

Design of SiGe BiCMOS monolithic pixel sensors with picosecond-level time resolution

Lorenzo Paolozzi Université de Genève

(2018)

110 ps

220 ps

(2017)

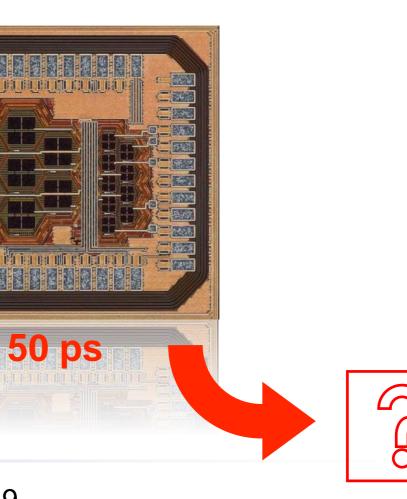
Heidelberg November 13, 2019



Lorenzo Paolozzi

Heidelberg 2019

(2019)



- Back in 2014 G. lacobucci, R. Cardarelli and M. Nessi proposed a strategy to use SiGe HBTs for ultra-fast, low noise signal amplification in particle detectors.
- The goal was to produce a monolithic pixelated silicon detector with 100 ps time resolution.
 - L. Paolozzi and P. Valerio joined shortly later as chip designers.



Funded by:



Fonds national suisse de la recherche scientifique



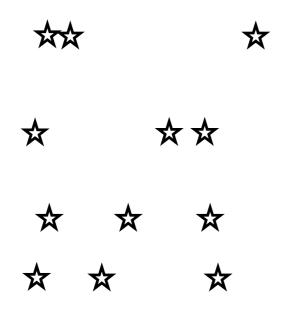
Five years of (hard) R&D



Lorenzo Paolozzi

Hartmut F-W Sadrozinski et al 2018 Rep. Prog. Phys. 81 026101

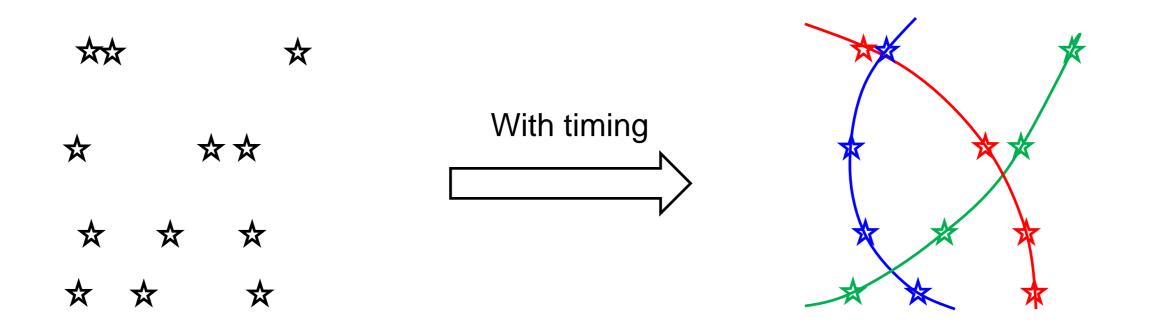
Advanced track reconstruction





Hartmut F-W Sadrozinski et al 2018 Rep. Prog. Phys. 81 026101

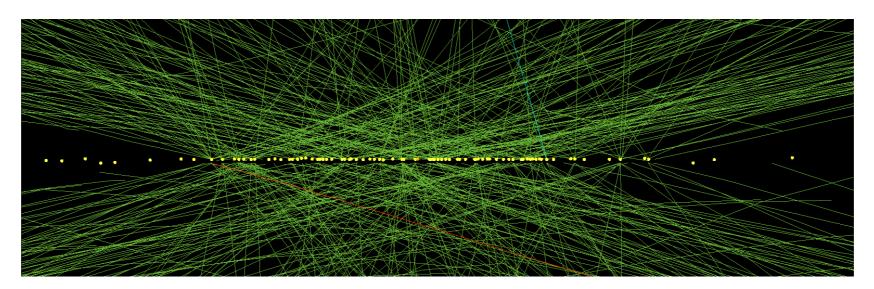
Advanced track reconstruction





Hartmut F-W Sadrozinski et al 2018 Rep. Prog. Phys. 81 026101

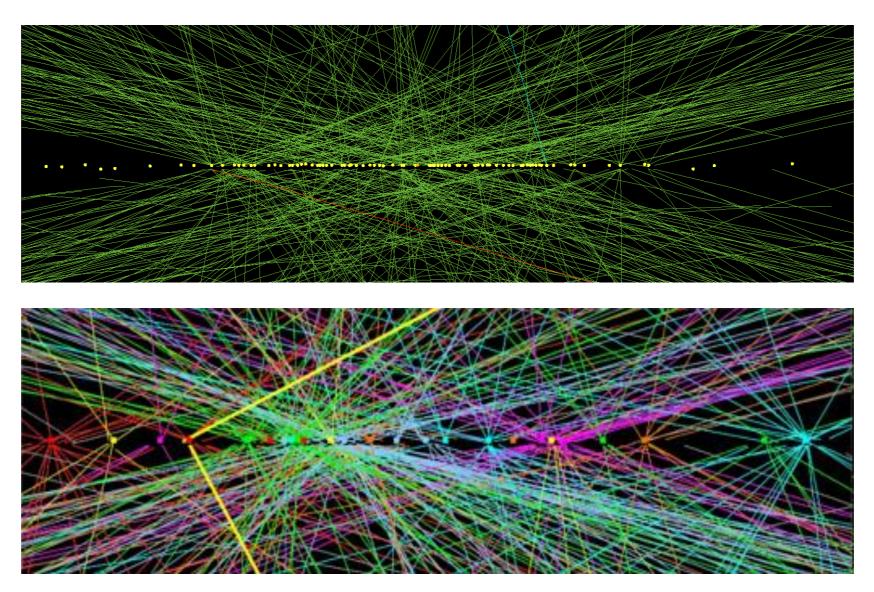
Pile-up suppression





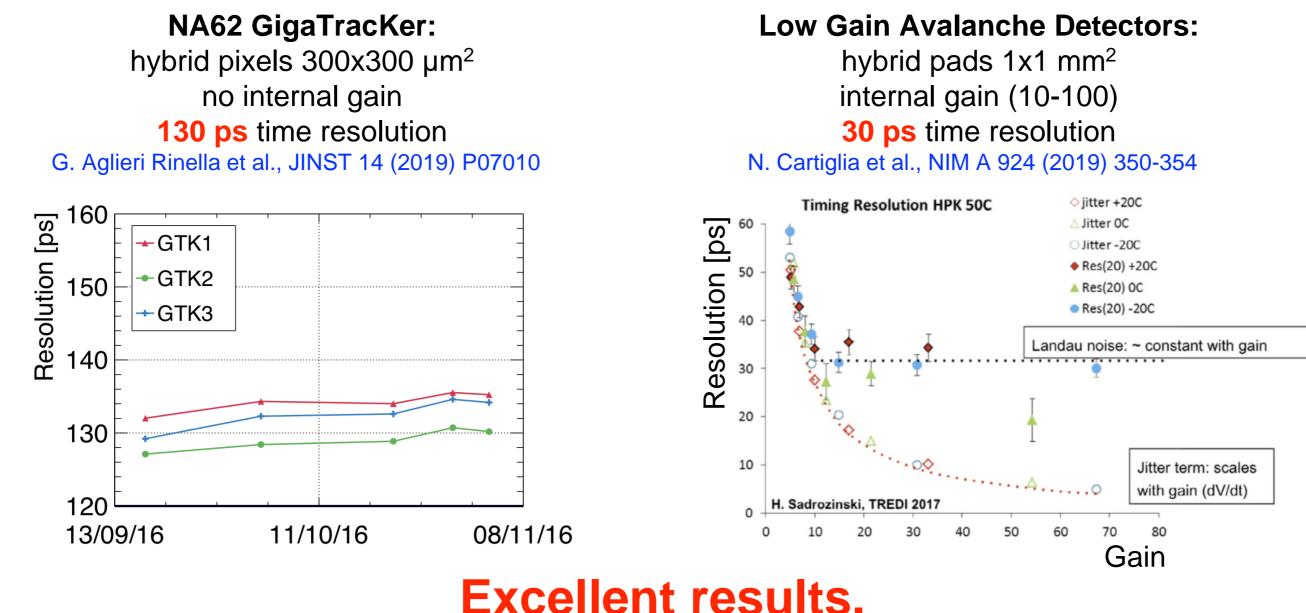
Hartmut F-W Sadrozinski et al 2018 Rep. Prog. Phys. 81 026101

Pile-up suppression





Situation today: technologies in HEP experiments



Is timing performance of silicon fully exploited ? How far are we from producing a monolithic 4D sensor with small pixels?



Timing with silicon detectors

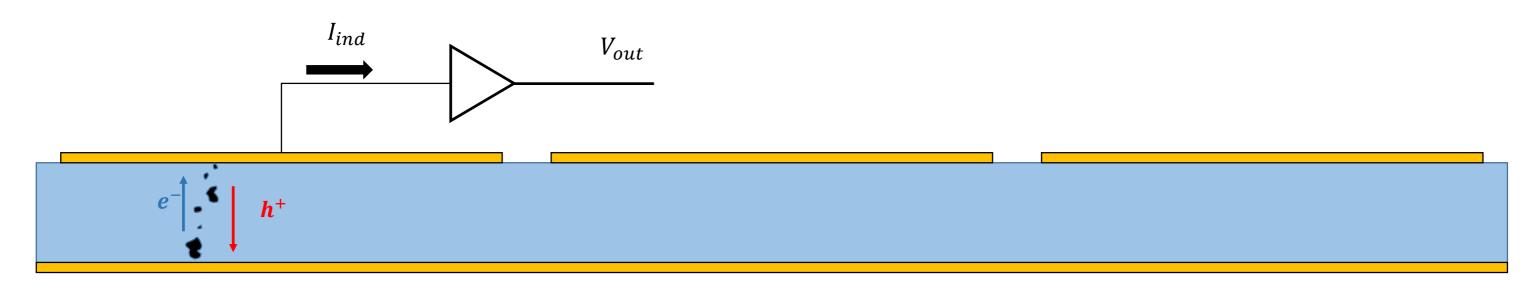


Time resolution of silicon pixel detectors

W. Riegler and G. Aglieri Rinella, Time resolution of silicon pixel sensors, JINST 12 (2017) P11017) (Recommended reading

What are the main parameters that control the time resolution of semiconductor detectors?

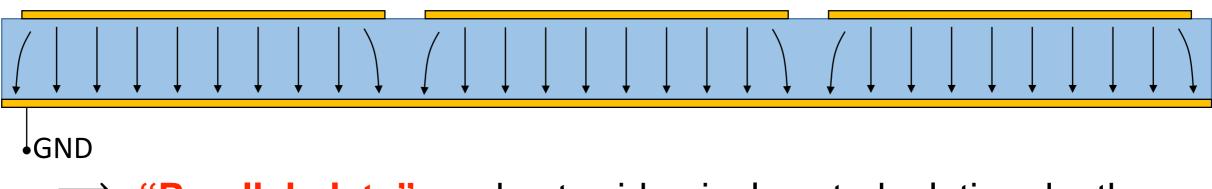
- 1. Geometry & fields
- 2. Charge collection (or Landau) noise
- 3. Electronics noise





1. Geometry and fields

Sensor optimization for time measurement means: sensor time response independent from the particle trajectory



 \implies "Parallel plate" read out: wide pixel w.r.t. depletion depth

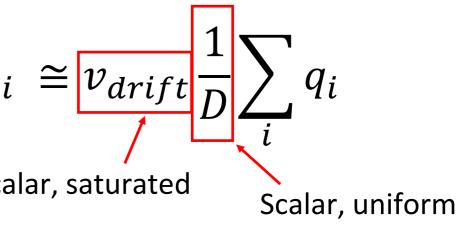
Induced current for a parallel plate readout from Shockley-Ramo's theorem:

$$I_{ind} = \sum_{i} q_{i} \bar{v}_{drift,i} \cdot \bar{E}_{w,i}$$

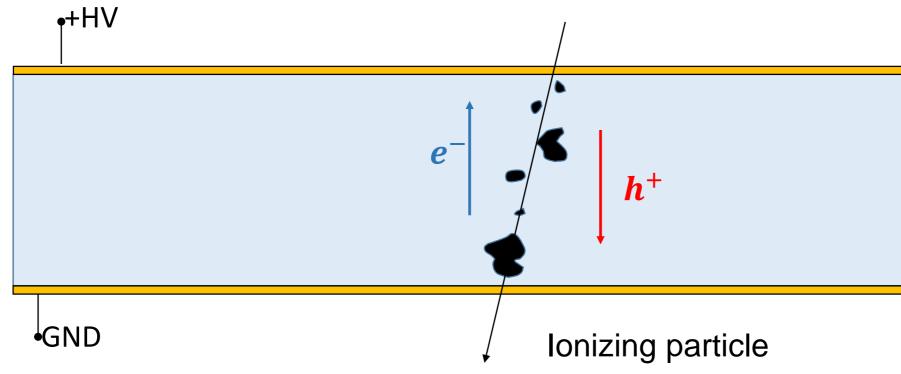
Desired features:

- **Uniform** Ramo field (signal induction)
- **Uniform** electric field (charge transport)
- Saturated charge drift velocity





2. Charge-collection (or Landau) noise



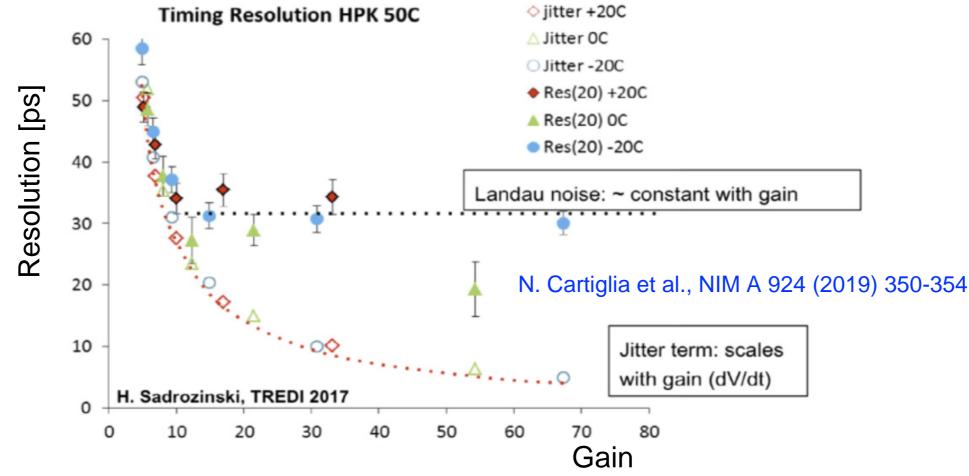
is produced by the **non uniformity of the charge deposition** in the sensor:

When **large clusters** are absorbed at the electrodes, their contribution is removed from the induced current. The **statistical origin** of this variability of I_{ind} makes this effect irreducible in PN-junction sensors.



$$I_{ind} \cong v_{drift} \frac{1}{D} \sum_{i}^{} q_i$$

2. Charge-collection (or Landau) noise



Charge collection noise represents an intrinsic limit to the time resolution for a semiconductor PN-junction detector.

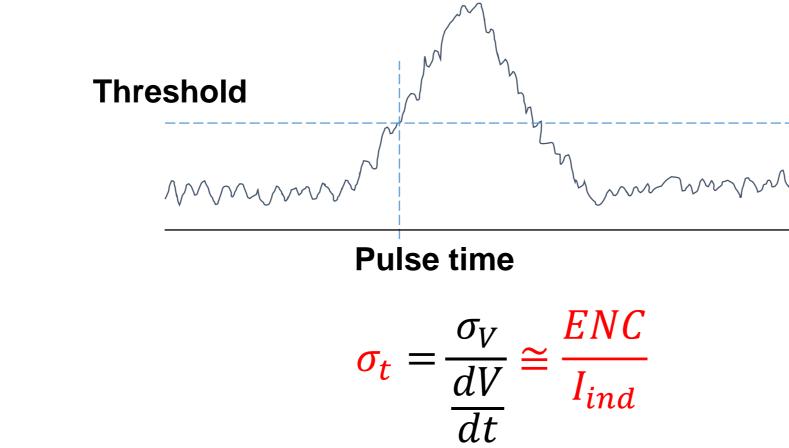
~30 ps reached by present LGAD sensors.

Lower contribution from sensors without internal gain



3. Electronics noise

Once the geometry has been fixed, the time resolution depends mostly on the amplifier performance.



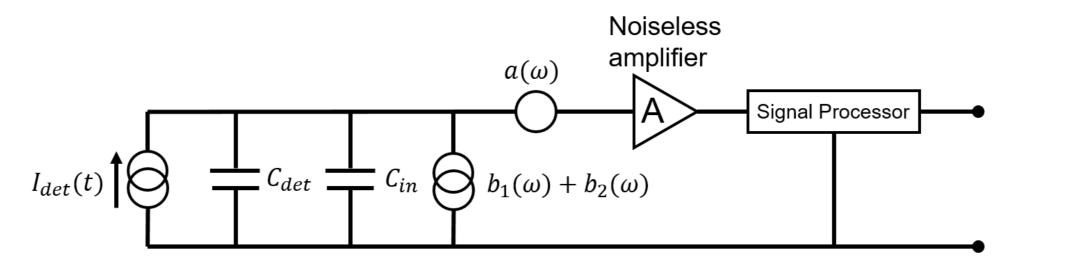
Need an ultra-fast, low noise, low power-consumption electronics with fast rise time and small capacitance. Our solution:

High f_t , single transistor preamplifier.



Time

Equivalent Noise Charge: device comparison



$$ENC^{2} = A_{1} \frac{a_{W}}{\tau_{M}} (C_{det} + C_{in})^{2} + A_{2} \frac{ln2}{\pi} c(C_{det} + C_{in})^{2}$$

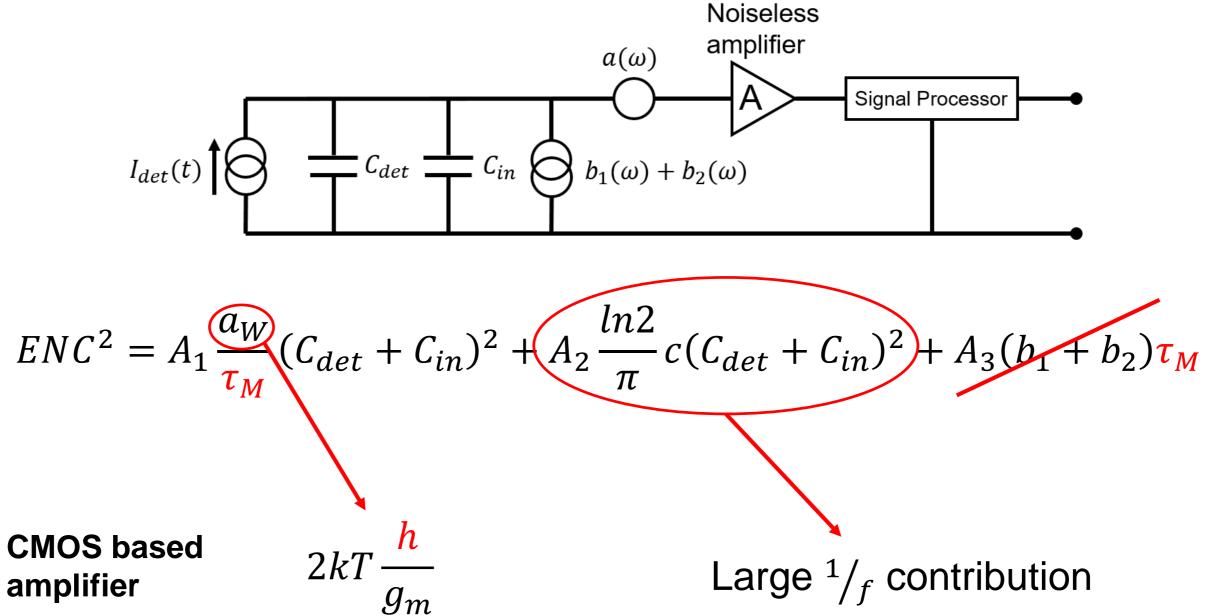
 $\tau_M \sim 1 ns$

How do MOS-FET and BJT compare in terms of noise?



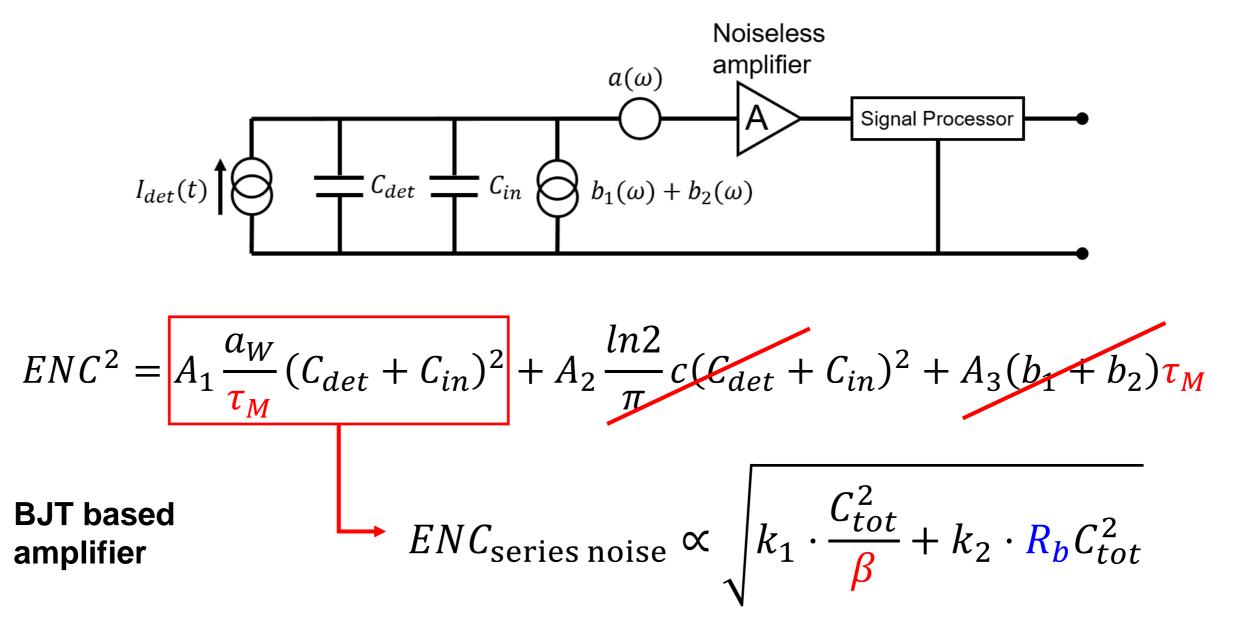
 $(L_{in})^2 + A_3(b_1 + b_2)\tau_M$

Equivalent Noise Charge: device comparison





Equivalent Noise Charge: device comparison



Goal: maximize the current gain β at high frequencies while keeping a low base resistance R_b



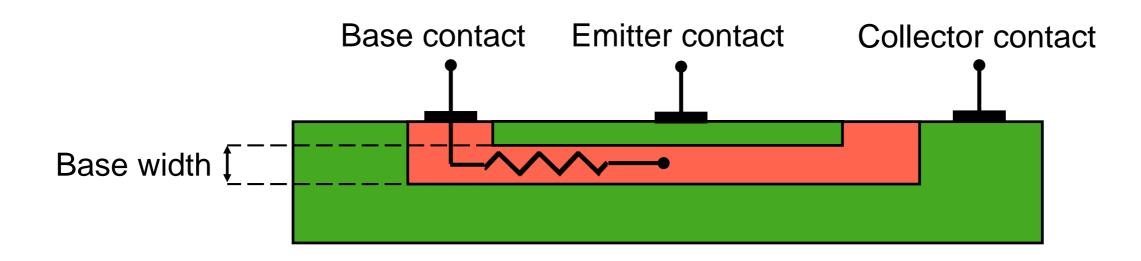
Equivalent Noise Charge

For a NPN BJT, the amplifier current gain β can be expressed as:

$$\boldsymbol{\beta} = \frac{i_C}{i_B} = \frac{\tau_p}{\tau_t}$$

 T_p = hole recombination time in Base

Large $\beta \implies$ Minimize the electron transit time

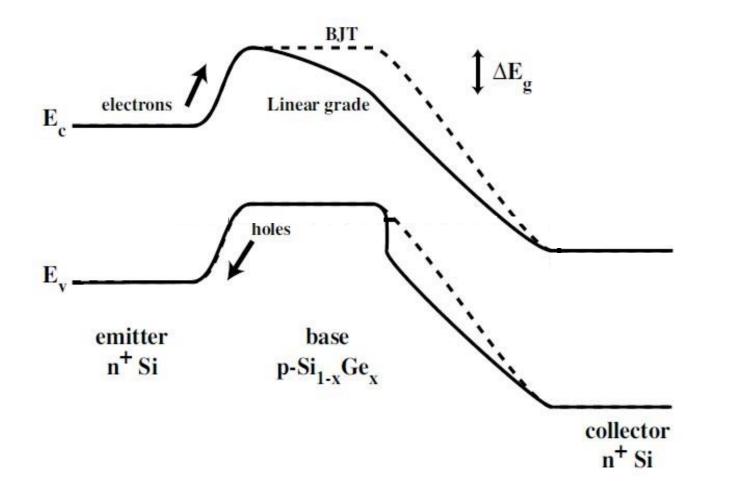




- \mathcal{T}_t = electron transit time (Emitter to Collector)

SiGe HBT technology for low-noise, fast amplifiers

In SiGe Heterojunction Bipolar Transistors (HBT) the grading of the bandgap in the Base changes the **charge-transport mechanism** in the Base from **diffusion** to **drift**:



Grading of germanium in the base: field-assisted charge transport in the Base, equivalent to introducing an electric field in the Base

- \Rightarrow short e⁻ transit time in Base \Rightarrow very high β

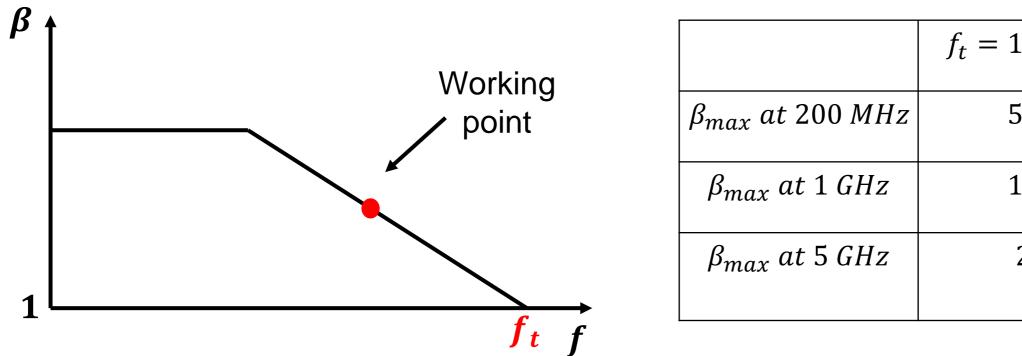


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 \Rightarrow smaller size \Rightarrow reduction of R_{h} and very high

Hundreds of GHz

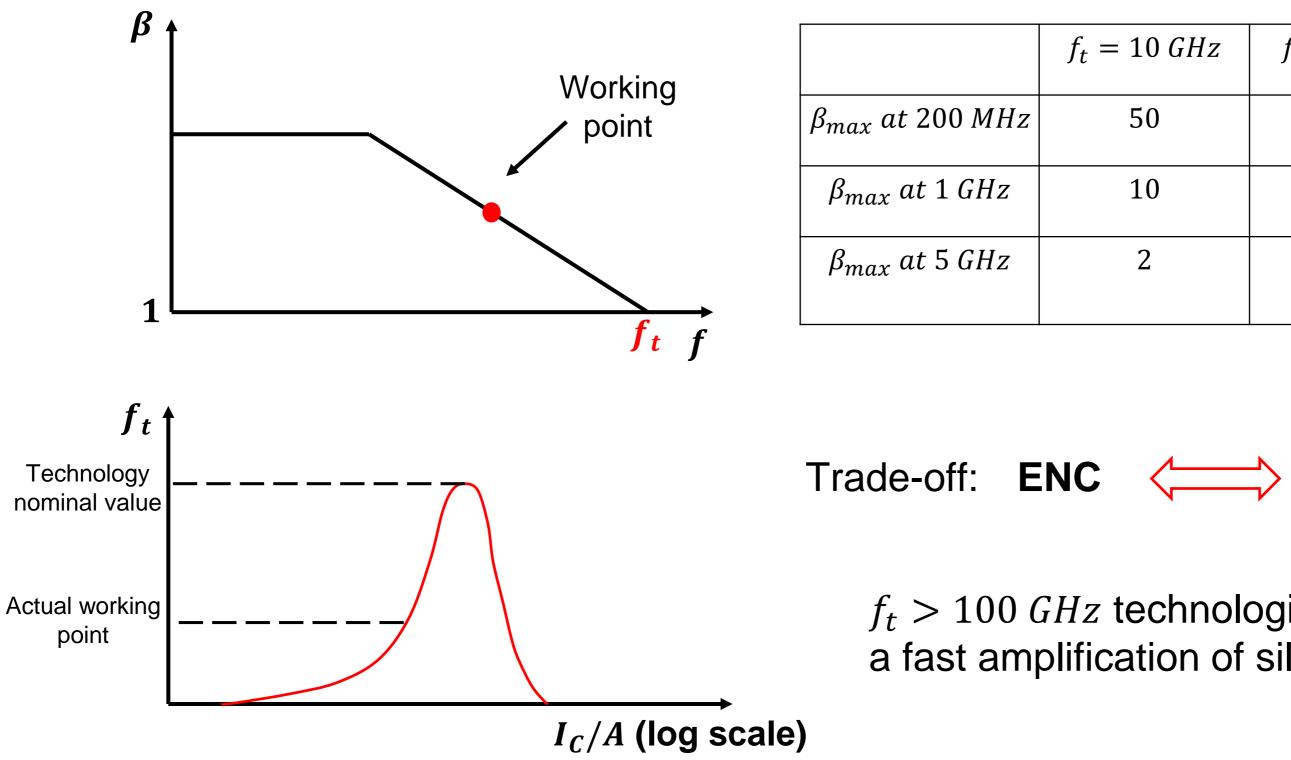
Current gain and power consumption: f_t is the key





| 10 <i>GHz</i> | $f_t = 50 \ GHz$ | $f_t = 100 \; GHz$ |
|---------------|------------------|--------------------|
| 50 | 250 | 500 |
| 10 | 50 | 100 |
| 2 | 10 | 20 |

Current gain and power consumption: f_t is the key





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| 10 <i>GHz</i> | $f_t = 50 \; GHz$ | $f_t = 100 \; GHz$ |
|---------------|-------------------|--------------------|
| 50 | 250 | 500 |
| 10 | 50 | 100 |
| 2 | 10 | 20 |

Power Consumption

$f_t > 100 \; GHz$ technologies are necessary for a fast amplification of silicon pixel signals.

SiGe BiCMOS applications **Commercial** VLSI CMOS foundry processes available SiGe BiCMOS Markets Served









Optical fiber networks

Smartphones

IoT Devices

Microwave Communication

TowerJazz

• TSMC

• STM

• AMS

•

Automotive: LiDAR, Radar and Ethernet

https://towerjazz.com/technology/rf-and-hpa/sige-bicmos-platform/ source:

Applications:

- Automotive radars (27/77 GHz)
- Satellite communications
- LAN RF transceivers (60 GHz)
- Point-to-point radio (V-band, E-band)
- Defense
- Security

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Instrumentation

A fast growing technology: $f_t = 700$ GHz transistor under development

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HDD preamplifiers, line drivers, Ultra-high speed DAC/ADCS

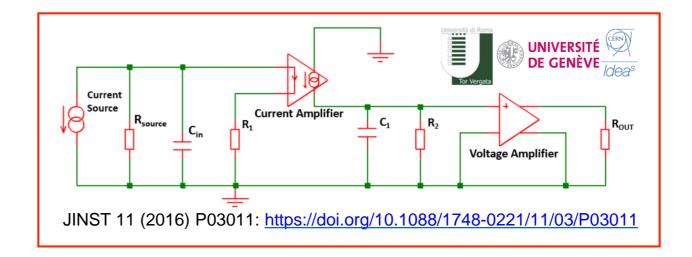
Foundries offering SiGe process: • IHP Mikroelektronik (\rightarrow Research Inst.)

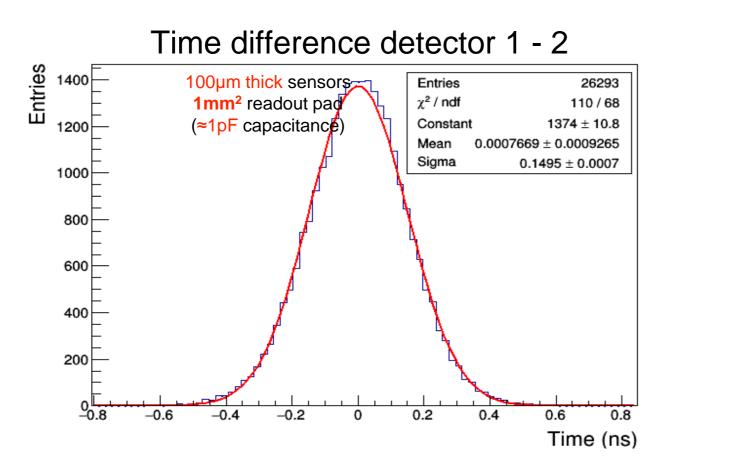
Globafoundries

Discrete-component SiGe HBT amplifier

In 2015:

- Proof-of-concept SiGe amplifier and produced it with **discrete components**
- This amplifier was coupled to a 100µm thick n-on-p silicon sensor with readout pad of **1mm²** area (~1pF capacitance)





Published in JINST 11 (2016) P03011: https://doi.org/10.1088/1748-0221/11/03/P03011



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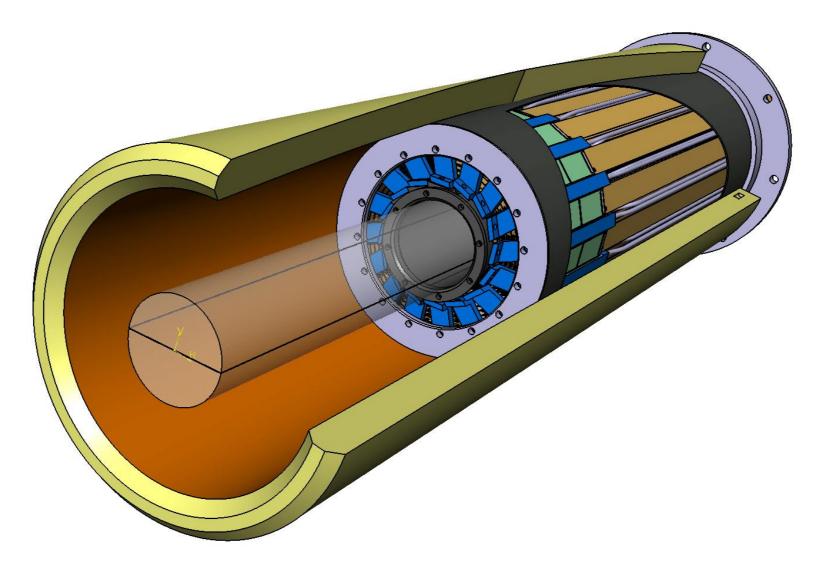


$\sigma_T = \frac{(150 \pm 1)\text{ps}}{\sqrt{2}} = (106 \pm 1)\text{ps}$

measured with MIPs

Remarkable result for a 1mm² silicon pad (1pF capacitance) without internal gain

The TT-PET project: a 30 ps⁺ Time-of-Flight PET scanner with monolithic SiGe silicon pixels



(+ GEANT4 simulation shows that 100 ps for MIPs corresponds to ~30 ps in case of the 511 keV photons of a PET)





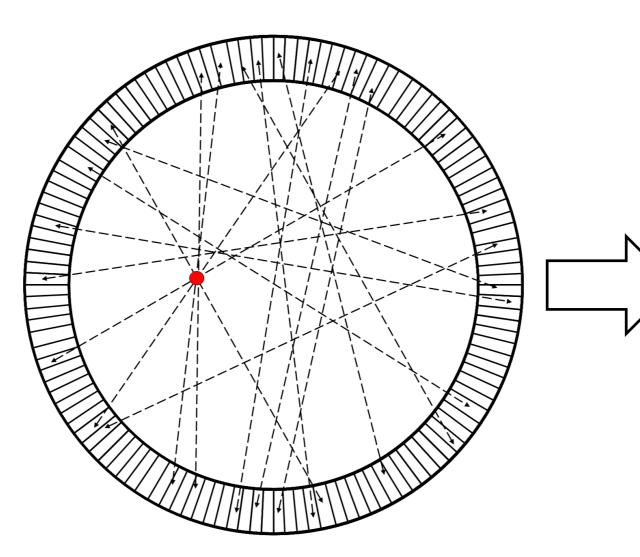
Time-Of-Flight PET

Improved background rejection by measurement of difference in arrival time of the two photons.

Goal:

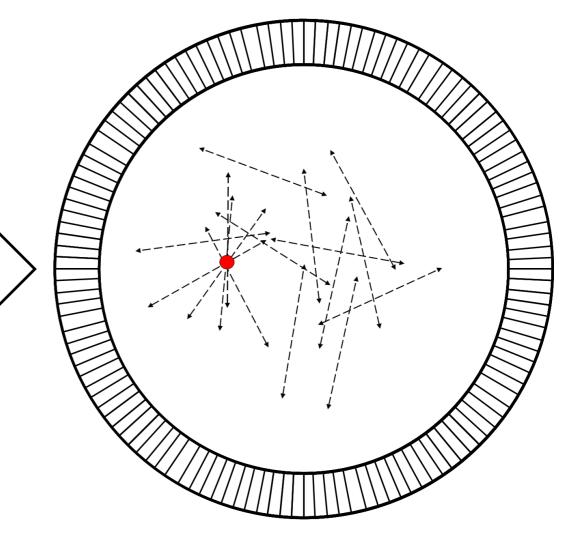
30 ps time resolution for 1 cm spatial measurement











The TT-PET team funded by



DPNC Geneva:



Giuseppe lacobucci

- P.I.
- Scanner design



Lorenzo Paolozzi

- Sensor design
- Analogue electronics design

HUG Geneva:



Osman Ratib

Scanner operation



Emanuele Ripiccini

- Scanner simulation
- Image reconstruction



Pierpaolo Valerio

- Electronics design
- Chip design

Collaboration with:

and their research teams



Roberto Cardarelli (INFN Roma Tor Vergata)

Holger Ruecker (IHP Microelectronics)

Marzio Nessi (CERN & UNIGE)

Daiki Hayakawa

- Sensor simulation
- Image reconstruction



Frank Cadoux

Stéphane Debieux

Yannick Favre

Readout system

Mathieu Benoit

• Sensor and guard ring simulation

Didier Ferrere

Scanner assembly support



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SWISS NATIONAL SCIENCE FOUNDATION





LHEP Bern:



Michele Weber

• Scanner assembly



A. Miucci/D. Forshaw

- Readout system
- Scanner assembly

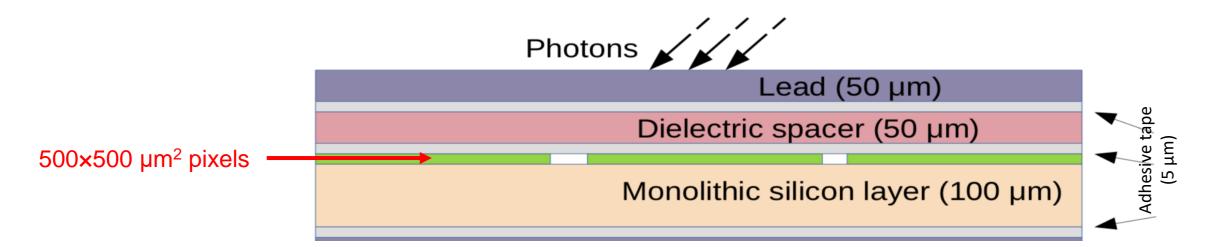


Yves Bandi

Readout system

- Mechanics design and assembly, thermal management
- Board design, system-level electronics

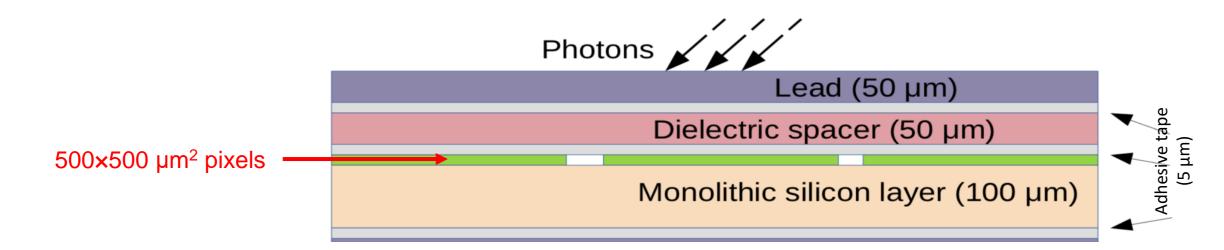
TT-PET: Basic detection unit

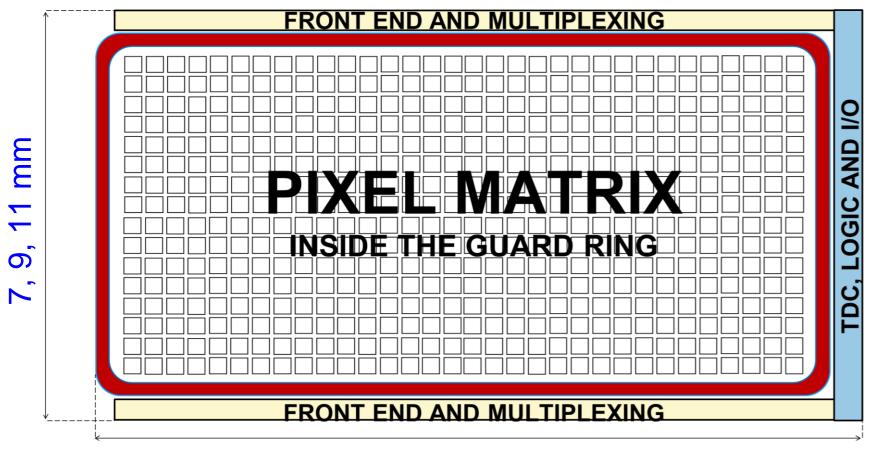






TT-PET: Basic detection unit





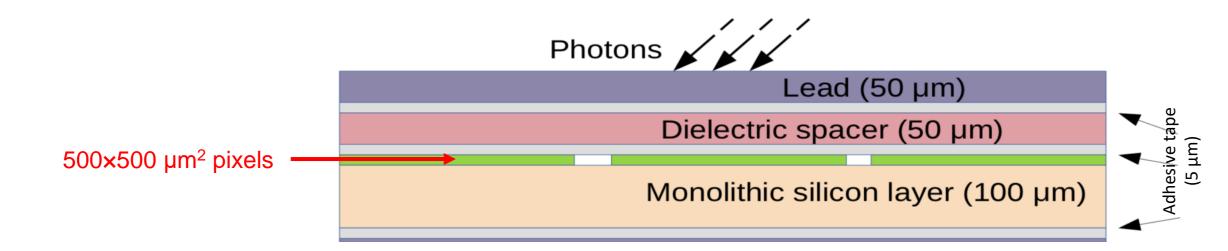
24 mm

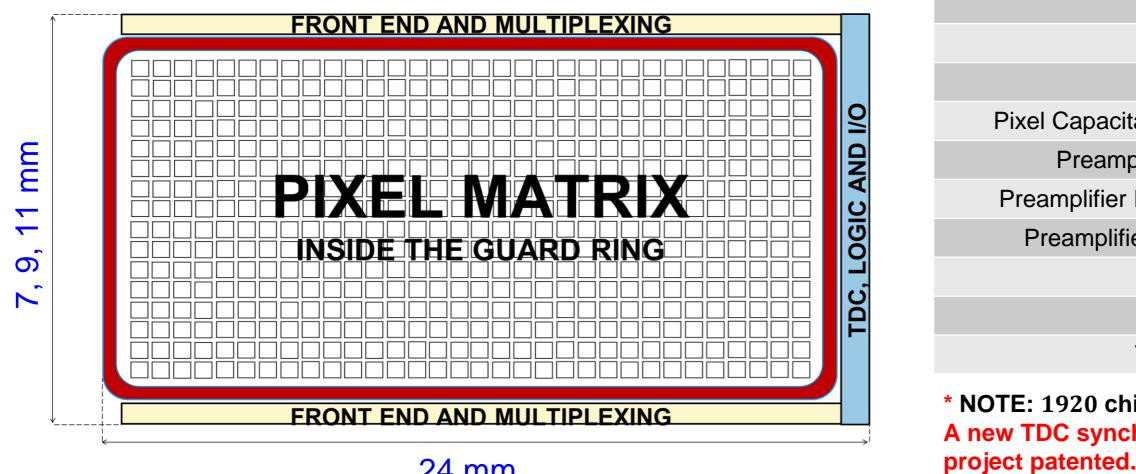


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TT-PET: Basic detection unit





24 mm



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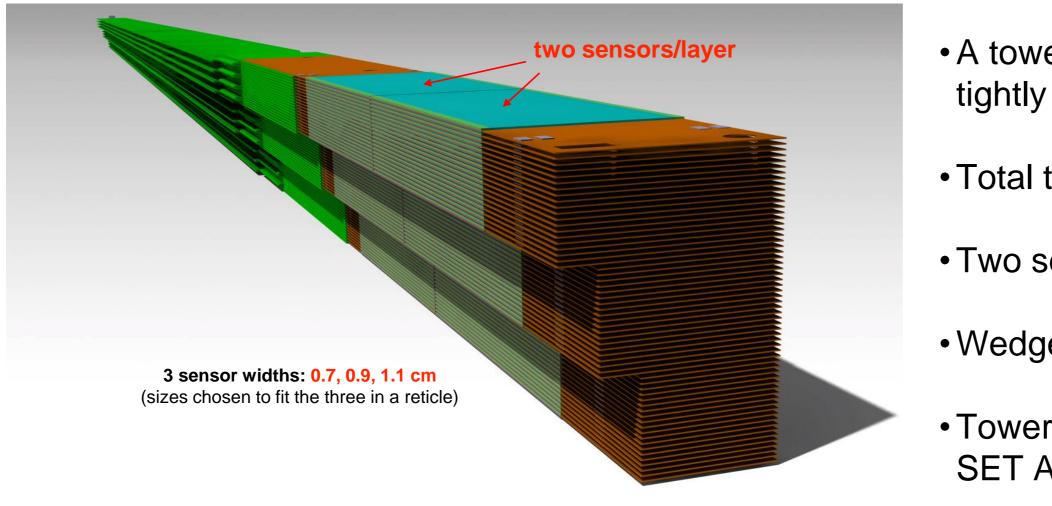


| ASIC length | 24 mm | | | | |
|----------------------------|---------------------------|--|--|--|--|
| ASIC width | 7, 9, 11 mm | | | | |
| Pixel Size | $500 	imes 500 \ \mu m^2$ | | | | |
| itance (comprised routing) | 750 <i>fF</i> | | | | |
| plifier power consumption | $80 \ mW/cm^2$ | | | | |
| r Equivalent Noise Charge | $600 e^- RMS$ | | | | |
| fier Rise time (10% - 90%) | 800 ps | | | | |
| Time resolution for MIPs | 100 ps RMS | | | | |
| TDC time binning* | 50 ps | | | | |
| TDC power consumption | < 1 mW/ch | | | | |
| | | | | | |

* NOTE: 1920 chips synchronized at O(10) ps precision. A new TDC synchronization technique developed for this



TT-PET: Scanner Tower



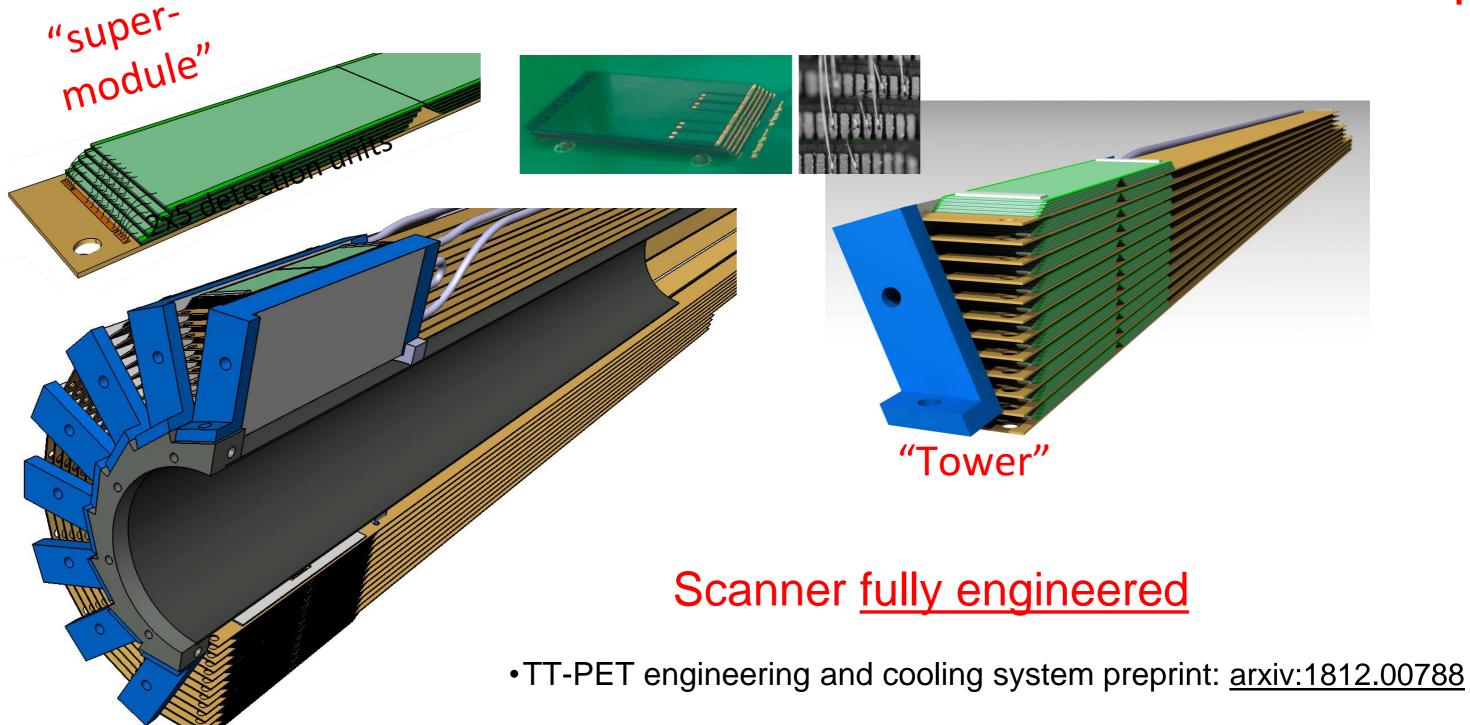
Results of GEANT and FLUKA simulations: Tower efficiency for 511 keV photons: 27% Scanner sensitivity: 4.1%





- A tower is a stack of **60 detection units**, tightly coupled.
- Total tower thickness: 1.5 cm
- Two sensors/layer: 4.8 cm length
- Wedge-shaped: three sensor widths
- Tower assembly will be done with the SET Accµra100 DPNC flip-chip machine.

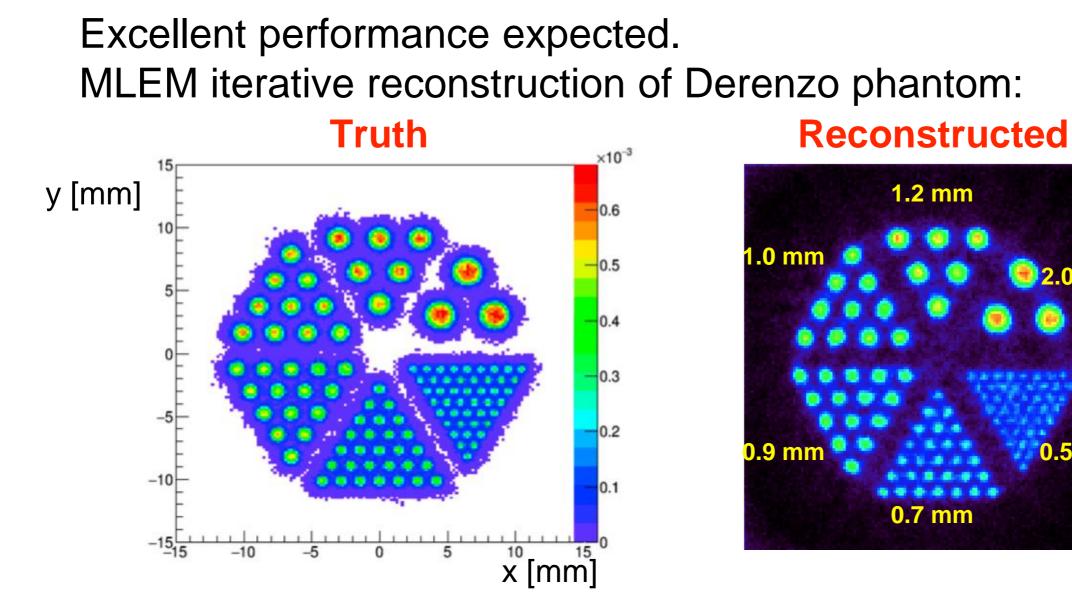
The TT-PET small-animal scanner







The TT-PET small-animal scanner



High FWHM resolutions in entire Field-Of-View:

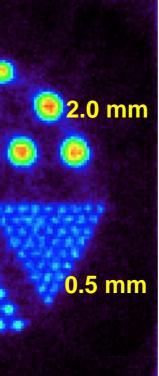
| Z position [mm] | | 0 | | | | 12.5 | | | |
|-----------------|------------|------|------|------|------|------|------|------|------|
| X position [mm] | | 0 | 5 | 10 | 15 | 0 | 5 | 10 | 15 |
| FWHM [mm] | Radial | 0.59 | 0.57 | 0.56 | 0.52 | 0.65 | 0.61 | 0.60 | 0.56 |
| | Tangential | 0.60 | 0.60 | 0.67 | 0.71 | 0.64 | 0.65 | 0.65 | 0.70 |
| | Axial | 0.50 | 0.49 | 0.50 | 0.51 | 0.45 | 0.45 | 0.45 | 0.45 |

TT-PET simulation & performance preprint: https://arxiv.org/abs/1811.12381



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Challenges towards a monolithic ASIC

Time resolution of 30 ps for $E\gamma = 511$ keV: ultra-fast electronics Achieved in discrete SiGe components, but need to implement it in ASIC. Need to identify technology that

allows for it.

Power consumption

Proof-of-concept results were obtained with a power consumption of ≈ 1.4 W/cm². The target for the chip power is 80mW/cm²

Synchronization of a thousand chips at few ps precision Given the low power budget, we needed a new concept for the TDC and synchronisation system

Monolithic integration

Requires to define a strategy for the sensor design to have a simple and effective structure, a detailed simulation and possibly a collaboration with the foundry



Technology choice

Exploit the properties of state-of-the-art SiGe Bi-CMOS transistors to produce an ultra-fast, low-noise, low-power consumption amplifier



• DC Current gain: $\beta = 900$

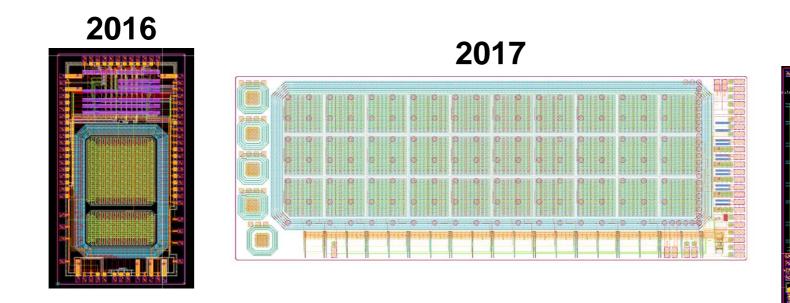


Time digitization:

- 4 ps inverter; delay precision ~100 fs
- > 40GHz oscillation frequency achievable with purely digital schematics

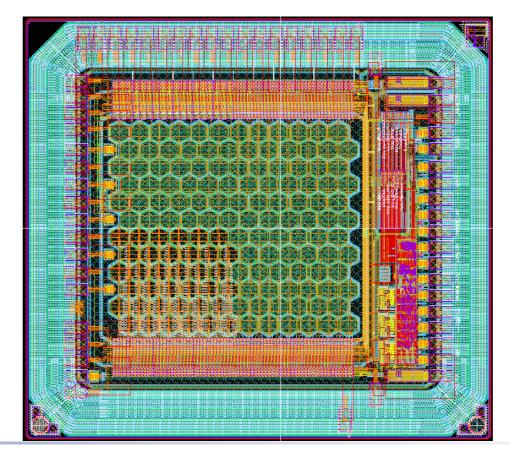
We were able to design a TDCs with a time binning down to 4ps and power consumption of few tens mW/ch with simple architecture



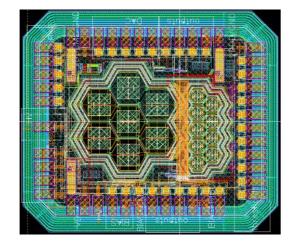


The prototype chips

2019



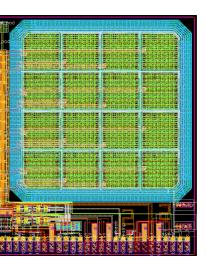
2018





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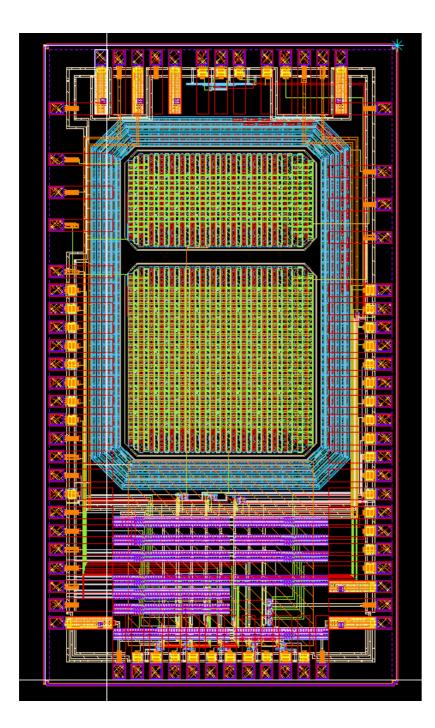
For the TT-PET Project





For generic timing sensor R&D

Analogue ASIC prototype submission

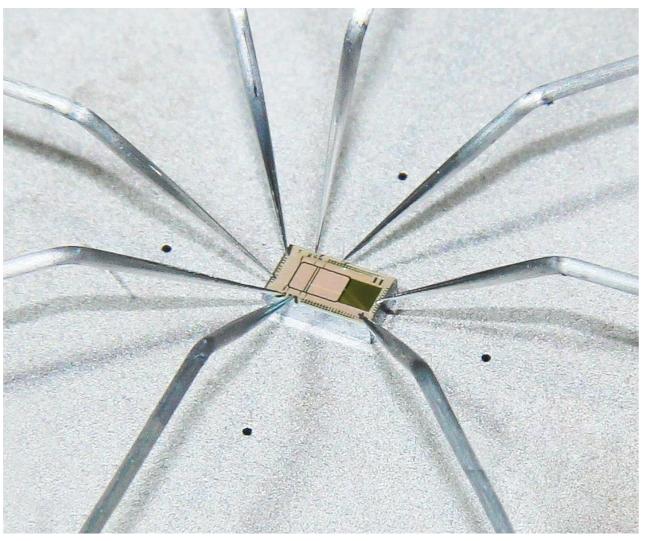


- Monolithic sensor with two n-on-p pads: $900 \times 900 \ \mu m^2$ and $900 \times 450 \ \mu m^2$, spaced by $100 \ \mu m$.
- Inside a guard ring.
- SiGe HBT amplifier and MOSFET discriminator with TOT capability, placed outside the guard ring





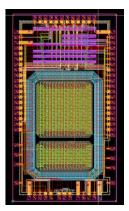
Operation of the ASIC



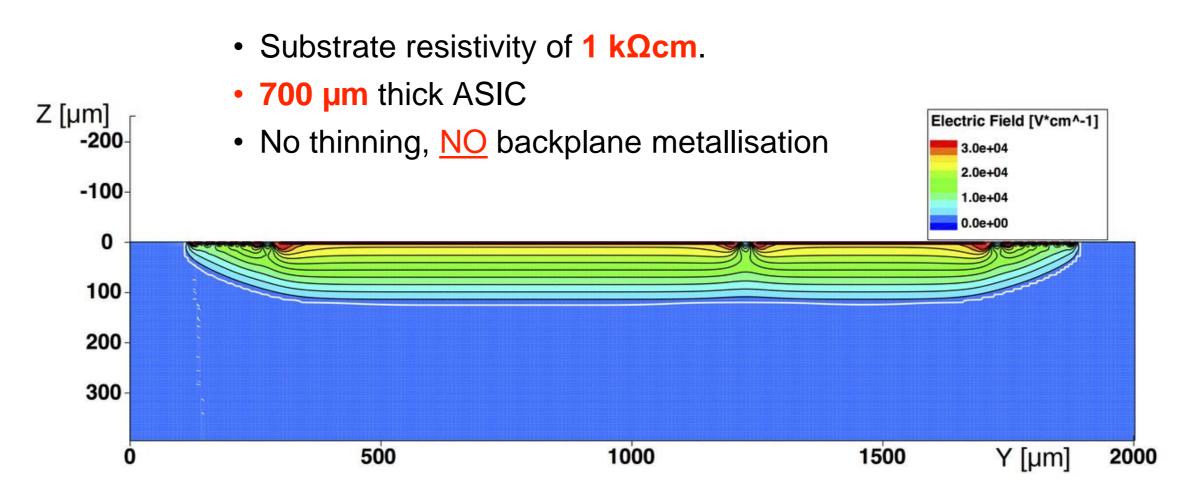
Prototype ASIC under test in the DPNC probe station

- Estimated pixel capacitance:
 0.8 pF for the small pixel
 1.2 pF for the large pixel
- ENC (CADENCE estimation): 600 e- RMS (small pixel) 750 e- RMS (large pixel)
- +ve bias voltage applied to pixels using poly-silicon biasing resistors
- Breakdown voltage: 165 V
- Power consumption ≈ 350 µW/ch





TCAD simulation of the ASIC

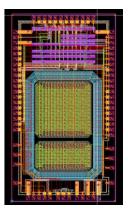


Depletion depth \approx 130 µm.

Due to the **absence of thinning and backplane metallisation**:

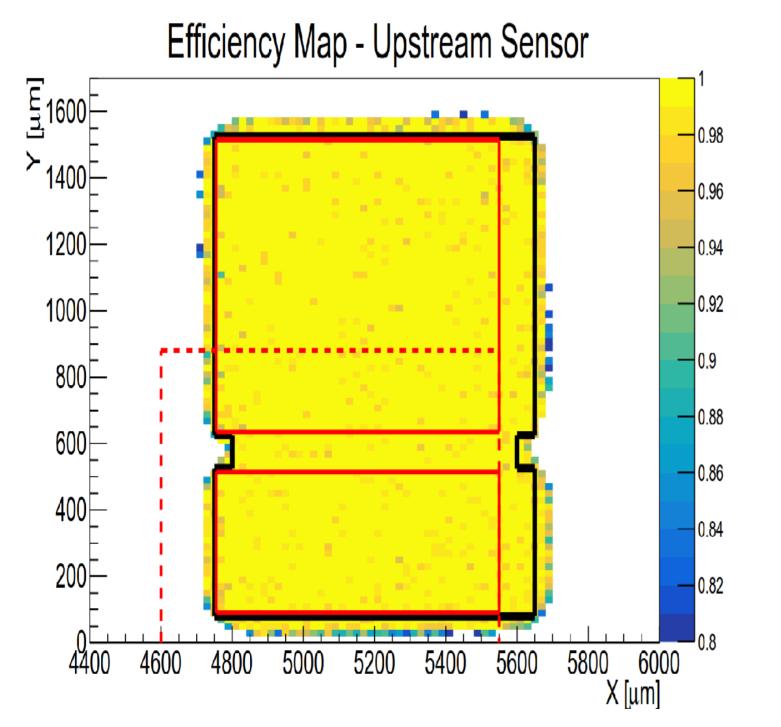
- electric field non-uniform in depth and well below 2-3 V/µm
- the drift velocity of the charge carriers was NOT saturated
- ⇒ sensor NON optimal for time resolution





allisation: w 2-3 V/µm saturated

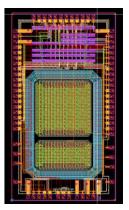
Testbeam results: efficiency



Published in JINST 13 (2018) P04015: <u>https://doi.org/10.1088/1748-0221/13/04/P04015</u>



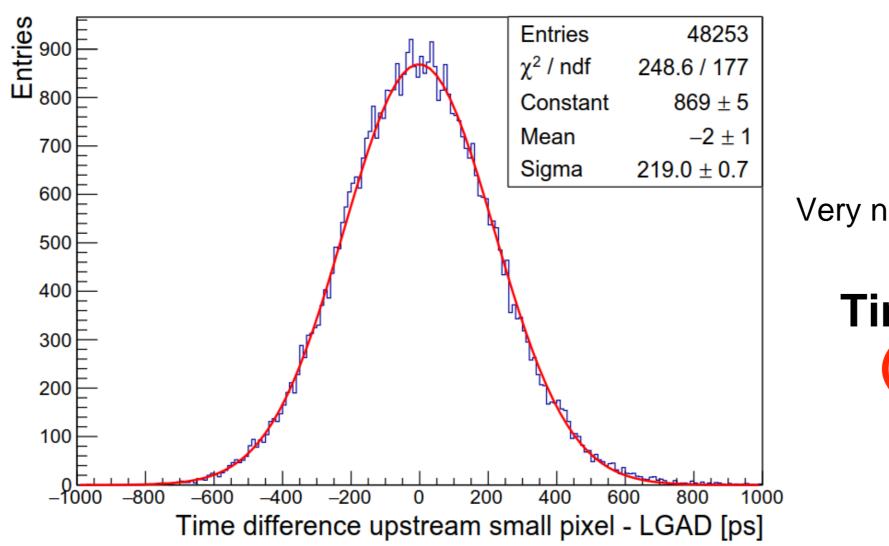
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Efficiency = 99.8 %

even in the inter-pixel region

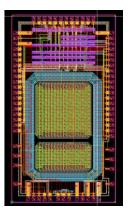
Testbeam results: time resolution



Published in JINST 13 (2018) P04015: <u>https://doi.org/10.1088/1748-0221/13/04/P04015</u>



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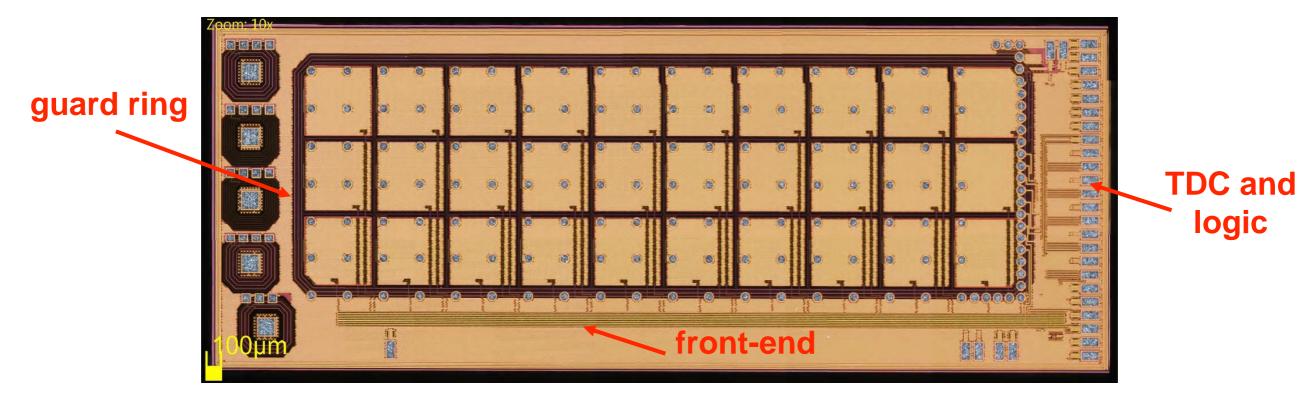


Very nice Gaussian distribution

Time resolution: (220 ± 1) ps

The TT-PET "demonstrator" chip

Matrix of 3×10 n-on-p pixels, of $470 \times 470 \ \mu m^2$ (C_{tot} = 750 fF) spaced by 30 μm .



- SiGe HBT preamplifier
- CMOS-based open-loop tri-stage discriminator (adjustable threshold with) an 8-bit DAC), that preserves the **TOA** and the **TOT** of the pixel
- Discriminator output sent to fast-OR chain
- **50ps binning TDC**, R/O logic, serializer





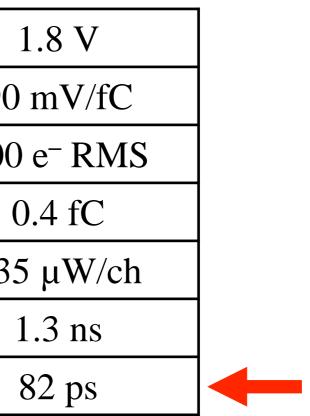
The frontend

Main specifications of the simulated front-end for $C_{TOT} = 500 \text{ fF}$

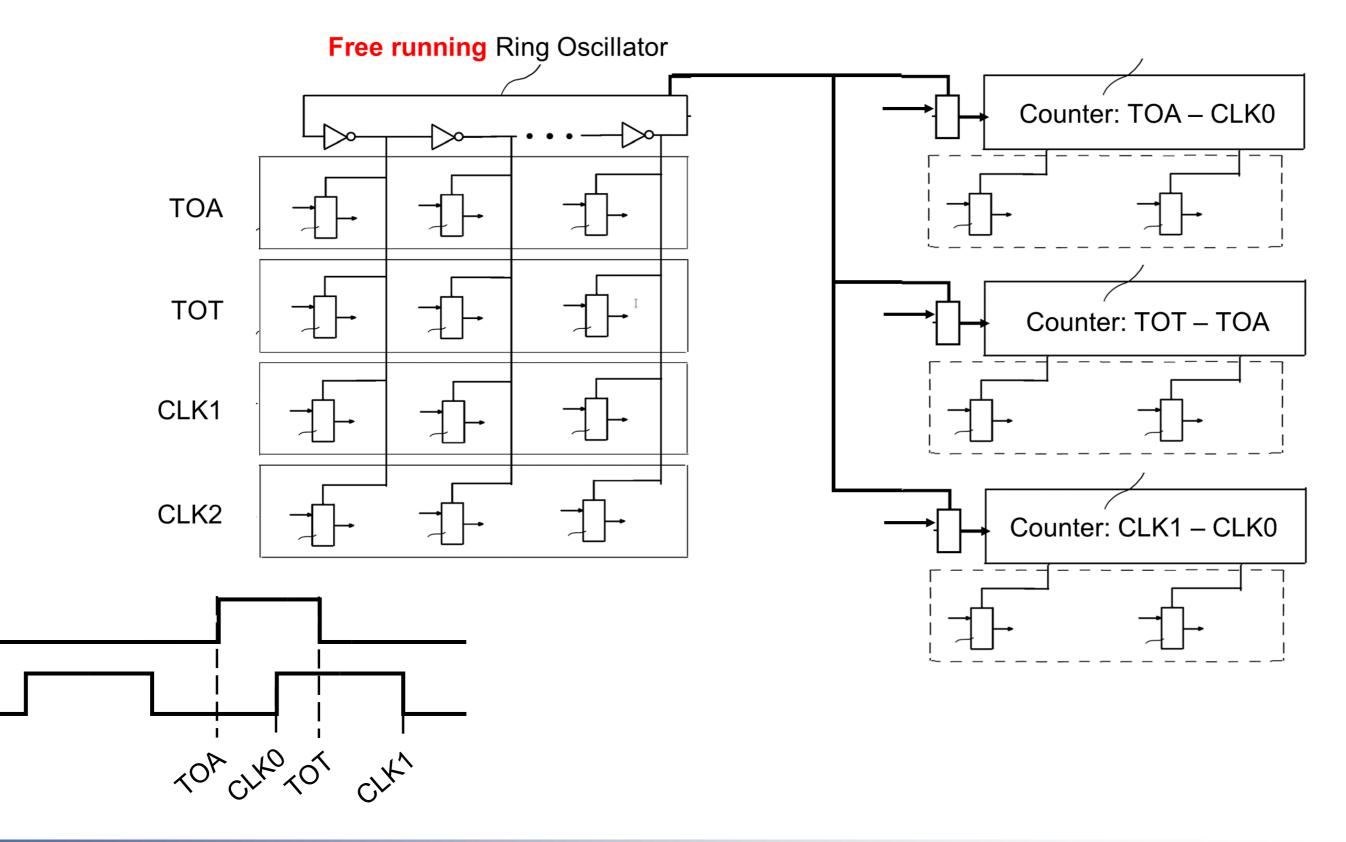
| Power supply | |
|--|-----|
| Gain | 90 |
| ENC | 300 |
| Minimum threshold | (|
| Power consumption | 135 |
| Peaking time | |
| Simulated ToA jitter (for 1 fC signal) | |



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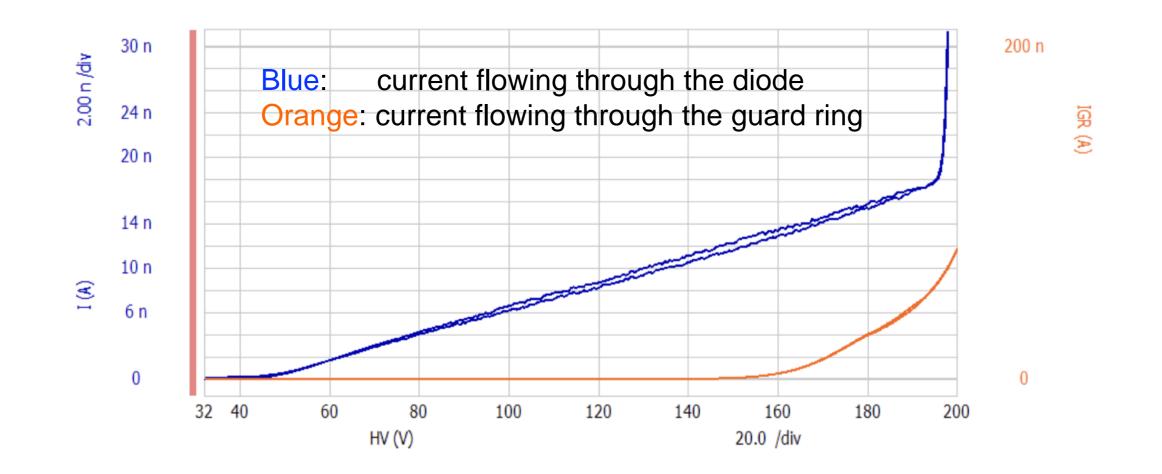
The TDC





| | Г | | Ľ | 2 | Ľ | Ľ | 2 | Ľ | - | Ľ | | Ľ | | Ľ | | Ľ | | Ľ | 1 |
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| ۳, | | • | 10 | | 1 | 1 | | r i | | P | | 1 | | 8 | 8 | 1 | | 1 | -86 |
| | ŀ. | * | * | * | * | • | | e. | * | ٩ | - | ø. | - | 8 | * | | * | a. | F |
| | F | | 0 | 0 | | | N. N | ŀ | | ŀ | | | | ċ | * | a a | | | |
| REAL | | | | | | | | | | | | | | | | | | 0.01 | 1000 |
| 181 | | | | | 1 | - | | 1 | | | - | | | | | | - | | - |

Sensor I-V curve



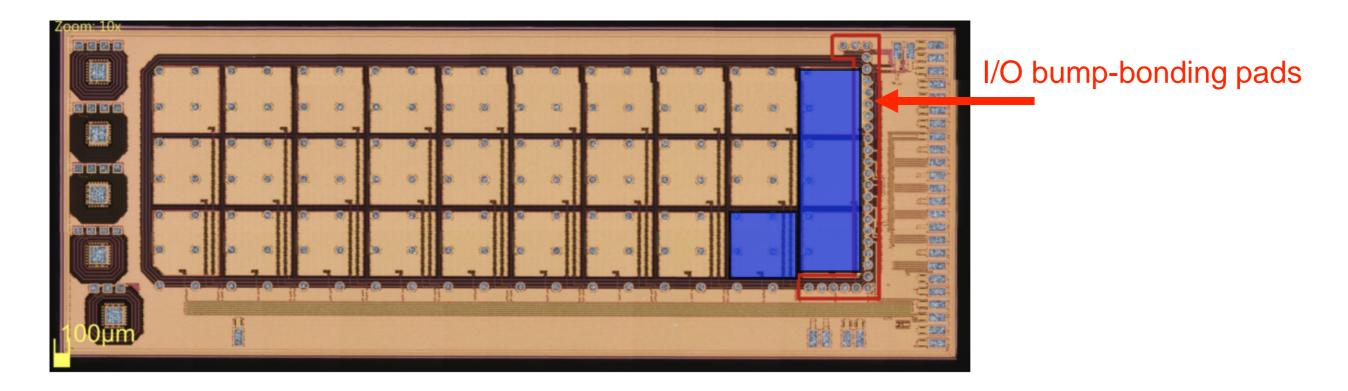
Breakdown at ≈ 200 V

Resistive behaviour produced by non-ideal ground contact through the backplane



| | Г | | Г | | Г | | r | | Ľ. | | ľ. | | £. | | r | | £. | | r. | 1 |
|-----|---|----|----|-----|-----|-----|---|----|----|-----|----|----|----|----|----|----|----|----|------|---|
| | r | ۰. | r. | °., | r. | ÷., | r | ۰. | Ľ | ÷., | Ľ. | ۰. | Ľ. | * | r. | * | 1 | ۰. | P | |
| | | | 10 | | P | | P | * | r | | P | 1 | 6 | 8 | 8 | -8 | 10 | | | |
| | • | * | * | * | × | | | | а. | * | • | * | 8 | 10 | | | e. | * | a. | |
| | F | 8 | | | | | | 8 | | | ŀ | | , | | 0 | 2 | × | | , | |
| - | | - | | 1 | | | | - | | - " | | γď | | - | | | | - | 0.00 | |
| 181 | | | | | 110 | | - | | | | | - | | | | - | | - | - | - |

TT-PET "demonstrator" chip



The four pixels (in blue) closer to the I/O pads were masked on hardware, due to **noise induced by the single-ended clock line** by the I/O bump-bonding pads (inside the red lines), which were not used but still connected. (These pads will be removed and the clock distributed using differential lines.)

- Front-end ENC = 350 e^{-} RMS (on a capacitance of \approx 750 fF).
- Therefore the nominal threshold was set to to $1750 e^{-1}$ (5 σ above noise).
- Noise hit rate per chip of 4.3×10^{-3} Hz measured at the nominal threshold.

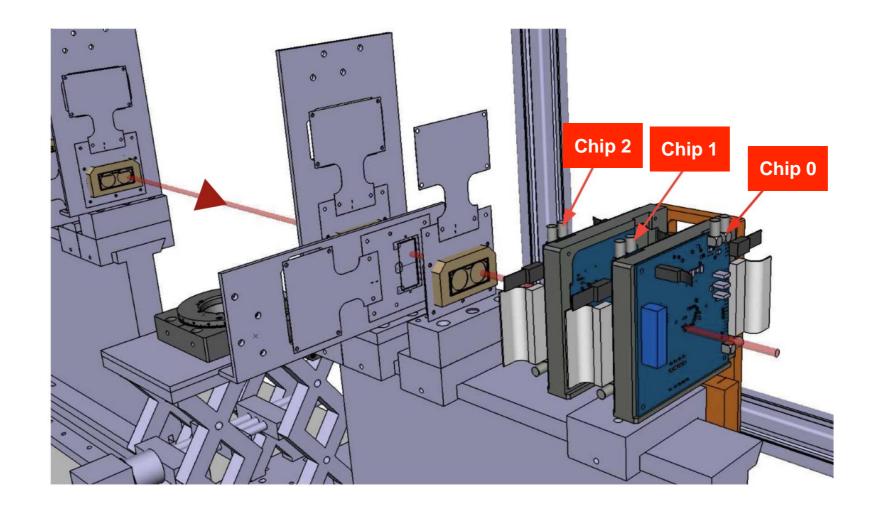
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| | I. | | Ľ | | E | | | - | 0 | | Ľ | - | E | | £. | | £ | | 1 | 1 |
|------|----|-----|---|---|----|----|----|-----|----|---|----|---|----|---|----|----|----|---|-------|-------|
| | | - | | | 1 | - | | - 1 | | - | | - | | _ | | _ | L | _ | | _ |
| | | | Ľ | | | | Ľ | | Ľ | | Ľ | | | | Ľ | | Г | | Ľ | |
| | Ľ | - | Ľ | | Ľ | | Ľ | | Ľ | | Ľ | | Ľ | - | Ľ | - | Ľ | * | 1 | |
| | | | ľ | 1 | | 1 | ľ | | 1 | | r | 1 | ľ | | 1 | 1 | ľ | | | |
| | Ľ | . 1 | • | | | ." | ۴. | .1 | ۰. | | Ľ | | ۰. | | 0 | .* | ×. | | ۰. | |
| RES. | | | 1 | 1 | H. | 1 | | 1 | d. | | R. | 1 | 1 | 1 | 1 | 18 | | 1 | 19.01 | mag . |

Testbeam experiment with MIPs



Three chips were installed downstream our beam telescope.

Chips operated at two preamplifier power-consumption working points:

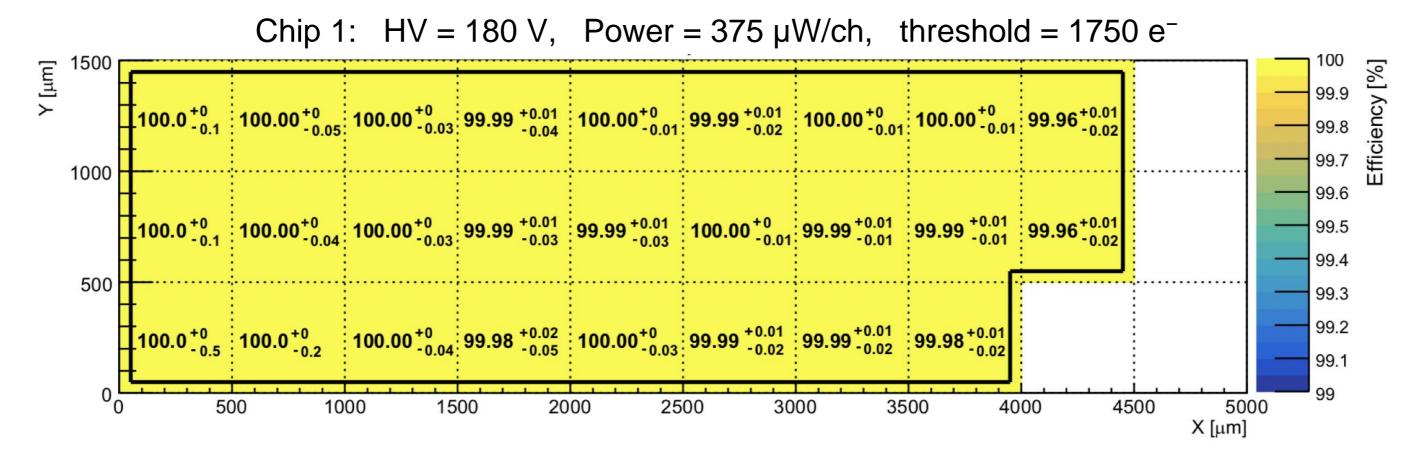
- 160 µW/channel, compliant with the TT-PET power requirements
- 375 μ W/channel, expected to perform better in terms of gain and noise (larger I_c \Rightarrow larger transistor f_T \Rightarrow better matching of the pixel capacitance)



| 4 | I. | | L | | E | | | | L | | ľ. | | E | | I. | | 1 | | 1 | |
|------|----|---|---|---|---|----|----|----|---|----|----|----|----|---|----|---|---|---|------|--------|
| | - | | | | | H | | - | ┝ | | | - | | 8 | | 8 | | | | -11 |
| | ŀ | * | * | * | | | ŀ | | ŀ | * | 0 | * | а. | - | 8 | * | | * | 2 | |
| | r | - | 1 | • | • | 1 | r | 1 | t | 1 | ۴ | 1 | r | 1 | r | 1 | • | 1 | | |
| | Ŀ | | 9 | | • | .* | P. | .* | Ŀ | ." | • | .* | e. | | 0 | | × | | ۰. | |
| 18.6 | | | 1 | 1 | 1 | 1 | r. | | | | R. | 1 | | 1 | 1 | 1 | | 1 | 1000 | Made . |

working points: requirements ns of gain and noise pixel capacitance)

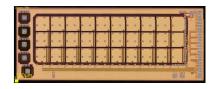
Test beam results: efficiency



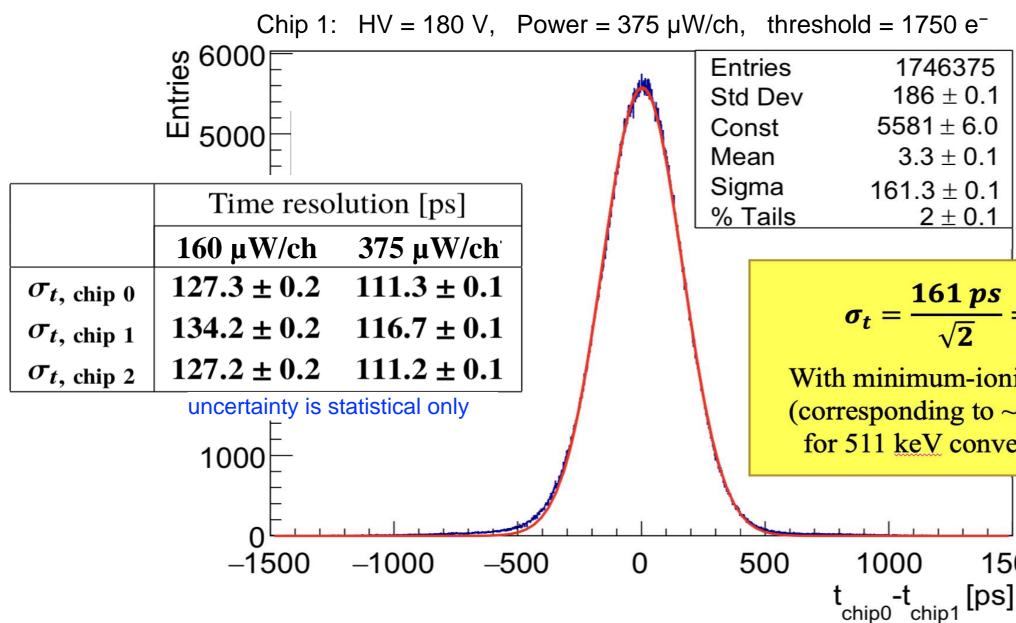
Full efficiency, even in the inter-pixel region.

L. Paolozzi *et al.*, 2019 JINST **14** P02009, <u>https://doi.org/10.1088/1748-0221/14/02/P02009</u> P. Valerio *et al.*, 2019 JINST **14** P07013, <u>https://doi.org/10.1088/1748-0221/14/07/P07013</u>





Test beam results: time resolution



Excellent result for a silicon pixel detector without internal gain, obtained on a large capacitance (750 fF) and power consumption of 150 mW/cm².

L. Paolozzi et al., 2019 JINST 14 P02009, https://doi.org/10.1088/1748-0221/14/02/P02009 P. Valerio et al., 2019 JINST 14 P07013, https://doi.org/10.1088/1748-0221/14/07/P07013



| | | 10 | | * | L | | | | L | | L | | 1. | | 1 | * | L | | | 1 |
|------|---|----|---|----|---|----|----|----|---|----|----|----|----|---|----|----|----|---|------|-------|
| 8 | - | | | | | - | | - | ┝ | | ÷ | - | | 8 | | | | | | -i - |
| | ŀ | * | 2 | * | | | - | | | * | | * | | - | | | | * | | 1 |
| _ | F | 1 | 1 | - | | - | • | Ť | t | 1 | ۴ | 1 | ŀ | 1 | t- | 1 | r | 1 | | |
| 1 | Ŀ | .* | 0 | | • | ." | ŀ | .* | ŀ | ." | • | .* | • | | 0 | 30 | ×. | | ۰. | |
| REG. | | 1 | 1 | P. | 1 | 1 | r. | 1 | | | R. | 2 | 1 | 1 | 1 | 18 | | 1 | 2.00 | 800 · |

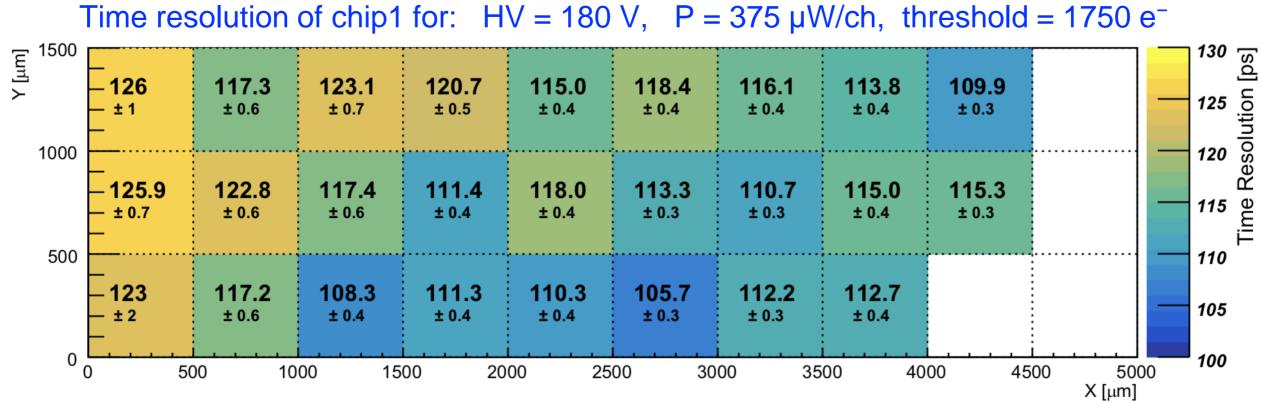
1746375 186 ± 0.1 $\textbf{3.3}\pm\textbf{0.1}$ 2 ± 0.1

 $\sigma_t = \frac{161 \, ps}{\sqrt{2}} = 114 \, ps$

With minimum-ionizing particles (corresponding to $\sim 114/4 \sim 30$ ps for 511 keV converted photons)

1500

CAVEAT 1: Uniformity of response



The map of pixels shows a steady small worsening towards the left. Hypothesis: larger impedance of the ground line for the front-end channels far from the chip ground connection that is done in the right side of the chip ("IR drop" of the supply voltage).

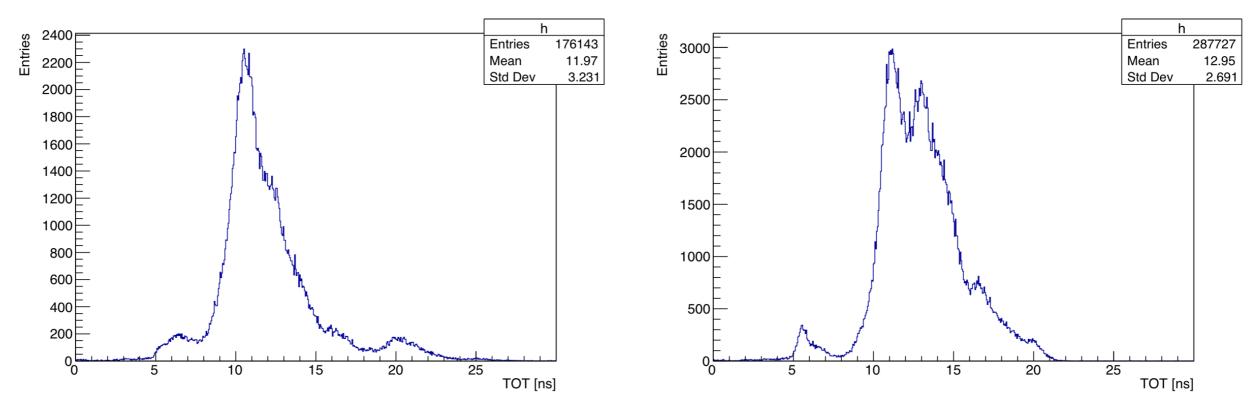
Mitigation measures implemented: improvement of the power-distribution network (larger distribution lines & power pads at the corners of the chip)



| H | r | | r | | ľ | | r | | r | | r | | r | | r | | r | | r | 1 |
|---------|----|-----|----|-----|----|---|----|-----|----|---|---|-----|----|----|---|---|----|-----|----|------|
| STATES. | | 10 | Ľ | × . | Ľ | | r. | × . | Ľ | | Ľ | Ξ. | Ľ | * | 8 | * | ×. | ۰. | P. | |
| | P. | | 10 | | r | | P | | r | | P | | I. | 8 | 8 | | 1 | | 1 | |
| | ŀ | * | ŀ | * | ŀ. | - | 2 | | ŀ | * | 0 | * | 25 | 10 | 8 | * | ۲ | * | 2 | |
| - | Г | 1 | ľ | | Ľ | 1 | ľ | | E | 1 | ľ | | ľ | | ľ | 1 | ° | 1 | ľ | |
| | Ľ, | . 1 | Ľ | . 1 | Ľ | , | Ľ | . 1 | Γ. | . | Ľ | . 1 | Ľ | | Ľ | | Ľ | ,] | Ľ. | - 11 |
| 1 | | 1 | | | | | | | | | | | | | | | | | | |

CAVEAT 2: TOT distribution

It was found that the single-ended digital trigger signal affected the grounding of the pixel matrix and induced a small residual noise. Consequence: the TOT distributions show **peaks**, with time difference between peaks caused by the delay of the fast-OR line.



This modulation of the TOT distribution **degrades** the time-walk correction, and therefore the time resolution

Mitigation measure: introduction of trigger signals in a differential configuration



| | Г | | Ľ | 2 | Ľ | Ľ | 2 | Ľ | - | Ľ | | Ľ | | Ľ | | Ľ | | Ľ | 1 |
|------|----|-----|----|-----|----|-------|-----|-----|---|---|-----|----|-----|----|-----|--------|----|------|------|
| 100 | r. | Ľ., | r | Ľ., | r. | r | ×., | r. | | r | ÷., | r. | ÷., | r. | ×., | r | ۰. | r | |
| ۳, | | • | 10 | | 1 | 1 | | r i | | P | | 1 | | 8 | 8 | 1 | | 1 | -86 |
| | ŀ. | * | * | * | * | • | | e. | * | ٩ | - | ø. | - | 8 | * | | * | a. | F |
| | F | | 0 | 0 | | | 8 | ŀ | | ŀ | | | | ċ | * | a a | | | |
| REAL | | | | | | | | | | | | | | | | | | 0.01 | 1000 |
| 181 | | | | | 1 | - | | 1 | | | - | | | | | | - | | - |

The "hexagonal" prototype sensor

Developed in IHP SG13G2 technology (130nm).

Matrices with hexagons of two sizes:

- \rightarrow hexagon side 130µm and 65µm, with 10µm inter-pixel spacing
- \rightarrow C_{TOT} = 220 and 70 fF

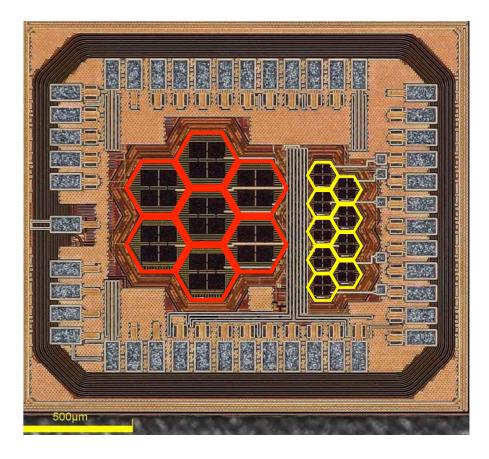
Exploits:

- → New dedicated custom components developed together with foundry
- → New guard-ring structure

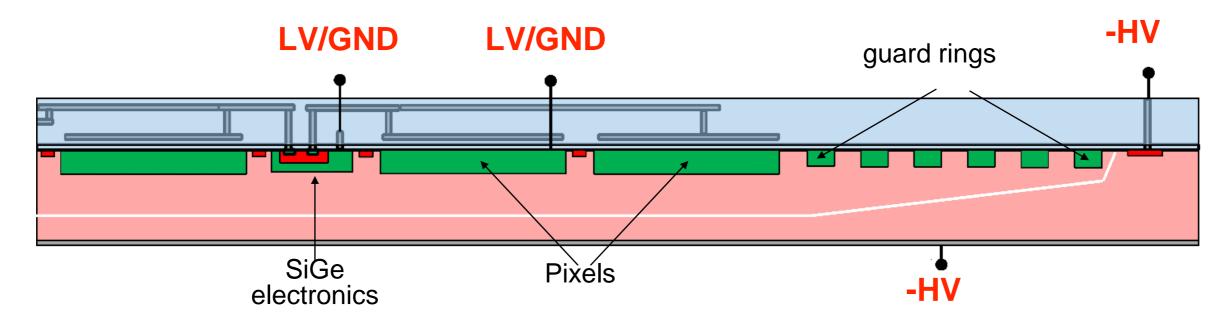








The "hexagonal" prototype sensor

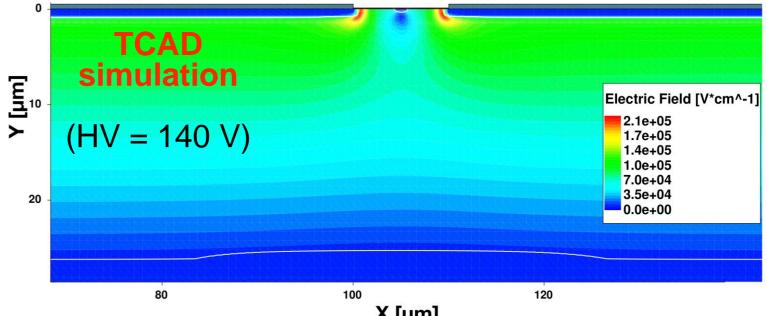


Standard substrate resistivity $\rho = 50 \Omega cm$ <u>No</u> backside metallisation \implies **not fully depleted PRO:** much easier **production**, but

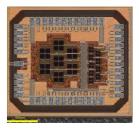
> → slightly degraded performance because of regions where drift velocity is not saturated

Depletion depth is $26\mu m$ at HV = 140 V

- \rightarrow Most probable deposited charge for a MIP \approx 1600 electrons
- \rightarrow CADENCE Spectre simulation for 1600e⁻ (0.25 fC): ideally, ToA jitter = 22 ps

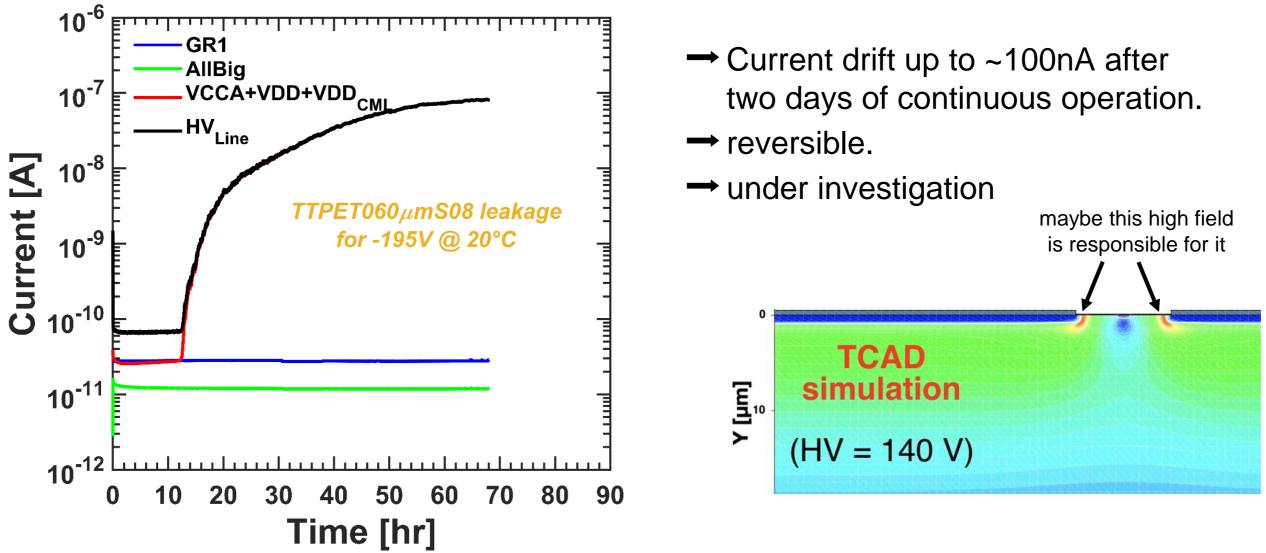






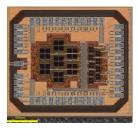
X [µm]

CAVEAT:

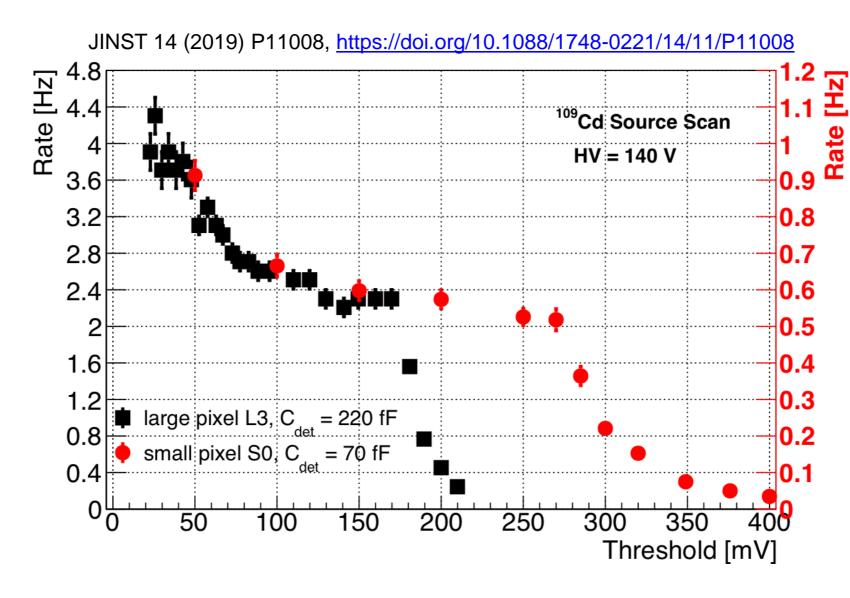


This behavior does not compromise the chip performance. Therefore, we made measurements with a source and at a testbeam





¹⁰⁹Cd radioactive source calibrations



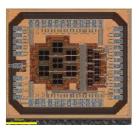
Rate \approx constant for low thresh. values \implies good discrimination of γ peak.

 109 Cd photons (~22 keV) energetic enough for measurement of the gain:

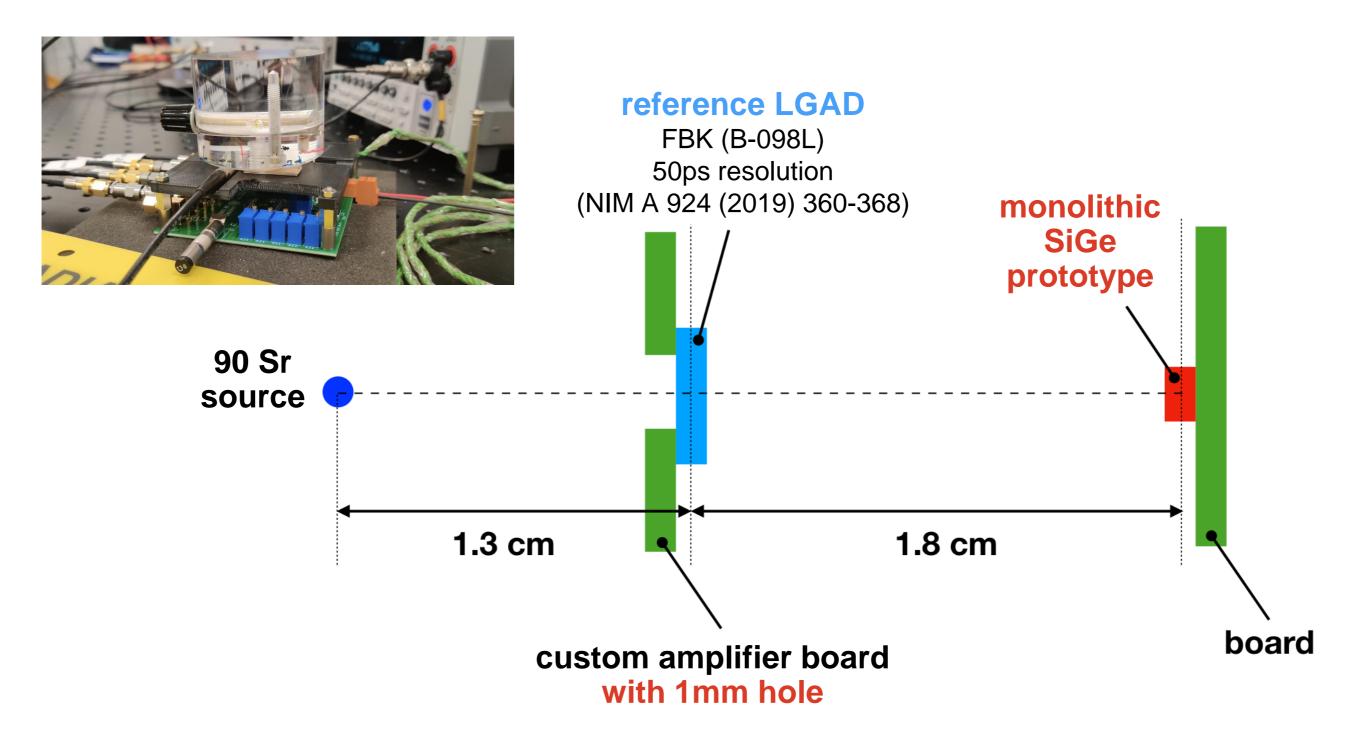
• $A_Q = 290 \text{ mV fC}^{-1}$ for the small pixel $\implies ENC = \sigma_V/A_Q = 90 \text{ electrons}$

• $A_Q = 185 \text{ mV fC}^{-1}$ for the large pixel $\implies ENC = \sigma_V/A_Q = 160 \text{ electrons}$



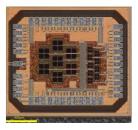


⁹⁰Sr source experimental setup

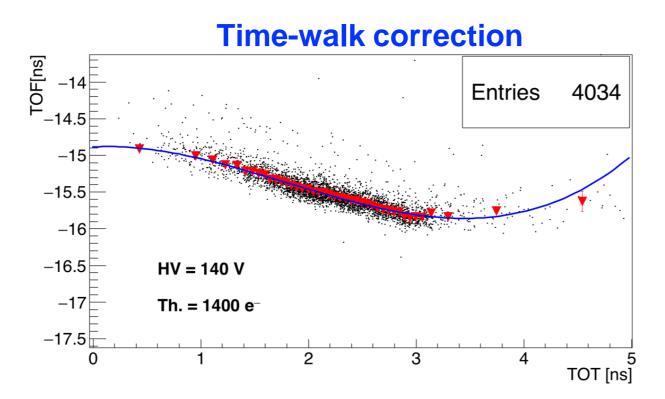


No analysis selection applied to the events in our monolithic SiGe prototype

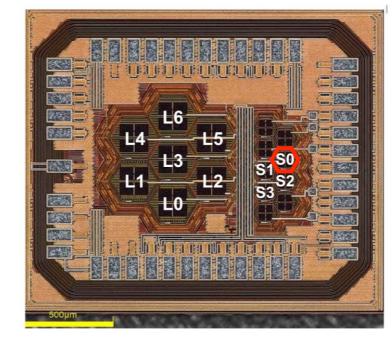




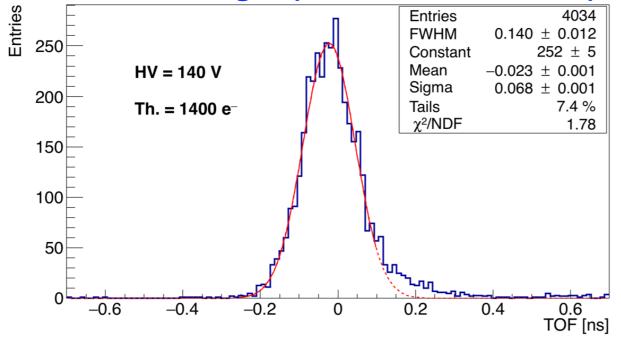
Time-walk correction and TOF



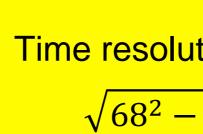
Small pixel S0, C = 70 fF



Time of Flight (time-walk corrected)



non-Gaussian tail ($\approx 10\%$) for TOF ≥ 100 ps, maybe due to e⁻ from the ⁹⁰Sr source crossing the 10µm region between two pixels. Requires to be investigated in a testbeam.





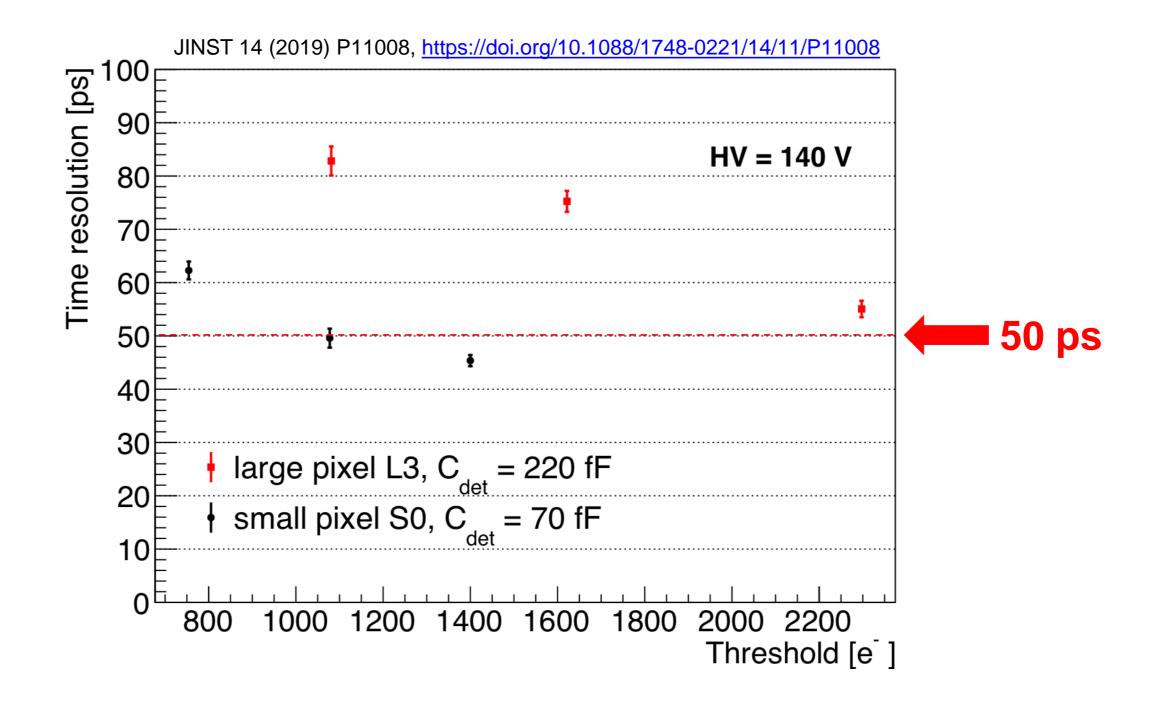
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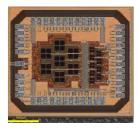
Time resolution of Gaussian part:

 $\sqrt{68^2 - 50^2} \simeq (46 \pm 2)$ ps

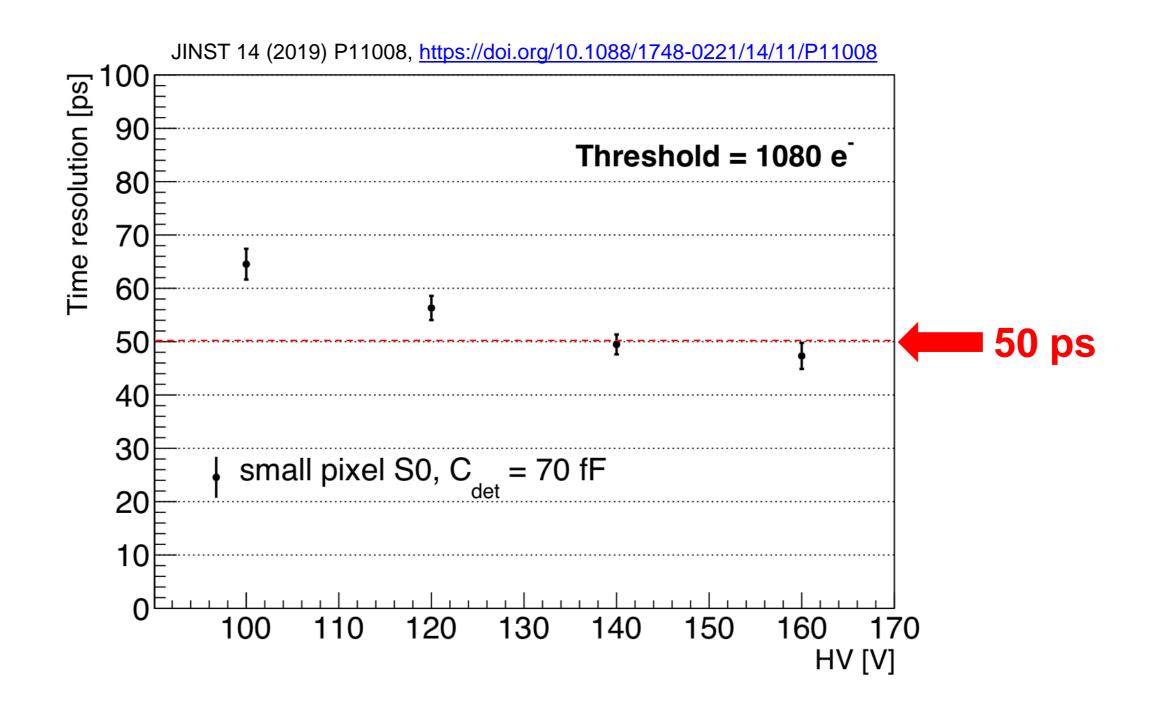
Time resolution vs. threshold



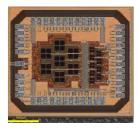




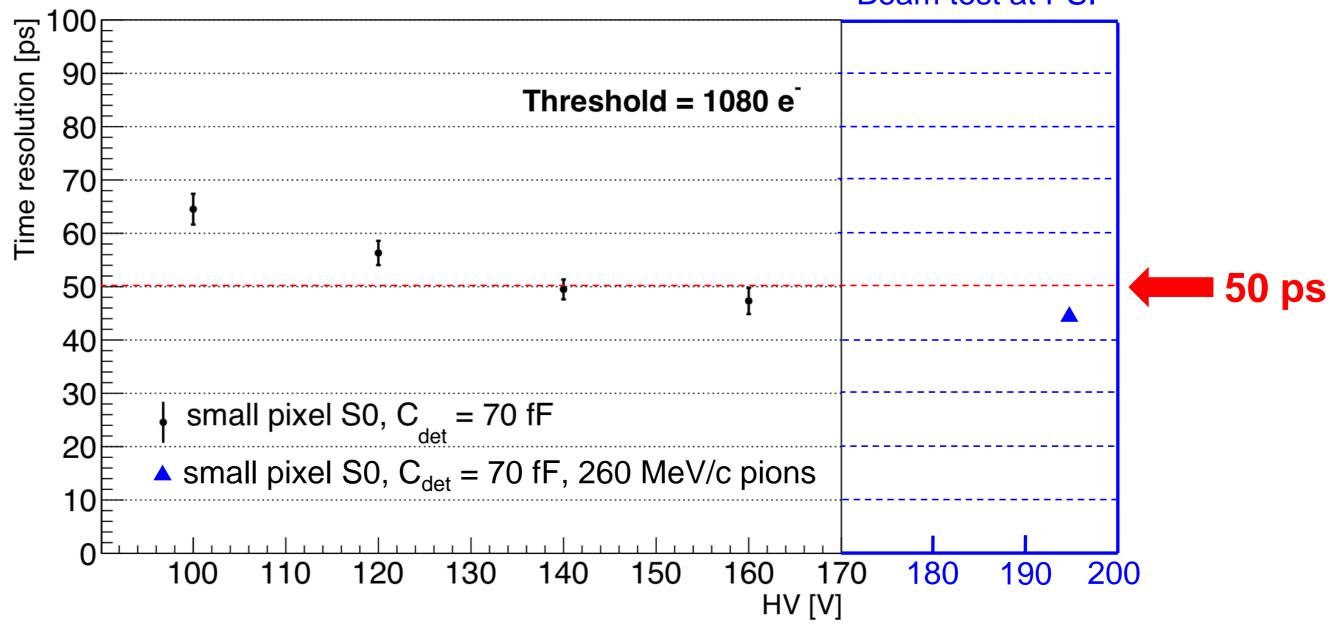
Time resolution vs. HV





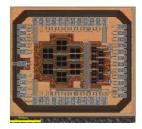


Time resolution vs. HV



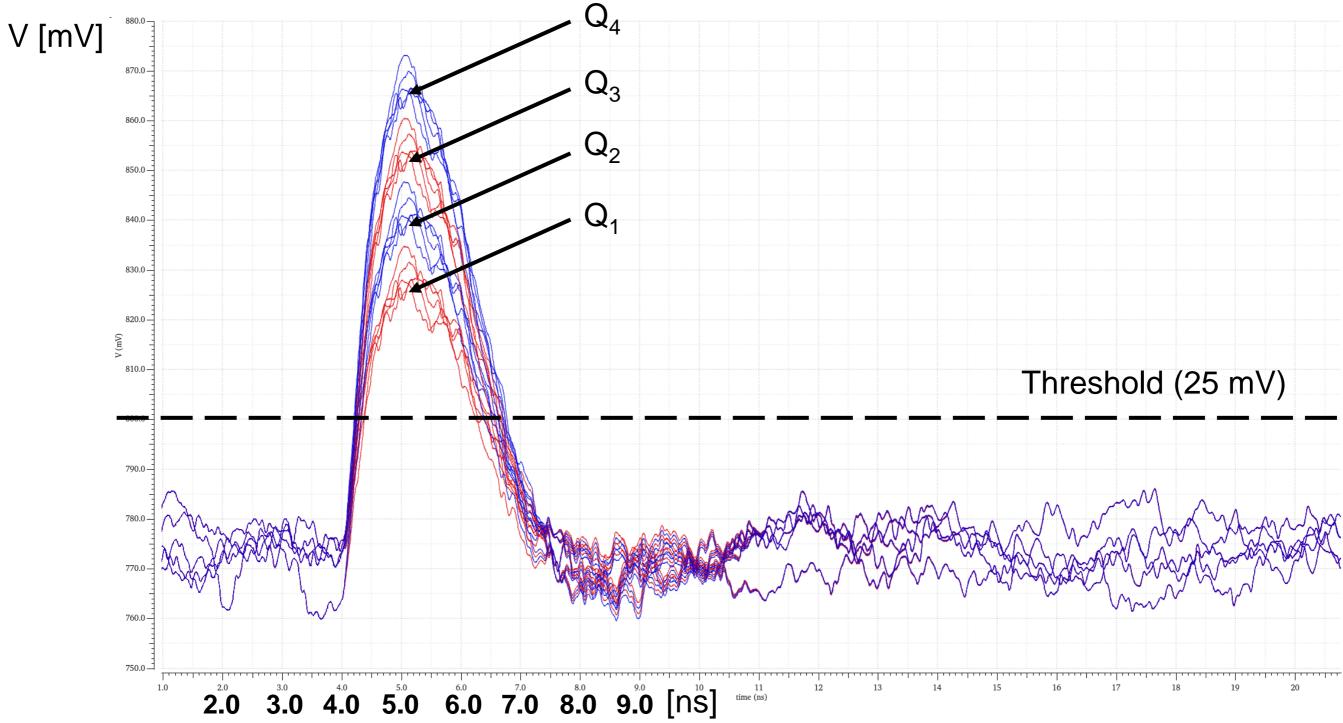


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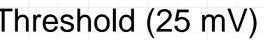


Beam test at PSI

Time walk correction

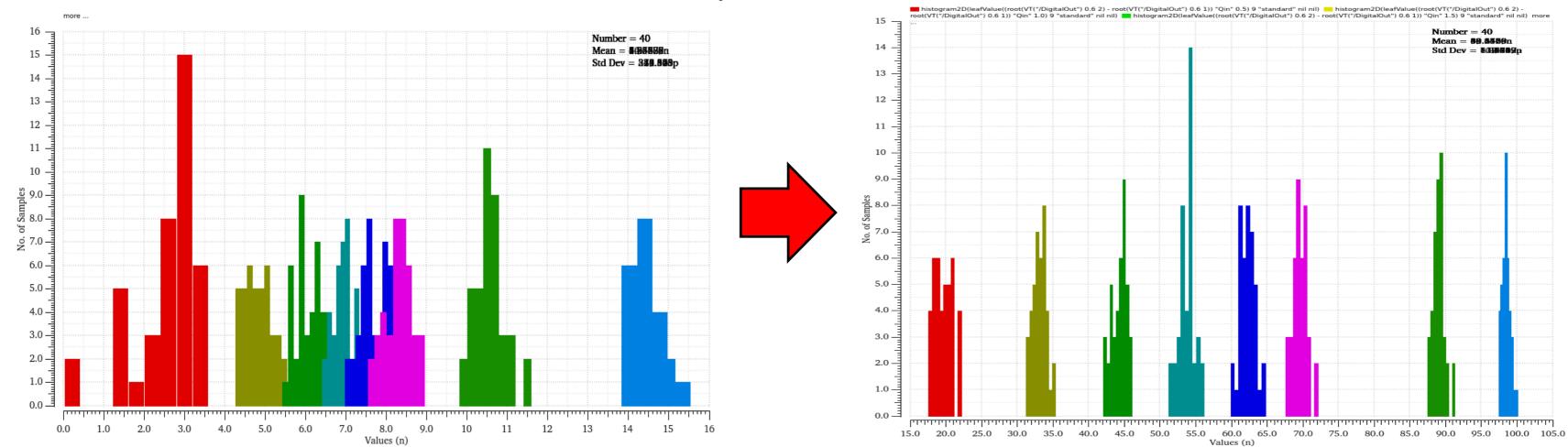






Improved time walk correction **Charge resolution** (Cadence spectre simulation)

Present prototypes

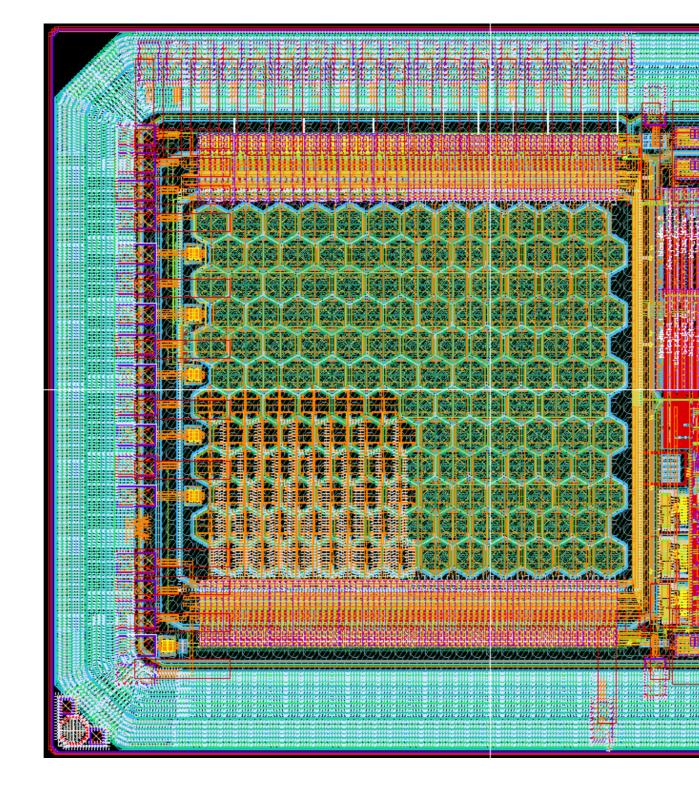




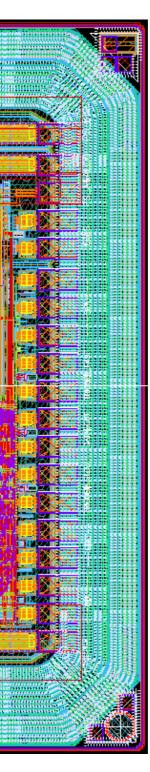
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New technique

Next steps







CONCLUSIONS

- Timing capability of silicon still to be fully exploited.
- SiGe HBT allows for low-noise and fast amplifiers and picosecond readout
- Monolithic ASICs in IHP 130nm SiGe processes without internal gain provided
 - full efficiency
 - **excellent time resolution**: $220 \rightarrow 115 \rightarrow 50 \text{ ps RMS} \rightarrow ???$



Publications and patents

Articles:

- •Hexagonal small-area pixels
- •TT-PET demonstrator chip testbeam:
- •TT-PET demonstrator chip design:
- First TT-PET prototype
- Proof-of-concept amplifier
- •TT-PET engineering:
- •TT-PET simulation & performance:

JINST 14 (2019) P11008, <u>https://doi.org/10.1088/1748-0221/14/11/P11008</u> JINST 14 (2019) P02009, https://doi.org/10.1088/1748-0221/14/02/P02009 JINST 14 (2019) P07013, https://doi.org/10.1088/1748-0221/14/07/P07013 JINST 13 (2017) P02015, https://doi.org/10.1088/1748-0221/13/04/P04015 JINST 11 (2016) P03011, https://doi.org/10.1088/1748-0221/11/03/P03011

arxiv:1812.00788 arxiv:1811.12381

Patents:

- PLL-less TDC & synchronisation System: EU Patent EP18181123.3
- Picosecond Avalanche Detector (pending):

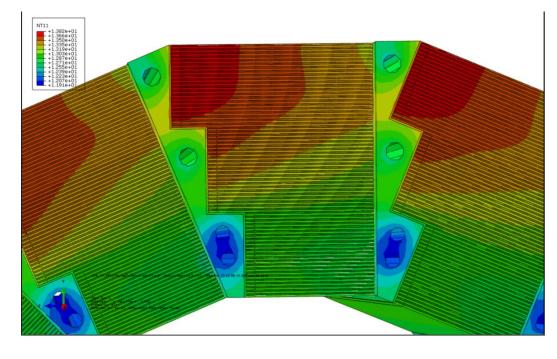
EU Patent Application EP18207008.6

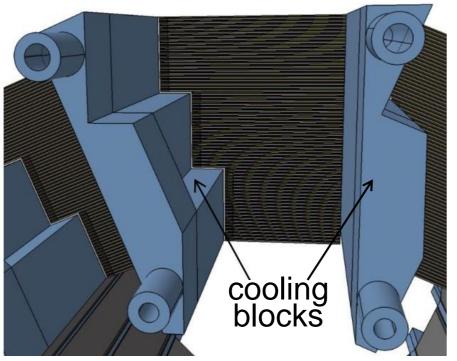


Extra Material



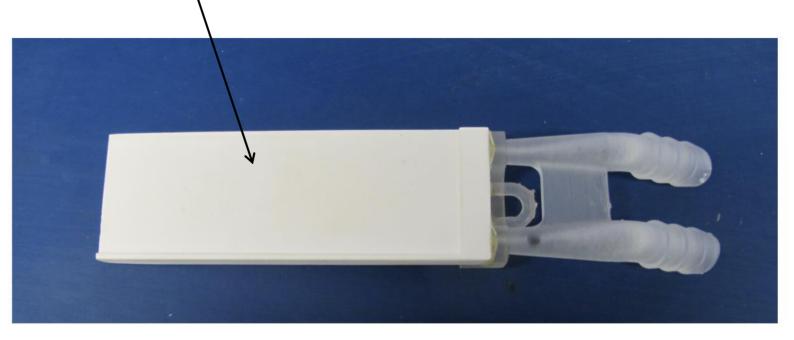
The TT-PET small-animal scanner





Thermal studies:

- High density of silicon pixel sensors
- Sensor power budget < 80mW/cm²
- Finite-Element Analysis performed
- Active cooling: $\Delta T < 1^{\circ}C$ in the sensitive volume
- Cooling block produced and tests made



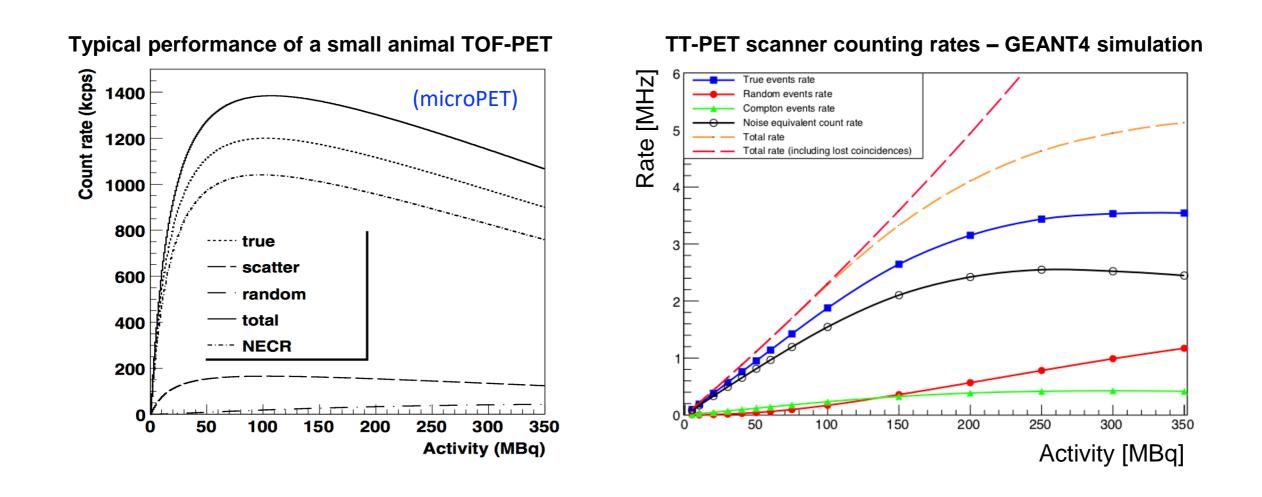


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The TT-PET scanner performance

The high segmentation of the scanner and fast response of the silicon pixel detector allow for a very high counting rate.

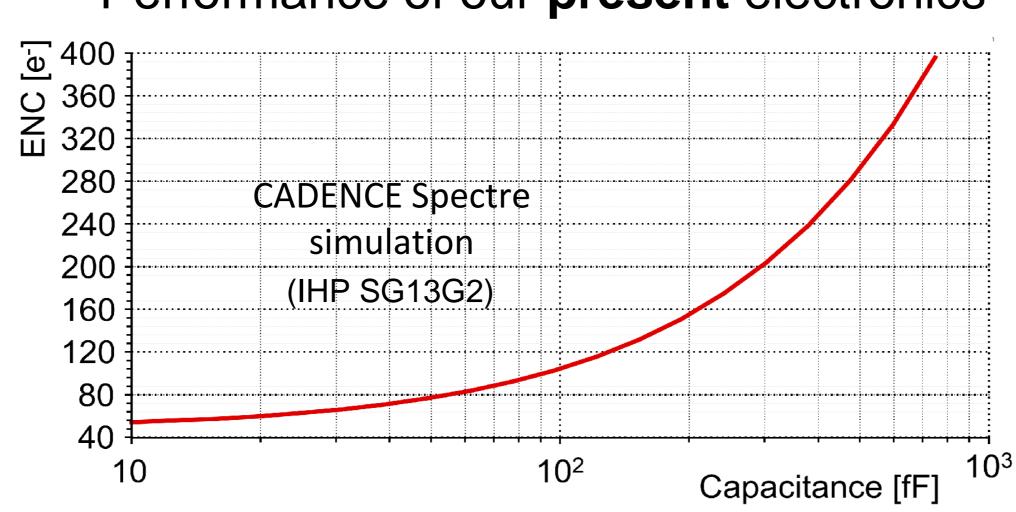






Towards **1** ps time resolution: SiGe electronics

Performance of our **present** electronics

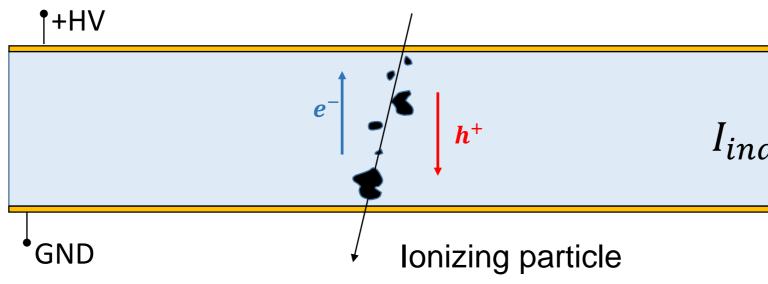


Frontend ENC (CADENCE simulation): 80 e⁻ RMS for C_{in} = 50 fF and Gain = 30 $\implies \sigma_{time} = 4 \text{ ps}$

67 We are working on new version of FE electronics and on a ps TDC

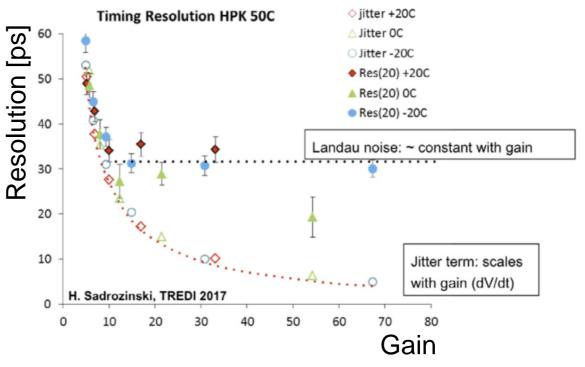


Towards 1 ps time resolution: Landau noise



Landau fluctuations of the

charge deposition constitute an irreducible effect of standard PN-junction sensors



Need for a **novel** silicon sensor to go beyond this



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 $I_{ind} \cong v_{drift} \frac{1}{D} \sum_{i} q_i$

N. Cartiglia et al., NIM A 924 (2019) 350-354



Towards 1 ps time resolution

We designed a new sensor, the

PicoAD: Picosecond Avalanche Detector

Patent pending (EP 18207008.6)



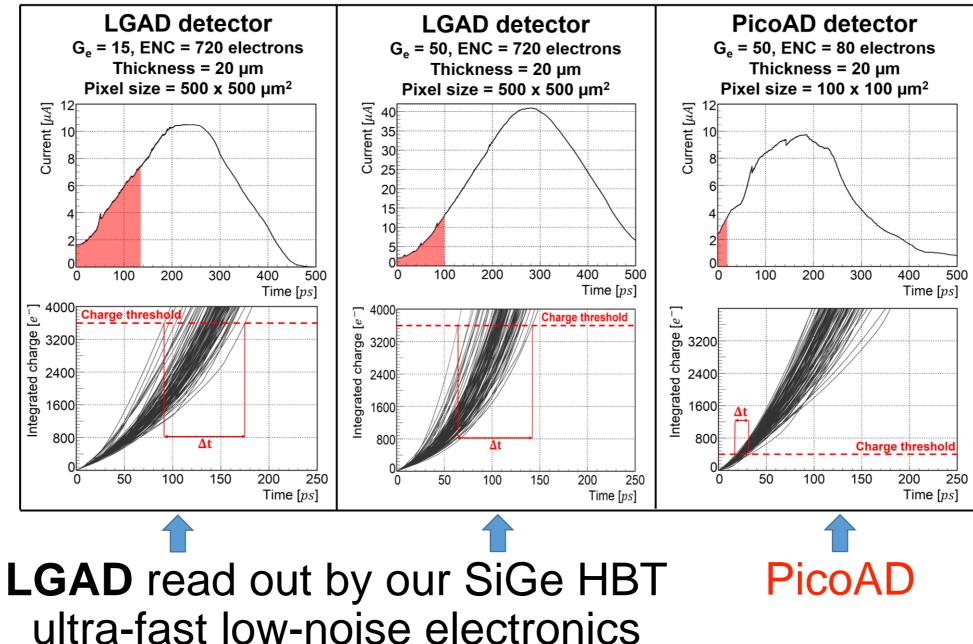
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69

The PicoAD time resolution

One order of magnitude better than present best results

GEANT4 + TCAD + CADENCE Spectre **simulation**

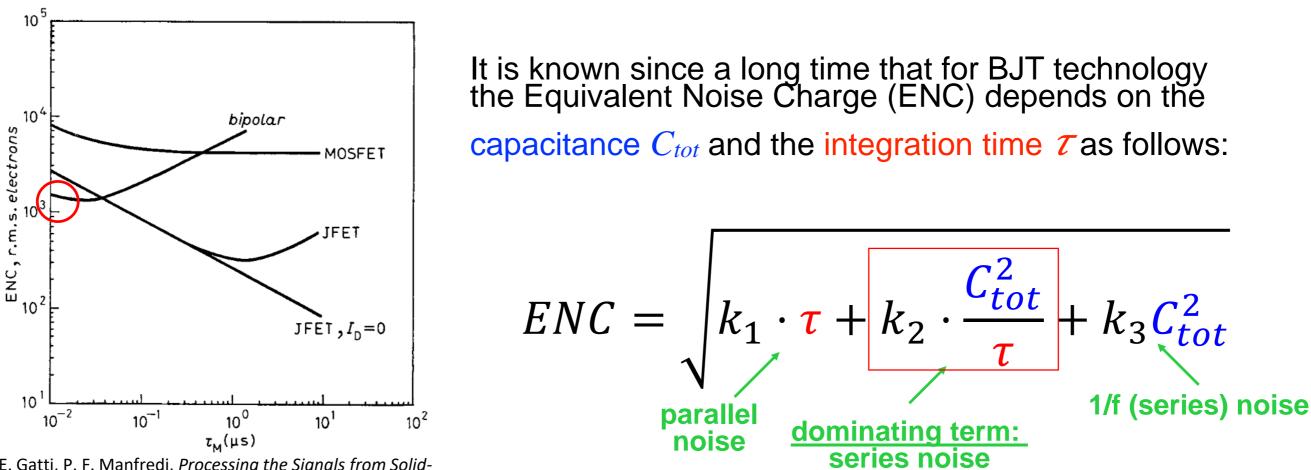


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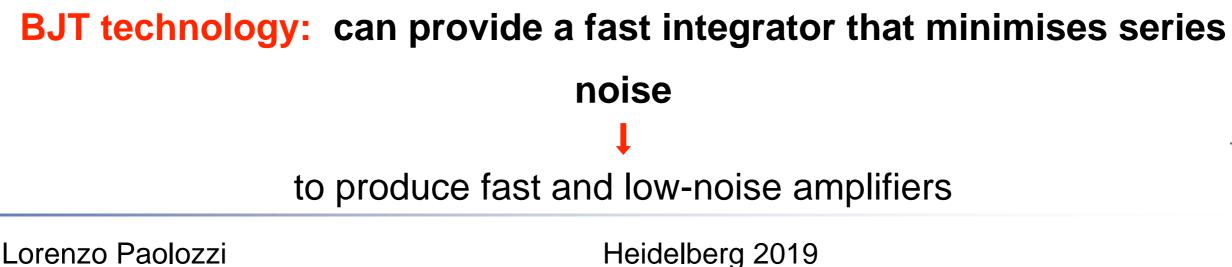
Bipolar transistors for fast low-noise amplifiers



E. Gatti, P. F. Manfredi, Processing the Signals from Solid-State Detectors in Elementary-Particle Physics, rivista del Nuovo Cimento Vol. 9, No. 1 (1986).

UNIVERSITÉ

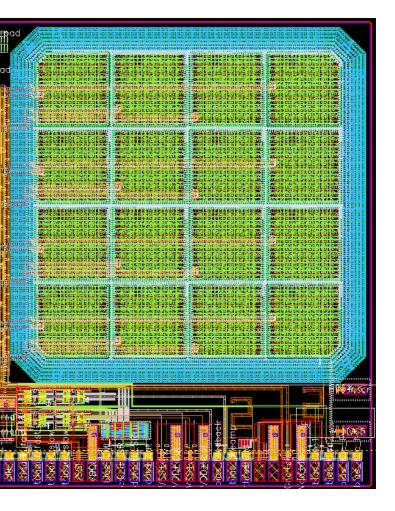
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- These two caveats are fixed in a new chip, that we just received back from IHP.
- The chip contains also front-end test structures:
 - peak-sensing fast ADC
 - higher gain pre-amp
 - new differential driver



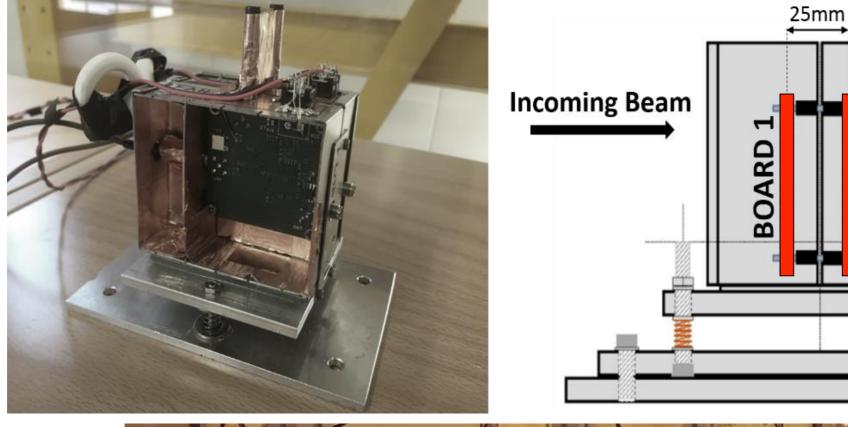
BK

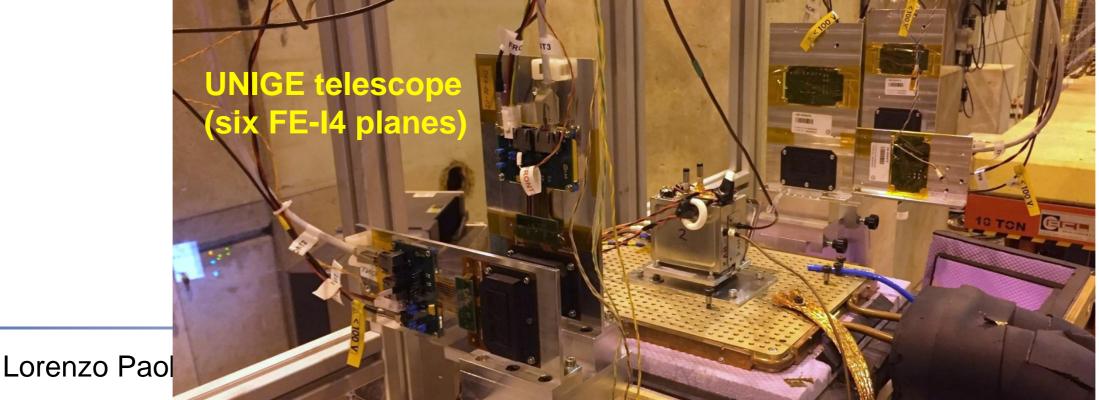


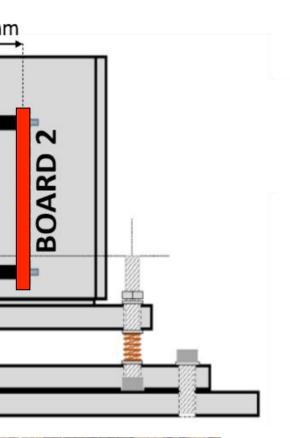
CERN testbeam experimental setup

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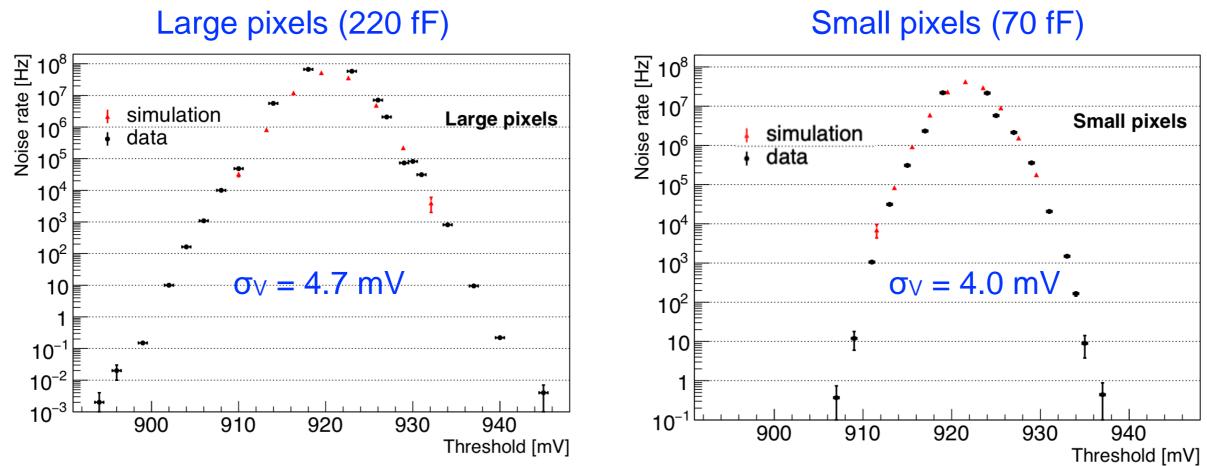
Mechanical support





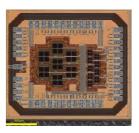


Noise rates

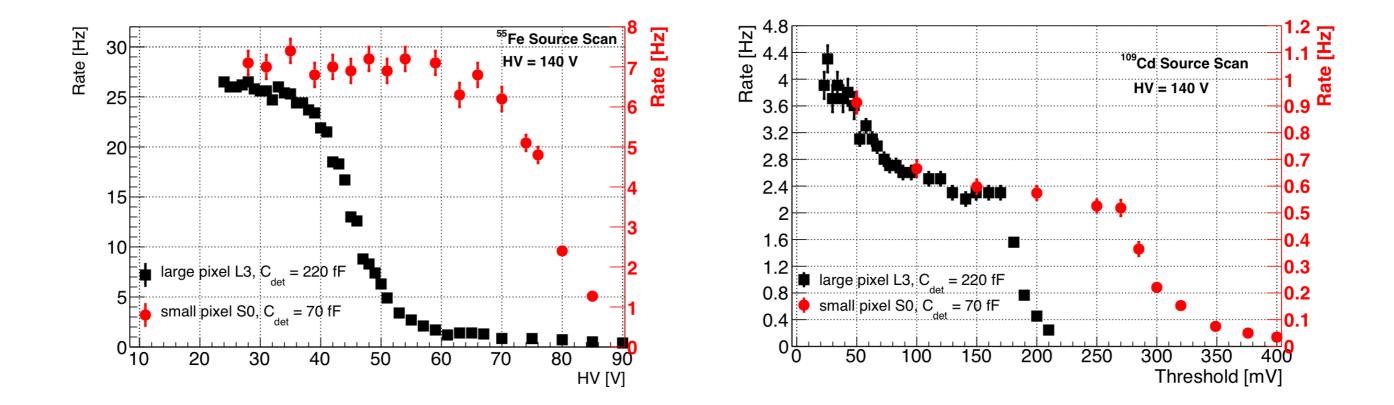


Measured noise rates agree well with CADENCE Spectre simulation

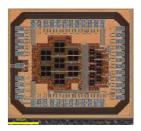




⁵⁵Fe and ¹⁰⁹Cd source calibrations

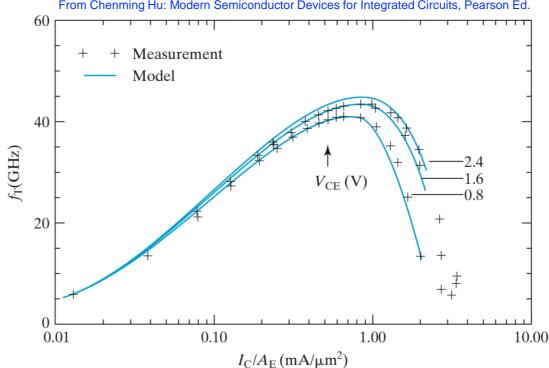


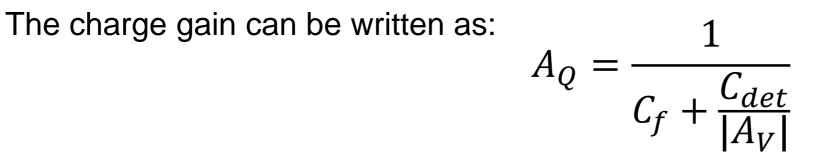




Time resolution vs. power consumption

 f_T depends on the collector current I_c (that is proportional to the power: $P = I_c V_{cc}$)





In our case, the capacitance C_f between the Base and the Collector of the HBT is much smaller than the detector capacitance: $C_{det}/|A_V| \gg C_f$

Therefore, since A_V is proportional to f_T : larger power \Rightarrow larger $f_T \Rightarrow$ larger $A_V \Rightarrow$ smaller ratio $C_{det}/|A_V| \Rightarrow$ higher A_Q



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CADENCE simulation

Signal in the hexagonal small pixels:

