# First ideas on a VVLE beam

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## Optics & Characteristics – The "dogleg" version

Bending Plane (Horizontal)



- 4 MBPS and 4 QPS ٠
- 4 power supplies in total
- Large acceptance in both planes and good intrinsic resolving power
- To be placed in an angle from the target (~200 mrad)
- **QPS & MPBS all available**
- Cabling and cooling necessary to be upgraded
- Standard EN-EA equipment (brides, connectors...)
- ToF (XBTF) + XBPF + XCET low pressure ?



### Optics & Characteristics – The "field-lens" version



A first trial on SLE beam – FL version



- 2 MBPS and 7 QPS
- 5 power supplies in total
- Large acceptance in both planes descent intrinsic resolving power
- To be placed in an angle from the target (~200 mrad) or at a 0 production angle
- QPS & MPBS all available
- Cabling and cooling to be seen
- ToF (XBTF) + XBPF + XCET low pressure ?
- More sensitive to chromatic aberrations



### Preliminary CATIA designs (V. Clerc)



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### Shortening the length with **EXISTING** elements

- Goal: Preserving the existing elements and the acceptance (in the FDplane)
- Sacrificing (a little) the full momentum recombination and the spotsize in the bending plane

30.00 MM 1.00 M



A first trial on SLE beam — MDX





A first trial on SLE beam – MDX



30.00 MM 1.00 M

### Shortening the length with **NEW** elements

### New shorter elements assumed



* VVLE BEAT	CH VERSION 0.1*										
	X-COORDINATE	Y-CO	ORDINAT	re –co	ORDINATE	GISEMEN	H T ANG	OR LE	VERT ANGLE		
INITI	AL 0.00000		0.00000	) (	0.00000	500.000	00 0.00	0000	0.000000		
I ELEMENT		K	L	DEFL ANG	TILT LE	x	¥	Z	HOR ANGLE	VERT ANGLE	BEAM LENGTH
			М	RAD	DEG	M	М	м		RAD	М
1 SEC.TARGET 2	TARGET	20 1	0.000	0.00000	0.00	0.00000	0.00000	0.000	0.000000	0.000000	0.000
3 QPS 099001 4	Ql	3 1	0.500 0.500			1.10000 1.60000	0.00000 0.00000	0.000	0.000000	0.000000	1.100 1.600
5 QPS 099002 6 7 OPS 099003	Q2 03	3 1 3	0.700			2.30000 2.80000 3.30000	0.00000 0.00000	0.000	0.000000	0.000000	2.300 2.800 3.300
8 9 MBPS099005	20 B1	1 4	0.500	0.216000	0.00	3.80000 4.29709	0.00000	0.000	0.000000	0.000000	3.800 4.300
10 11 COLL099008	Cl	1 10 1	0.250	0.000000	0.00	4.54128 4.73663 4.98082	0.10748 0.15034	0.000	0.216000	0.000000	4.550 4.750 5.000
13 QP7 099007 14	Q4	3	0.700			5.66455 5.90875	0.35395 0.40753	0.000	0.216000	0.000000	5.700 5.950
15 XCON099008 16	ABS	17 1	0.200	0.000000	0.00	6.10410 6.34829	0.45040	0.000	0.216000	0.000000	6.150 6.400
18 19 QPS 099012	Q5	1	0.500	0.210000	0.00	7.27634 7.73040	0.87250	0.000	0.432000 0.432000 0.432000	0.000000	7.400
20 21 QPS 099012	Q6	1 3	0.400			8.09366 8.72935	1.24932 1.54240	0.000	0.432000	0.000000	8.300 9.000
22 23 XBPF 09901 24	XBPF2	1 9 1	0.500 0.200 0.300	0.000000	0.00	9.18341 9.36504 9.63748	1.75175 1.83548 1.96109	0.000 0.000 0.000	0.432000 0.432000 0.432000	0.000000 0.000000 0.000000	9.500 9.700 10.000
25 EXPMT	EXPT	20	0.000	0.000000	0.00	9.63748	1.96109	0.000	0.432000	0.000000	10.000

### Survivals



### Particle production – FLUKA Simulations

- 40 GeV/c beam
- From Atherton: 78.04 % pions, 6.17% kaons, 15.78% protons
- Renormalizing to add 30% electrons:
  - Beam comp: 54.62% pions, 4.31% kaons, 11.046% protons, 30% electrons
- Custom FLUKA routine (source.f) with EMF=ON
- Spot size: 2cm FWHM both planes, 1.5% dp flat
- Simple Geometry:



Scoring the particle yield in the momentum range of interest and for different particles and angles in the range 0 – 500 mrad polar

### W-target, 5 cm radius and 30 cm length



#### Pion yield very similar between 0-200 mrad

Positron yield drops by ~ 1 order of magnitude between 0 and 200 mrad, and even in the forward direction suppressed by ~ 0.5 - 1 order of magnitude compared with the pions.

### Be-target, 5 cm radius and 50 cm length



Pion yield very similar between 0-200 mrad and very similar with Tungsten 30 cm

Positron yield higher than Tungsten by at least 1 order of magnitude between 0 and 200 mrad

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### Be-target, 5 cm radius and 20 cm length



Pion yield very similar between 0-200 mrad and slightly suppressed from Be-500 (no surprise)

Positron yield still quite higher than Tungsten between 0 and 200 mrad

### Time of flight and Cherenkov counters



Better ToF than 800 ps resolution needed for electron tagging, but pions < 1.2 GeV 4 sigma separation from Kaons Always relativistic electrons give light, can be easily tagged



### Conclusions

- Some preliminary ideas of a VVLE beam (max 2.5 GeV/c) have been studied.
- Detailed FLUKA simulations should be done, in order to optimize the necessary beam line acceptance and the choice of elements.
- An integration study with possible positions should follow, given that the budget is found (designers – FSUs).
- Main expected cost drivers :
  - Cabling, cooling and infrastructure (necessary at any case)
  - New magnetic elements (?)
  - Power supplies + transformers
  - Construction of extension inside the NP-04 pit
  - Manpower / resources for the construction
- More detailed studies require approval of the physics case.

### EXTRA SLIDES

### **Geometrical Acceptances**

• Ignoring the optics, the first acceptance cut is made by the first element after the production target.



### Lau vvle10p2 TRANSPORT in/out

VVLE nev	w shorter magnets - LAU vvlel0p2
)	
.5. 1. "1	MM" 0.1 ;
.3.0 18.0	D ;
.3.0 19.0	D ;
. 3. 5.	3. 15. 0. 4.5 2.5 "CRD1" ;
3.0	0.000 "LETG" ;
3.0	0.600 ;
5.0D	0.500 19.86877 100.0 "Q1" ;
3.0	0.500 ;
5.0E	0.700 -19.34149 100.0 "Q2";
3.0	0.500 ;
5.0F	0.500 19.86877 100.0 "Q3" ;
3.0	0.500 ;
4.0	0.500 18.0 0.0 "B1" ;
3.0	0.700 ;
5.0A	0.350 38.23307 50.0 "QFLD";
10.0 -1	1. 2.0 0.0 0.0001 ;
10.0 -3	3. 4.0 0.0 0.0001 ;
5.0A	0.350 38.23307 50.0 "QFLD";
3.0	0.700 ;
4.0	0.500 18.0 0.0 "B2" ;
3.0	0.500 ;
5.0X	0.500 -10.0 100.0 "Q5" ;
3.0	0.400 ;
5.0Y	0.700 10.0 100.0 "Q6" ;
3.0	1.000 ;
3.0	0.000 "EXPT" ;
.02.	2. 00001 "HF2" ;
.04.	4. 00001 "VF2" ;
.0.0 -1.0	0 6.0 0.0 0.0001 ;
.3. 41.	"PRIN" ;
ENTINEL	
ENTINEL	

#### COVARIANCE (FIT 0.44839E-02 ) VVLE new shorter magnets - LAU vvle10p2

*QUAD*		5.	_"Q1 "		.50000	М	48.030	54 KG	100.0000	0 MM (	0.44	707 M					
VARY	COD	E = 0	D														
*QUAD*	COD	5.	"Q2 "		.70000	M	-20.06957 KG		100.0000	OMM (	-0.49	119 M	)				
VARI	COD	E = 0	E		50000	м	22 10560 80		100.0000	0.104	0.91	242 M					
VADY	COD		- Q3		. 50000	M	23.10360 KG		100.0000	0 19191 (	0.01	242 M	)				
*OUND*	COD	E – 0	P NOFI DU		25000	м	11 120	AS PC	50 0000	0 MM (	1 1 2	010 M					
VADV	COD	ਦ = ਹ	v A		. 33000	FI	11.15510 1.5		50.0000	0 1111 (	1.13	010 1	)				
*FTT*	COD	10 0	A	-1			00000 /	0 00010		0 00000	<b>`</b>						
*FTT*		10.0		-3	. 2.	ſ	0.00000 /0.00010		(-0.00001)								
*OUAD*		5.	"OFLD"	0	35000	м	11.13846 KG		50.00000 MM ( 1.13018 M		018 M	)					
VARY	COD	E = 0	A				11.100	10 110	00.0000	5 I.M. (	1.10	010 11					
*OUAD*	002	5.	"05 "	0	. 50000	м	-15.17081 KG		100.00000 MM ( -1.02025 M		025 M	)					
VARY	COD	E = 0	x						100.00000 III ( -1.02020 II								
*QUAD*		5.	"Q6 "	0	.70000	М	7.46709 KG		100.00000 MM ( 1.1		1.71	833 M	)				
VARY	COD	$\mathbf{E} = 0$	Y														
*FIT*		10.0	"HF2 "	-2	. 2.	C	.00000 /	0.00010	( –	0.00000	)						
*FIT*		10.0	"VF2 "	-4	. 4.	C	.00000 /	0.00010	(	0.00000	)						
*FIT*		10.0		-1	. 6.	C	.00000 /	0.00010	(	0.00000	)						
0*LENGTH*		1	0.00000 1	1													
1VVLE new	sho	rter m	agnets -	LAU VV	lel0p2							TRANSPOR	RT R	UN14/01/	20		
OPOSITION	TYP	E	STRENGTH		H	ORIZ	ONTA	L *		VERT	ICAL			D	ISPE	RSIO	N
METERS			T*M, T/M*M	* 1	R11	R12	R21	R22 *	R33	R34	R43	R44		R16	R26	R36	R46
			T/M**2*M	[* ]	MM/MM	MM/MR	MR/MM	MR/MR *	MM/MM	MM/MR	MR/MM	MR/MR		MM/PC	MR/PC	MM/PC	MR/P
******	****	*****	*******	*****	*****	******	******	******	******	******	******	******	****	******	******	*******	*****
0.000	3	LETG			1.000	0.000	0.000	1.000 *	1.000	0.000	0.000	1.000		0.000	0.000	0.000	0.00
0.600	3				1.000	0.600	0.000	1.000 *	1.000	0.600	0.000	1.000		0.000	0.000	0.000	0.00
1.100	5	Q1	24.0153		0.362	0.606	-2.237	-0.980 *	1.811	1.715	3.622	3.984		0.000	0.000	0.000	0.00
1.600	3			* -	0.756	0.116	-2.237	-0.980 *	3.622	3.707	3.622	3.984		0.000	0.000	0.000	0.00
2.300	5	Q2	-14.0487		3.140	-0.637	-5.230	-1.380 *	3.754	4.000	-3.283	-3.232		0.000	0.000	0.000	0.00
2.800	3			* _	5.754	-1.328	-5.230	-1.380 *	2.113	2.384	-3.283	-3.232		0.000	0.000	0.000	0.00
3.300	5	Q3	11.5528	* -	5.197	-1.507	3.562	0.705 *	1.050	1.450	-1.210	-0.719		0.000	0.000	0.000	0.00
3.800	3				4.416	-1.155	3.562	0.705 *	0.445	1.090	-1.210	-0.719		0.000	0.000	0.000	0.00
4.300	4	B1	0 9000		n <u> </u>	0 706	3 CAA							0.270	1.077	0.000	0.00
5.000		22	0.0000		2.012	-0.796	3.044	0.728 *	-0.161	0.731	-1.210	-0.719					
	3			* _	0.061	-0.287	3.644	0.728 *	-0.161 -1.008	0.731	-1.210	-0.719		1.024	1.077	0.000	0.00
5.350	35	QFLD	7.7969	* =	0.061	-0.287	3.644	0.728 * 0.728 * 0.865 *	-0.161 -1.008 -1.624	0.731 0.227 -0.000	-1.210 -1.210 -2.408	-0.719		1.024	1.077	0.000	0.00
5.350 5.700	- 3 5 5	QFLD QFLD	7.7969	* _  * _	0.061 1.155 2.004	-0.287 0.000 0.287	3.644 3.118 1.600	0.728 * 0.728 * 0.865 * 0.728 *	-0.161 -1.008 -1.624 -2.787	0.731 0.227 -0.000 -0.227	-1.210 -1.210 -2.408 -4.416	-0.719 -0.719 -0.616 -0.719		1.024 1.217 1.024	1.077 -0.000 -1.077	0.000 0.000 0.000	0.00
5.350 5.700 6.400	3553	QFLD QFLD	7.7969	*	0.061 1.155 2.004 3.124	-0.287 0.000 0.287 0.796	3.644 3.118 1.600 1.600	0.728 * 0.728 * 0.865 * 0.728 * 0.728 *	-0.161 -1.008 -1.624 -2.787 -5.879	0.731 0.227 -0.000 -0.227 -0.731	-1.210 -1.210 -2.408 -4.416 -4.416	-0.719 -0.719 -0.616 -0.719 -0.719		1.024 1.217 1.024 0.270	1.077 -0.000 -1.077 -1.077	0.000 0.000 0.000 0.000	0.00
5.350 5.700 6.400 6.900	355340	QFLD QFLD B2	7.7969 7.7969 0.9000	* _  * _  * _	2.012 0.061 1.155 2.004 3.124 3.904	-0.798 -0.287 0.000 0.287 0.796 1.155	3.644 3.118 1.600 1.600 1.518	0.728 * 0.728 * 0.865 * 0.728 * 0.728 * 0.728 *	-0.161 -1.008 -1.624 -2.787 -5.879 -8.087	0.731 0.227 -0.000 -0.227 -0.731 -1.090	-1.210 -1.210 -2.408 -4.416 -4.416 -4.416	-0.719 -0.719 -0.616 -0.719 -0.719 -0.719		1.024 1.217 1.024 0.270 0.000	1.077 -0.000 -1.077 -1.077 -0.000	0.000 0.000 0.000 0.000 0.000	0.00
5.350 5.700 6.400 6.900 7.400	3 5 5 3 4 3 1	QFLD QFLD B2	7.7969 7.7969 0.9000	*	2.012 0.061 1.155 2.004 3.124 3.904 4.663	-0.798 -0.287 0.000 0.287 0.796 1.155 1.507	3.644 3.118 1.600 1.600 1.518 1.518	0.728 * 0.728 * 0.865 * 0.728 * 0.728 * 0.705 *	-0.161 -1.008 -1.624 -2.787 -5.879 -8.087 -10.295	0.731 0.227 -0.000 -0.227 -0.731 -1.090 -1.450	-1.210 -1.210 -2.408 -4.416 -4.416 -4.416 -4.416	-0.719 -0.719 -0.616 -0.719 -0.719 -0.719 -0.719		1.024 1.217 1.024 0.270 0.000 0.000	1.077 -0.000 -1.077 -1.077 -0.000 -0.000	0.000 0.000 0.000 0.000 0.000 0.000	0.00
5.350 5.700 6.400 6.900 7.400 7.900	1 3 5 5 3 4 3 5 0	QFLD QFLD B2 Q5	7.7969 7.7969 0.9000	* _  * _  * *	0.061 1.155 2.004 3.124 3.904 4.663 5.582	-0.798 -0.287 0.000 0.287 0.796 1.155 1.507 2.243	3.644 3.118 1.600 1.600 1.518 1.518 6.446	0.728 * 0.728 * 0.865 * 0.728 * 0.728 * 0.705 * 0.705 * 2.348 *	-0.161 -1.008 -1.624 -2.787 -5.879 -8.087 -10.295 -10.086	0.731 0.227 -0.000 -0.227 -0.731 -1.090 -1.450 -1.465	-1.210 -1.210 -2.408 -4.416 -4.416 -4.416 -4.416 5.221	-0.719 -0.719 -0.616 -0.719 -0.719 -0.719 -0.719 0.659		1.024 1.217 1.024 0.270 0.000 0.000 0.000	1.077 -0.000 -1.077 -1.077 -0.000 -0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000	
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5.350 5.700 6.400 6.900 7.400 7.900 8.300 9.000	* ? 5 5 ? 4 ? 5 ? 5 ?	QFLD QFLD B2 Q5 Q6	7.7969 7.7969 0.9000 -7.5854 5.2270	) * _  ) * ; ) * ; ) * ; ; * ; *	0.061 1.155 2.004 3.124 3.904 4.663 6.582 9.160 1.413	-0.796 -0.287 0.000 0.287 0.796 1.155 1.507 2.243 3.182 4.035	3.644 3.644 3.118 1.600 1.518 1.518 6.446 6.446 6.446	0.728 * 0.728 * 0.865 * 0.728 * 0.728 * 0.705 * 0.705 * 2.348 * 2.348 *	-0.161 -1.008 -1.624 -2.787 -5.879 -8.087 -10.295 -10.086 -7.998 -5.889	0.731 0.227 -0.000 -0.227 -0.731 -1.090 -1.450 -1.465 -1.202 -0.979	-1.210 -1.210 -2.408 -4.416 -4.416 -4.416 -4.416 5.221 5.221 1.022	-0.719 -0.719 -0.616 -0.719 -0.719 -0.719 -0.719 -0.719 0.659 0.659 0.000		1.024 1.217 1.024 0.270 0.000 0.000 0.000 0.000 0.000 0.000	1.077 -0.000 -1.077 -1.077 -0.000 -0.000 0.000 0.000 -0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	
5.350 5.700 6.400 7.400 7.900 8.300 9.000 10.000	* ? 5 5 ? 4 ? 5 7 5 5 6	QFLD QFLD B2 Q5 Q6	7.7965 7.7965 0.9000 -7.5854 5.2270	*	2.012 0.061 1.155 2.004 3.124 3.904 4.663 6.582 9.160 1.413 1.165	-0.287 0.000 0.287 0.796 1.155 1.507 2.243 3.182 4.035 4.035	3.644 3.644 3.118 1.600 1.600 1.518 1.518 6.446 6.446 -0.248 -0.248	0.728 * 0.728 * 0.865 * 0.728 * 0.728 * 0.705 * 2.348 * 2.348 * -0.000 *	-0.161 -1.008 -1.624 -2.787 -5.879 -8.087 -10.295 -10.086 -7.998 -5.889 -4.868	0.731 0.227 -0.000 -0.227 -0.731 -1.090 -1.450 -1.465 -1.202 -0.979 -0.979	-1.210 -1.210 -2.408 -4.416 -4.416 -4.416 5.221 5.221 1.022 1.022	-0.719 -0.719 -0.616 -0.719 -0.719 -0.719 -0.719 0.659 0.659 0.000 0.000		1.024 1.217 1.024 0.270 0.000 0.000 0.000 0.000 0.000 0.000	1.077 -0.000 -1.077 -1.077 -0.000 -0.000 0.000 -0.000 -0.000 -0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	