



# Accelerator Physics

## Lecture 7: Momentum Effects

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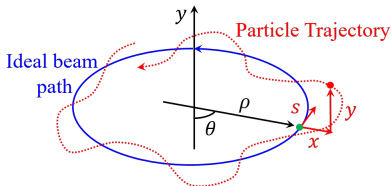
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Summary



# Curvilinear Co-ordinates



- $(x, y, s)$ , often called the standard co-ordinate system in accelerator physics
- The origin is defined by the vector  $\vec{S}(s)$  following the ideal reference path
- $x = r - \rho$        $s = \rho\theta$
- $X = r \sin \theta = (\rho + x) \sin \theta$ ,  $Y = y$ ,  $Z = r \cos \theta = (\rho + x) \cos \theta$



## Transverse Equation of Motion - 1

- Start with the basics

$$\begin{aligned} F_x &= m \frac{d^2 r}{dt^2} - \frac{mv^2}{r} \\ &= \frac{d^2(x + \rho)}{dt^2} - \frac{mv^2}{x + \rho} = -eB_y v \end{aligned} \quad (1)$$

- Factorise the equation

$$m \frac{d^2 x}{dt^2} - \frac{mv^2}{\rho} \left(1 + \frac{x}{\rho}\right)^{-1} = -eB_y v \quad (2)$$

- Utilise the binomial approximation

$$m \frac{d^2 x}{dt^2} - \frac{mv^2}{\rho} \left(1 - \frac{x}{\rho}\right) = -eB_y v \quad (3)$$



## Transverse Equation of Motion - 2

- Replace  $t$  with  $s$  and rearrange

$$mv^2 \frac{d^2x}{ds^2} - \frac{mv^2}{\rho} \left(1 - \frac{x}{\rho}\right) = -eB_y v \quad (4)$$

$$\frac{d^2x}{ds^2} - \frac{1}{\rho} \left(1 - \frac{x}{\rho}\right) = -\frac{eB_y}{mv} \quad (5)$$

- Consider small displacements in  $x$

$$\frac{d^2x}{ds^2} - \frac{1}{\rho} \left(1 - \frac{x}{\rho}\right) = -\frac{e}{mv} \left(B_0 + x \frac{\partial B_y}{\partial x}\right) \quad (6)$$



## Transverse Equation of Motion - 3

- Set field gradient,  $g = \frac{\partial B_y}{\partial x}$

$$\frac{d^2x}{ds^2} - \frac{1}{\rho} \left( 1 - \frac{x}{\rho} \right) = -\frac{eB_0}{mv} - \frac{exg}{mv} \quad (7)$$

This is a modified Hill's equation

- Consider small momentum offsets  $\Delta p = p - p_0 \ll p_0$

$$\begin{aligned} \frac{1}{p_0 + \Delta p} &= \frac{1}{p_0} \left( 1 + \frac{\Delta p}{p_0} \right)^{-1} \\ &\approx \frac{1}{p_0} - \frac{\Delta p}{p_0^2} \end{aligned} \quad (8)$$



## Transverse Equation of Motion - 4

- Insert equation 8 into modified Hill's equation 7

$$\frac{d^2x}{ds^2} - \frac{1}{\rho} \left(1 - \frac{x}{\rho}\right) = -\frac{eB_0}{p} - \frac{exg}{p}$$
$$\frac{d^2x}{ds^2} - \frac{1}{\rho} \left(1 - \frac{x}{\rho}\right) = -\frac{eB_0}{p_0} + \frac{eB_0\Delta p}{p_0^2} - \frac{exg}{p_0} + \frac{exg\Delta p}{p_0^2} \quad (9)$$

- Remember magnetic rigidity??.  $B\rho = p/e$

$$\frac{d^2x}{ds^2} + \frac{x}{\rho^2} = \frac{1}{\rho} \frac{\Delta p}{p_0} + kx \quad (10)$$

where  $k = eg/p_0$  and the last term is the product of two small terms ( $\approx 0$ )



## Transverse Equation of Motion - 5

- Finally a new **modified Hill's equation**

$$\frac{d^2x}{ds^2} + \left( \frac{1}{\rho^2} - k \right) x = \frac{1}{\rho} \frac{\Delta p}{p_0} \quad (11)$$

- Compare to the original Hill's equation from transverse lectures

$$\frac{d^2x}{ds^2} + \left( \frac{1}{\rho^2} - k \right) x = 0 \quad (12)$$

- **Particles with different momenta/energy have different orbits**



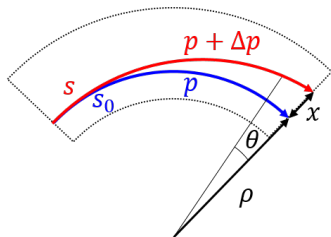


## Dispersion

- General solution will be of the form  $x(s) = x_h(s) + x_i(s)$
- From previous lecture, **dispersion** is defined as

$$D(s) = \frac{x_i(s)}{\Delta p/p_0} \quad (13)$$

- It is just another orbit and is subject to the focusing properties of the lattice
- The orbit of any particle is the sum of the well-known  $x_h$  and dispersion



## Matrix formalism

- Recall transfer matrices from transverse lectures and add dispersion

$$\begin{pmatrix} x \\ x' \end{pmatrix}_1 = \begin{pmatrix} C & S \\ C' & S' \end{pmatrix} \begin{pmatrix} x \\ x' \end{pmatrix}_0 + \frac{\Delta p}{p_0} \begin{pmatrix} D \\ D' \end{pmatrix} \quad (14)$$

where  $C = \cos \sqrt{|k|}s$ ,  $S = \frac{1}{\sqrt{k}} \sin \sqrt{|k|}s$ ,  $C' = \frac{dC}{ds}$ ,  $S' = \frac{dS}{ds}$

and  $D'(s) = \frac{x'_i(s)}{\Delta p/p_0}$

- One can show that

$$D(s) = S(s) \int_{s_0}^{s_1} \frac{1}{\rho} C(s) ds - C(s) \int_{s_0}^{s_1} \frac{1}{\rho} S(s) ds \quad (15)$$

## Examples of Dispersion - 1

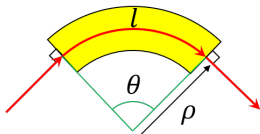
- Start with something simple, a **drift**!

$$M_{\text{drift}} = \begin{pmatrix} 1 & l \\ 0 & 1 \end{pmatrix}, \quad C(s) = 1, \quad S(s) = l \quad (16)$$

- Importantly  $\rho = \infty$  so immediately  $D_{\text{drift}} = 0$
- OK, how about a **pure sector dipole**?

$$M_{\text{dipole}} = \begin{pmatrix} \cos \frac{l}{\rho} & \rho \sin \frac{l}{\rho} \\ -\frac{1}{\rho} \sin \frac{l}{\rho} & \cos \frac{l}{\rho} \end{pmatrix}$$

$$C(s) = \cos \frac{l}{\rho}, \quad S(s) = \rho \sin \frac{l}{\rho} \quad (17)$$





## Examples of Dispersion - 2

- Putting this in the equation for dispersion

$$\begin{aligned}D_{\text{dipole}}(s) &= \sin \frac{l}{\rho} \int_0^l \cos \frac{s}{\rho} ds - \cos \frac{l}{\rho} \int_0^l \sin \frac{s}{\rho} ds \\&= \sin \frac{l}{\rho} \left[ \rho \sin \frac{s}{\rho} \right]_0^l - \cos \frac{l}{\rho} \left[ -\rho \cos \frac{s}{\rho} \right]_0^l \\&= \rho \sin^2 \frac{l}{\rho} + \rho \cos \frac{l}{\rho} \left( \cos \frac{l}{\rho} - 1 \right) \\&= \rho \left( 1 - \cos \frac{l}{\rho} \right)\end{aligned}\tag{18}$$

- And  $D'_{\text{dipole}}(s) = \sin \frac{l}{\rho}$

## Examples of Dispersion - 3

- Assuming  $\theta$  is small we can expand this

$$\begin{aligned} D(s)_{\text{dipole}} &= \rho \left( 1 - \cos \frac{l}{\rho} \right) \\ &\approx \rho \left( 1 - \left[ 1 - \frac{1}{2} \left( \frac{l}{\rho} \right)^2 \right] \right) \\ &\approx \frac{\rho}{2} \left( \frac{l}{\rho} \right)^2 = \frac{\rho \theta^2}{2} \end{aligned} \quad (19)$$

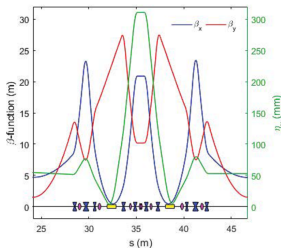


## Matrix formalism continued

- Can now expand the transfer matrix to include dispersion

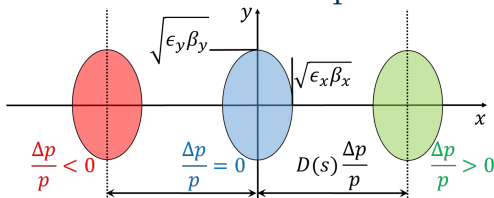
$$\begin{pmatrix} x \\ x' \\ \Delta p/p \end{pmatrix}_1 = \begin{pmatrix} C & S & D \\ C' & S' & D' \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} x \\ x' \\ \Delta p/p \end{pmatrix}_0 \quad (20)$$

- Dispersion can be calculated by an optics code for a real machine
- $D(s)$  is created by the **dipoles**...
- ... and focused by the **quadrupoles**
- *Diamond DBA example*  $\Rightarrow$





## Dispersed Beam Orbits

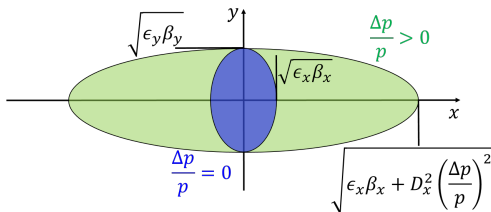


- These are 2D ellipses defining the beam
- The central and extreme momenta are shown (there is a distribution in between)
- The vacuum chamber must accommodate the full spread
- With dispersion the **half height** and **half width** are (assuming  $D_y = 0$ )

$$a_y = \sqrt{\eta_y \beta_y}, \quad a_x = \sqrt{\eta_x \beta_x} + D(s) \frac{\Delta p}{p} \quad (21)$$



## Dispersed Beam Size

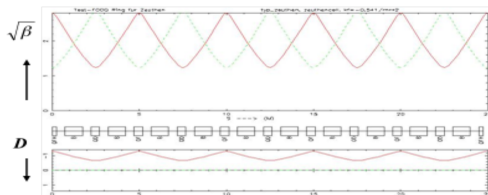


- Dispersion also contributes to the beam size
- Therefore we can **measure the dispersion** by measuring beam sizes at different locations with different amounts of dispersion and different  $\beta$ s





# Dispersion Suppression

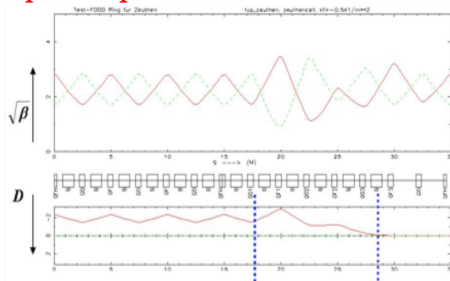


- Given a periodic lattice what can we do about dispersion?
- We can't get rid of it completely as it's produced by the dipoles
- Answer ... **suppress the dispersion elsewhere**



## Dispersion Suppression: Easy option

- Use **extra quadrupoles** to match  $D(s)$  and  $D'(s)$
- Given an optical solution in the arc, suppressing dispersion can be achieved with **2 additional quadrupoles**
- **But that's not enough!** Need to match the Twiss, optical parameters too
- An **extra 4 quadrupoles** are needed to match  $\alpha$  and  $\beta$





## Dispersion Suppression: Easy option

### Advantages:

- Straight forward
- Works for any phase advance per cell
- Ring geometry is unchanged
- Flexible! Can match between different lattice structures

### Disadvantages:

- Additional quadrupole magnets and power supplies required
- The extra quadrupoles are, in general stronger
- The  $\beta$  function increases so the aperture increases



## Dispersion Suppression: Missing Bend

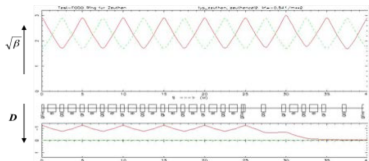
- Start with  $D = D' = 0$  and create dispersion such that the conditions are matched in the first regular quadrupoles
- Utilise  $n$  cells **without dipole magnets** at the end of an arc, followed by  $m$  arc cells
- ... hence **“missing bend” dispersion suppression**
- Condition:

$$\frac{2m + n}{2} \Phi_C = (2k + 1) \frac{\pi}{2} \quad (22)$$

where  $\Phi_C$  = cell phase advance,

$$\sin \frac{m\Phi_C}{2} = \frac{1}{2}, \quad k = 0, 2, \dots \text{ or}$$

$$\sin \frac{m\Phi_C}{2} = -\frac{1}{2}, \quad k = 1, 3, \dots$$





## Dispersion Suppression: Missing Bend

### Advantages:

- No additional quadrupoles or new power supplies
- Aperture requirements are the same as those in the arc as  $\beta$  is unchanged

### Disadvantages:

- Only works for certain phase advances restricting optics options in the arc
- The geometry of the ring is changed



## Dispersion Suppression: Half Bend

- How about inserting **different strength dipoles**? Does it help?
- Assume you have a FODO arc cell, a lattice insertion and then a dispersion free section without dipoles
- Condition for vanishing dispersion can be calculated for  $n$  cells with dipole strength  $\delta_{\text{sup}}$

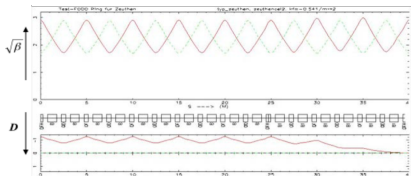
$$2\delta_{\text{sup}} \sin^2 \left( \frac{n\Phi_C}{2} \right) = \delta_{\text{arc}} \quad (23)$$

- So if we require  $\delta_{\text{sup}} = \frac{1}{2}\delta_{\text{arc}}$  we get

$$\begin{aligned} \sin^2 \left( \frac{n\Phi_C}{2} \right) = 1 &\Rightarrow \sin(n\Phi_C) = 0 \\ \Rightarrow n\Phi_C = k\pi, \quad k = 1, 3, \dots &\quad (24) \end{aligned}$$



## Dispersion Suppression: Half Bend



**Advantages** and **Disadvantages** are the same as for the missing bend only there is an extra **disadvantage**:

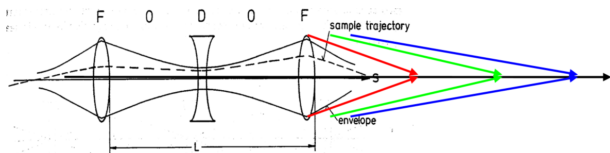
A special half strength dipole is required which may add extra cost to the design

*Note that this is not an exhaustive list of dispersion suppression techniques, just a taster!*



# Chromaticity - 1

- What about off-momentum effects through quadrupoles?
- The focusing strength of a quadrupole depends on the momentum of the particle  $1/f \propto 1/p$



- Particles with  $\Delta p > 0$ ,  $\Delta p < 0$ , ideal momentum
- Off-momentum particles oscillate around a **chromatic closed orbit** NOT the design orbit





## Chromaticity - 2

- Normalised quadrupole strength  $k = \frac{g}{p/e}$
- In case of a momentum spread

$$k = \frac{eg}{p_0 + \Delta p} \approx \frac{eg}{p_0} \left(1 - \frac{\Delta p}{p_0}\right) = k_0 + \Delta k \quad (25)$$

$$\Delta k = -\frac{\Delta p}{p_0} k_0 \quad (26)$$

- This acts like a quadrupole error in the machine and leads to a **tune spread**

$$\Delta Q = \frac{1}{4\pi} \int \Delta k(s) \beta(s) ds = -\frac{1}{4\pi} \frac{\Delta p}{p_0} \int k_0(s) \beta(s) ds \quad (27)$$



## Chromaticity - 3

- This spread in tune is expressed via **chromaticity,  $Q'$**  or the **normalised chromaticity,  $\xi$**

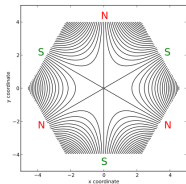
$$Q' = \frac{\Delta Q}{\Delta p/p_0}, \quad \xi = \frac{\Delta Q/Q}{\Delta p/p_0} \quad (28)$$

- Note that chromaticity is produced by the lattice itself
- It is determined by the focusing strength of all the quadrupoles
- The **“natural” chromaticity** is negative and can lead to a large tune spread and consequent instabilities
- For example, for a FODO lattice  $\xi \approx -1$



## Correcting Chromaticity - 1

- Want to “**sort**” the particles by their momentum
- Utilise dispersive trajectory! Apply magnetic field that is zero at small amplitudes and rises quickly outward
- Use **sextupoles**!

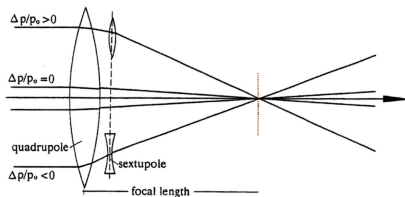


$$B_x = \tilde{g}xz, \quad B_y = \frac{1}{2}\tilde{g}(x^2 - y^2) \quad (29)$$

- This results in a linear gradient in  $x$ ,  
$$\frac{\partial B_x}{\partial y} = \frac{\partial B_y}{\partial x} = \tilde{g}x$$
- And a normalised quadrupole strength  
$$k_{\text{sext}} = \frac{\tilde{g}x}{p/e} = m_{\text{sext}}x = m_{\text{sext}}D\Delta p/p$$



## Correcting Chromaticity - 2



- This all results in a corrected chromaticity

$$Q' = -\frac{1}{4\pi} \oint \beta(s) [k(s) - mD(s)] ds \quad (30)$$

- **Chromatic sextupoles:** Sextupoles at nonzero dispersion can correct natural chromaticity
- Usually **2 families**, one horizontal and one vertical
- Place where  $\beta_{x/y}D$  is large to minimise their strength



## Summary

- Reminder of co-ordinate system
- Transverse equation of motion: **modified Hill's equation** with momentum spread
- **Dispersion** revisited in matrix form
- Effect of dispersion on beam orbit and beam size
- **Dispersion suppression**
- **Chromaticity** and chromatic tune spread
- Chromatic sextupoles and **chromaticity correction**



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