

Thermally induced deformations of the TCLPX jaw

Engineering actions HiCoIDEM Meeting #35

R. Key EN-MME-EDS



ENGINEERING
DEPARTMENT

TCLPX JAW

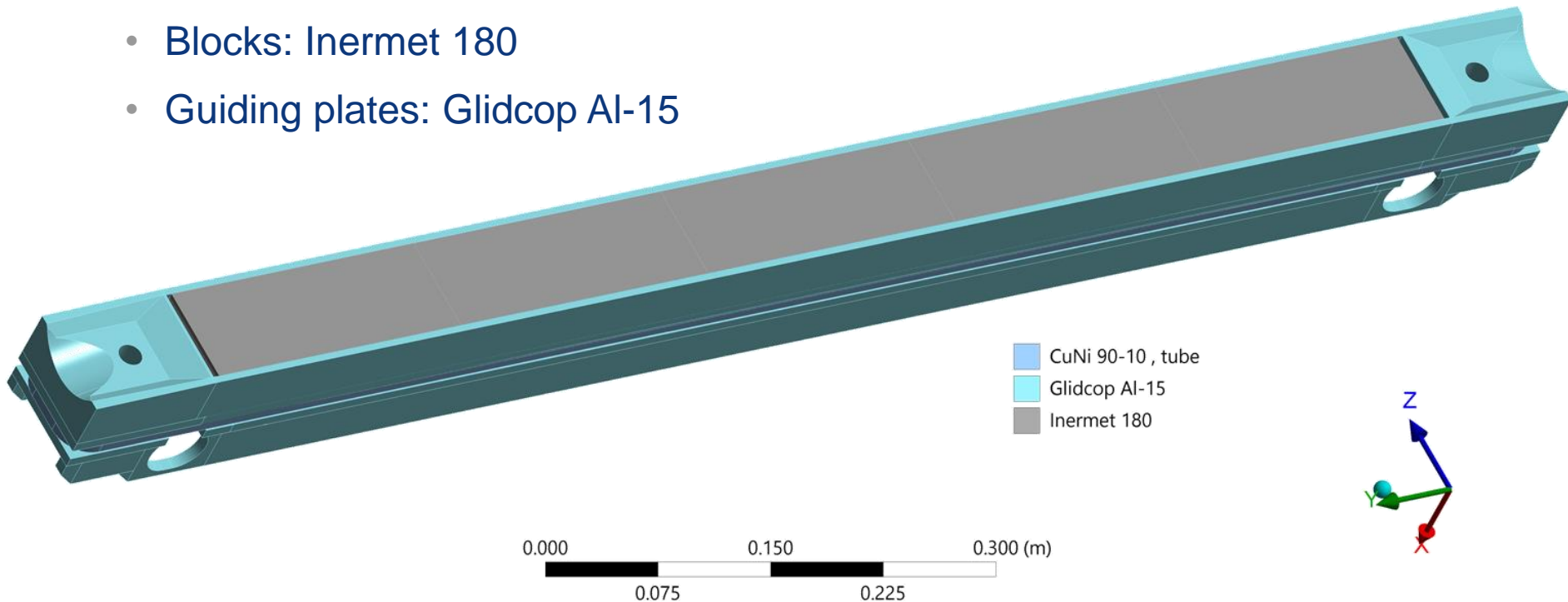
Request:

- Load on the jaw coming from collision debris
- Out-plane deformation at the JAW's active face under energy deposition in "Continuos flow" from Fluka maps

TCLPX JAW

Materials¹:

- Housing: Glidcop Al-15
- Stiffener: Glidcop Al-15
- Pipes: CuNi 90-10
- Blocks: Inermet 180
- Guiding plates: Glidcop Al-15



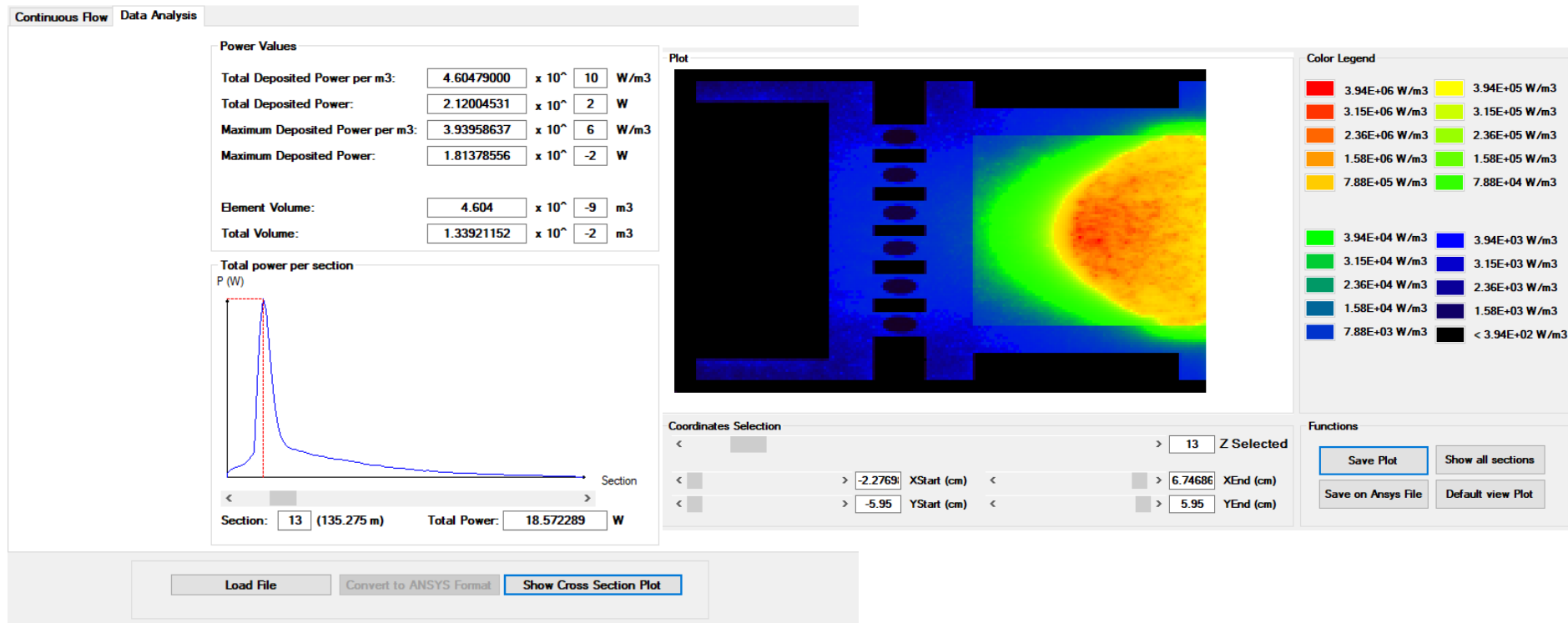
¹ [1] E. M. D. Office, Ansys Workbench material database

TCLPX JAW

Fluka map²

- Energy deposition: 212 W
- Type: Continuous flow

FLUKAToANSYSConverter - Current File Name: hilumi_ir1-hx_jawIN.txt

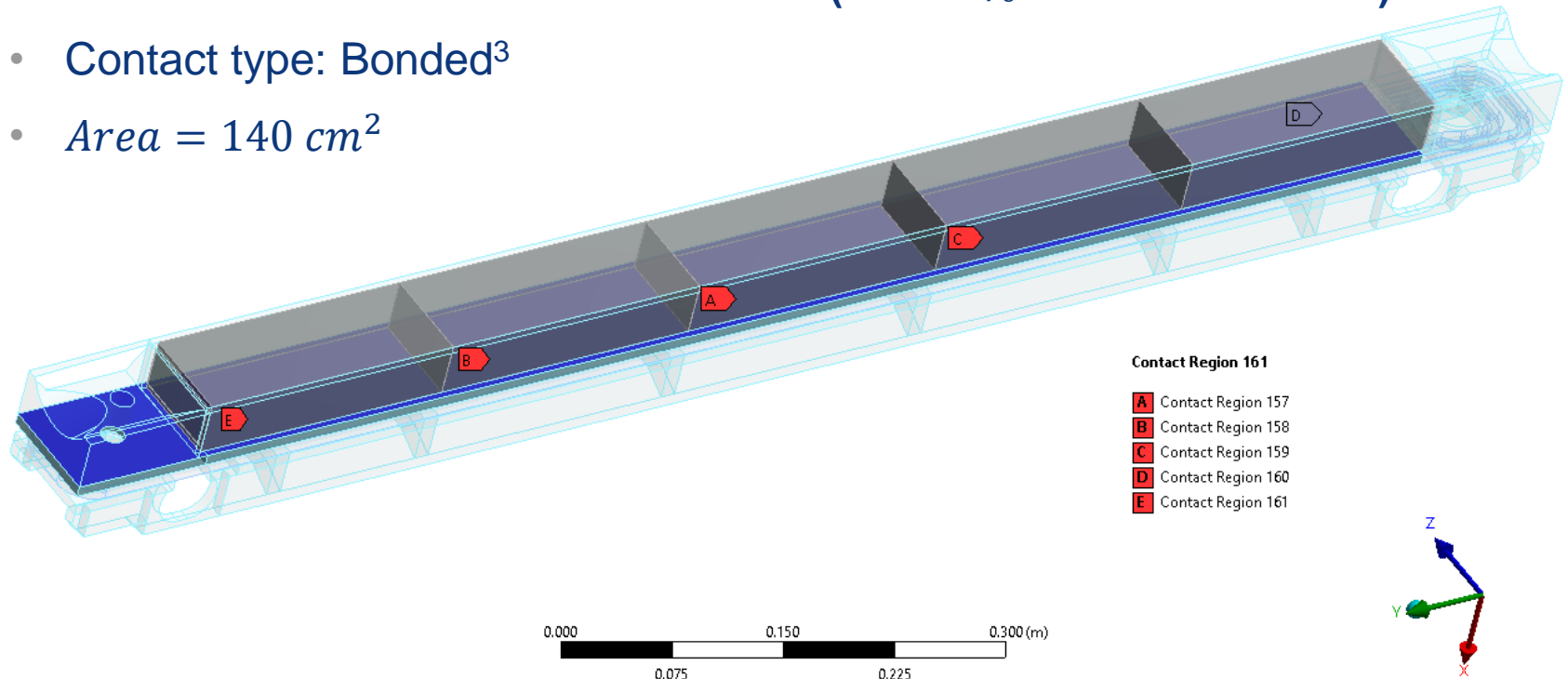


² Provided by Marta Sabate Gilarte

TCLPX JAW

Thermal contact resistance calculations:

- Brazing between CuNi pipes and Glidcop: $25000 \frac{W}{m^2 \cdot K}$
- Contact (@ ~24bar) between Glidcop and Inermet 180 block: $7954 \frac{W}{m^2 \cdot K}$
 - Effective Contact Pressure: $23.956 \text{ bar} \cong 24 \text{ bar}$
 - **20x M4 Screws SS Cr.Ni.18.12 Mo ($\nu = 60\%$ Utilization factor)**
 - Contact type: Bonded³
 - $Area = 140 \text{ cm}^2$

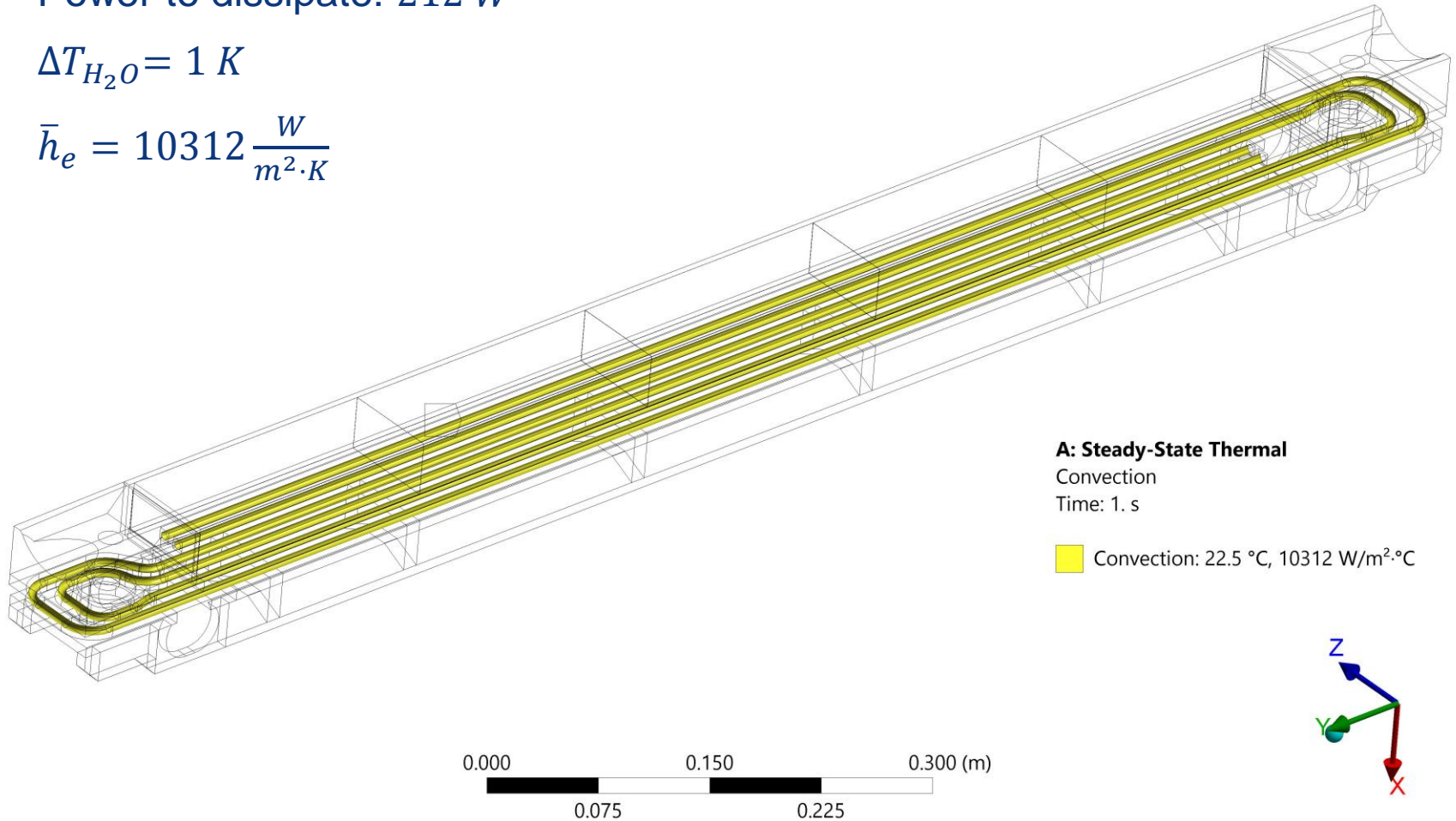


³Simplification procedure proofed to be equivalent for executed simulations on TCSP and TCTP calculations see: EDMS [1212639](#) & [1297290](#)

TCLPX JAW

Film coefficient on cooling pipes calculations (Convection)

- Power to dissipate: 212 W
- $\Delta T_{H_2O} = 1 K$
- $\bar{h}_e = 10312 \frac{W}{m^2 \cdot K}$



TCLPX JAW

Steady-State Thermal Results

- Nett power 204.85 W (3.37% Error)

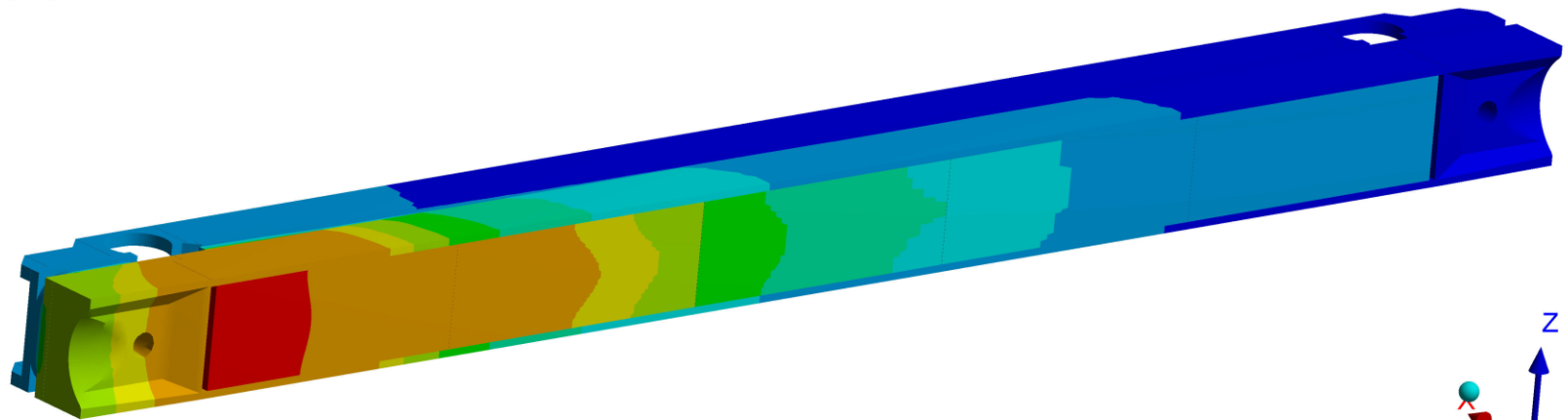
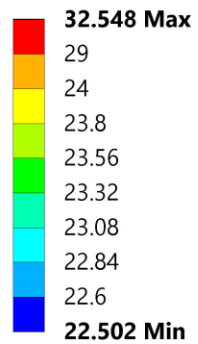
A: Steady-State Thermal

Temperature

Type: Temperature

Unit: °C

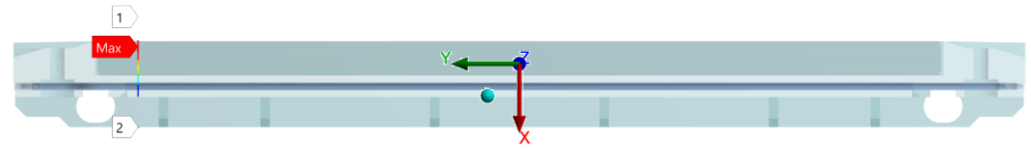
Time: 1



TCLPX JAW

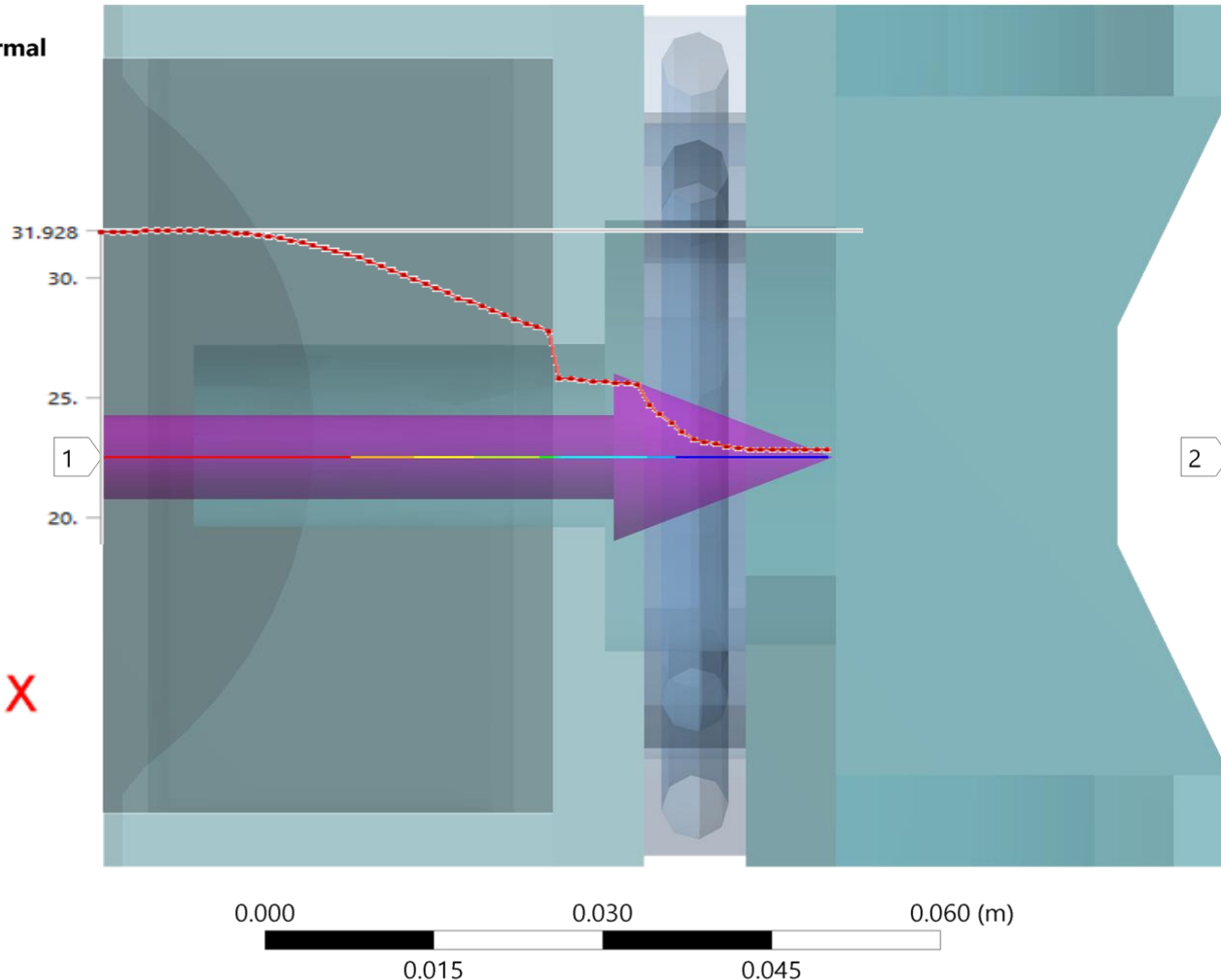
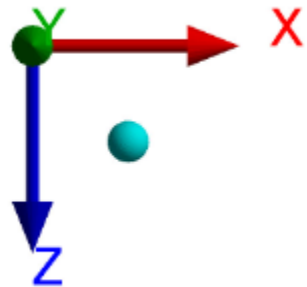
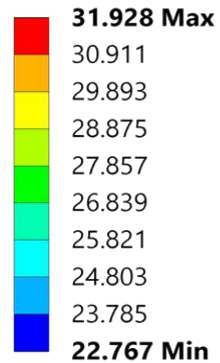
Steady-State Thermal Results

- Temperature through path – GCS (x,0.45,0.002) m



A: Steady-State Thermal

Path Temperature
Type: Temperature
Unit: °C
Time: 1
29/01/2020 17:20

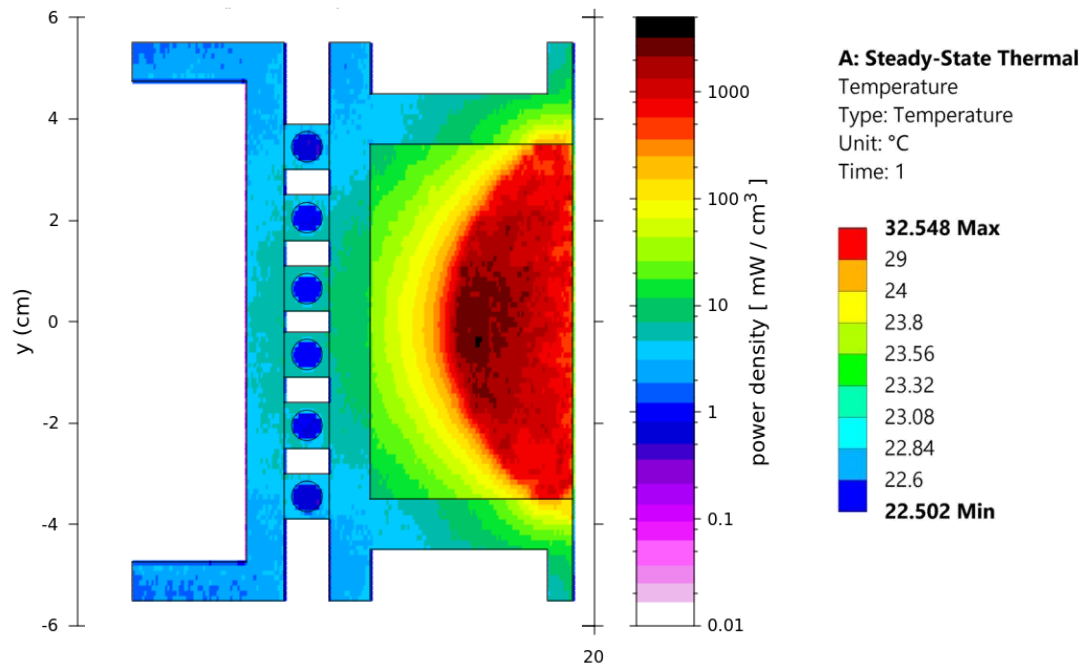


TCLPX JAW

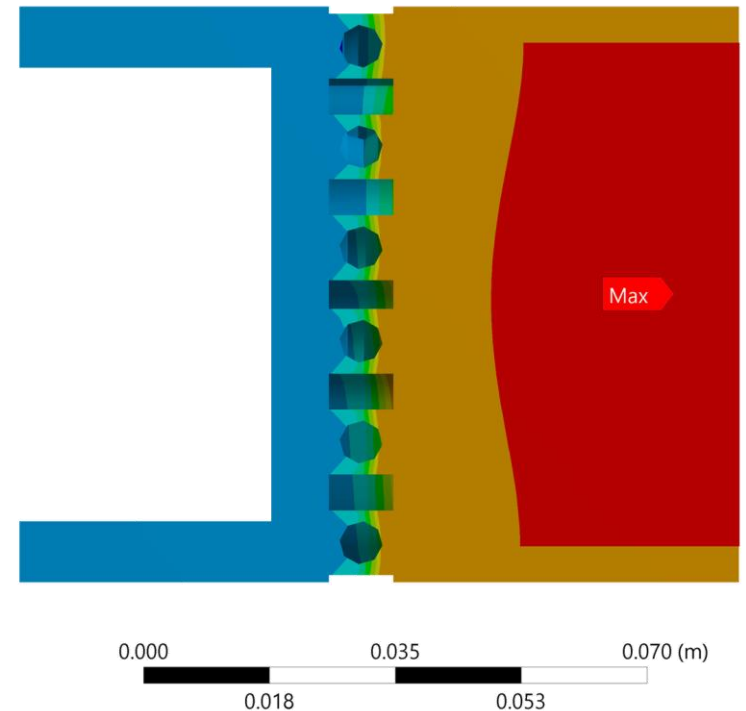
Steady-State Thermal Results vs. power density FLUKA

INPUT POWER

power density at the peak of the deposition in TCLX4 (ultimate conditions) *



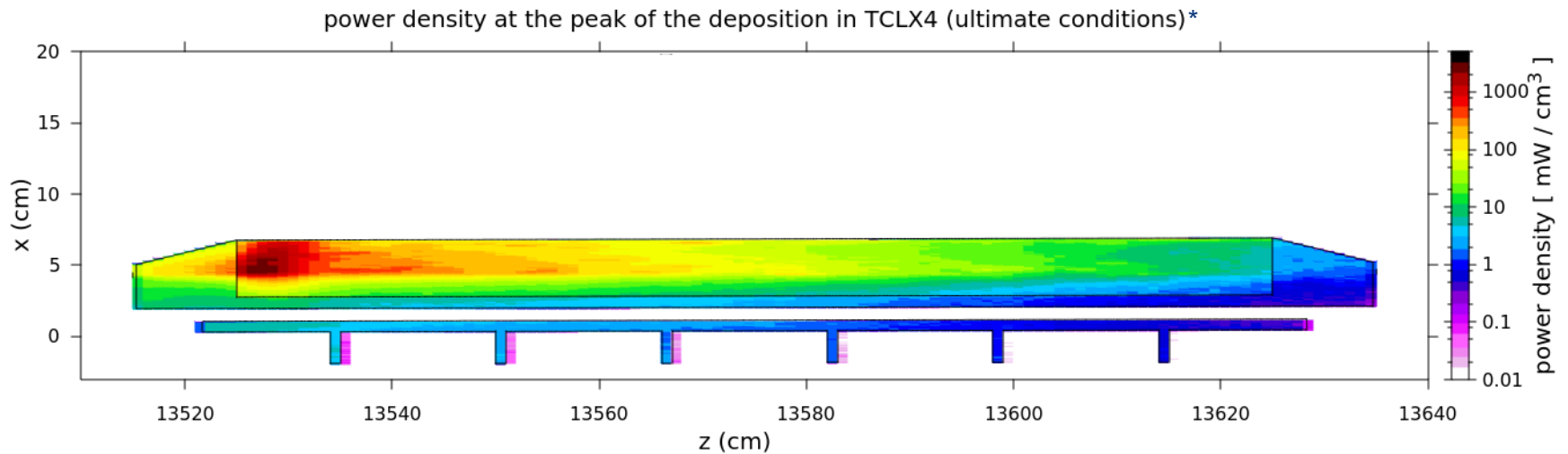
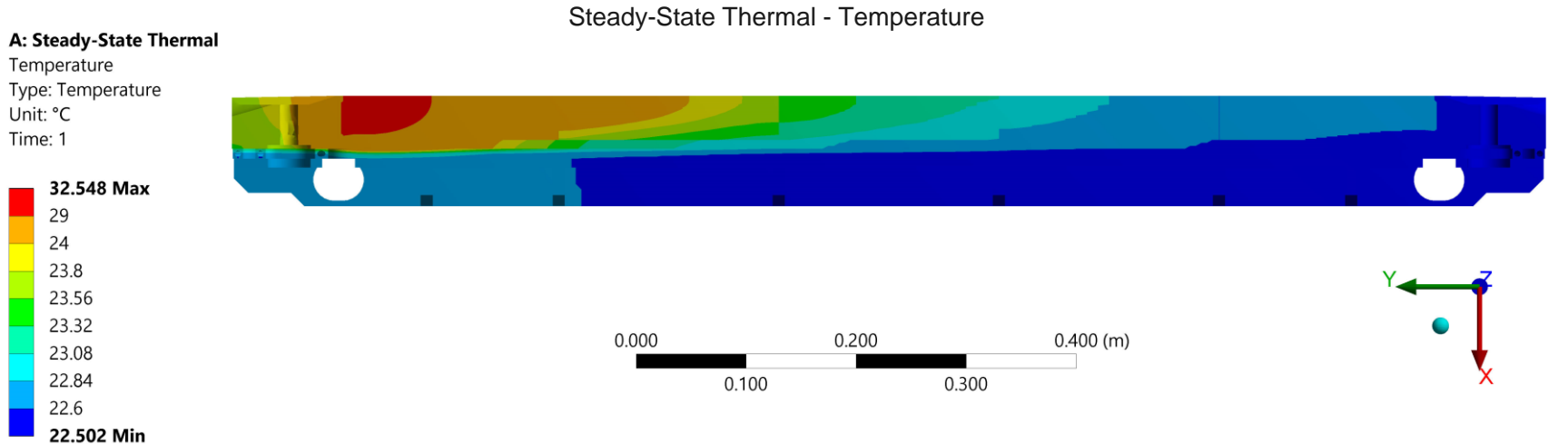
RESULTING TEMPERATURE



*Provided by Marta Sabate Gilarte

TCLPX JAW

Steady-State Thermal Results vs. power density FLUKA



*Provided by Marta Sabate Gilarte

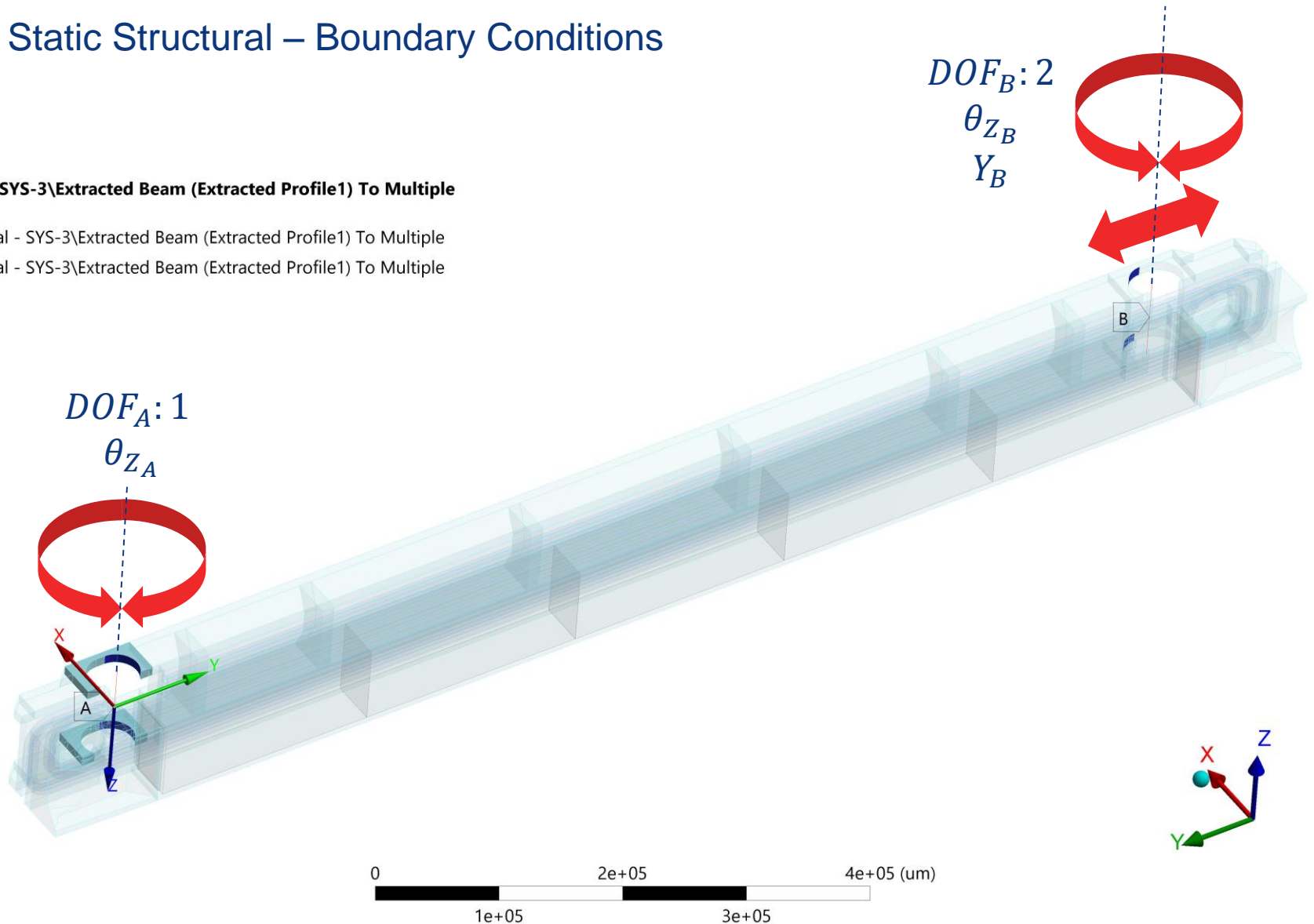
TCLPX JAW

- Static Structural – Boundary Conditions

Cylindrical - SYS-3\Extracted Beam (Extracted Profile1) To Multiple

A Cylindrical - SYS-3\Extracted Beam (Extracted Profile1) To Multiple

B Cylindrical - SYS-3\Extracted Beam (Extracted Profile1) To Multiple



TCLPX JAW

- Static Structural – Results

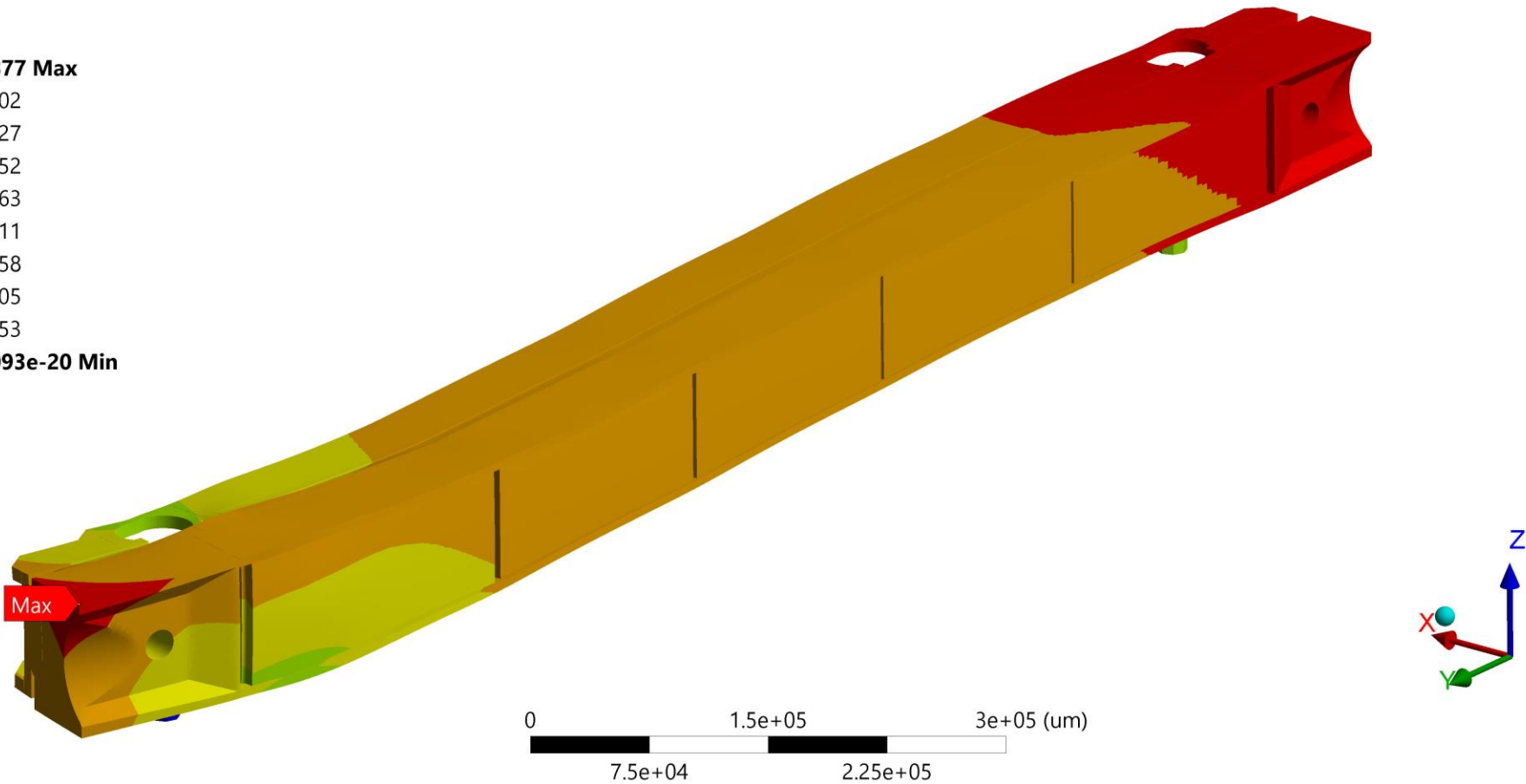
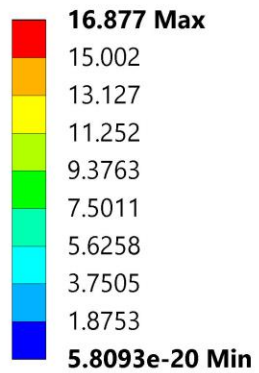
B: Static Structural

Total Deformation

Type: Total Deformation

Unit: μm

Time: 1



TCLPX JAW

- Static Structural Results

B: Static Structural

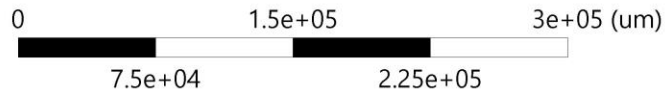
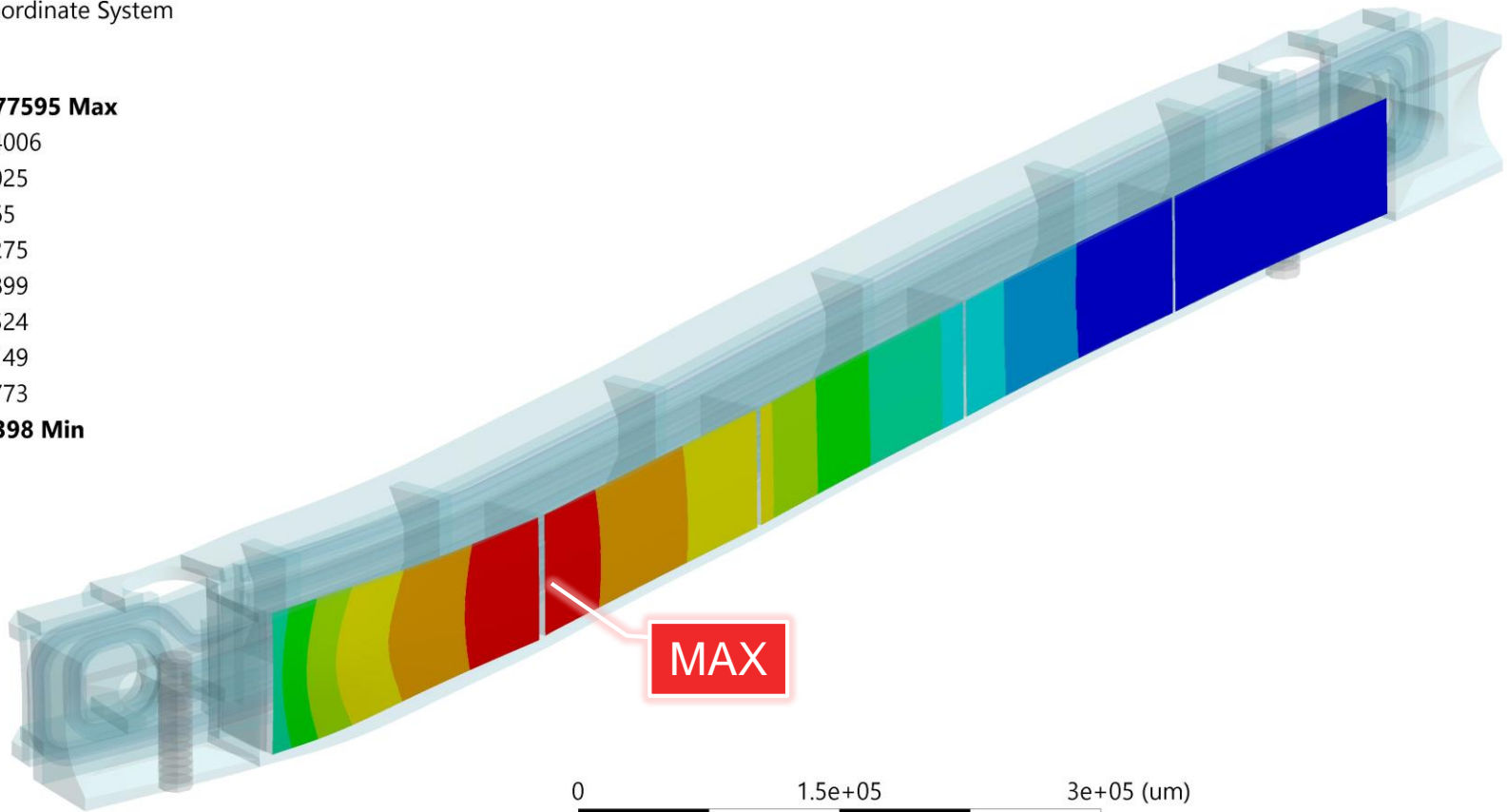
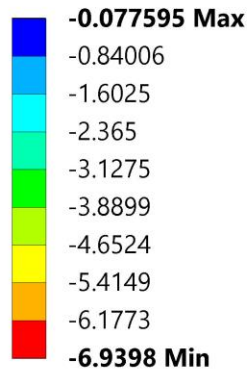
X Axis - Directional Deformation - Multiple - 1. s

Type: Directional Deformation(X Axis)

Unit: μm

Global Coordinate System

Time: 1



Conclusions

- The specification for a collimator jaw is a maximum deformation in operation, in the beam direction, **of 100 μm** . In the worst possible case (errors summing up), the typical budget is:
 - 40 μm manufacturing tolerances
 - 30 μm self weight
 - 30 μm thermal deformations
- **We have in this case < 50 μm**
 - 40 μm manufacturing tolerances
 - 0 μm self weight (horizontal collimator)
 - 7 μm thermal deformations
- For the **TCLPX, we will thus be dominated by the manufacturing tolerances.**



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Thank you!