

Outline

- Motivation for thin films in SRF cavities
- How to realize a thin film coating?
- State of the art in Nb thin films (accelerators using thin film technology)
- Characteristics of Nb thin films

Cristian Pira

• R&D on Nb thin films

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Why thin films for SRF?

- 1. Reduce material cost
- 2. Change the surface properties (bulk properties ≠ surface properties)
- 3. Use materials with poor mechanical properties (but excellent SRF properties)
- 4. Realize complex structures



Why thin films for SRF?

1. Reduce material cost

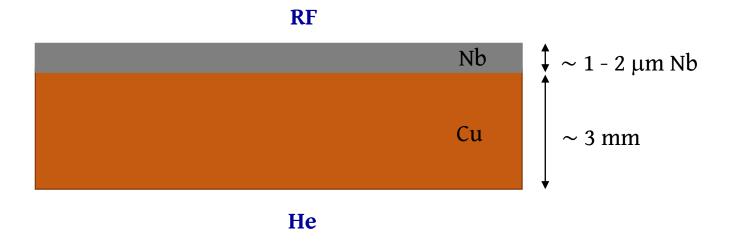
- Change the surface properties (bulk properties ≠ surface properties)
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Reduce material cost

RF penetration in Nb is **limited by** λ_L (less than 100 nm)

Not necessary more than 1 micron of Nb at the surface



Cu is more than 50 times cheaper than high pure Nb

It is possible to **increase the mechanical stability** of the cavities increasing wall thickness

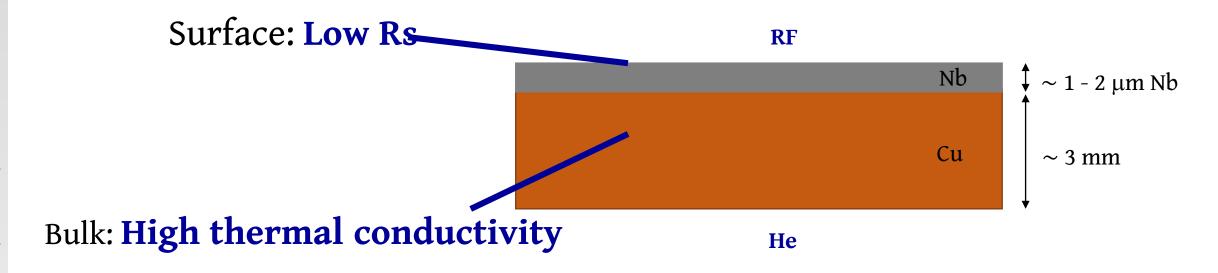


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Change the surface properties

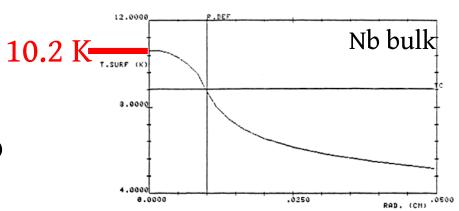


Cu presents high thermal conductivity resistance to quench



Temperature distribution in Nb-Cu

Temperature distribution simulation for an iron based defect imbedded in Nb or Cu

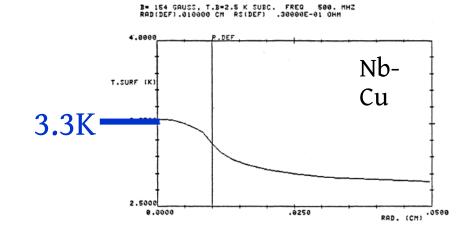


B= 154 GAUSS, T.B=2.5 K SUBC. FREG 500. MHZ

Copper prevents Quench

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due to thermo-magnetic breakdown

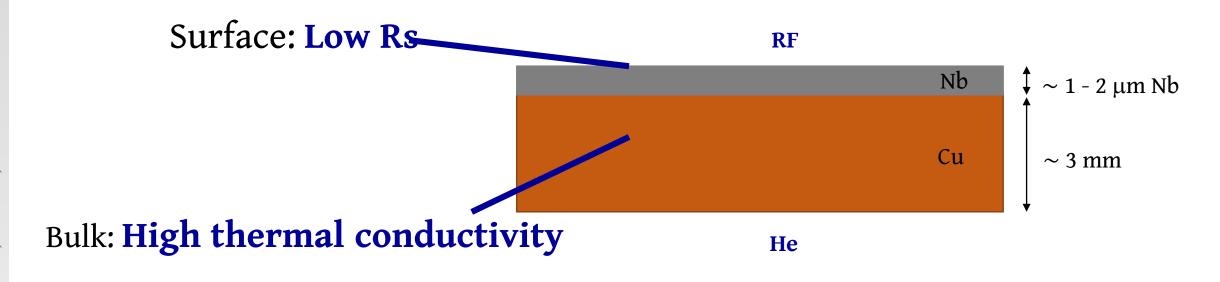


Joachim Tuckmantel Thermal effects in superconducting RF cavities: some new results from an improved program CERN-EF-RF-84-6. - 1984





Change the surface properties

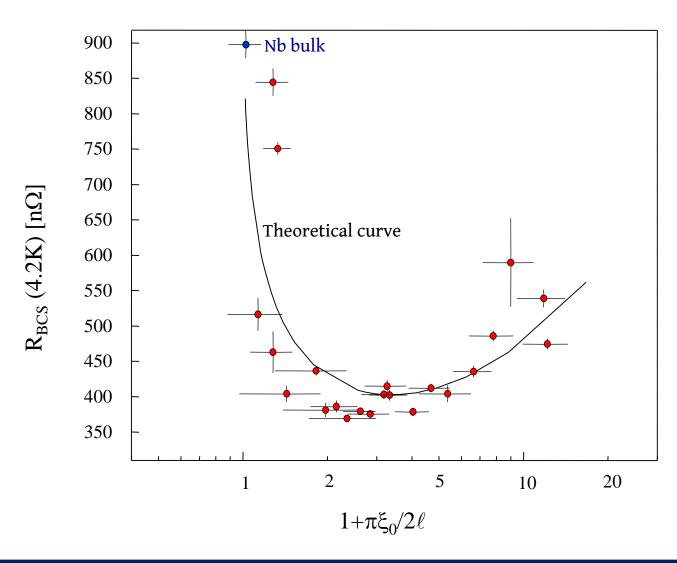


Cu presents high thermal conductivity \rightarrow resistance to quench

Nb surface resistance could be modulated



BCS resistance depends on mean free path



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R_{BCS} @ 4.2 K

Nb bulk: ~900 n Ω

Nb films: $\sim 400 \text{ n}\Omega$

R_{BCS} @ 1.7 K

Nb bulk: $\sim 2.5 \text{ n}\Omega$

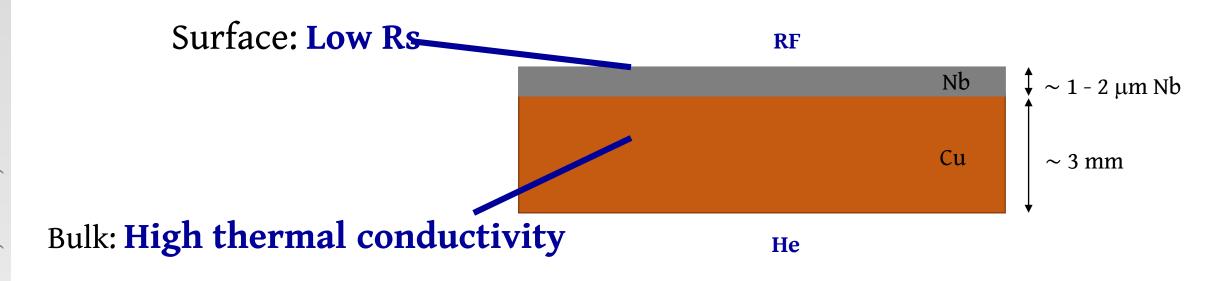
Nb films: $\sim 1.5 \text{ n}\Omega$

Benvenuti C et al 1999 Physica C 316 153





Change the surface properties



Cu presents high thermal conductivity → resistance to quench

Nb surface resistance could be modulated

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Safer handling for the chemical surface treatments



Cu polishing VS Nb polishing

Nb Chemical Polishing

BCP composition (1:1:1 or 1:1:2)

- HF Hydrofluoric acid (49%)
- HNO₃ Nitric acid (70%)
- H₃PO₄ Phosphoric acid (85%)

Nb Electrochemical Polishing

EP bath composition (1:9)

- HF Hydrofluoric acid (49%)
- H₂SO₄ Sulphoric acid (96%)





Cu Chemical Polishing

SUBU5 composition

- sulfamic acid (5g/l)
- hydrogen peroxide 32% (50ml/l)

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- n-butanol 99% (50ml/l)
- ammonium citrate (1g/l)

Cu Electrochemical Polishing

EP bath composition (3:2)

- H₃PO₄ Phosphoric acid (85%)
- N-buthanol (99%)



No HF for Cu polishing

No chemical post treatment on Nb film necessary





Why thin films for SRF?

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Use materials with poor mechanical properties (but excellent SRF properties)

A15 materials (Nb₃Sn, V₃Si, Nb₃Ge, etc.) present high T_c and High H_{c1} but are very brittle: can not be used as bulk materials for SRF cavities

(WAIT THE NEXT LECTURE)

T _C (K)	ρ_{n}	μ_0H_{C1}	μ_0H_{C2}	$\mu_0 H_C$	$\mu_0 H_{SH}$	λ	ξ	Δ	Туре
10(4)	(μΩcm)	(mT)*	(mT)*	(mT)*	(mT)*	(nm)*	(nm)*	(meV)	
7,1		n.a.	n.a.	80		48			ı
9,22	2	170	400	200	219	40	28	1.5	П
17,1	70	20	15 000	230	214	200-350	<5	2.6	II
		4-13	>11 000	100-200	80-160	210-420	5,4		
17,3	35	30				150-200	<5	2.8	II
18,3	20	50	30 000	540	425	80-100	<5	<5	II
15	10-30	30	3 500	430	170	140			II
39	0.1-10	30	3 500	430	170	140	5	2.3/7.2	II- 2gaps**
7,1	68	13	2680- 15000	120	95	100-160	8-10		II- 2gaps**
93		10	100 000	1400	1050	150	0,03/2		d-wave**
38		30	>50000	900	756	200	2	10-20	s/d wave**
	9,22 17,1 17,3 18,3 15 39 7,1	T _C (K) (μΩcm) 7,1 9,22 2 17,1 70 17,3 35 18,3 20 15 10-30 39 0.1-10 7,1 68 93	T _C (K) (μΩcm) (mT)* 7,1 n.a. 9,22 2 170 17,1 70 20 4-13 17,3 35 30 18,3 20 50 15 10-30 30 39 0.1-10 30 7,1 68 13 93 10	T_{C} (K) (μΩcm) (mT)* (mT)* 7,1 n.a. n.a. 9,22 2 170 400 17,1 70 20 15 000 4-13 >11 000 17,3 35 30 18,3 20 50 30 000 15 10-30 30 3 500 39 0.1-10 30 3 500 7,1 68 13 2680-15000 93 10 100 000	T _C (K) (μΩcm) (mT)* (mT)* (mT)* 7,1 n.a. n.a. 80 9,22 2 170 400 200 17,1 70 20 15 000 230 17,3 35 30 100-200 18,3 20 50 30 000 540 15 10-30 30 3 500 430 39 0.1-10 30 3 500 430 7,1 68 13 2680- 15000 120 93 10 100 000 1400	T _C (K) (μΩcm) (mT)* (mT)* (mT)* (mT)* 7,1 n.a. n.a. 80 219 17,1 70 20 15 000 230 214 4-13 >11 000 100-200 80-160 17,3 35 30 30 000 540 425 15 10-30 30 3 500 430 170 39 0.1-10 30 3 500 430 170 7,1 68 13 2680- 15000 120 95 93 10 100 000 1400 1050	T_{C} (K) $(\mu\Omega cm)$ (mT)* (mT)* (mT)* (mT)* (mT)* (nm)*	T_{C} (K) $(\mu\Omega cm)$ (mT)* (mT)* (mT)* (mT)* (nm)*	T_{C} (K) (μΩcm) (mT)* (mT)* (mT)* (mT)* (nm)* (nm)* (meV) 7,1 n.a. n.a. 80 48 9,22 2 170 400 200 219 40 28 1.5 17,1 70 20 15 000 230 214 200-350 <5 2.6 4-13 >11 000 100-200 80-160 210-420 5,4 17,3 35 30 150-200 <5 2.8 18,3 20 50 30 000 540 425 80-100 <5 <5 15 10-30 30 3 500 430 170 140 39 0.1-10 30 3 500 430 170 140 5 2.3/7.2 7,1 68 13 2680-15000 1050 150 0,03/2

^{* @ 0}K





^{** 2}D => orientation problems ?

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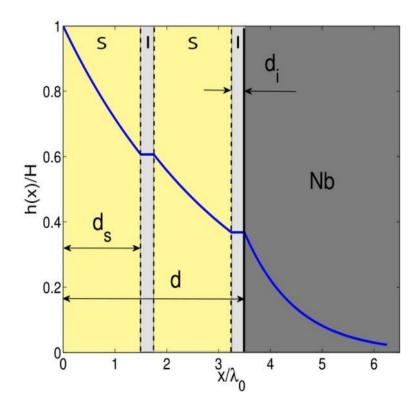
4. Realize complex structures



Realize complex structures

SIS Multilayer

(WAIT THE NEXT LECTURE)



Alex Gurevich, Appl. Phys. Lett. 88, 012511 (2006)



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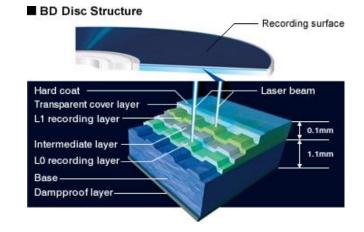


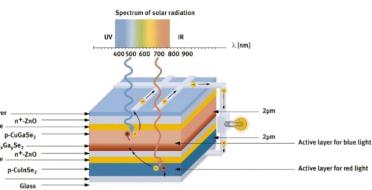
Thin film applications

Some of the most utilized applications of thin film deposition processes include:

- Single and multilayer films and coatings
- · Nanolayered materials
- Optical films for transmission and reflection
- Decorative films
- · Decorative and wear-resistant (decorative/functional) coatings
- · Permeation barriers for moisture and gases
- Corrosion-resistant films
- Electrically insulating layers for microelectronics
- Coating of engine turbine blades
- Coating of high strength steels to avoid hydrogen embrittlement
- · Diffusion barrier layers for semiconductor metallization
- · Magnetic films for recording media
- Transparent electrical conductors and antistatic coatings
- Wear and erosion-resistant (hard) coatings (tool coatings)
- Dry film lubricants
- Composite and phase-dispersed films and coatings
- Nanocomposite materials
- Thin-walled freestanding structures and foils











Thin film deposition techniques

Chemical Deposition

- Plating/Electroplating
- Dip/Spin coating



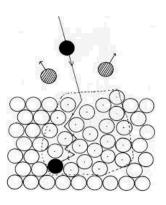
- Thermal CVD
- Plasma Enhanced CVD
- Atomic Layer Deposition (ALD)

Phisical Deposition

Physical Vapour Deposition

- Evaporation
- Laser Ablation
- Plasma Spray
- Sputtering
- Cathodic Arc







Thin film deposition techniques

Chemical Deposition

- Plating/Electroplating
- Dip/Spin coating



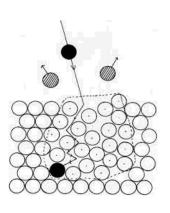
- Thermal CVD
- Plasma Enhanced CVD
- Atomic Layer Deposition (ALD)



Physical Vapour Deposition

- Evaporation
- Laser Ablation
- Plasma Spray
- Sputtering
- Cathodic Arc







PVD deposition techniques

Physical vapor deposition processes (often just called thin film processes) are atomistic deposition processes in which material is vaporized from a solid or liquid source in the form of atoms or molecules and transported in the form of a vapor through a vacuum or low pressure gaseous (or plasma) environment to the substrate, where it condenses

Donald M. Mattox, Handbook of Physical Vapor Deposition PVD) Processing

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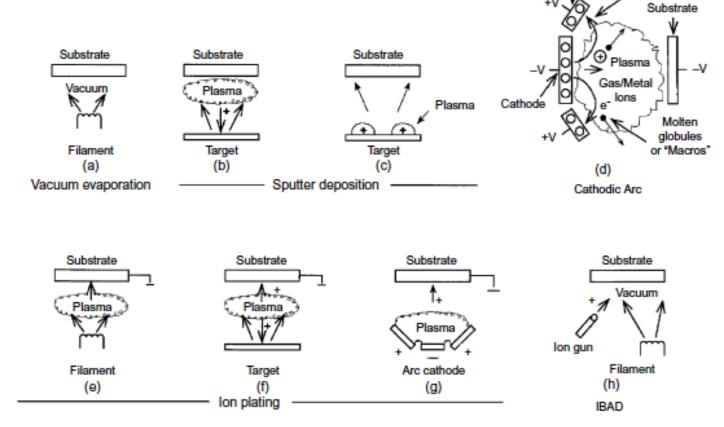
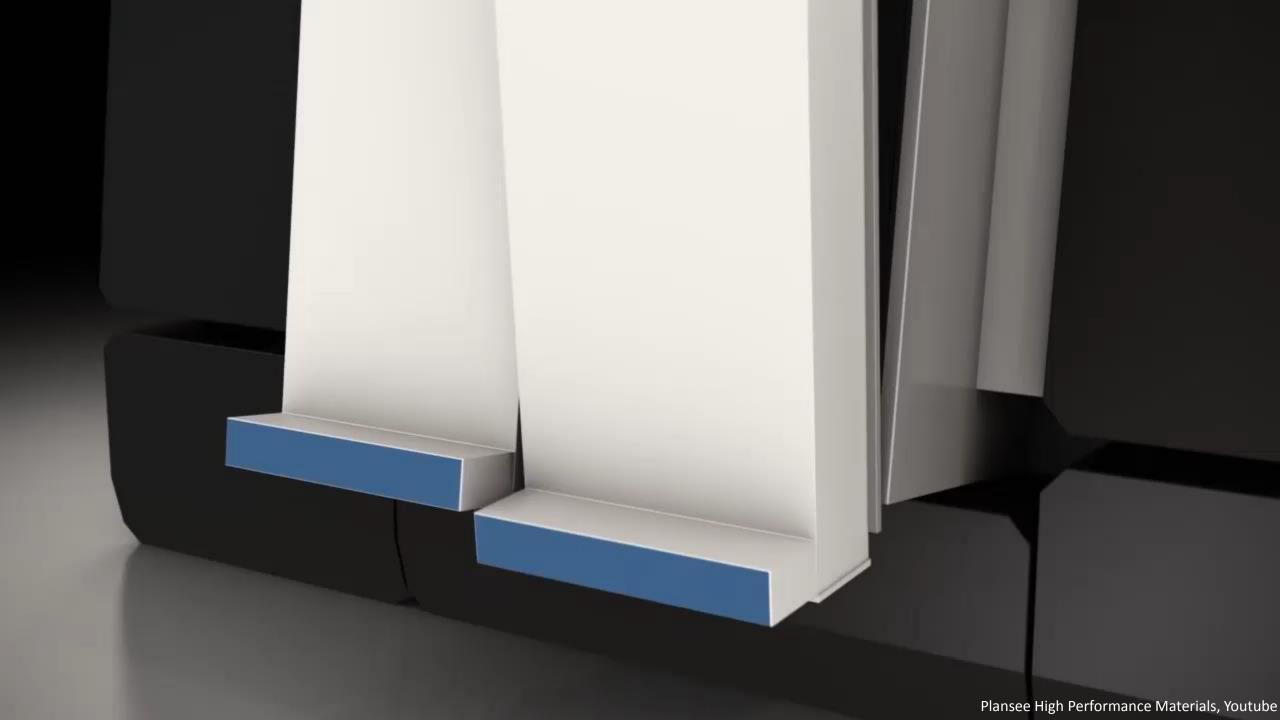


Figure 1.1: PVD Processing Techniques: (a) Vacuum Evaporation, (b) and (c) Sputter Deposition in a Plasma Environment, (d) Sputter Deposition in a Vacuum, (e) Ion Plating in a Plasma Environment with a Thermal Evaporation Source, (f) Ion Plating with a Sputtering Source, (g) Ion Plating with an Arc Vaporization Source, and (h) Ion Beam-Assisted Deposition (IBAD) with a Thermal Evaporation Source and Ion Bombardment from an Ion Gun

water cooled



Interface

The depositing film material may diffuse and react with the substrate to form a "interfacial region"

Nb-Cu case



Abrupt



Graded

Weak chemical reaction between atoms and substrate

Low deposition temperature

Surface contamination

Low nucleation density

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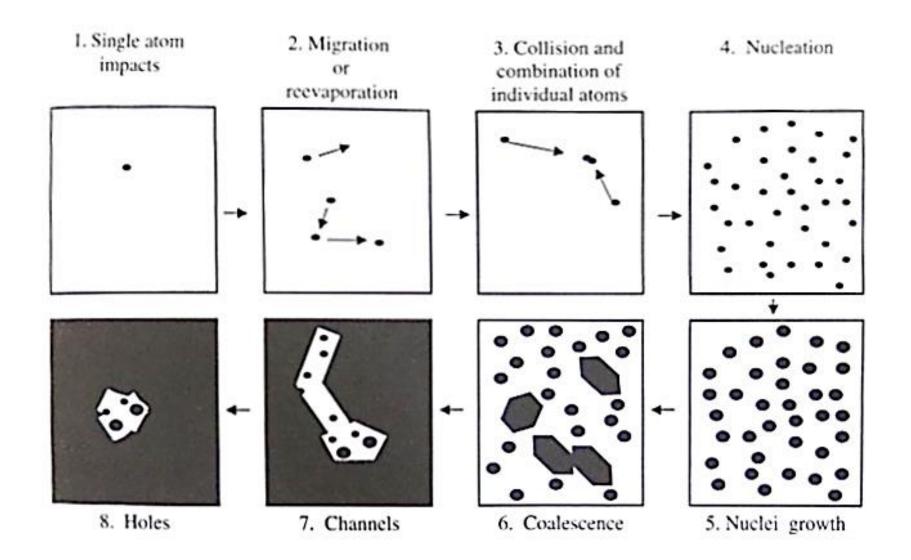
By diffusion (solubility, temperature, time, contaminations)

Chemical reaction (oxygen-active metals on oxide substrates)

By co-deposition or implantation of energetic ions of the material



Nucleation stages

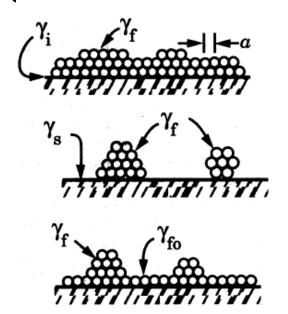




Phases of film growth: Nuclei growth

Nuclei grow by collecting adatoms which either impinge on the nuclei

or migrate over the surface



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binding energy atom-atom < binding energy atom-surface

Layer by layer growth (Frank-van der Merwe)

binding energy atom-atom > binding energy atom-surface

*Island growth (Volmer-Weber)

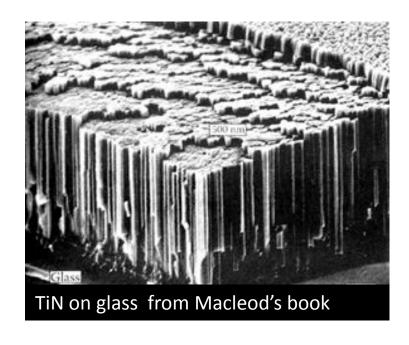
binding energy atom-atom = binding energy atom-surface

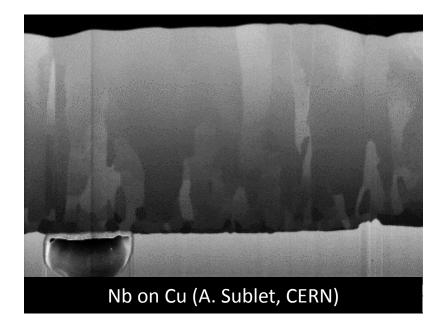
Layer by layer + island growth (Stranski-Krastanov)



Phases of film growth: Film growth

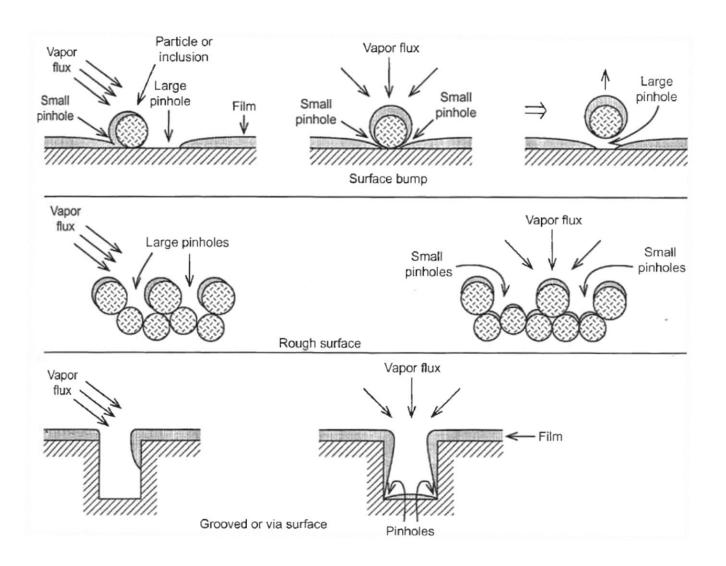
Is the evolution of the nucleation, where arriving atoms are deposited on the previously deposited material Usually exhibits a columnar morphology



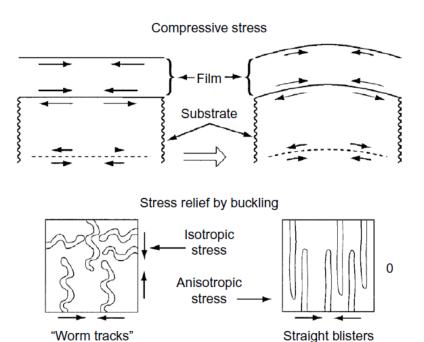




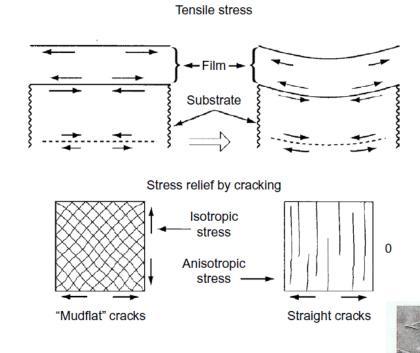
On growth and adhesion



Stress on thin films





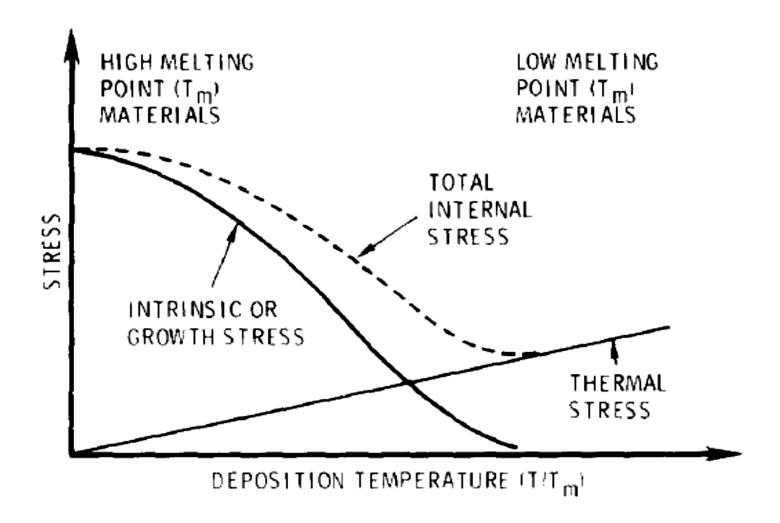


Donald M. Mattox, Handbook of Physical Vapor Deposition PVD) Processing



AS/LI FILM IN TENSION

How to reduce film stress? Temperature effect



J. A. Thornton and D. W. Hoffman, "Stress-related effects in thin films," Thin Solid Films, 1989

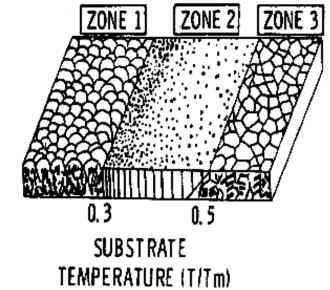


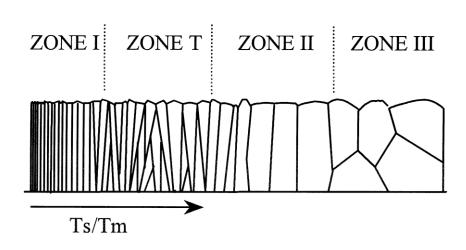


Temperature effect and Structure Zone Diagram (SZD)

- Based on the compilation of the experimental results, it is a guideline for "predicting" the structure of deposited thin films
- 1st proposed in 1969 by Movchan
 & Demchishin for films deposited
 by thermal evaporation.

$$T_h = \frac{T}{T_m}$$
 Homologous temperature

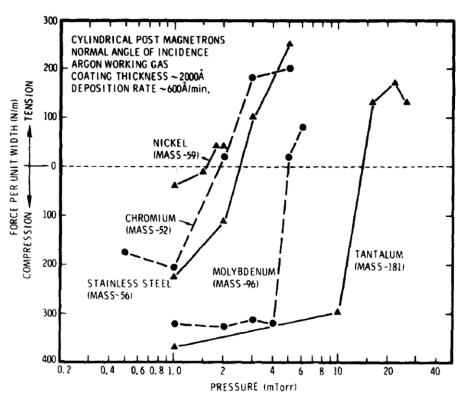






How to reduce film stress? Pressure effect

ZERO STRESS PRESSURE

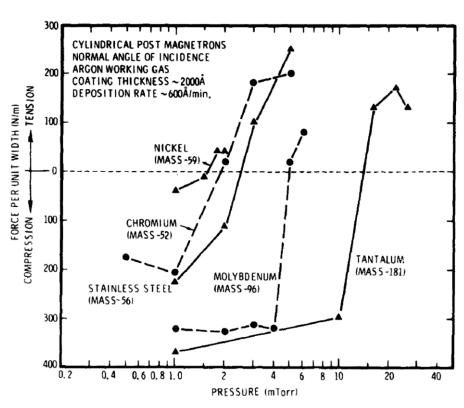


J. A. Thornton and D. W. Hoffman, "Stress-related effects in thin films," Thin Solid Films, 1989



How to reduce film stress? Pressure effect

ZERO STRESS PRESSURE



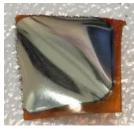
J. A. Thornton and D. W. Hoffman, "Stress-related effects in thin films," Thin Solid Films, 1989



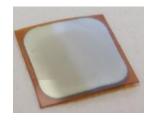
7 · 10⁻³ mbar



9 · 10⁻³ mbar



2 · 10⁻² mbar



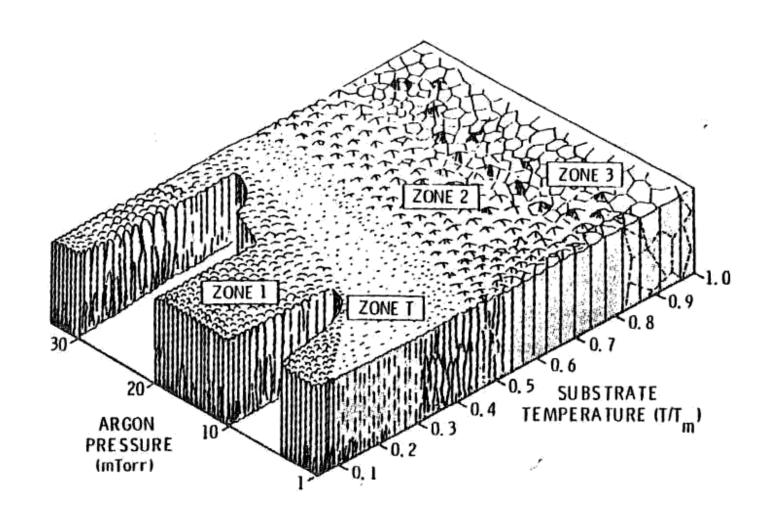
5 · 10⁻² mbar



Thorton Structure Zone Diagram

- ZONE 1: characterized by a fine-grained structure of textured and fibrous grains, pointing in the direction of the arriving vapor flux. The morphology is caused by the low mobility of the adatoms that produce a continued nucleation of grain.
- ZONE T: a dense fibrous structure with a smooth, highly reflective surface. Diffusion is "remarkable" but grain boundary diffusion is strongly limited. Ionic bombardment of the growing film can move the morphology from zone 1 to zone T.
- ZONE 2: surface diffusion sets in, leading to uniform columnar grains.
- ZONE 3: dense films with large grains, drive by bulk diffusion and recrystallization.

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J.A. Thornton and D.W. Hoffman, Thin Solid Films, vol. 171, no. 1, pp. 5–31, 1989



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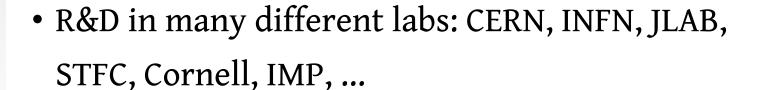
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• R&D on Nb thin films



Nb film is a well known technology

- 288 Nb/Cu cavities installed in LEP @ CERN
- 56 Nb/Cu cavities installed in ALPI @ LNL INFI
- 16 Nb/Cu cavities installed in LHC @ CERN
- 20 Nb/Cu cavities installed in HIE-ISOLDE @ CER





90's LEP2: 350MHz 4-cells



2000's LHC: 400MHz 1-cell



1998-2004 ALPI: 160 MHz QWR

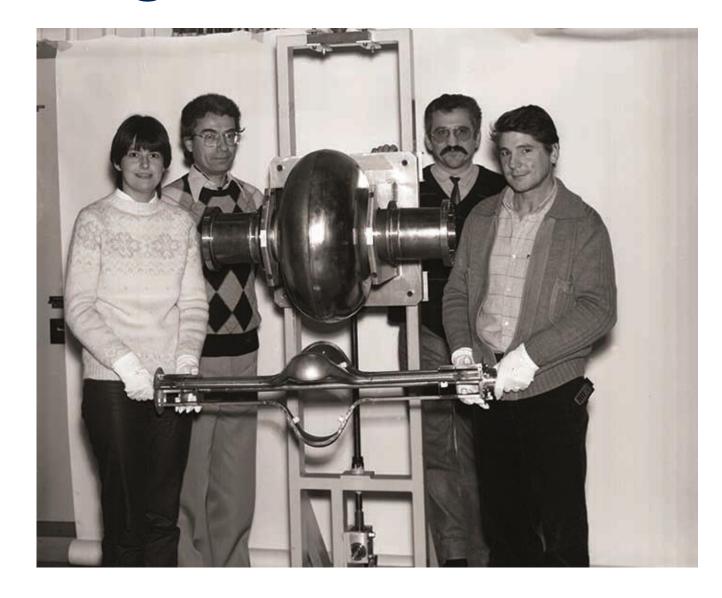


2010's HIE-ISOLDE: 100MHz QWR



LEP2 @CERN

The first prototype niobium-copper superconducting cavity, pictured in December 1983 with Nadia Circelli, **Cristoforo Benvenuti**, Jacques Genest and Max Hauer. Image credit: CERN



Elliptical cavities @CERN - LEP2, LHC and 1,5 GHz R&D

SPUTTERING PARAMETERS (1,5 GHz)

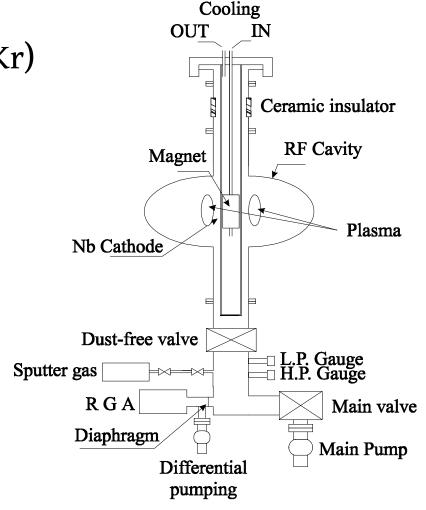
- Sputter gas pressure of 1.5x10⁻³ mbar (Ar or Kr)
- Plasma current stabilized at 3A DC
- Sputter potential ~ -360 V
- Coating temperature is 150 °C
- Thickness: 1.5 µm

SPUTTERING PARAMETERS (1,5 GHz)

- RRR: 11.5 ± 0.1
- Argon content: 435 ± 70 ppm

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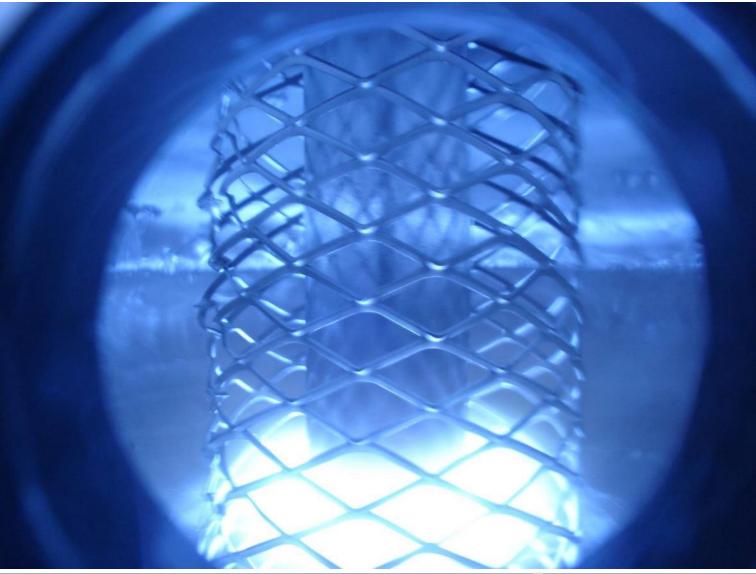
- Grain size: 110 ± 20 nm
- Tc: 9.51 ± 0.01 K

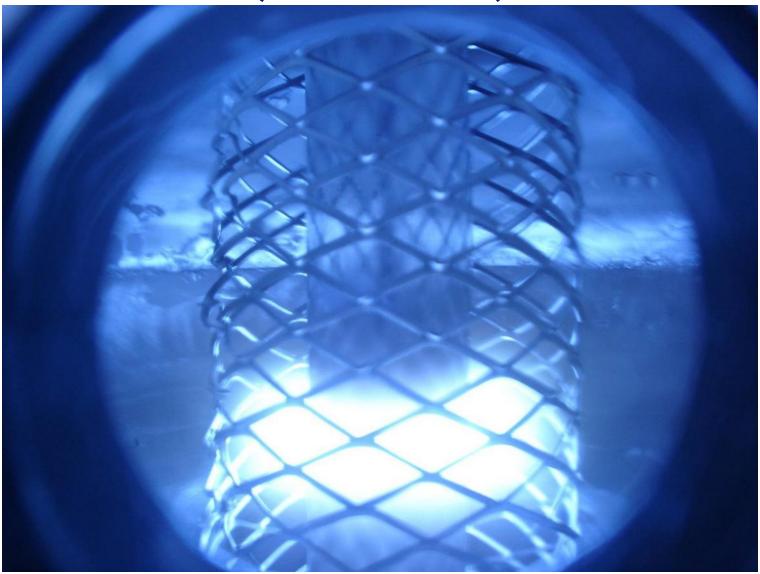


Courtesy of S. Calatroni (CERN)

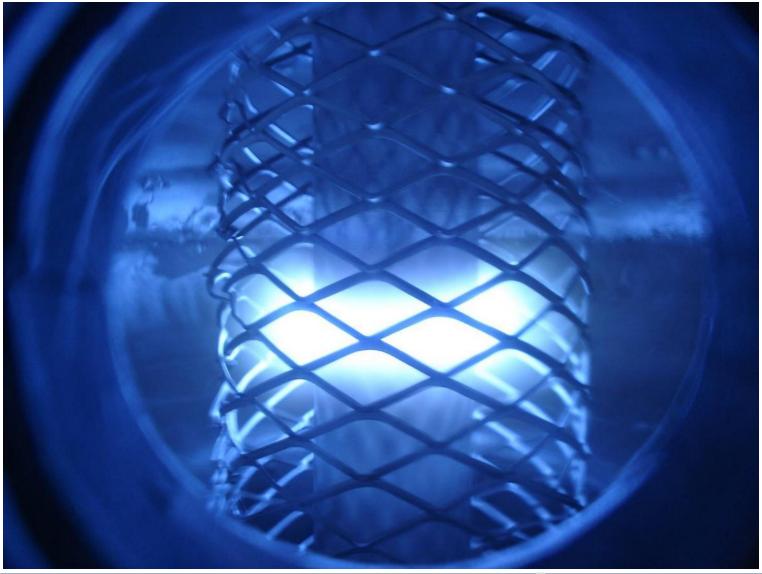






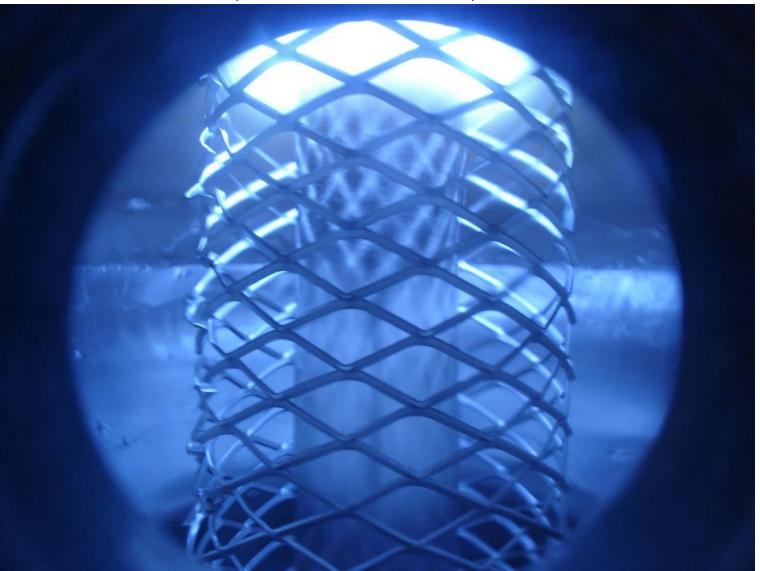




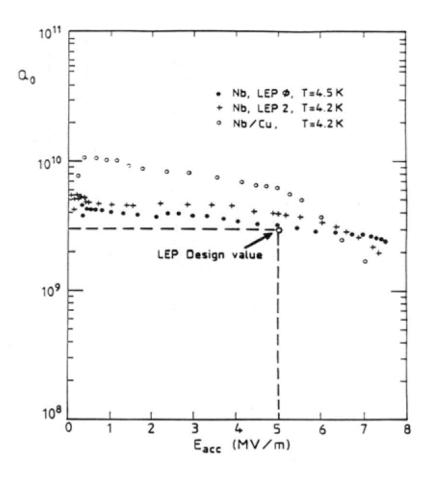








LEP2 Performances



Eight pre-series 4-cell cavities for LEP were built at CERN, the remaining 264 were made by three European industrial suppliers

No thermal quench (contrary to bulk Nb)

Higher performances compare to bulk Nb

Nb bulk cavities performance in the eighties were limited by the poor Nb thermal conductivity (RRR of 40)

Unexpected advantage

G. Arnolds-Mayer et al. 1988 Proc. of the 3rd Workshop on RF Superconductivity





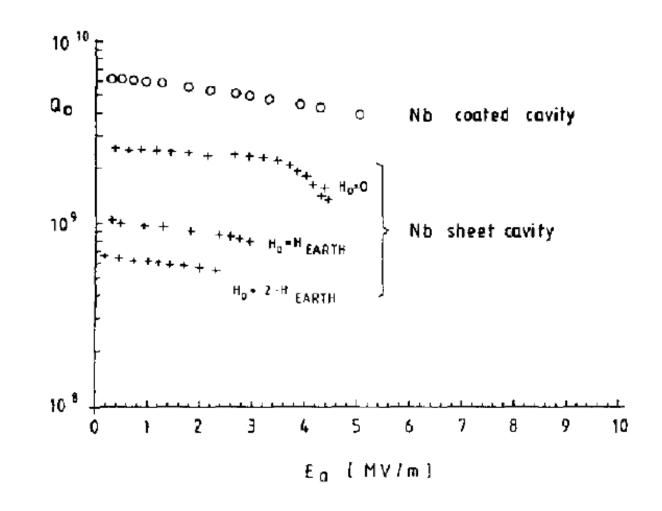
Almost insensitive to the Earth's magnetic field

• Bulk Nb: 100 n Ω /Gauss

• Nb films: $1 \text{ n}\Omega/\text{Gauss}$

cheaper cryostats

Not necessary complex magnetic shielding of the cavities



C. Benvenuti et al. I Physica B 197 (1994)

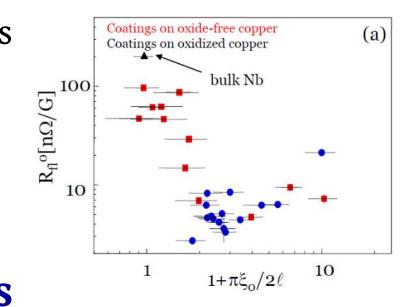


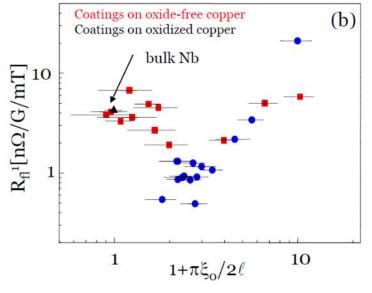


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• Nb films: $1 \text{ n}\Omega/\text{Gauss}$





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$$R_{fl} = (R_{fl}^{0} + R_{fl}^{1} H_{RF}) H_{ext}$$



C. Benvenuti et al., Physica C 316 (1999) 153–188

EASITrain EASIschool 3, Genova 30-09-2020

LHC cavities: from substrate fabrication to installation in the tunnel













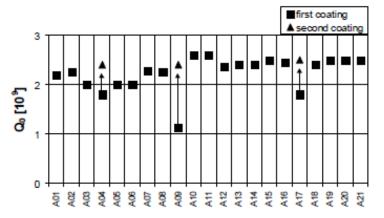
LHC Point 4, ~ 100 m deep shaft → LHC tunnel

Courtesy of A. Sublet (CERN)



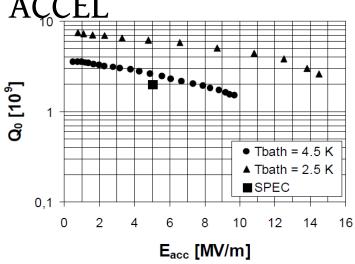
LHC

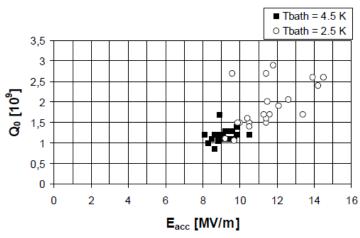




Distribution of cavity quality Q0 at a gradient of Eacc = 5 MV/m and a bath temperature of 4.5 K

21 cavities 400 MHz cavities produced at



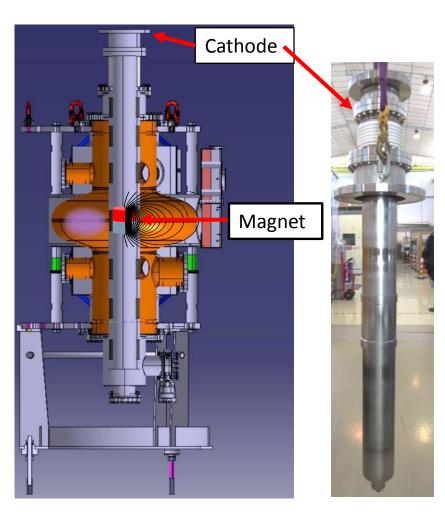


Highest gradients Eacc and quality factors Q0 at the highest gradients achieved at bath temperatures of 4.5 K and 2.5 K

S. Bauer et al., "Production of Nb/Cu sputtered superconducting cavities for LHC," 1999



LHC cavities coating setup

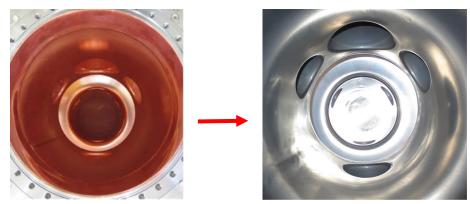


LHC cavity coating setup

- Cavity as UHV chamber (10⁻¹⁰ mbar base vacuum)
- Cavity = anode, grounded
- Nb cylindrical cathodes tubes
- movable electromagnet inside, liquid cooled
- → DC-magnetron sputtering, 6 kW, 1.10⁻³ mbar Kr
- → Cavity bake-out (bake-out tent) to 180°C
- → Coating 7 steps for the 7 different electromagnet positions
- → Duration = 1h 20' at low temperature (150°C)
- → Nb layer thickness ~ 2 mm



8 spare cavities produce

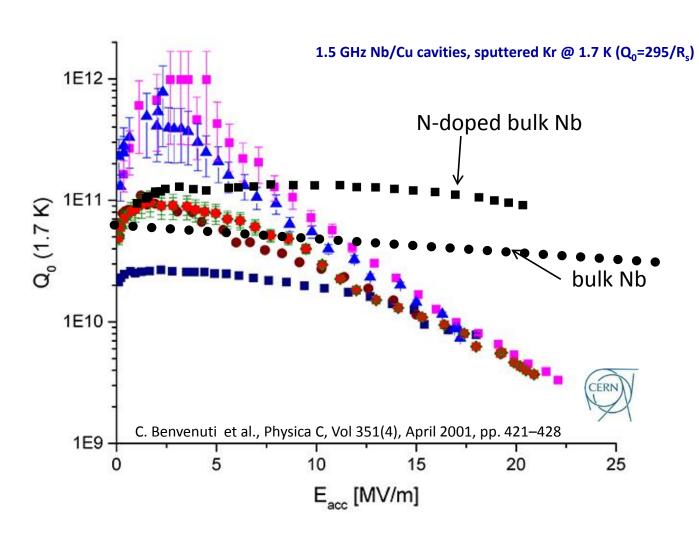


Before and after coating views from cavity main aperture

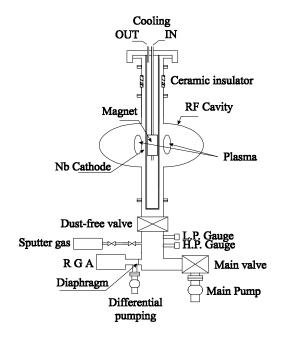
A. Sublet, Thinfilms Workshop 2018



R&D on 1,5 GHz - State of the art for Nb-Cu cavities



Cristian Pira



High Q at low field

Strong Q-slope still present



Increasing complexity: Quarter Wave Resonator



ALPI @ LNL - 160 MHz QWR



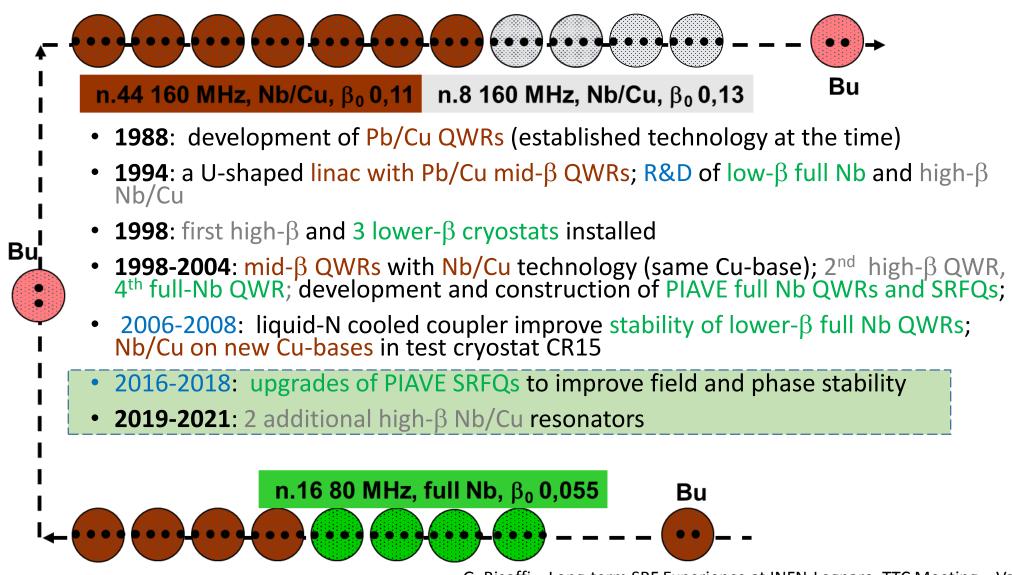




A more complex geometry than elliptical cavities

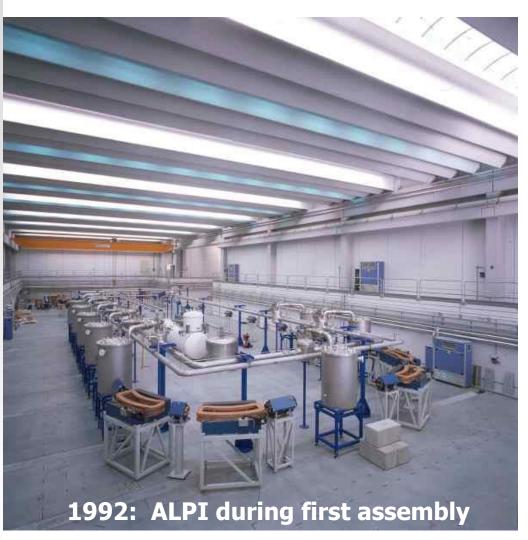


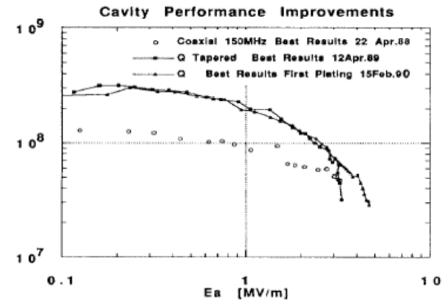
QWR in ALPI @ LNL INFN





The early ALPI with mid-β Pb/Cu QWRs





 $E_a = 2.3 \div 2.7 \text{ MV/m}$ $\beta_0 = 0.11$

Reliable operation

Cheaper than full Nb, mechanically stable, not susceptible to quench, ideal for complicated geometries

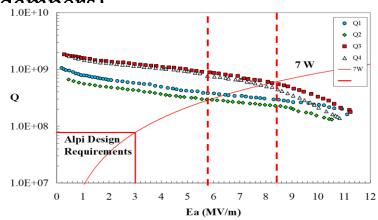
Limited performance, and some degradation





First 80 MHz low-β full Nb cavity in 1993

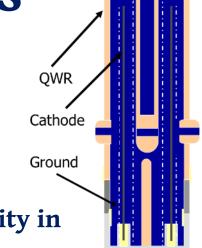
(double wall thin Nb outer conductor, equipped with original mechanical



Off-line O-curves: 6+8 MV/m at 7 W

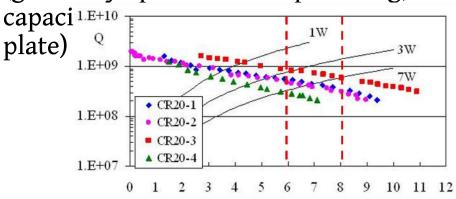






First 160 MHz high-b Nb/Cu cavity in 1993

(geometry optimized for sputtering,



Ea [MV/m] Off-line Q-curves: 6+8 MV/m at 7 W

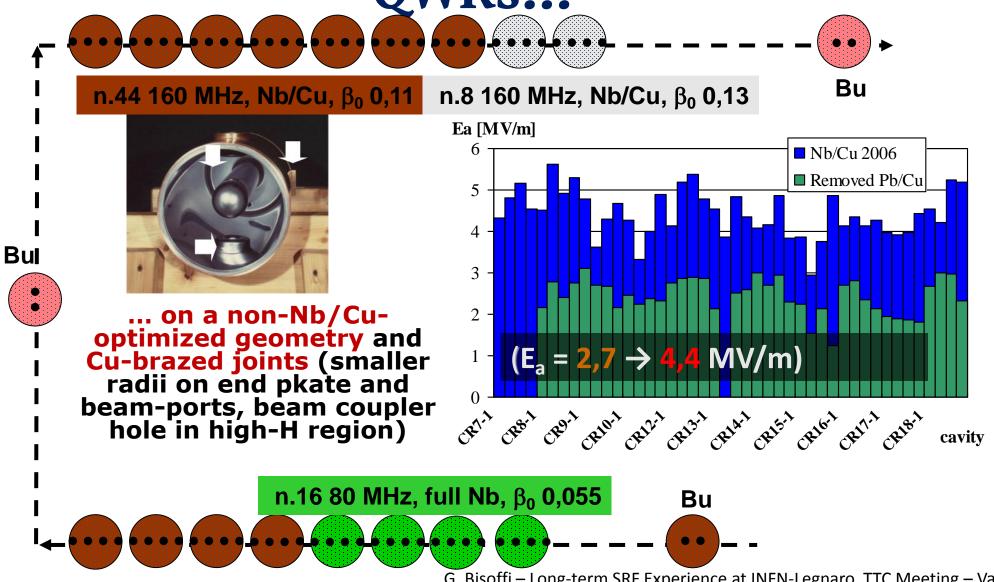
> Higher mechanical stability Less sensitive to microphonic

G. Bisoffi – Long-term SRF Experience at INFN-Legnaro, TTC Meeting – Vancouver 2019



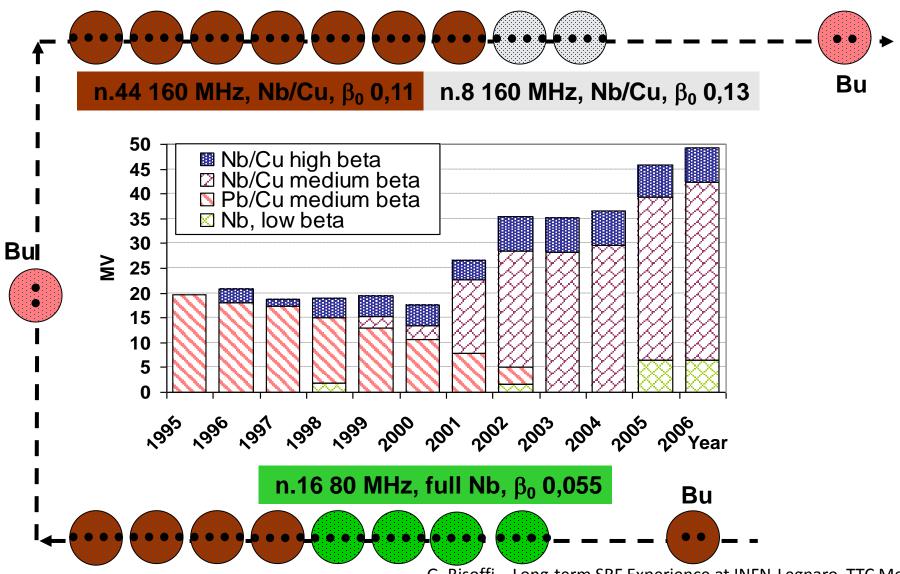


The next step: apply Nb/Cu to mid- β **QWRs**





ALPI V_{eq} from 20 to 48 MV





ALPI QWR - Effect of the substrate

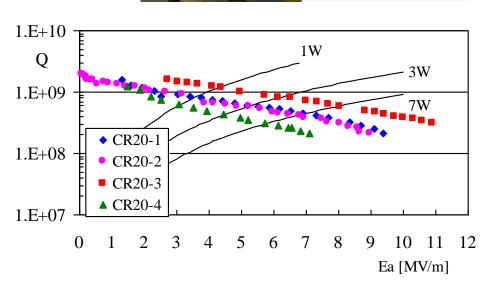
High β QWRs (β =0.13, 160 MHz)

Drilled by a billet of OFHC Cu, 99.95% grade

No brazed joints, beam ports jointed by indium gaskets

Rounded shorting plate



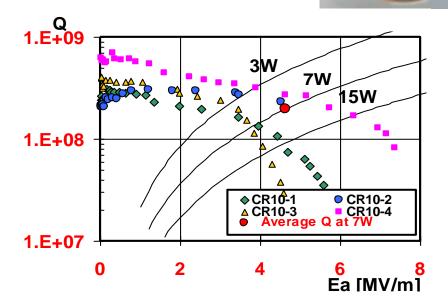


Medium β QWRs (β =0.13, 160 MHz)

Brazed joints (especially the ones in the outer resonator surface)

Flat shorting plate

Beam ports shape



A. Porcellato, Nb Sputtered Cu QWR, Thin Films Workshop LNL 2006



Nb thin films

Nb/Cu sputtering advantages

Mechanical stability (mechanical vibrations are not an issue)

Frequency not affected by changes He bath Dp (<0.01Hz/mbar)

Reduced over-coupling (smaller amplifier, coupler do not need cooling, rf lines have reduced size and limited rf dissipation)

High thermal stability (less prone to hot spots, conditioning easier)

Stiffness (in case of loss of isolation vacuum leak)

Absence of Q-disease (less demand on cryogenic system cooling velocity and reliability)

Insensitivity to small magnetic fields (no magnetic shielding)

High Q of the N.C. cavity (easier coupling in N.C state)

Absence of In vacuum joints (vacuum leaks less probable)

Price (both material and construction)

The lower performance of Nb/Cu cavities at high fields, due to the more pronounced Q-slope of Nb/Cu resonators, is not an issue in QWRs as it is in b>0.5 cavities, because beam dynamic constraints require to limit the accelerating gradient in the low b section of linacs to values well reachable by Nb sputtered resonators

A. Porcellato, Nb Sputtered Cu QWR, Thin Films Workshop LNL 2006



ALPI QWR - Substrate preparation

- Electropolishing (20µm, 2 hours)
- Rinsing (water, ultrasonic water, HPR)
- Chemical polishing (10μm, 4 min, SUBU5
- Passivation (sulphamic acid)
- Rinsing (water, ultrasonic water, HPR)
- Drying (ethanol, nitrogen)





ALPI QWR - Sputtering process



QWR (-130 V) Cathode (-800 V) Grids (0 V)

Parameters

Argon pressure: 0.2 mbar Substrate T: 300-500°C

Film characteristics

Thickness: 1-2 microns

RRR: 9-20

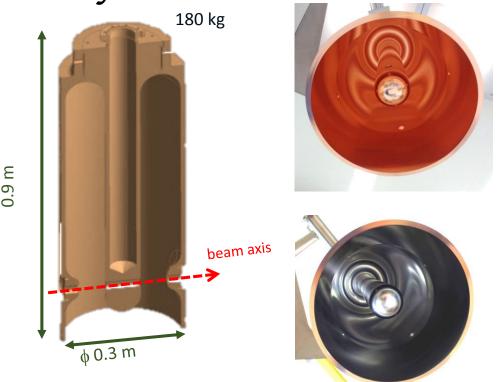


A. Porcellato, Nb Sputtered Cu QWR, Thin Films Workshop LNL 2006

HIE-ISOLDE @ CERN

Superconducting linear accelerator for energy upgrade of ISOLDE radioactive ion beam

facility



Cristian Pira



Cryomodule clean room assembly



4 cryomodules in HIE-ISODLE Linac



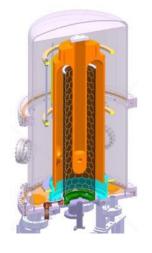
Courtesy of A. Sublet (CERN)

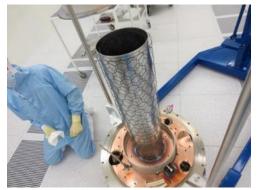
HIE-ISOLDE @ CERN

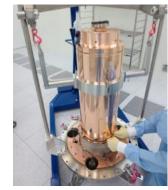
Nb thin films

Same sputtering configuration as in ALPI Clean room assembly improvement









Cavity in UHV chamber (10⁻⁸ mbar base vacuum)

3D-forged Cu cavity substrate, biased at -80 V

Nb cylindrical cathode used on both sides, not cooled

DC-bias diode sputtering, 8 kW, Ar 0.2 mbar

Coating at high temperature (300 \rightarrow 620°C)

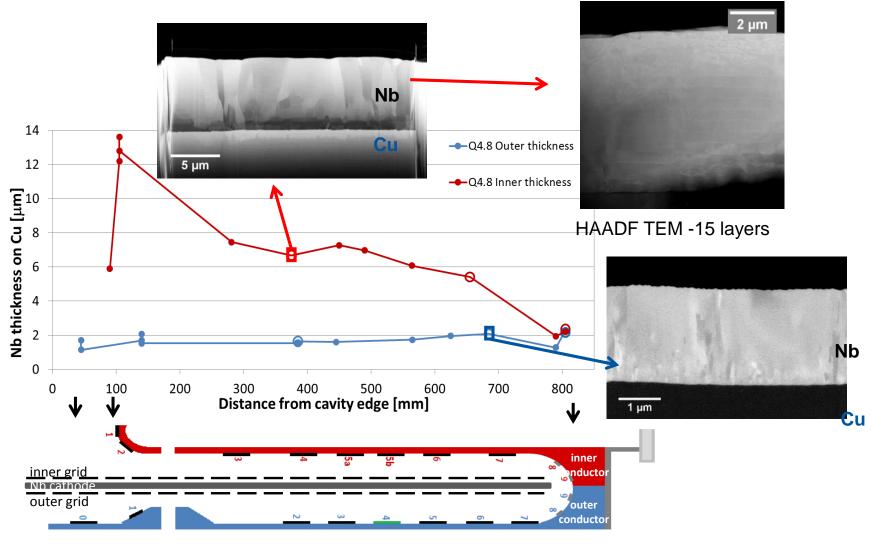
Done in 15 run/cool-down cycles (4 days)

Nb layer thickness ranging from 1.5 mm to 12 mm

Courtesy of A. Sublet (CERN)



HIE-ISOLDE film characteristics

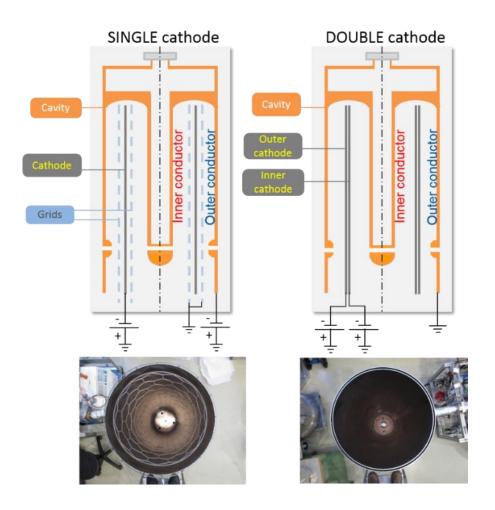


→ Influence of "multilayered" Nb film/dislocations/morphology on the RF performances?

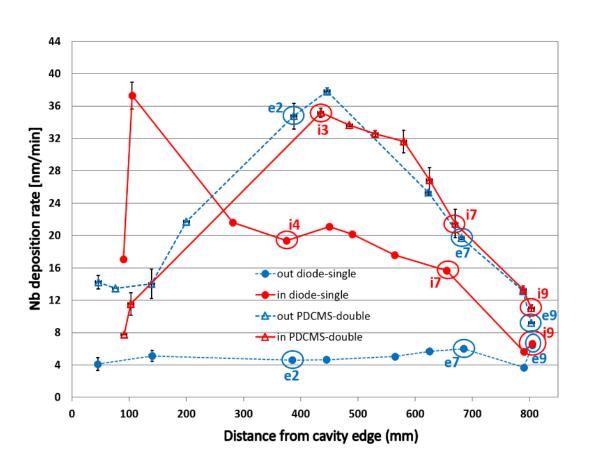




HIE-ISOLDE: double cathode scheme **DCMS**



Cristian Pira



→ Decouple inner/outer plasma, independent power control: tune layer uniformity



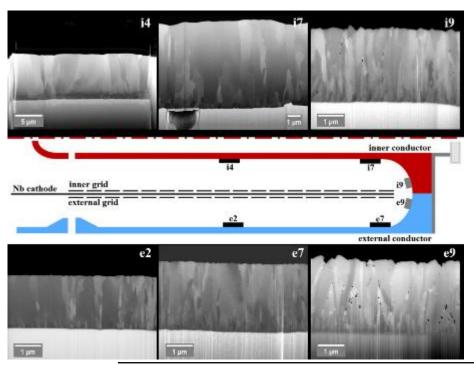
66



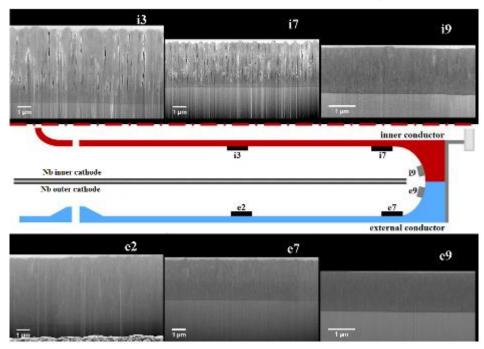
HIE-ISOLDE layer morphology

diode

p-DCMS



Cristian Pira



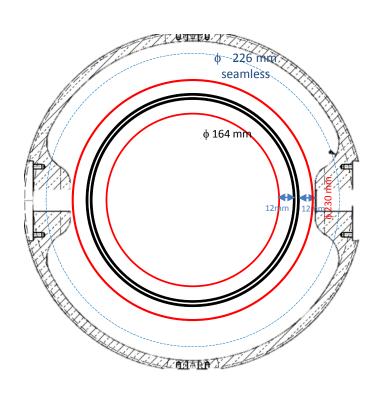
Technic	Que Cathod scheme		Magnetic field[G]	Cathode(s) power [kW]	Duration [min]	Energy [kWh]
Diod	e Single	2x10 ⁻¹	none	8 (5.4 in, 2.6 out)	345	43 (29 in, 14 out)
Pulsed D	CMS Double	e 1.6×10 ⁻²	118	2 in, 4.5 out	145	4.4 in, 9.8 out

- → Denser film outer and at the top in pulsed DCMS, but rough and porous on the inner
- → Geometry and transport at low pressure in DCMS may explain these observations

A. Sublet (CERN), Thinfilms Workshop, LNL 2018



HIE-ISOLDE double cathode + grids





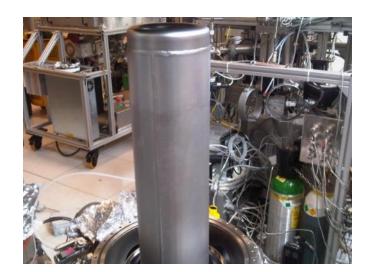


- → Bias on cavity (as for single cathode diode baseline) with diode or (p-)DCMS
- → Densify film by ion bombardment assistance



HIE ISOLDE R&D @LNL





Helicoidal magnetic







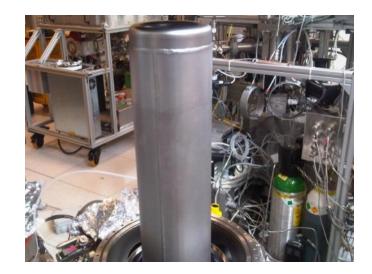
D. Franco, PhD Thesis



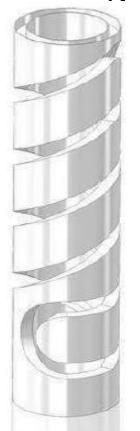


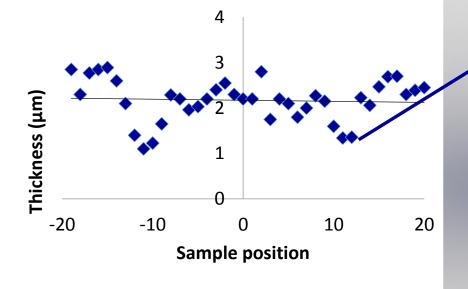
HIE ISOLDE R&D @LNL





Helicoidal magnetic configuration





Good thickness uniformity

R&D stopped due to difficulties in the handling of the chemical polishing

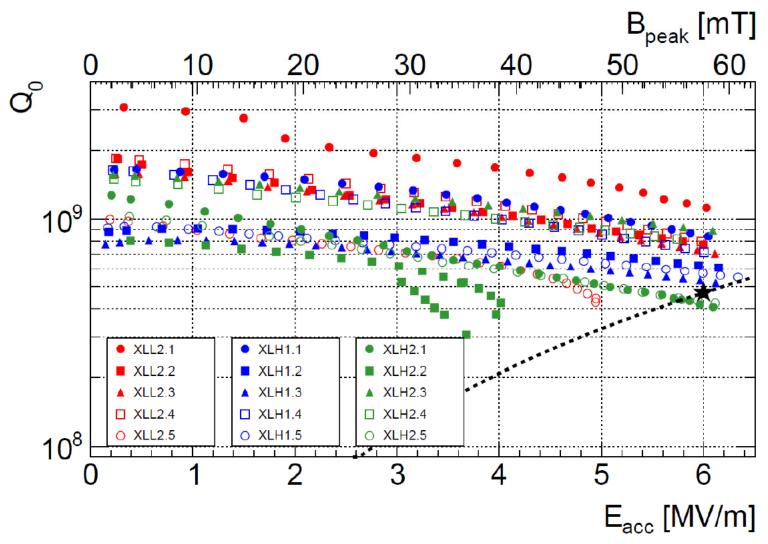
(HIE ISOLDE QWR larger than ALPI QWR)

D. Franco, PhD Thesis





HIE-ISOLDE QWR Performances

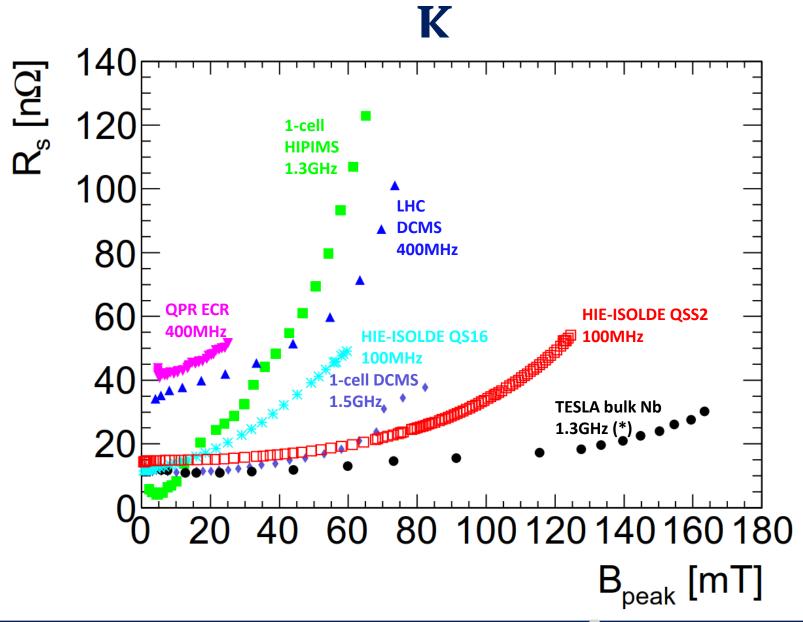


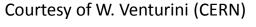
Courtesy of W. Venturini (CERN)





State of the art of Nb-Cu films around 2

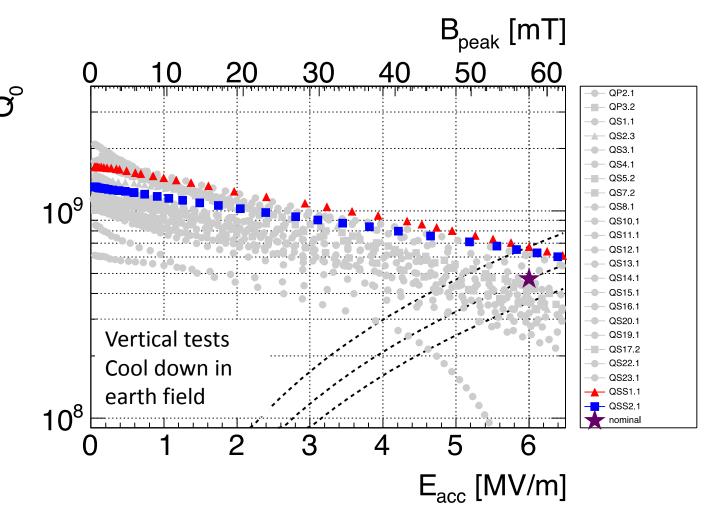


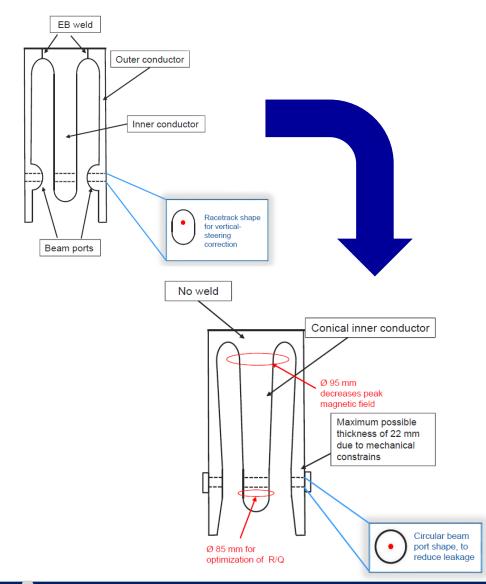






HIE-ISOLDE QWR Seamless Design



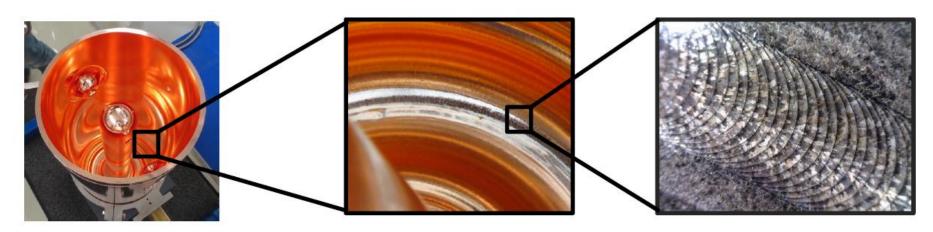


Courtesy of W. Venturini (CERN)

Cristian Pira



Motivation through the seamless design











→ Source of chemicals trap/release



Courtesy of A. Sublet (CERN)





QWR Main Lesson learned: the substrate is important!

Nb thin films



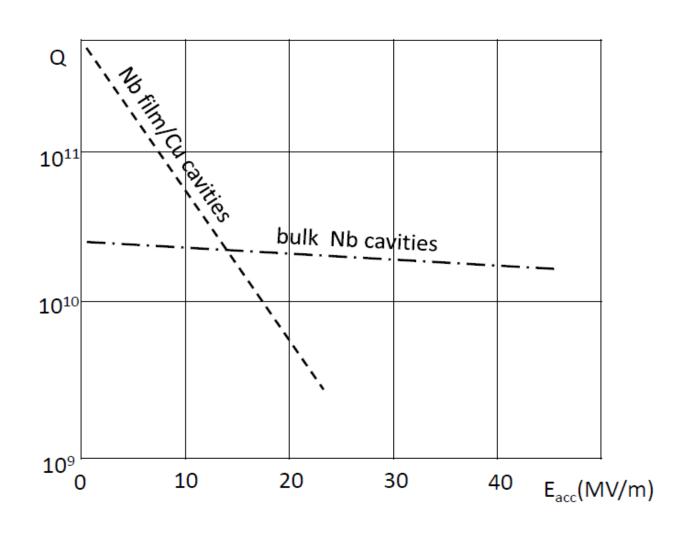
Outline

- Motivation for thin films in SRF cavities
- How to realize a thin film coating?
- State of the art in Nb thin films (accelerators using thin film technology)
- Characteristics of Nb films
- R&D on Nb films

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Q-slope problem



Cristian Pira

Unsolved problem since 1990s

Several theory proposed

Depinning of trapped flux

Low HC1

Early vortex penetration due to roughness

Grain boundaries

Bad thermal contact at the interface

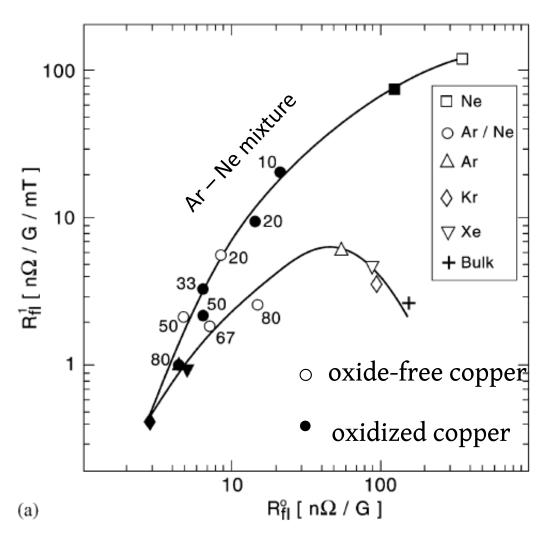
Not intrinsic problem of the films

Substrate is important



Nb thin films

Effect of the gas

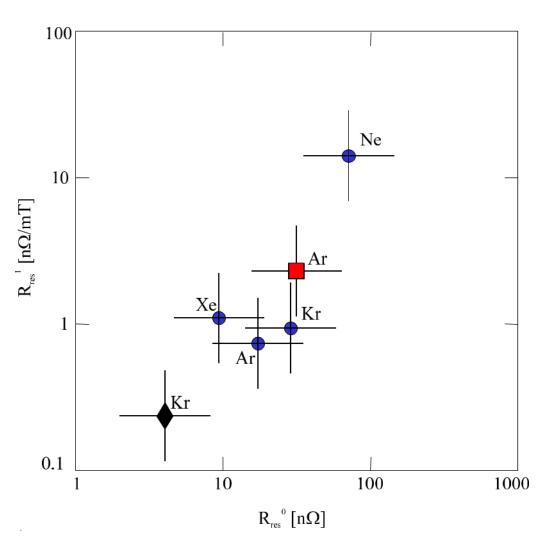






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Effect of Polishing



Cristian Pira

Average roughness of chemically polished spun cavities: 0.2µm

Average roughness of chemically polished hydroformed cavities: 0.8µm

Average roughness of electropolished spun cavities: 0.04µm Absence of defects (etching pits)

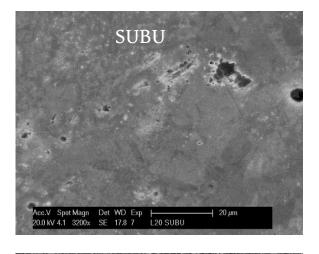
EP seems better than

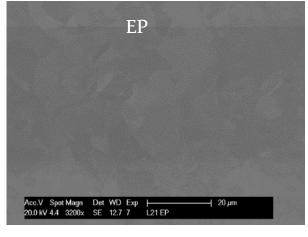


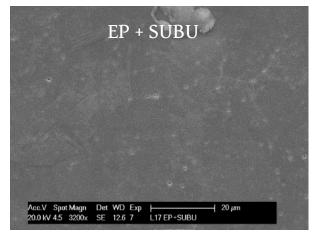


Effect of Polishing

Cu

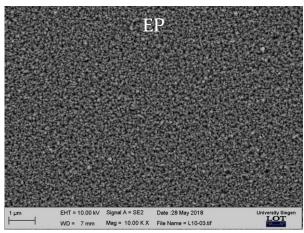


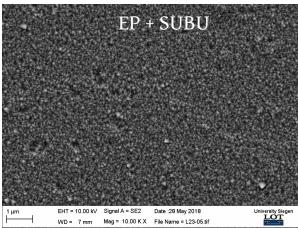




Nb film





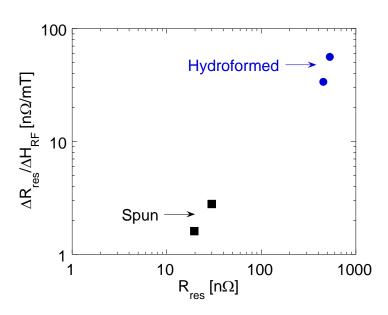


PVD film mimate the surface morphology

ARIES Collaboration (2018)



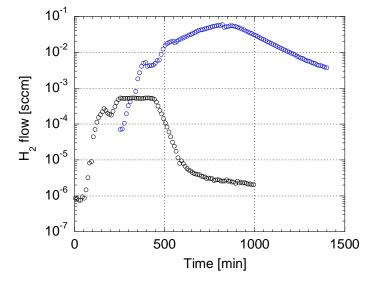
Effect of the Cu substrate forming process



Cristian Pira

Coatings on oxide-free hydroformed cavities consistently worse than for spun cavities? Why?

Possible answer: a larger quantity of **hydrogen** was migrating into the film from the hydroformed cavity

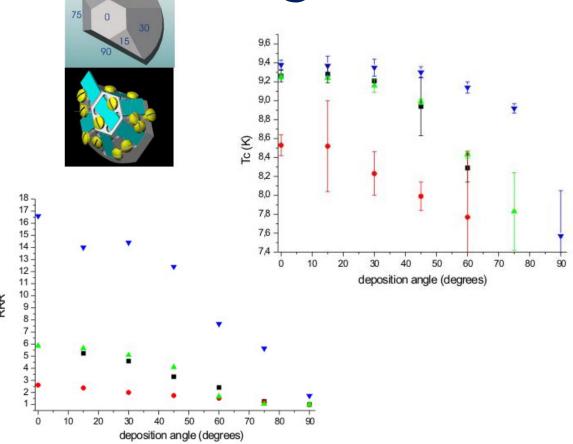


S. Calatroni (CERN), SRF 2001

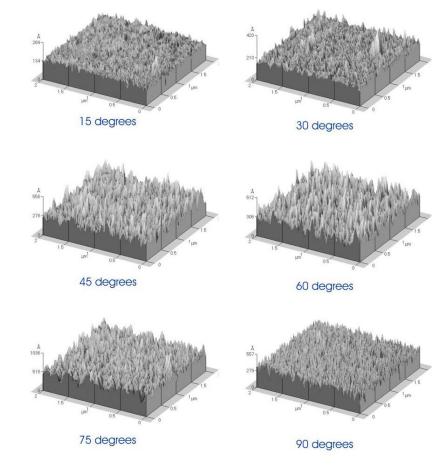




Angle of incidence of coating



Superconducting properties of niobium films depends on deposition angle between target



The effect is related to change in the coating morphology

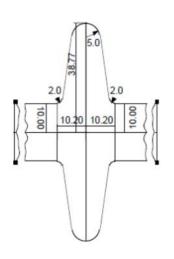
D. Tonini et al, Morphology of niobium films sputtered at different target-substrate angle, SRF99, THP11



Nb thin films

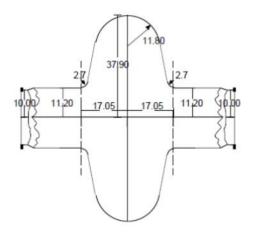
Angle of incidence of coating

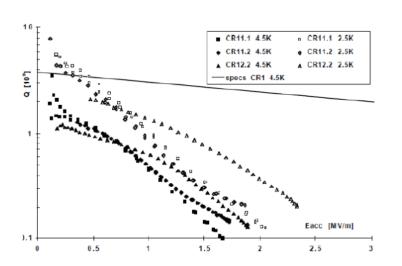
 $\beta = 0.48$

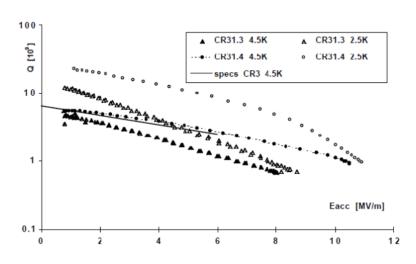


 $\beta = 0.8$

Cristian Pira







C. Benvenuti et al, Production and test of 352 MHz Niobium Sputtered Reduced Beta cavities, 1997, SRF97D25



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Nowadays the research is mainly focused on film morphology improvement





Next generation Nb films

ALL film properties are a direct consequence of the film structure, defect/impurity content... thus the technique, environment, substrate are key factors

Full control of the deposition process & tailored SRF performance

UNDERSTANDING OF

- ☐ The **chemistry** of the involved species
 - Reactivity
 - Stoichiometric sensitivity
 - Reaction process temperatures
 - stal structure **dependence on substrate structure**uence of deposition energy on resulting structure
 - sitivity to the presence of contaminating species, defects
 - **Mization** of desired film against subsequent **degradation**

Careful characterization of the attained composition and microstructure (RHEED, STM, XRD, EBSD, AFM, optical profilometry, XPS, SIMS, TEM, FIB).

Close association with resulting RF surface impedance & superconducting properties (λ , Δ , T_c, H_c, RRR)

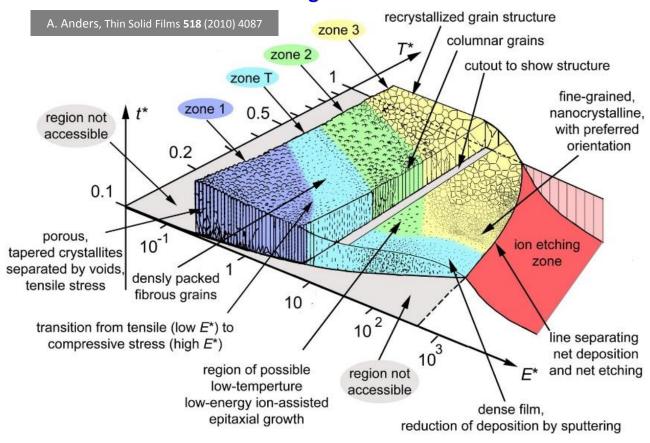
A-M Valente, SRF2017 Tutorials





Energetic Condensation

Generalized Structure Zone Diagram



Cristian Pira

Additional energy provided by fast particles arriving at a surface:

- residual gases desorbed from the substrate surface
- chemical bonds may be broken and defects created thus affecting nucleation processes & film adhesion
- enhanced mobility of surface atoms

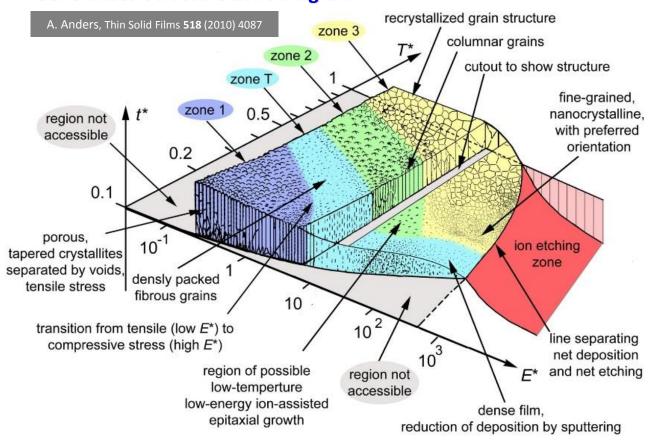
Changes & control in:

- Film density
- morphology
- microstructure
- Stress
- low-temperature epitaxy



Energetic Condensation

Generalized Structure Zone Diagram



Cristian Pira

A variety of techniques with distinct technologies

- Vacuum Arc Plasma & Coaxial Energetic Deposition (CED)
- Electron cyclotron Resonance (ECR)
- High Impulse Power Magnetron sputtering (HiPIMS)

Cathodic Arc Deposition

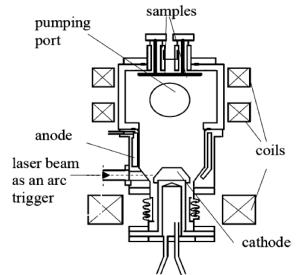
INFN/Poland CARE program (R. Russo et al.) Alameda Applied Science Corporation (M. Krishnan et al.)

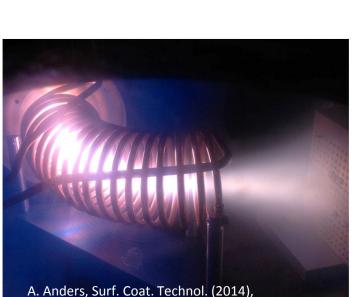


Cathodic Arc Deposition

- The Nb vapor is almost fully ionized
- In the plasma arc an electric discharge is established directly onto the Nb target, producing a plasma plume from which ions are extracted and guided onto the substi by a bias and/or magnetic guidance
- Magnetic filtering (and/or arc pulsing) is also necessary to remove droplets
- A **trigger** for the arc is necessary: either a third electrode, or a laser
- Arc spot moves on the Nb cathode at about 10 m/s
- Arc current is 100-200 A (~ 35 V)
- Voltage bias on samples 20-100 V

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Nb droplets

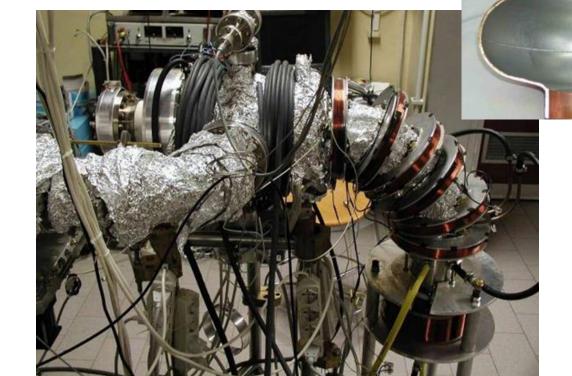




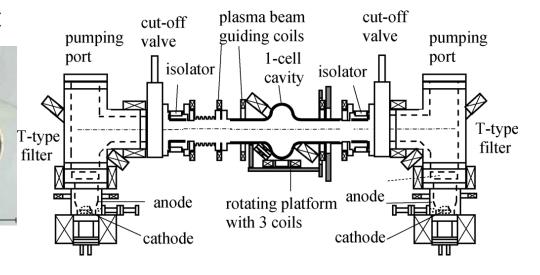
UHV Arc Nb thin films, INFN/Poland CARE project

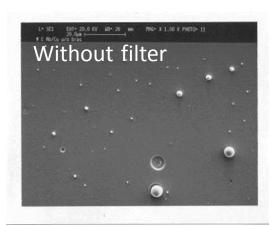
RRR up to 80 was reported with substrate heated to 200°C

No cavity measured



Cristian Pira







RUSSO, Thinfilms Workshop, LNL 2006

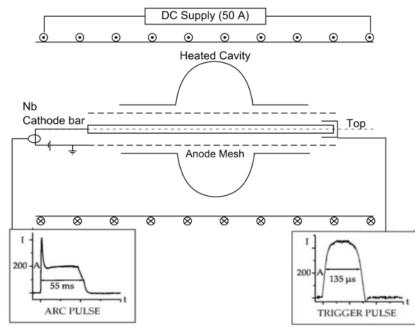


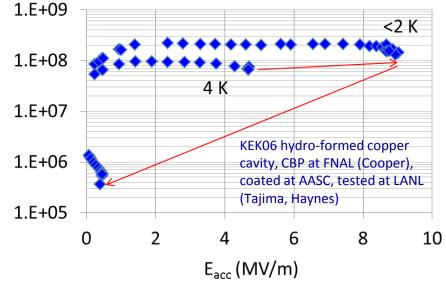
Coaxial Energetic Deposition (CEDTM) - AASC

- CED coater uses "welding torch" technology
- Arc source is scalable to high throughputs for large scale cavity coatings
- ~1 monolayer/pulse ~0.2 ms
- Good structure, RRR but presence of macro-particles

Cristian Pira







The difference between 4K and 2K is smaller than expected: BCS resistance should be about 40x less if all the surfaces are Nb.
Suggests presence of areas not well coated well and lossy presence of macro-particles

M. Krishnan, Thinfilms Workshop, LNL 2014





HiPIMS

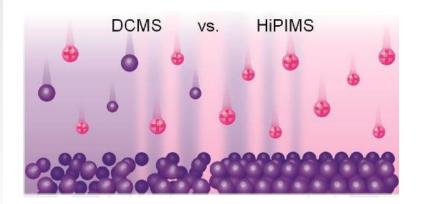
CERN (G. Rosaz et al.)
Jefferson Lab (A-.M. Valente et al.)
STFC ASTeC (R. Valizadeh et al.)
Siegen University (M. Vogel et al.)

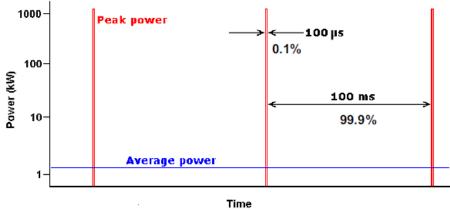
Lawrence Berkeley National Laboratories (A. Anders et al.)

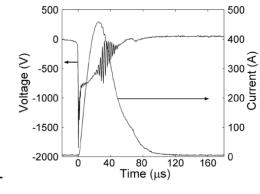


HiPIMS

- Pulsed sputtering where the peak power exceeds the average power by typically two orders of magnitude
- The target material is **partially** ionized
- Large concentration of ions producing high-quality homogeneous films
- Possibility to self sustain discharge







Very high purity Excellent adhesion better (normal) conductivity, Large crystal grains, low defect density Suppression of fiber structure Superior density

Decreased roughness

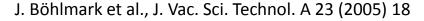
Homogeneous coating even on complex-shaped surfaces

Phase composition tailoring

Interface engineering

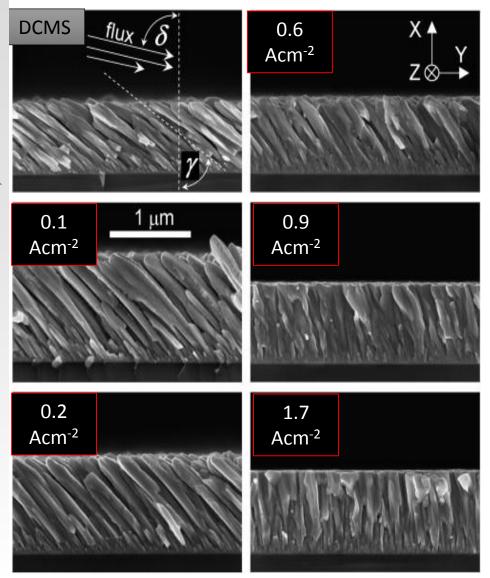


Lower coating rate: ions captured at the cathode Very sensitive to cathode surface state (roughness), induced arcing

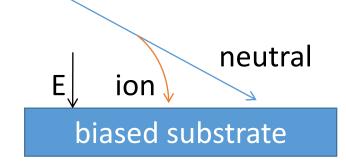




Conformal Coating



Inclination of columns is reduced at high target current densities due to high ion-to-neutral ratio

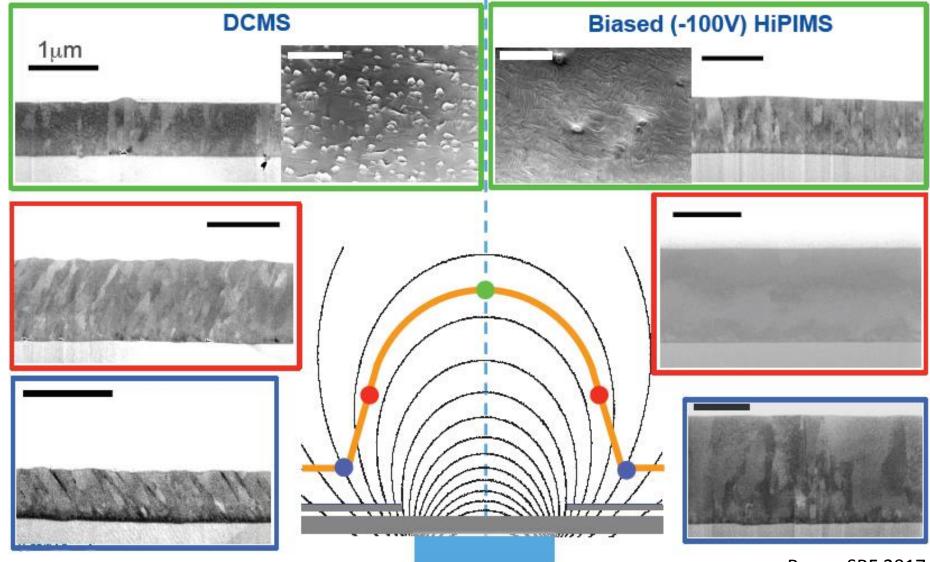


CrN Glancing Angle Deposition

G. Greczynski, et al., Thin Solid Films 519 (2011) 6354.

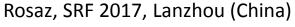


Conformal HiPIMS @CERN





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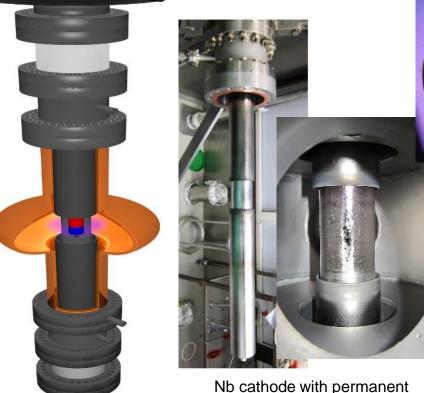


CERN HiPIMS Setup

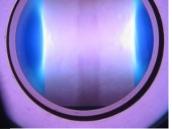


1.3 GHz cavity coating setup

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Nb cathode with permanent magnets inside and Nb anodes



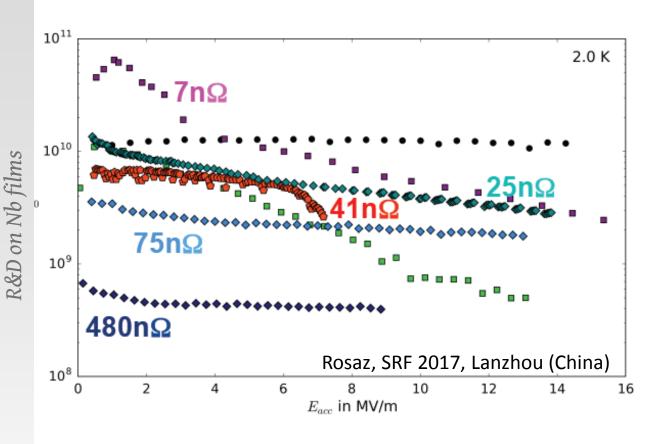
HiPIMS discharge

Same hardware as for DCMS

- Pulsed Power supply
 - 1% duty cycle
 - Short pulses: 200 µs
 - High peak current (200 A vs 3 A for DCMS)
 - High peak power (80 kW peak for 1kW avg)
- Ionization of sputtered species
- Lower coating rate of the property of the coating rate of the property of the coating rate of the coatin



HiPIMS Results @ CERN



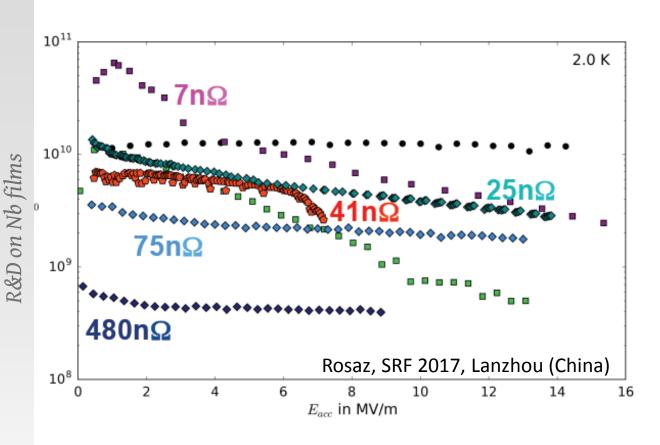
- Bulk Nb (R_{res} = 20 nΩ)
 M 2.9 (DCMS, 2015)
 M 5.1 (HIPIMS -100 V, 2016)
 M 5.2 (HIPIMS -50 V, 2016)
 M 1.5 (HIPIMS -50 V, 2016)
- M 5.3 (HIPIMS -25 V, 2017)
 M 2.3 (1.8 K) (HIPIMS unbiased, 2013)

- High Bias does not give good results (gas implantation, stress)
- Lower pressure tends to better performances (contamination, stress)

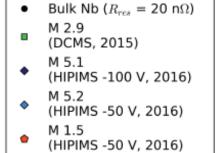
Q-slope looks mitigated vs DCMS coating

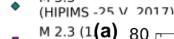
Courtesy of G. Rosaz (CERN)

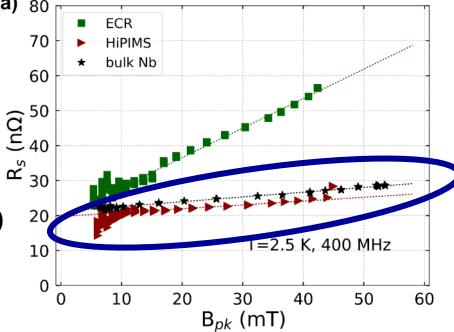
HiPIMS Results @ CERN



Cristian Pira



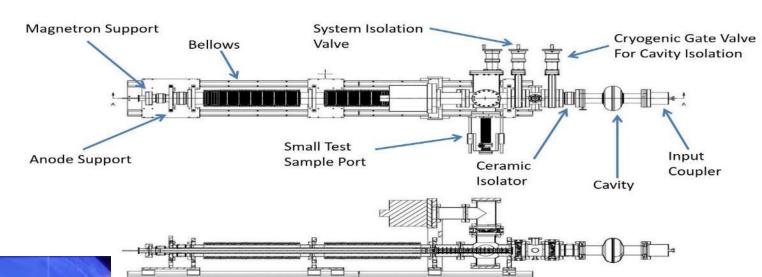




- High Bias does not give good results (gas implantation, stress)
- Lower pressure tends to better performances (contamination, stress)

Q-slope looks mitigated vs DCMS coating

HiPIMS @ JLAB



Courtesy of A.-M. Valente

- Movable cylindrical Nb cathode
- Background pressure in 10⁻⁹-10⁻¹⁰ Torr
- Coating temperatures up top 400 °C under external nitrogen flow
- Kr atmosphere



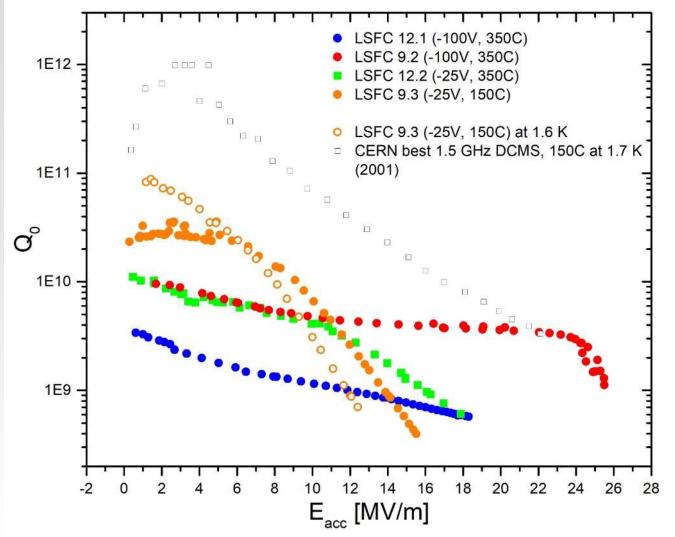
Cristian Pira



Courtesy of A-M. Valente (JLAB)

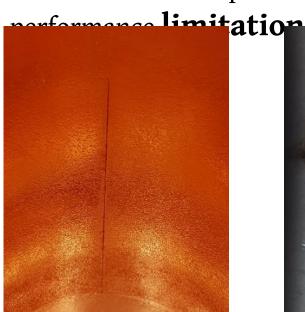
102

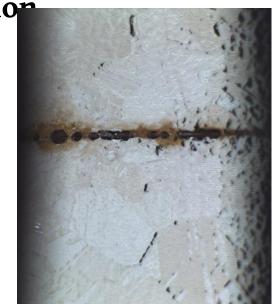
HiPIMS Results @JLAB



Some HiPIMS Nb/Cu cavities show **mitigation** of the characteristic **Q**-slope

Substrates are a possible cause of



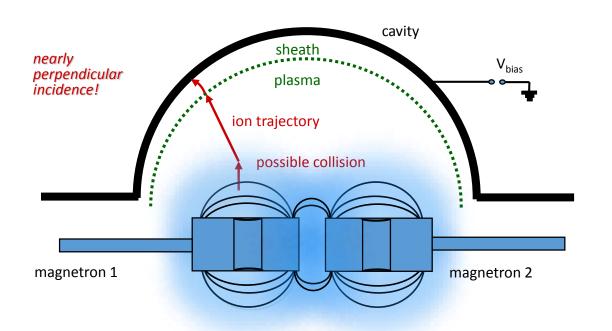


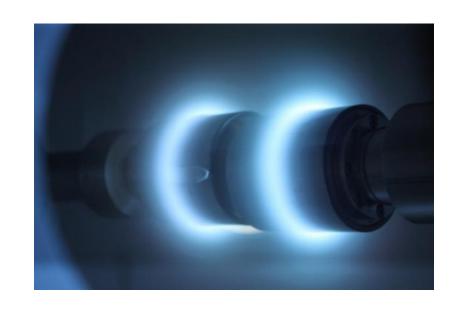
Courtesy of A-M. Valente (JLAB)



R&D on Nb films

HiPIMS configuration @ LBNL





- HiPIMS Dual Magnetron Configuration
- Most effective for Biasing & influencing Ion Energies & Trajectories
- High power mode (above runaway threshold)
- Dominated by Nb emission

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No cavity RF tested

A. Anders, Thinfilms Workshop 2016, JLab

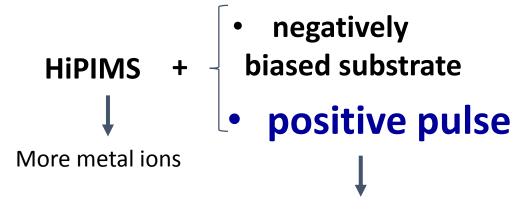


The WOW cavity coating challenge

Wide-Open Waveguide (WOW) crab cavity (Nb/Cu), 1st prototype completed in 2018

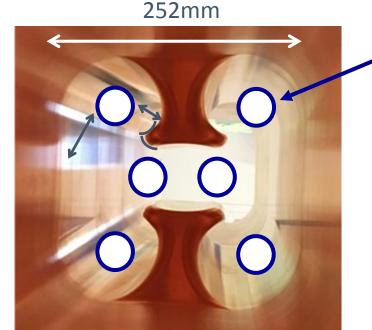


1.4m / 290kg



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High energy metal ions to densify the film



x6 Cylindrical magnetrons

- Distances (20 - 80 mm)
- Angles of incidence $(0 - 90^{\circ})$

F. Avino (CERN), TTC Meeting, CERN 2020





ECR

Jefferson Lab (A-.M. Valente et al.)



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Energetic Condensation with ECR @JLAB

ECR DEPOSITION PROCESS

- Nb is evaporated by e-beam in a separate vacuum chamber
- Nb vapours are ionized by an ECR process
 - RF power (@ 2.45GHz)
 - Static B \perp E_{RF} with ECR condition
- Nb ion are accelerate to the substrate (cavity) by a bias voltage

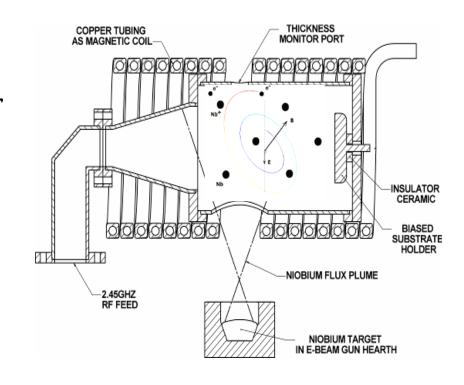


Good conformation Pirage

Singly charged ions (64eV) produced in vacuum

Controllable deposition energy with Bias voltage

Excellent bonding, No macro particles









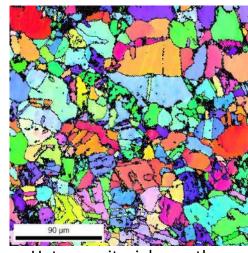
ECR film properties

Substrate		RRR max
Insulating	$a-Al_2O_3$	591
	r-Al ₂ O ₃	725
	c-Al ₂ O ₃	247
	MgO (100)	188
	MgO (110)	424
	MgO (111)	270
	Al ₂ O ₃ ceramic	135
	AIN ceramic	110
	Fused Silica	84
Metallic	Cu (100)	181
	Cu (110)	275
	Cu (111)	245
	Cu fine grains	193
	Cu large grains	305

SEQUENTIAL PHASE FOR FILM GROWTH

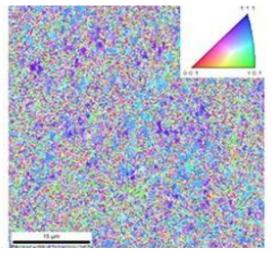
- Interface
- Film nucleation (184 eV)
- Growth of appropriate template for subsequent deposition (64
- Deposition of final surface optimized for minimum defect Bulkylike properties

Opportunity for film engineering

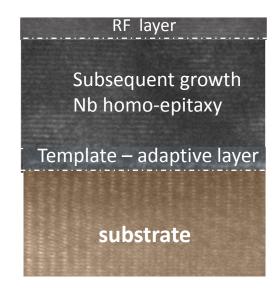


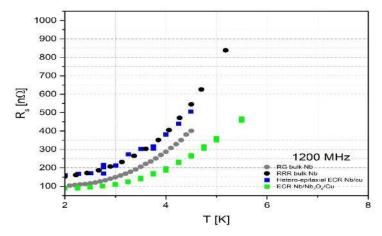


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Growth on amorphous interface





Fiber growth ECR Nb/Cu films perform better than heteroepitaxial ones

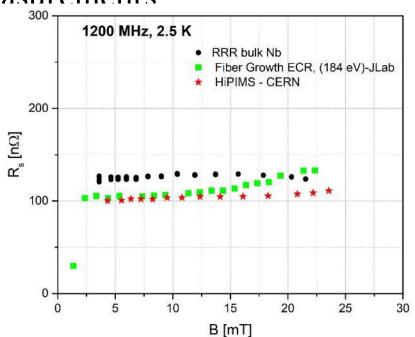
Courtesy of A-M. Valente (JLAB)

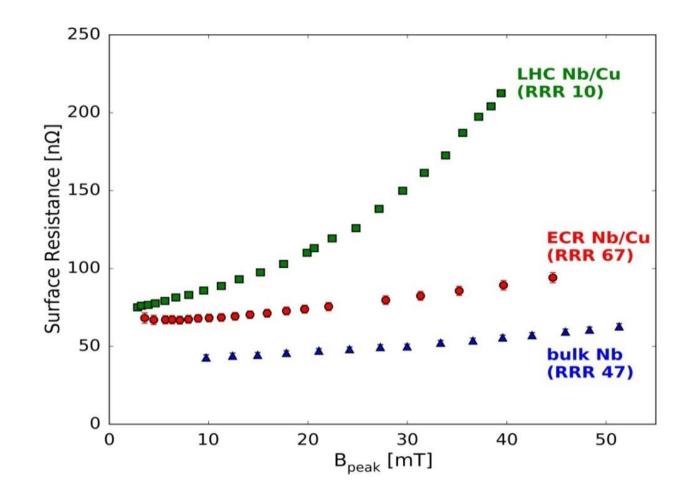


ECR Results

Mitigation of Rs slope possible

Energetic Condensation Nb/Cu films show similar RF behavior compare to bulk Nb in QPR measurements





Courtesy of A-M. Valente (JLAB)





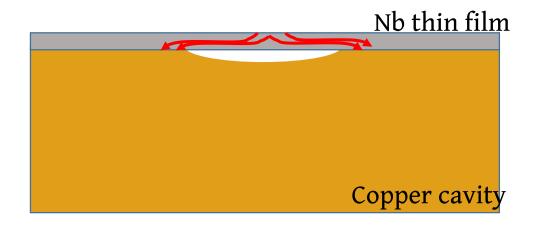
Nb thin films

THICK FILMS

DCMS @INFN LNL (C. Pira, V. Garcia et al.) CVD @CORNELL and ULTRAMET CVD @STFC (R. Valizadeh et al.)



Thick film motivation



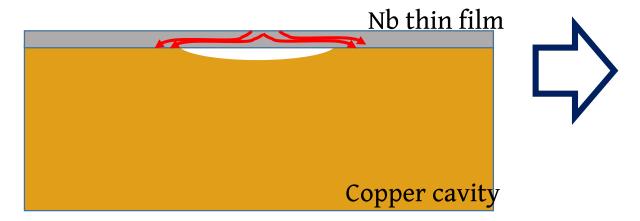
Q-slope is related to local enhancement of the **thermal boundary resistance at the Nb/Cu interface**, due to a poor thermal contact between film and substrate

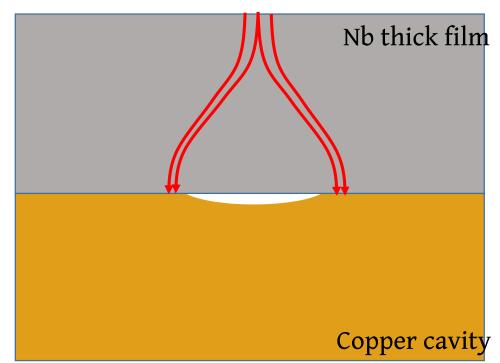
Theoretical model from Vaglio and Palmieri

V. Palmieri and R. Vaglio, Supercond. Sci. Technol., vol. 29, no. 1, p. 015004, Jan. 2016



Thick film motivation





Q-slope is related to local enhancement of the **thermal boundary resistance at the Nb/Cu interface**, due to poor thermal contact between film and substrate

Theoretical model from Vaglio and Palmieri

V. Palmieri and R. Vaglio, Supercond. Sci. Technol., vol. 29, no. 1, p. 015004, Jan. 2016



Chemical Vapour Deposition

Fundamental sequential steps in every CVD process

- Convective and diffusive transport of reactants from the gas inlets 1. to the reaction zone
- Chemical reactions in the gas phase to produce new reactive species and by-products
- Transport of the initial reactants and their products to the substrate surface
- Adsorption (chemical and physical) and diffusion of these species on the substrate surface
- 5. Heterogeneous reactions catalyzed by the surface leading to film formation
- Desorption of the volatile by-products of surface reactions 6.

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Convective and diffusive transport of the reaction by-products 7. away from the reaction zone

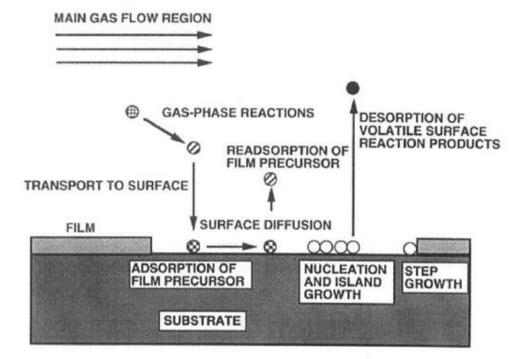


Figure 6-2 Sequence of gas transport and reaction processes contributing to CVD film growth. (From Chemical Vapor Deposition, edited by M. L. Hitchman and K. F. Jensen. Reprinted with the permission of Academic Press, Ltd., and Professor K. F. Jensen, MIT.)



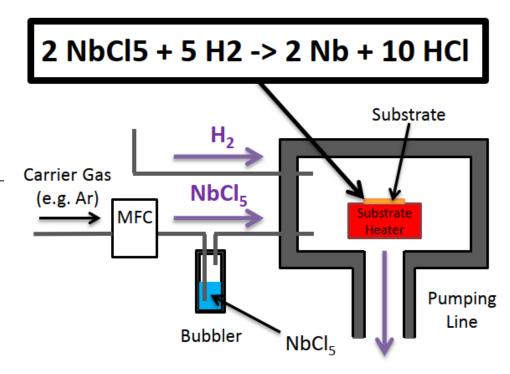
CVD Thick film @ Cornell University and Ultramet

Fundamental sequential steps in every CVD process

- 1. Convective and diffusive transport of reactants from the gas inlets to the reaction zone
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- 5. Heterogeneous reactions catalyzed by the surface leading to film formation
- 6. Desorption of the volatile by-products of surface reactions

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7. Convective and diffusive transport of the reaction by-products away from the reaction zone



Reactor diagram showing use of NbCl₅ to produce CVD niobium

P. Pizzolet al., (STFC) IPAC (2016)





CVD Thick film @ Cornell University and Ultramet



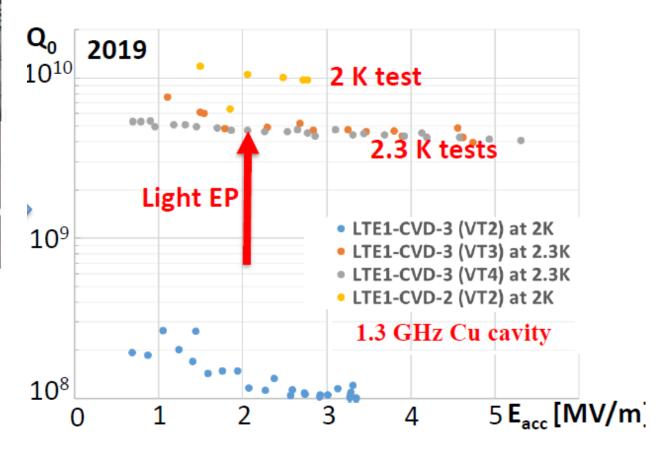
R&D on Nb films



Film optimization & process scale-up

High purity (high RRR)

Excellent adhesion

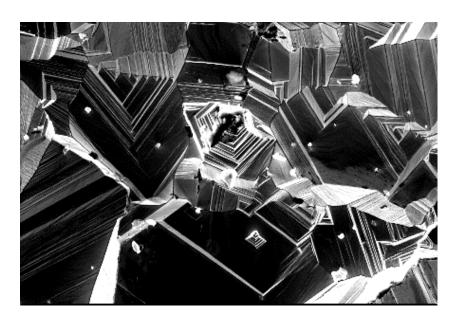


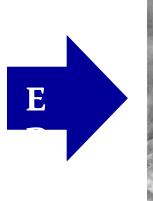
Zeming Sun Mingqi (Cornell), TTC Meeting, CERN 2020



Nb thin films

CVD Thick film @ Cornell University and **Ultramet**





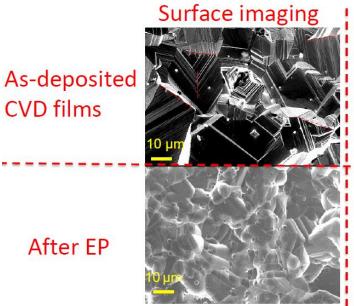


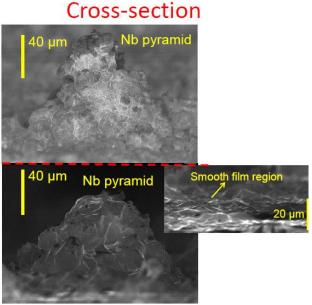
Very Rough Surface

EP smooth pyramids

After EP

CVD films





Zeming Sun Mingqi (Cornell), TTC Meeting, CERN 2020

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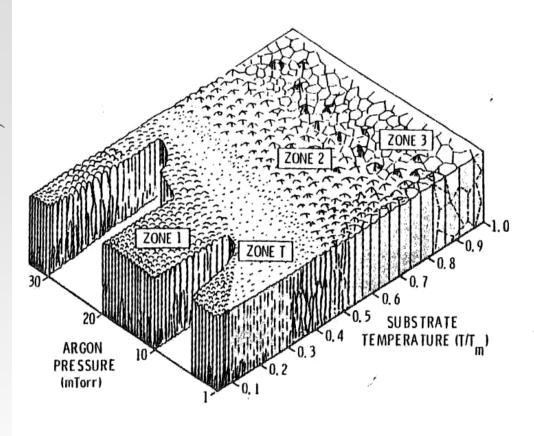
LNL Approach

Thick films

• High temperature



High Temperature Deposition Motivation



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Thorton SZ Diagram

J.A. Thornton and D.W. Hoffman, Thin Solid Films, vol. 171, no. 1, pp. 5-31, 1989

• CERN (550 °C)

C. Benvenuti et al., Physica B 197 (1994) 72-83

• LNL Alpi Linac (300-500 °C)

Stark et al., Proceedings of SRF1997

• Hie-Isolde (650 °C)

Sublet et al., Proceedings of SRF2013

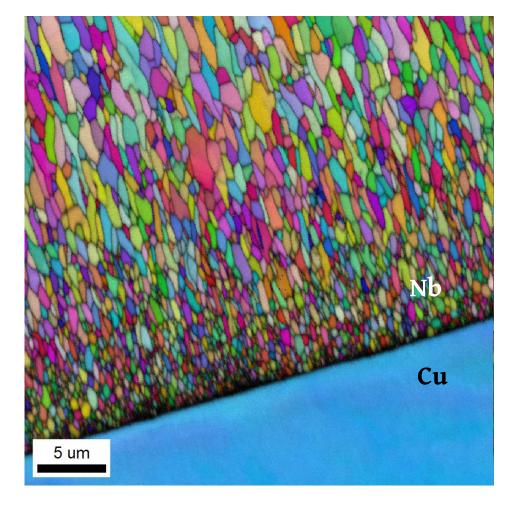


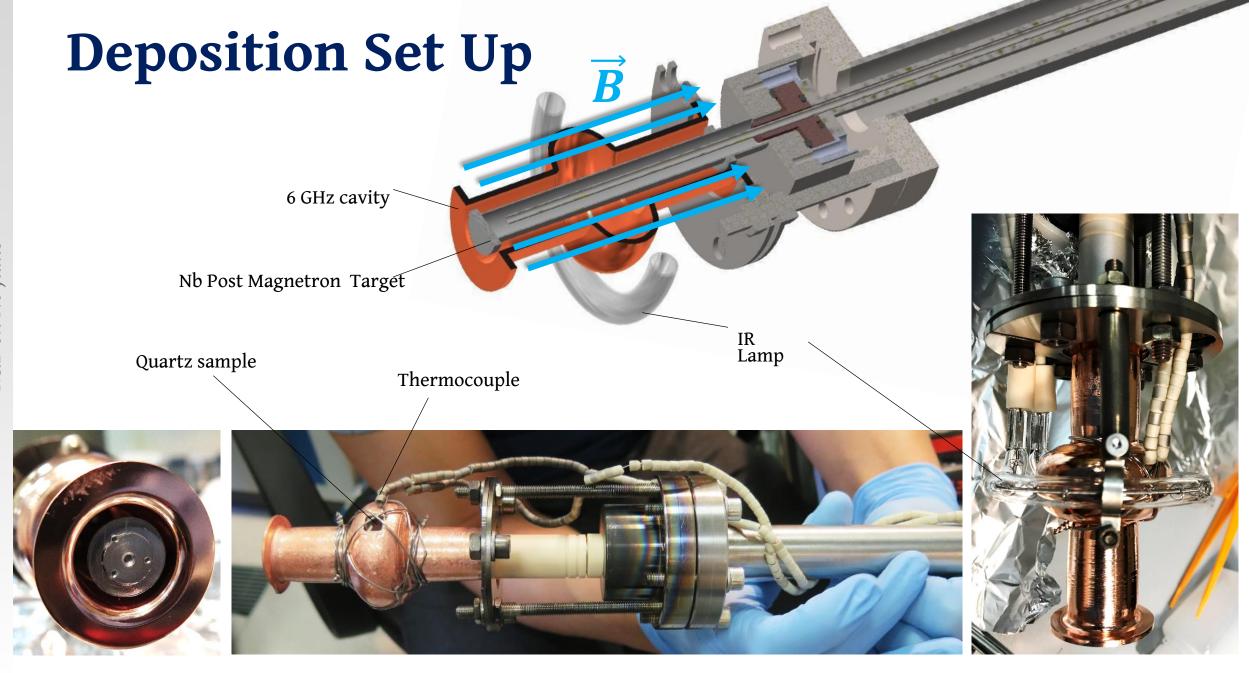
Thick films increase grain dimensions and RRR

Grain dimension ≈**1-10** µm

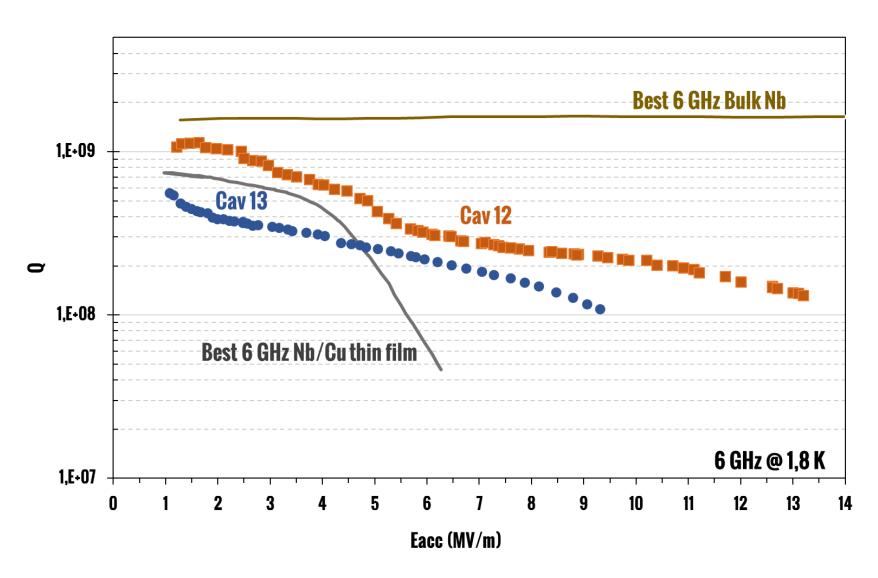
RRR > 60

Bulk like properties





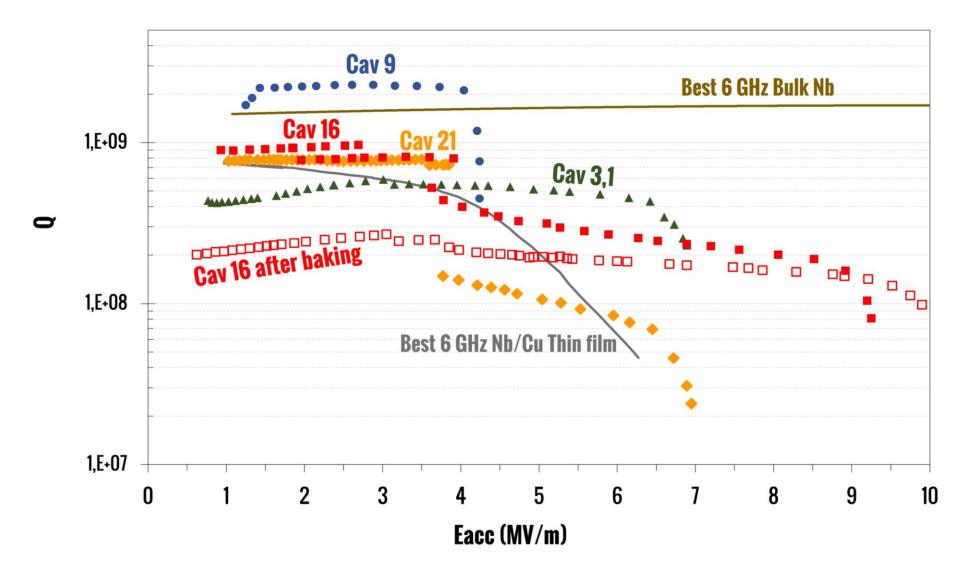
Q-slope remains in many cavities...





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...but not all!





Conclusions

Nb thin films are a great choice for low gradient/4.2 K applications

- Cost reduction
- $R_{BCS film} < R_{BCS bulk} \rightarrow Q_{0 film} > Q_{0 bulk}$
- Thermal stability
- Mechanical stability
- Less sensitivity to magnetic field trapping
- Safer handling for the chemical surface treatments

Mitigation of Q-slope for high gradient applications seems possible

We need to understand the reason of the Q-slope

Establish adequate process controls

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- Mandatory have better substrates and chemical processes
- Need more RF measurements statistics

