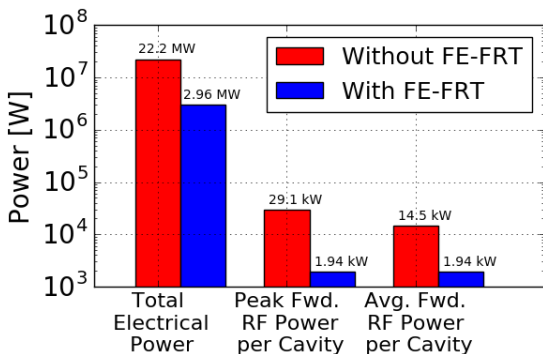
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- Peak power per cavity 29.1 kW → 1.94 kW
- Total Electrical Power **22.2 MW** → **2.96 MW**



Conclusion

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- Tested an FE-FRT with SC RF Cavity: World First!



Conclusion

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- Tested an FE-FRT with SC RF Cavity: World First!
- Ferroelectric parameters are excellent.



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- Ferroelectric parameters are excellent.
- Extremely fast $< 50 \mu\text{s}$



Conclusion

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- Tested an FE-FRT with SC RF Cavity: World First!
- Ferroelectric parameters are excellent.
- Extremely fast $< 50 \mu\text{s}$
 - Not limited by cavity time constant.
- Outside cryomodule, no moving parts → easy maintenance and high reliability.



Conclusion

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- Microphonics compensation must be experimentally demonstrated.



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- Outside cryomodule, no moving parts \rightarrow easy maintenance and high reliability.
- Microphonics compensation must be experimentally demonstrated.
- Brazing losses must be addressed.
- Could reduce power requirements by an order of magnitude or more.



Thank You

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Thank you for listening.

Any Questions?

- N. Shipman *et al.*, "A Ferroelectric Fast Reactive Tuner for Superconducting Cavities", in *SRF 2019*, Dresden, Germany, Jul. 2019.
- N. Shipman *et al.*, "A FerroElectric Fast Reactive Tuner (FE-FRT) to Combat Microphonics", in *ERL 2019*, Berlin, Germany, Sep. 2019.



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Case Study references

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- E. G. H. Hoffstaetter *et al.*, “Cornell Energy Recovery Linac Science Case and Project Definition Design Report”, *Cornell Tech. Rep.*, 2013, p. 518.
- E. C. Aschenauer *et al.*, “eRHIC Design Study: An Electron Ion Collider at BNL”, *Tech. Rep.*, Sep. 2014.
- W. Xu *et al.*, “RF and Mechanical Design of 647 MHz 5-CELL BNL4 Cavity for eRHIC ERL”, in *Proceedings of IPAC2016*, Busan, 2014.
- W. Xu *et al.*, “Progress of 650 MHz SRF cavity for eRHIC SRF linac”, in *18th International Conference on RF Superconductivity*, Lanzhou, 2017, pp. 64–66.
- D. Angal-Kalinin *et al.*, “PERLE. Powerful energy recovery linac for experiments. Conceptual design report”, *Journal of Physics G: Nuclear and Particle Physics*, vol. 45, no. 6, pp. 065 003, Jun. 2018.
- J. L. Abelleira Fernandez *et al.*, “A Large Hadron Electron Collider at CERN Report on the Physics and Design Concepts for Machine and Detector”, *Journal of Physics G: Nuclear and Particle Physics*, vol. 39, no. 7, pp. 075 001, Jul. 2012.
- R. Calaga, “A design for an 802 MHz ERL Cavity,” *CERN-ACC-NOTE-2015-0015*, 2015. .



Experimental Setup

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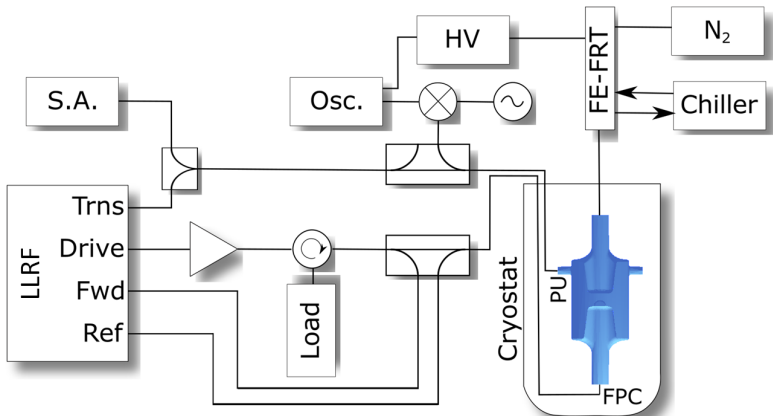
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Where is an FE-FRT likely to be most useful?

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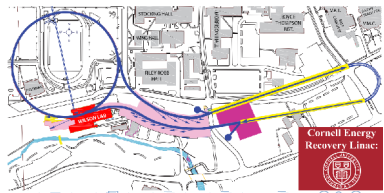
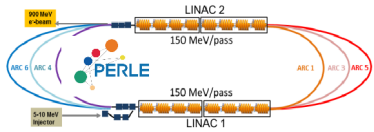
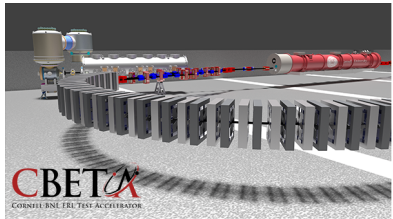
Prototype Tuner

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- Low beam loading machines
- ERLs
- Heavy Ion Accelerators
- If repetitive mechanical stresses must be avoided
- Whenever you need really fast tuning
- Where easy maintainability is a key concern





PERLE Case Study

A Ferroelectric Fast Reactive Tuner

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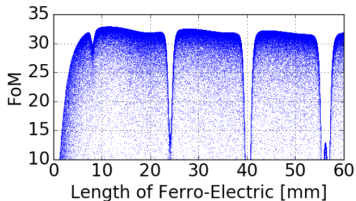
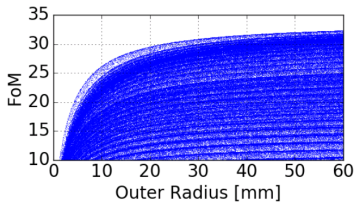
Table: PERLE SC 5-cell Cavity Parameters

Parameter	Value
ω_0	801.58 MHz
Q_0	2×10^{10}
R/Q	393 Ω
Q_{FPC}	10^7
P_{RF}	45 kW
Max. Δf_{μ}	40 Hz

Table: Material Properties at ≈ 800 MHz

Parameter	Value
Max. ϵ_r	140
Min. ϵ_r	131.6
$\tan \delta$	9.1×10^{-4}
$\frac{\Delta \epsilon_r}{E}$	$0.6 \text{ kV}^{-1} \text{ cm}$
σ_{Cu}	$5.96 \times 10^{-7} \text{ S/m}$

Monte Carlo method applied to FE-FRT Transmission Line Model for 801.58 MHz.





PERLE Case Study

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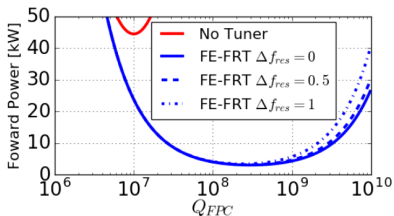
Prototype Tuner

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$$P_{RF} = \frac{V_c^2}{4^{R/Q} Q_L} \frac{\beta + 1}{\beta} \left[1 + \left(2Q_L \frac{\Delta\omega_\mu}{\omega_0} \right)^2 \right]$$



P_f vs Q_{FPC} for PERLE. **Without tuner** and **with tuner**.

Table: FE-FRT properties for PERLE

Parameter	Value
FoM	30
Δf_t	80
Q_{FPC}	3×10^8
P_{RF}	3 kW
P_t	2.4 kW
Max. \mathcal{P}_t	71 kVar

- ≈ 15 fold reduction in RF power
- We can do even better at lower frequencies!
- $\alpha_d = 9.11 \times 10^{-8} f \sqrt{\epsilon_r} \tan \delta$
- $\tan \delta \propto f$
- Dielectric losses $\propto f^2$



How does it work?

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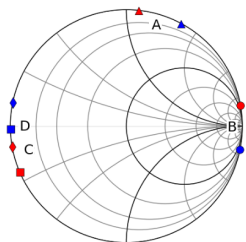
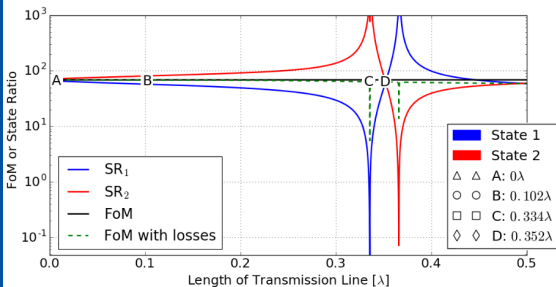
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$$\text{State Ratio}_n = \frac{\Delta\omega_{12}}{\Delta BW_n}$$

$$\text{FoM} = \sqrt{\text{SR}_1 \times \text{SR}_2}$$

$$\text{State Ratio}_n = \frac{\Delta B_t}{2G_{tn}}$$

$$\text{FoM} = \sqrt{\frac{(\Delta B_t)^2}{4G_1 G_2}}$$

$$\text{FoM} = \frac{\Delta\omega_{12}}{\sqrt{\Delta BW_1 \Delta BW_2}} \approx \frac{2 \left| \sin \frac{\Delta\theta_{12}}{2} \right|}{\sqrt{(1 - |\Gamma_1|^2)(1 - |\Gamma_2|^2)}}$$



Case Studies - eRHIC

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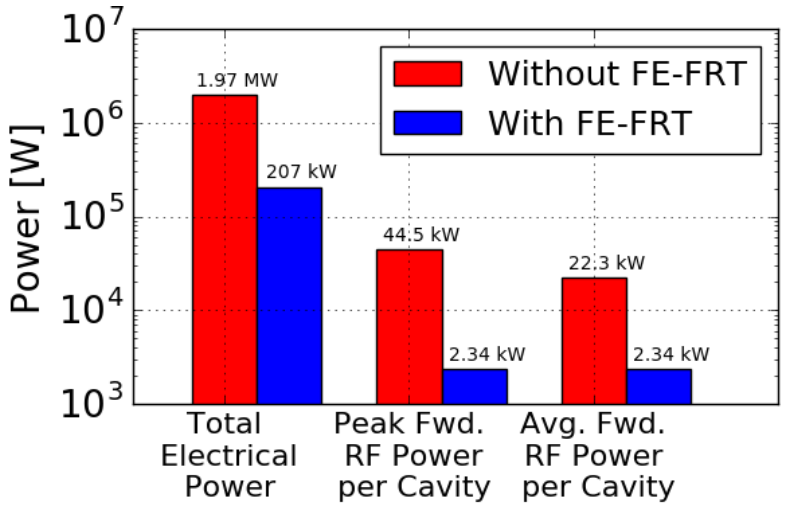
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Case Studies - Cornell Light Source ERL

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