

DFX – Meeting 37

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**06 December 2019** 

# DFX vertical section – Essential topics drawn from actions list (02-12-2019)

#### **Action list for SOTON**

- 1. Compile list of dimensions taken from the CERN 3-D model and check coherence with the SOTON stress analysis models
  - Full list compiled and circulated amongst the teams and differences between two models being addressed sequentially. Phonecall between WB and DO on Tuesday to discuss version 2 of list Further dimensional changes implemented by SOTON to reduce localised stress concentration over the last two days to be discussed today
- 2. SOTON to complete design report of vertical part and send by Friday 13 Dec. Compilation of design report in progress
- 3. CERN to send SOTON a list of ST numbers and equipment names TXT. file containing the a list of ST numbers and the part name/identifier supplied
- 4. SOTON and CERN to clarify bellows parameters (horizontal and vac. barrier) and contact Kompaflex

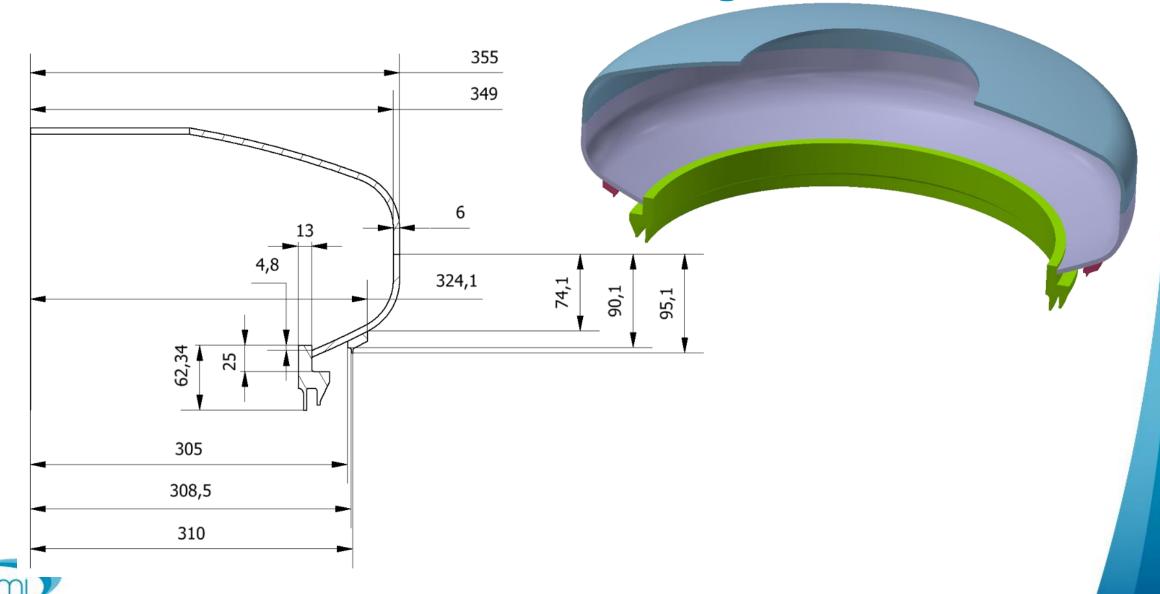
Tighter specification for custom design of vacuum barrier membrane bellows sent to Kompaflex First iteration of offer by Kompaflex to be discussed today



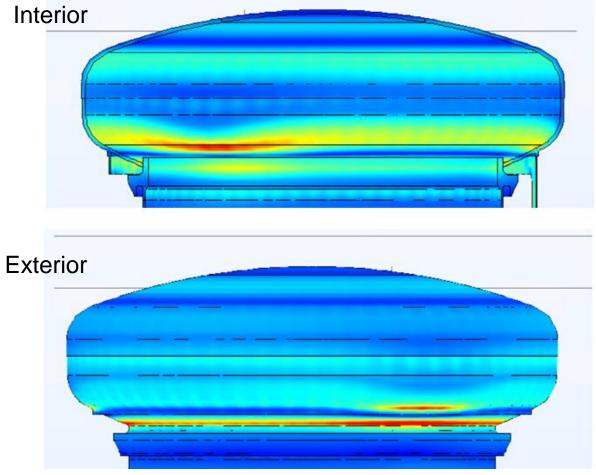
#### **Domes**

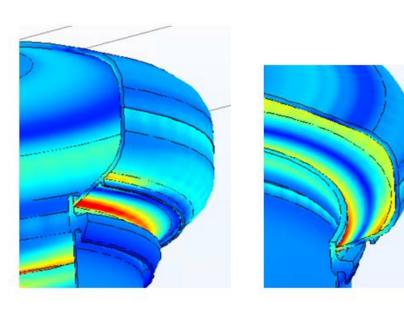
- a. General strengthening required for particular load cases achieved by increasing the thickness domes from 5 mm to 6 mm. (Note: This change in dimensions already implemented by CERN in CATIA 3-D model)
- b. Further reduction of the localised stresses identified in welding ring attached to the bottom of the dome under a few load cases achieved by increasing of thickness from 8 mm to 13 mm (STP now available for CERN)
- c. Increasing the width of the mounting ring used for attaching the cage to the bottom dome add both local reinforcement to the bottom dome and help dissipate stresses developing at the top of cage structure. (STP now available for CERN)





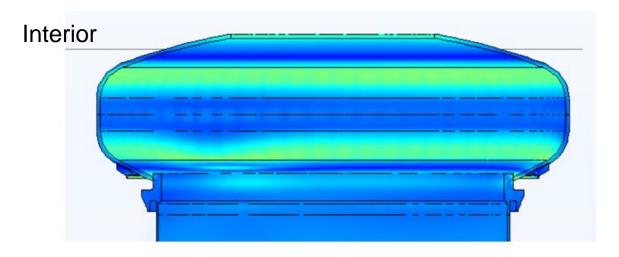
BEFORE implementing change a) – c)

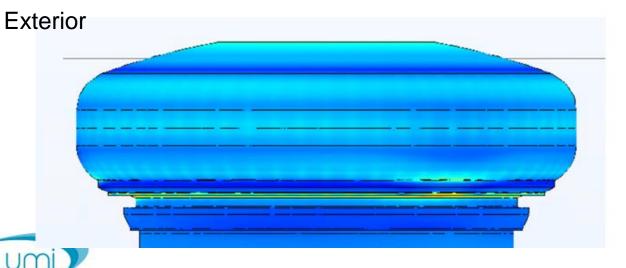


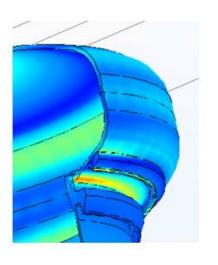


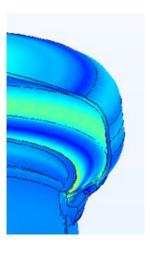


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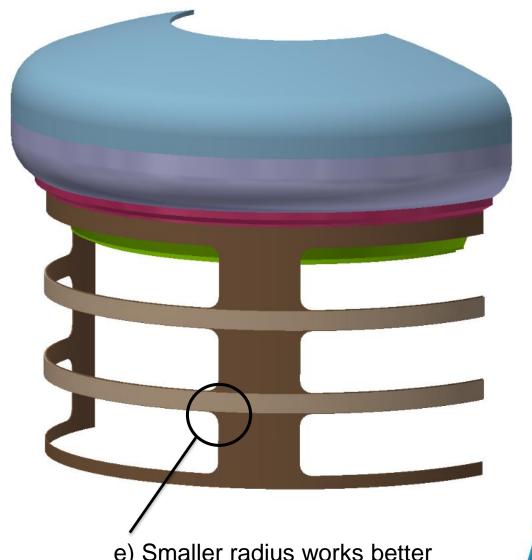






## Cage

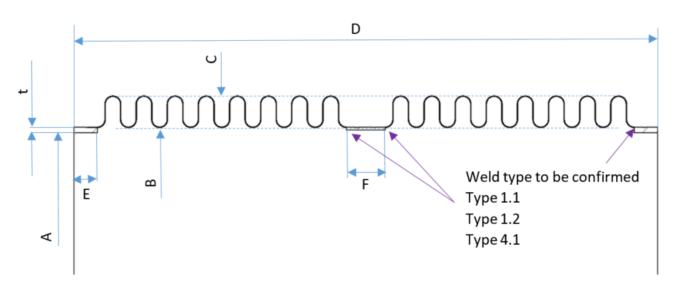
- d. Position of cage changed to converge with current position in CATIA 3-D model (i.e. ID = 617, OD = 624. This shift therefore enables 12 mm MLI blankets to be located on the outside of cage and inside the vacuum wall (650 ID).
- e. Profile of cut-out in cage adapted to alleviate stress concentration. (STP now available for CERN)





#### Vacuum barrier membrane

f. Indicative proposal supplied by SOTON to Kompaflex



**Figure 1** – Double bellows arrangement proposed for vacuum barrier membrane

**Table 1** provides the technical requirements for the design

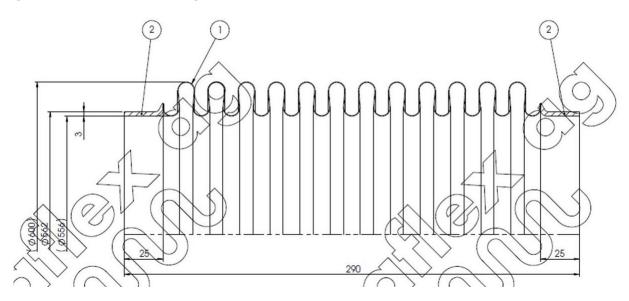
	Parameters	Value
	Design temperature	-269 °C
	Working fluid	Helium (liquid and gas)
Ps int	Relative internal pressure	1.5 bar
Ps ext	Relative external pressure	1.5 bar
	PED Category	Category I
	Convolution material*	EN 1.4404 or EN1.4435
	Bellow end material*	EN 1.4404 or EN1.4435
$\Delta x$	Axial movement	+/- 5 mm
$Nb_{\Delta x}$	Axial cycles	500
$\Deltay$	Lateral movement	5 mm
Nb $_{\Delta y}$	Lateral cycles	10
$\Delta\Theta$	Angular movement	2.5 degrees
Nb ∆Θ	Angular cycles	10
В	Minimum convolution diameter	556 mm
С	Maximum convolution diameter	600 mm
Α	Tube end inner diameter	556 mm
t	Tube end thickness	3 mm
D	Overall assembly length	290 mm
E	Straight end length	>20 mm
F	Inter bellow length	>30 mm
Kx	Max. axial elastic spring rate	200 N/mm
Ку	Max. lateral elastic spring rate	100 N/mm
KΘ	Max. angular elastic spring rate	N/A
np	Number of plies	Single ply (requested)
ер	Ply thickness	As thin as possible
w	Convolution height	As tall as can be tolerated
q	Convolution pitch	To be defined



#### Vacuum barrier membrane

Changed to 592

### g. First design iteration supplied from Kompaflex to SOTON



- Single bellows with Omega profile
- Single ply (ply thickness = 0.4 mm)
- Welding ends = 25 mm sections (as shown) in material 1.4429 to guarantee Cobalt content
- Weld type = Edge weld (Type 4.1 as per EN 14917).
- X-ray content: 25 % of bellows longitudinal seam and longitudinal seams of welded ends

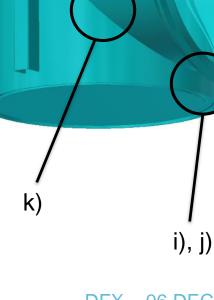
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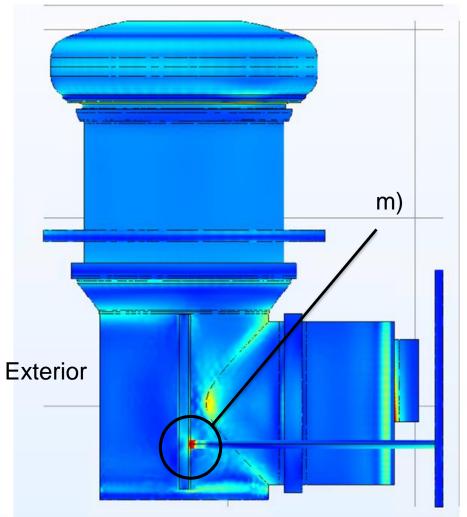


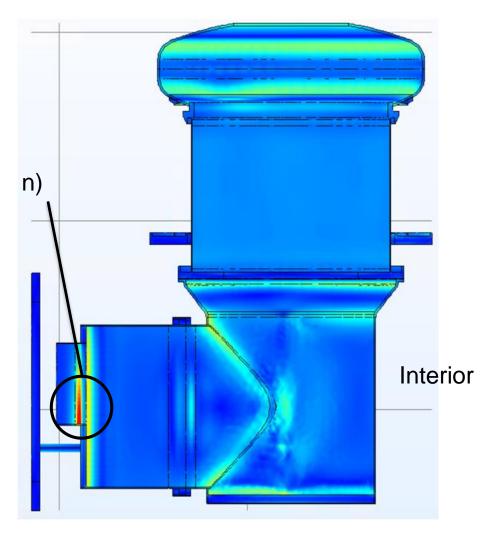
#### **Elbow**

- Increasing the thickness of the bottom flange from 15 mm to 20 mm has reduced the high stress concentration appearing in the bottom of the vertical-horizontal intersection
- j. Removing the horizontal stiffeners further reduced stress in same location even after increasing bottom flange thickness.
- k. Reducing the stresses appearing circumferentially along the vertical-horizontal intersection achieved by increasing the wall thickness of both tubes from 3 mm to 4 mm. (New STP now available for CERN)











# **DFX System – New actions**

- 1. High stresses in **point m)** to be resolved by adapting the feature for fixing the horizontal restrain (INVAR) bar to the elbow. We are also experimenting and trying to optimise its vertical position
- 2. High stress in **point n**) to be resolved by increasing the wall thickness and flange thickness in this reducer section

