

# RF-Thermo-Structural study of CLIC Accelerating Structures

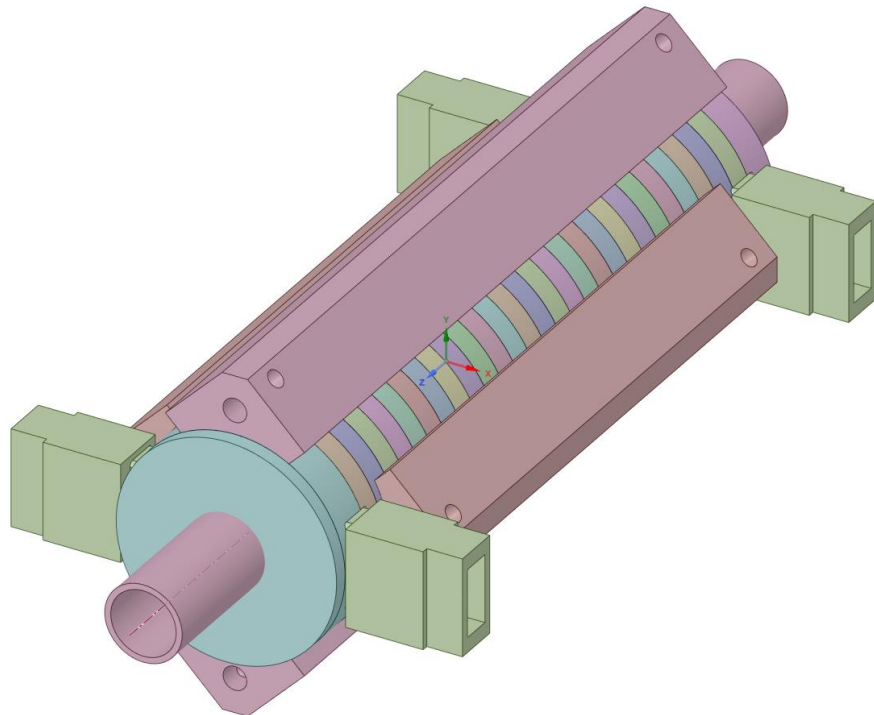
Kai Papke

11.03.2020

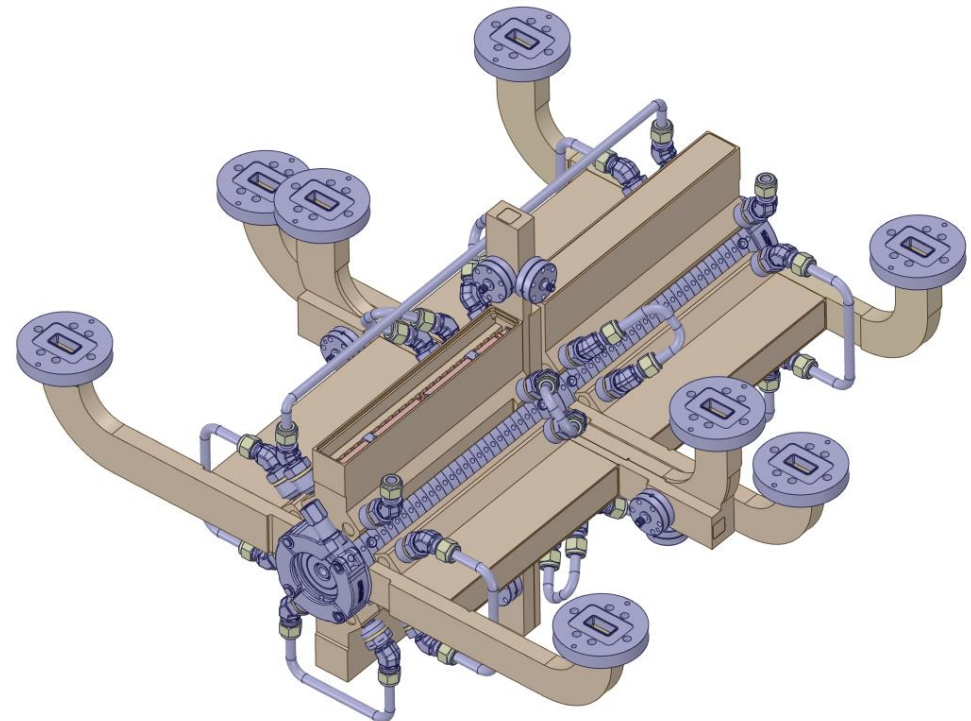
# Structures of Interest

- Damped traveling wave accelerating structure using 26 cells and 2 matching cells
- Bending radius: 0.5mm

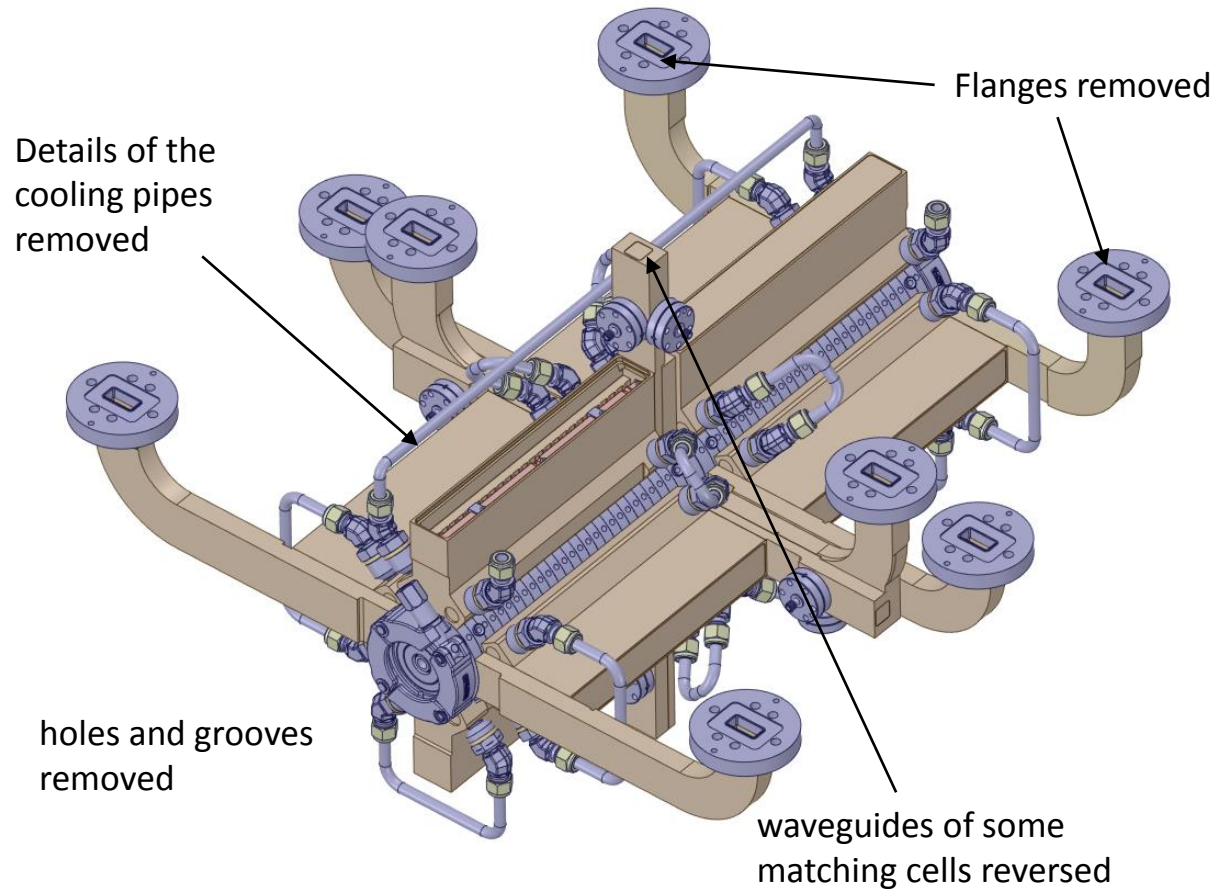
TD26R05CC



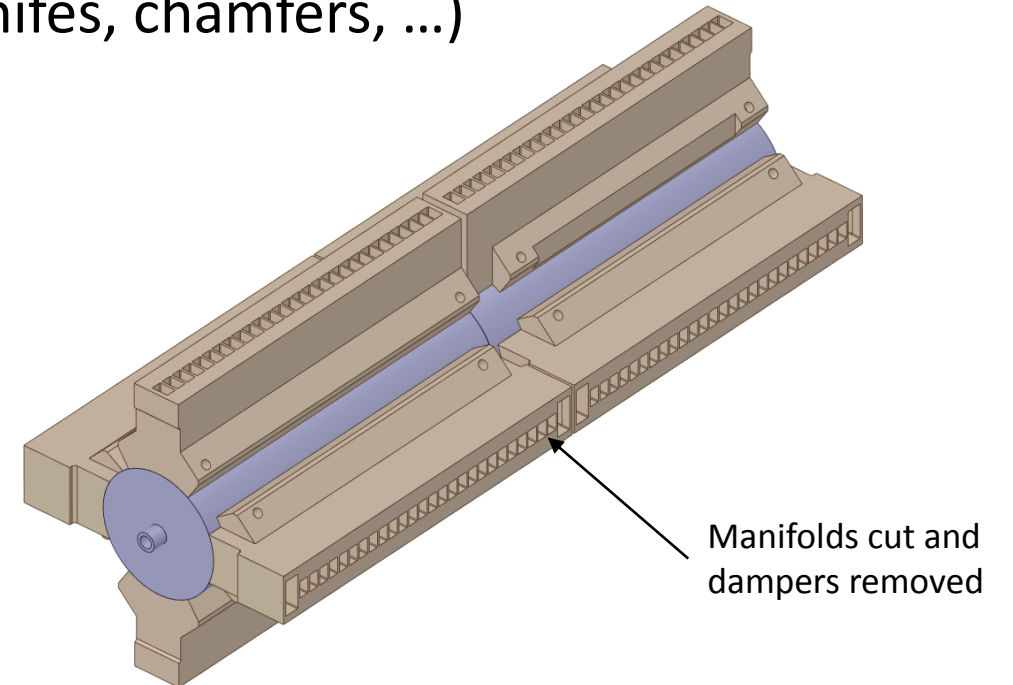
TD26R05SS



# Model simplification

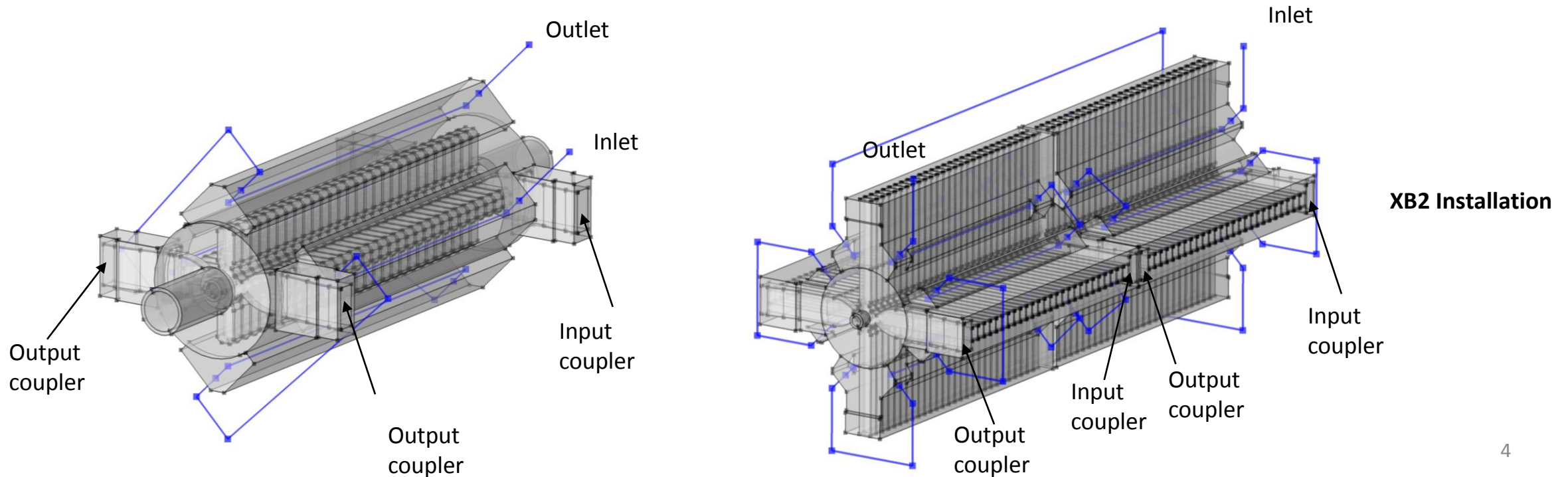


- Avoid healing
- Cooling circuit represented by polygon (1D)
- Clean contact between parts (no rounding, knives, chamfers, ...)



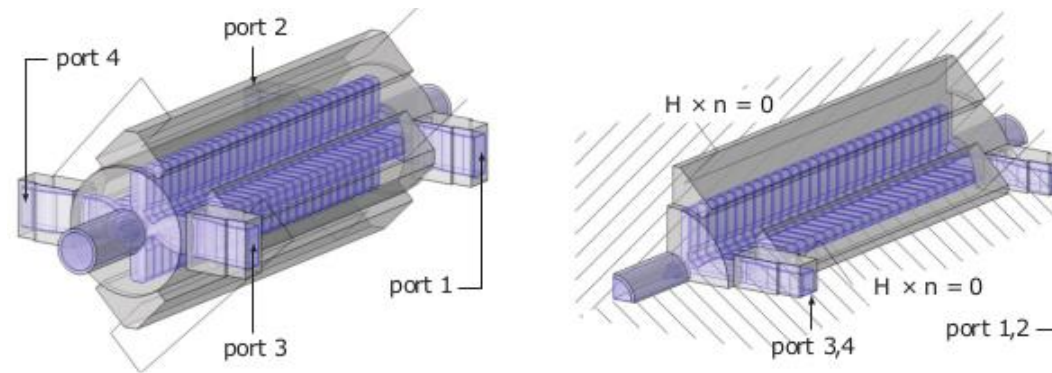
# Cooling path

- 1D fluid flow model based on surface roughness, pipe diameter, inlet temperature, flow rate (no predefined convection heat transfer coefficient)
- Self-consistent with heat transfer in solid
- Single circuits for TD26R05CC and TD26R05SS (default):

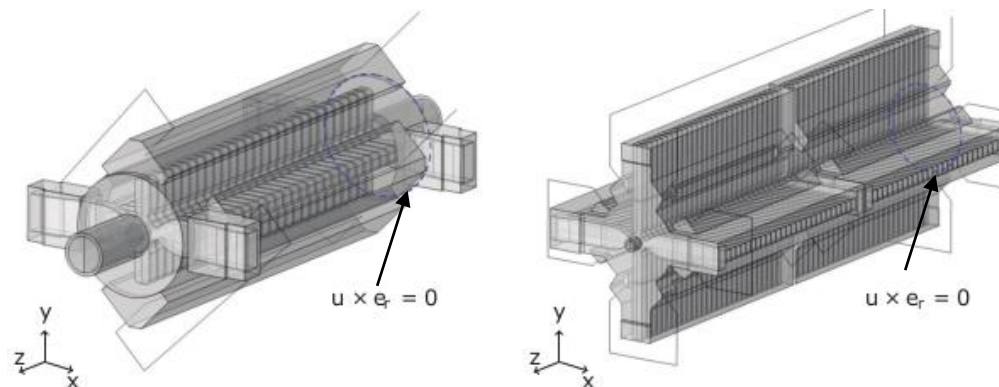


# Symmetry

- If no symmetric cooling paths, thermal deformations break the symmetry
- Scattering Parameters calculated as for symmetric structure (combine ports)

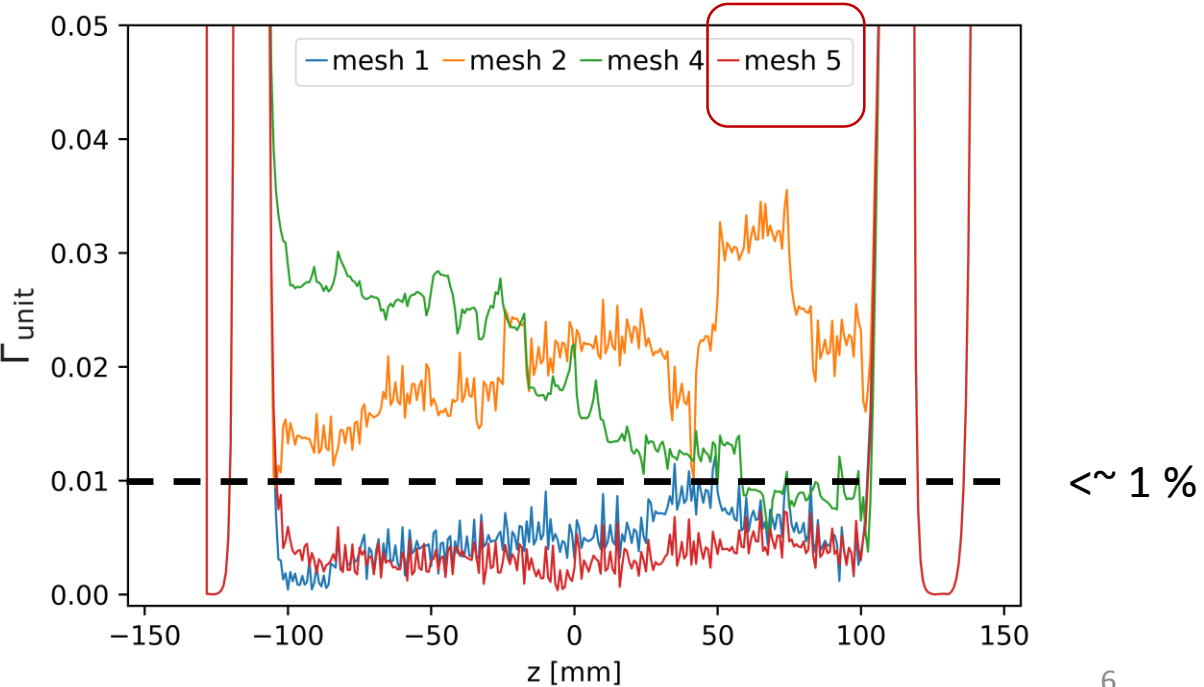
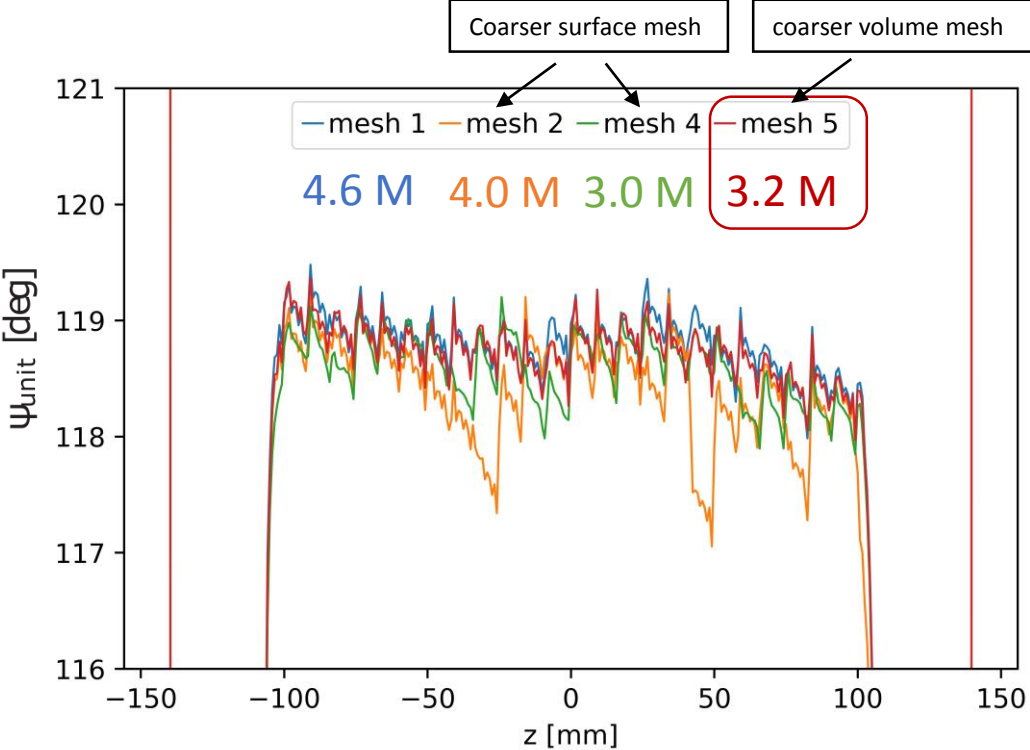


- Structure is fixed by allowing radial displacements at dashed edges



# Mesh

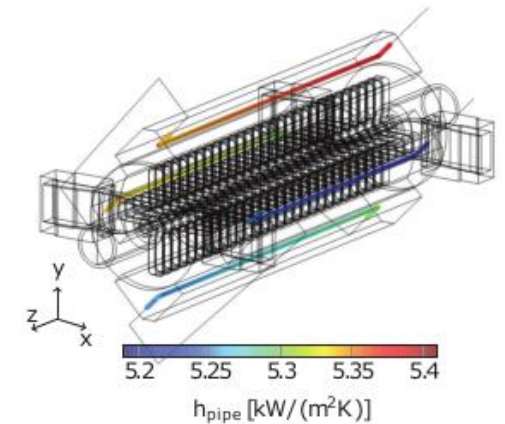
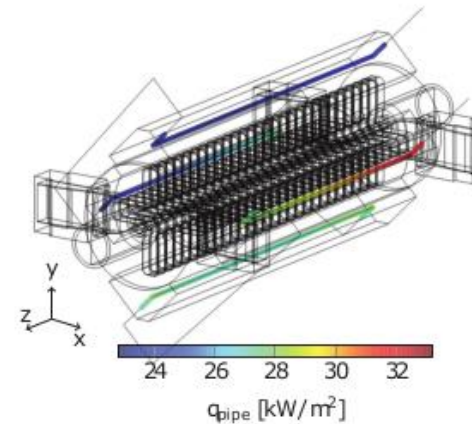
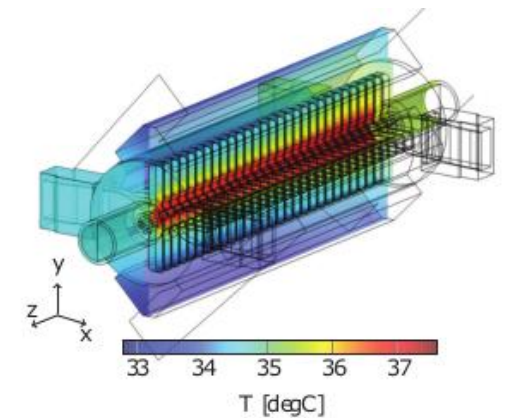
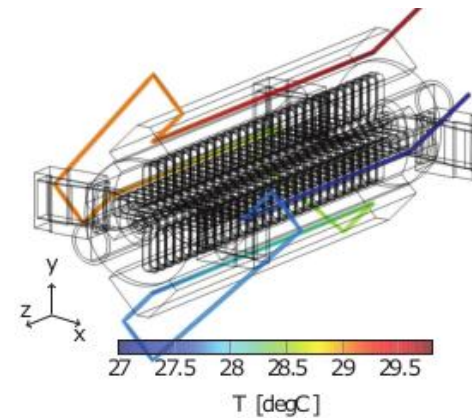
- Convergence criteria: Kroll Parameters (phase advance per cell, Internal reflections)
- Manual mesh adaption (partitioning, refinements around beam line/ cavity surface)
- Example for TD26R05CC:



# Heat Transfer and Pipe Flow

- Heat concentration around irises despite of large thermal conductivity
- Resulting heat transfer coefficient  $h_{\text{pipe}}$  verified by analytical calculations

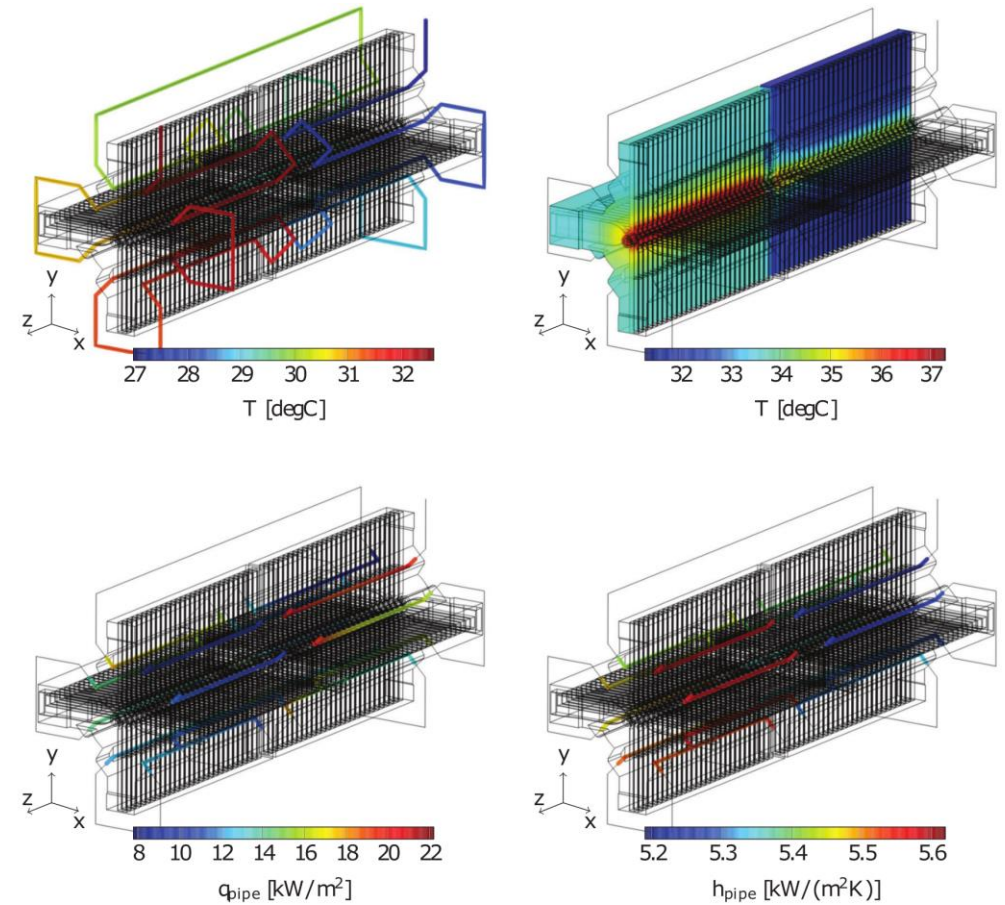
**TD26R05CC: 1kW** input RF power, **3l/min** water flow rate, **5W/(m<sup>2</sup>K)** air convective heat transfer coefficient,  $T_{\text{amb}} = 28\text{degC}$ ,  $T_{\text{inlet}} = 27\text{degC}$



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- Delta T of 2 K between the structures of TD26R05SS

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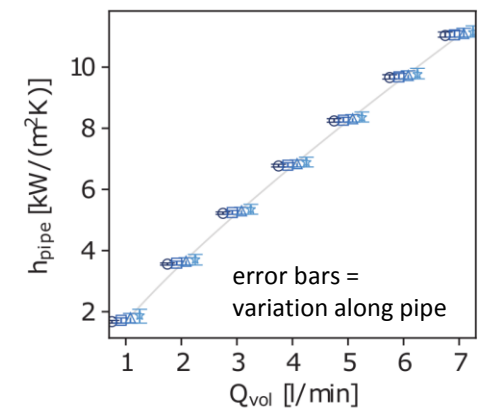
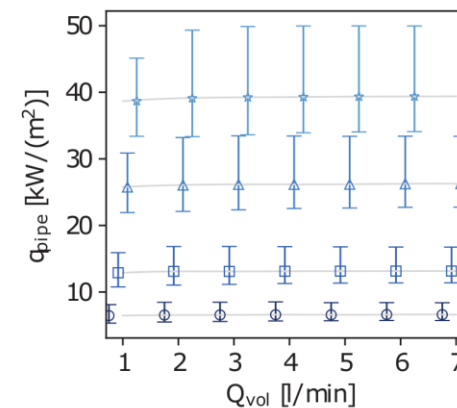
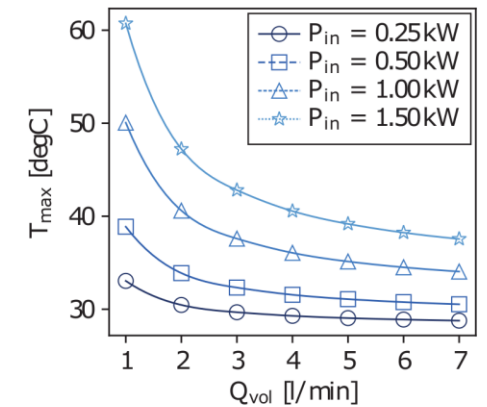
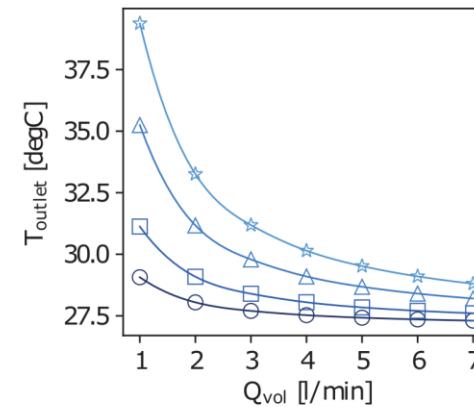




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- Saturation of cooling  $Q_{\text{vol}} > 3\text{l/min}$

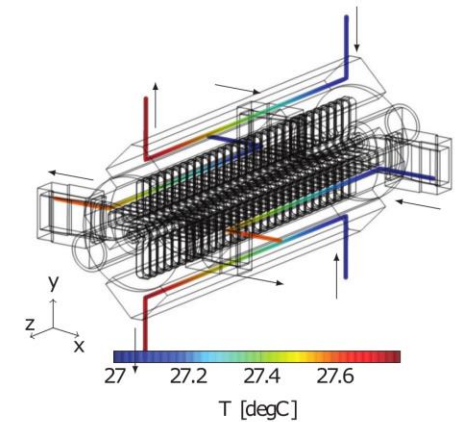
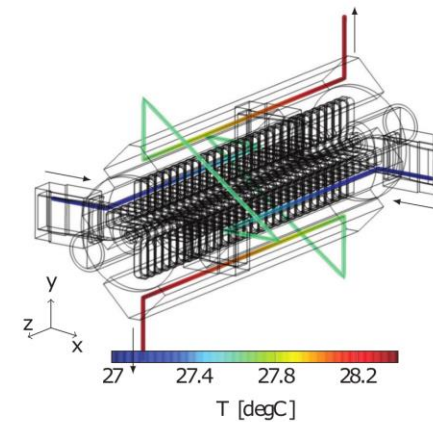
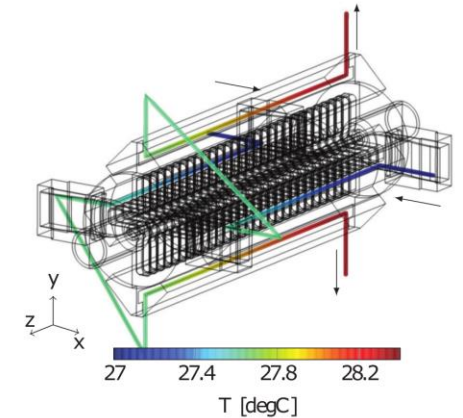
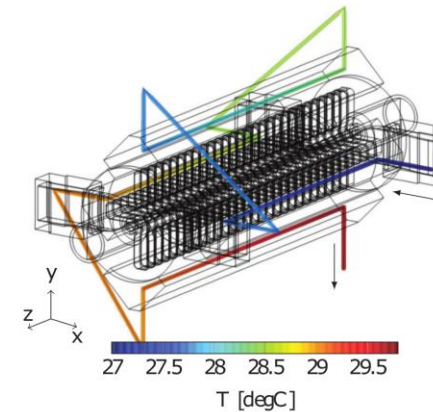
**TD26R05CC: var** input RF power, **var** water flow rate, **5W/(m<sup>2</sup>K)** air convective heat transfer coefficient,  $T_{\text{amb}} = \mathbf{28\text{degC}}$ ,  $T_{\text{inlet}} = \mathbf{27\text{degC}}$



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- Changes of cooling path has marginal impact on temperature distribution

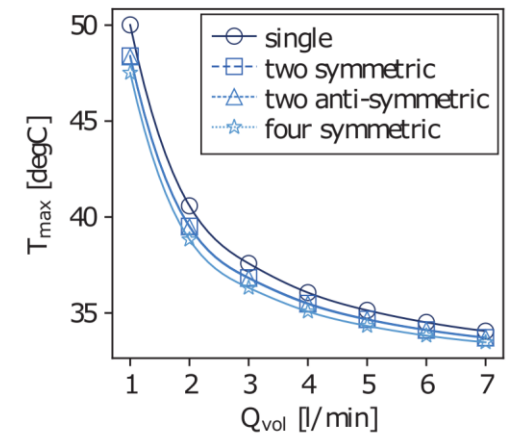
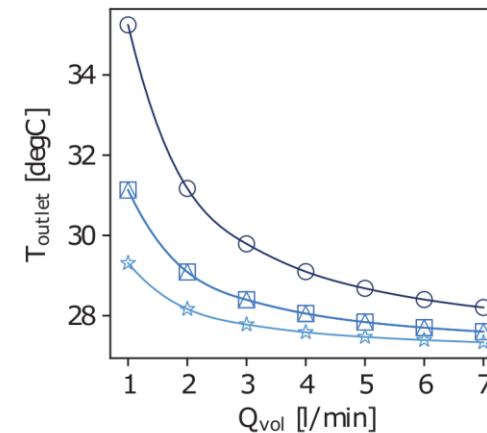
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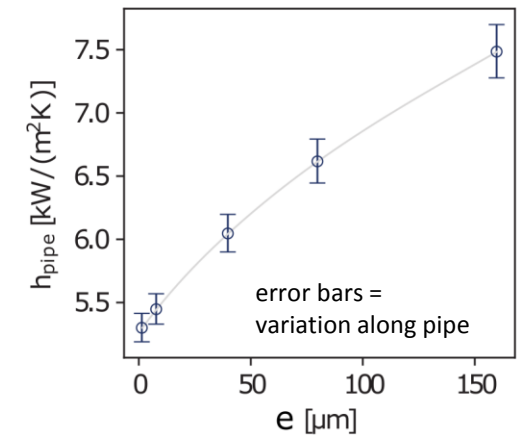
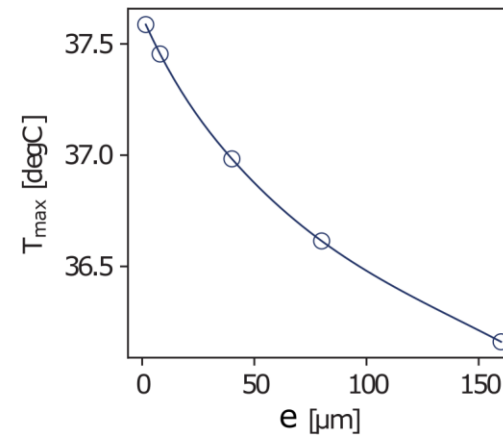
**TD26R05CC: 1kW** input RF power, **var** water flow rate, **5W/(m<sup>2</sup>K)** air convective heat transfer coefficient,  $T_{\text{amb}} = \mathbf{28degC}$ ,  $T_{\text{inlet}} = \mathbf{27degC}$



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- Delta T of 2 K between the structures of TD26R05SS
- Saturation of cooling  $Q_{\text{vol}} > 3\text{l/min}$
- Changes of cooling path has marginal impact on temperature distribution
- Significant impact by surface roughness of the cooling pipes

**TD26R05CC: 1kW** input RF power, **3l/min** water flow rate, **5W/(m<sup>2</sup>K)** air convective heat transfer coefficient,  $T_{\text{amb}} = 28\text{degC}$ ,  $T_{\text{inlet}} = 27\text{degC}$

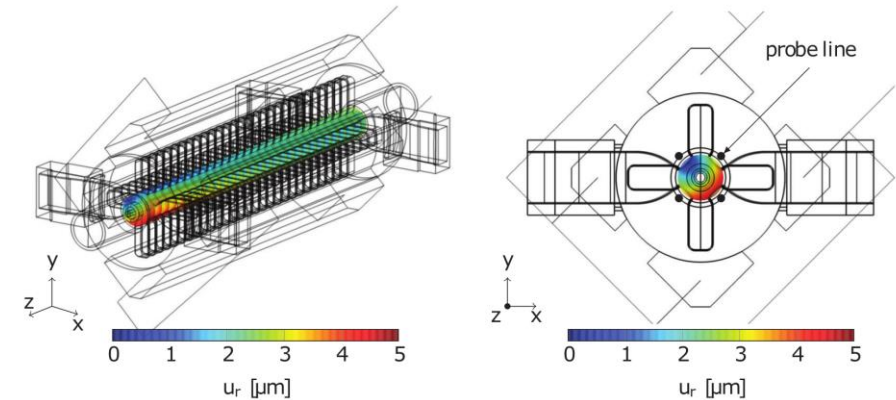


$e = 1.5 \mu\text{m}$  corresponds to **drawn tubes** and was considered so far to be on the conservative side

# Structural Deformation

- Thermal expansion using  $T_{amb}$  as reference temperature
- Single cooling circuit result in slight

**TD26R05CC: 1kW** input RF power, **3l/min** water flow rate, **5W/(m<sup>2</sup>K)** air convective heat transfer coefficient,  $T_{amb} = 28\text{degC}$ ,  $T_{inlet} = 27\text{degC}$

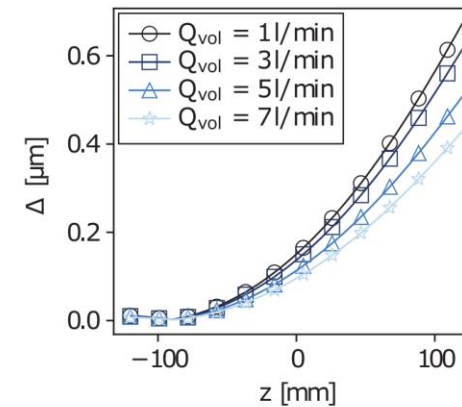


Transverse displacement of center axis as sum of x and y components of structural displacement over four probe lines (black dots)

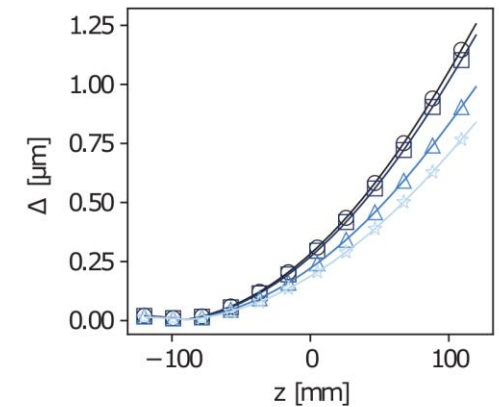
# Structural Deformation

- Thermal expansion using  $T_{amb}$  as reference temperature
- Single cooling circuit may result in few micron transverse center displacement

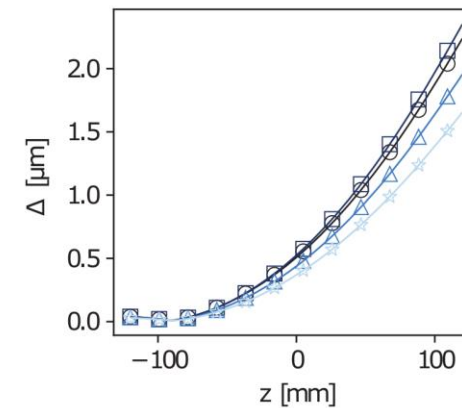
**TD26R05CC: var input RF power, var water flow rate,  $5W/(m^2K)$  air convective heat transfer coefficient,  $T_{amb} = 28degC$ ,  $T_{inlet} = 27degC$**



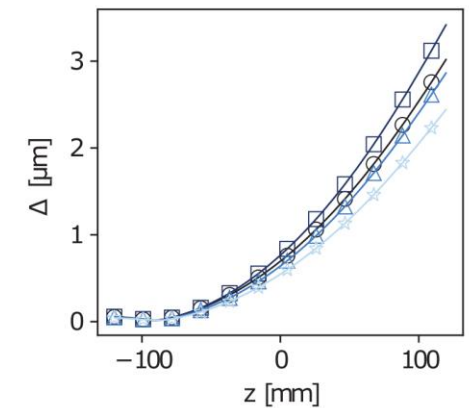
(a)  $P_{in} = 250W$



(b)  $P_{in} = 500W$



(c)  $P_{in} = 1000W$

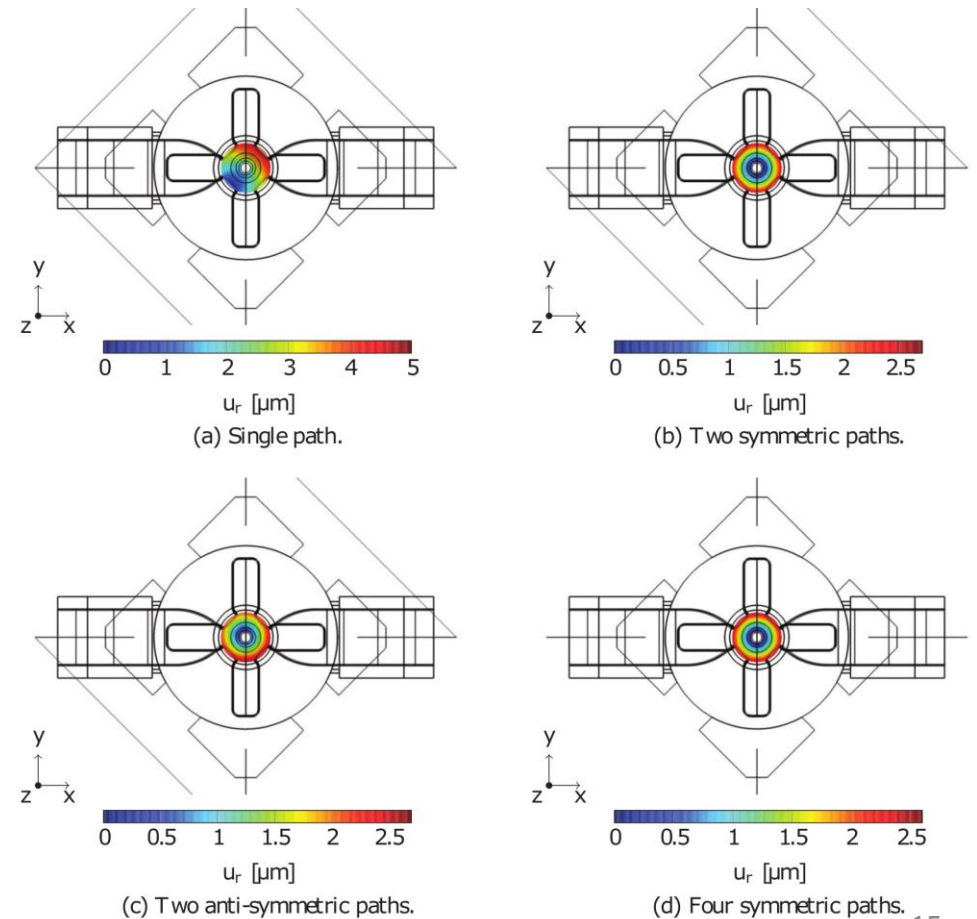


(d)  $P_{in} = 1500W$

# Structural Deformation

- Thermal expansion using  $T_{amb}$  as reference temperature
- Single cooling circuit may result in few micron transverse center displacement
- Symmetry of displacements follows from symmetry of cooling paths

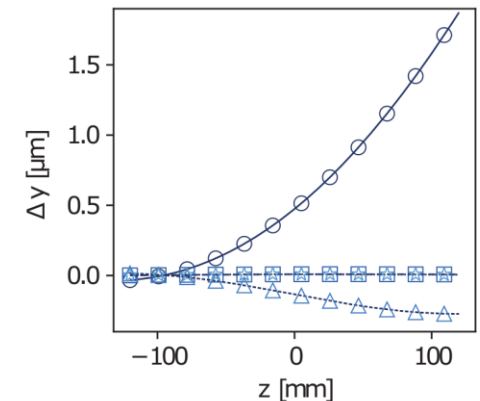
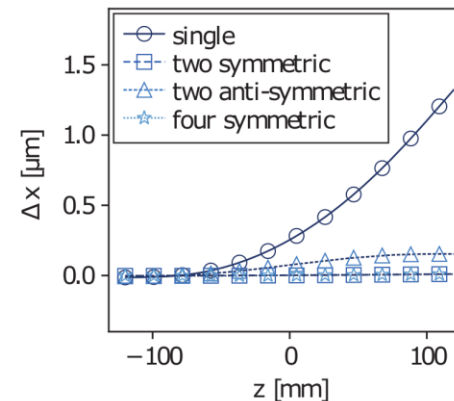
**TD26R05CC: 1kW** input RF power, **3l/min** water flow rate, **5W/(m<sup>2</sup>K)** air convective heat transfer coefficient,  $T_{amb} = 28\text{degC}$ ,  $T_{inlet} = 27\text{degC}$



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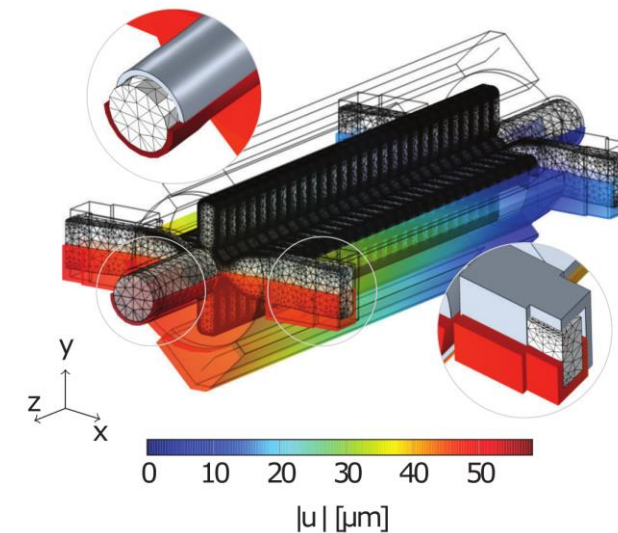
“two symmetric paths” and “four symmetric paths” allow to consider only a quarter for the coupled problem



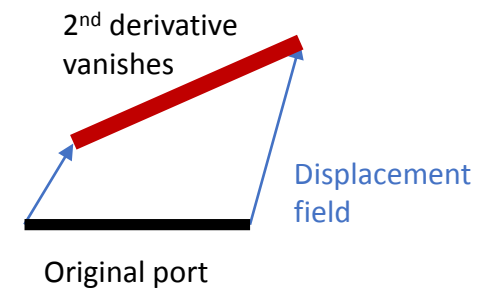
# Structural Deformation

- Thermal expansion using  $T_{amb}$  as reference temperature
- Single cooling circuit may result in few micron transverse center displacement
- Symmetry of displacements follows from symmetry of cooling paths
- Mesh displacement of the vacuum part according to the surrounding structure deformation except for beam line

**TD26R05CC: 1kW** input RF power, **3l/min** water flow rate, **5W/(m<sup>2</sup>K)** air convective heat transfer coefficient,  $T_{amb} = 28\text{degC}$ ,  $T_{inlet} = 27\text{degC}$



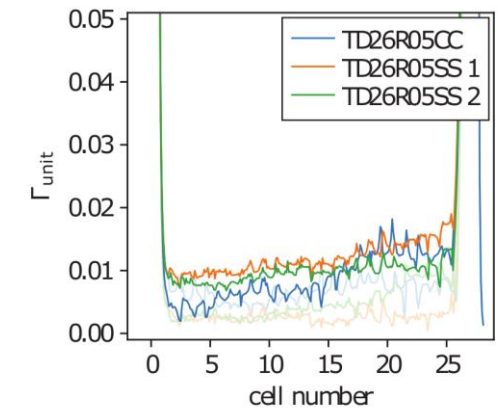
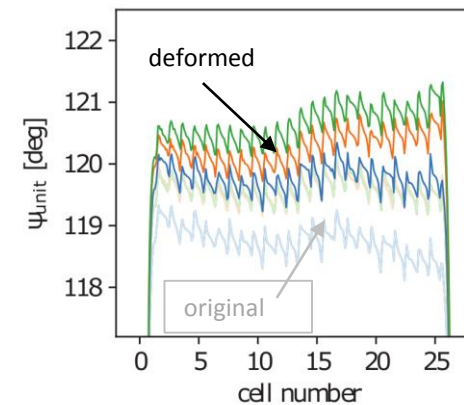
Displacement of port surface by solving Laplace-like equation taking into account the surrounding structural deformation as Dirichlet boundary condition



# Studies on Perturbed Structures

- Phase advance  $\Psi_{\text{unit}}$  and internal reflections  $\Gamma_{\text{unit}}$  generally increases when accounting thermal conditions

**TD26R05XX: 1kW** input RF power, **3l/min** water flow rate, **5W/(m<sup>2</sup>K)** air convective heat transfer coefficient,  $T_{\text{amb}} = 28\text{degC}$ ,  $T_{\text{inlet}} = 27\text{degC}$

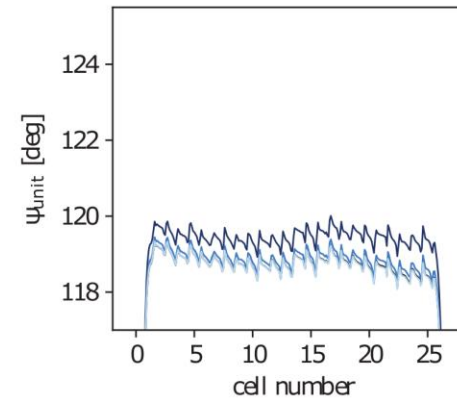


Cell-to-cell phase advance of TD26R05CC by design around 119 deg due to shorter and rounded waveguides

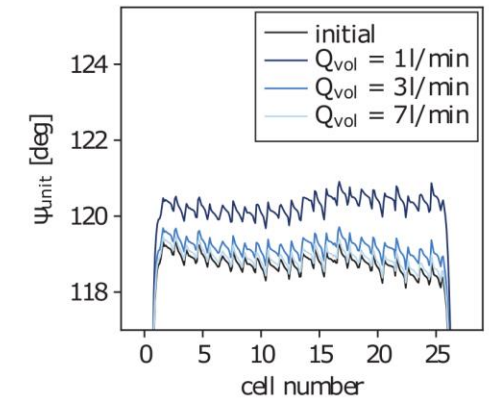
# Studies on Perturbed Structures

- Phase advance  $\Psi_{\text{unit}}$  and internal reflections  $\Gamma_{\text{unit}}$  generally increases when accounting thermal conditions
- Flow rate  $\geq 3\text{l/min}$  required to reduce impact of RF heating on  $\Psi_{\text{unit}}$  and  $\Gamma_{\text{unit}}$

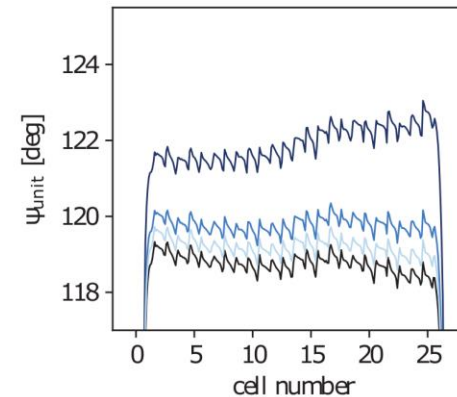
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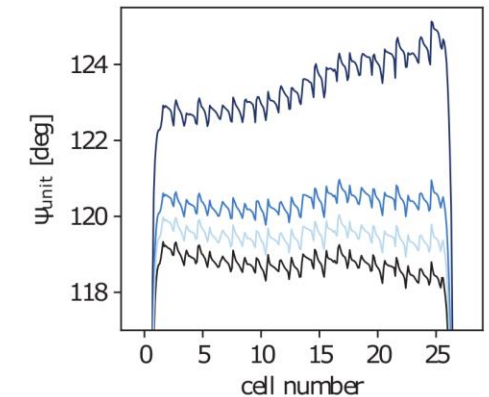
(a)  $P_{\text{in}} = 250\text{W}$



(b)  $P_{\text{in}} = 500\text{W}$



(c)  $P_{\text{in}} = 1000\text{W}$

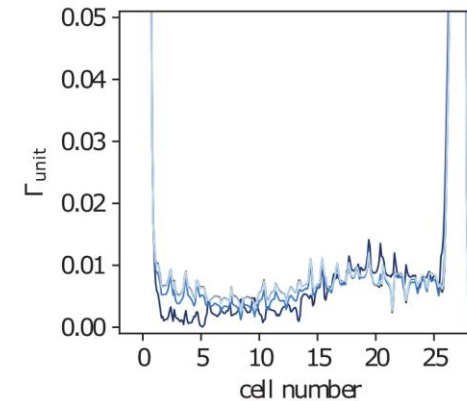


(d)  $P_{\text{in}} = 1500\text{W}$

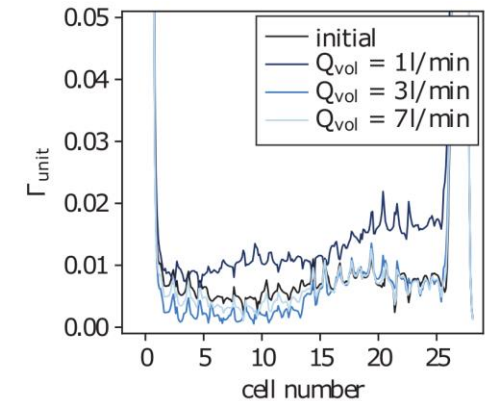
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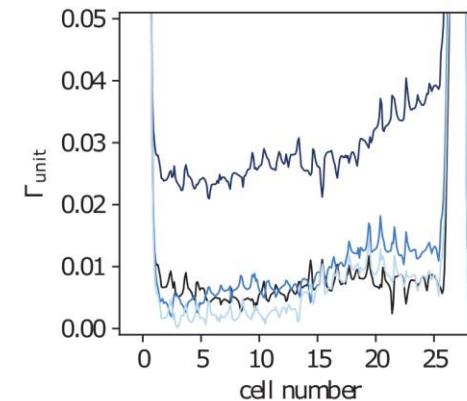
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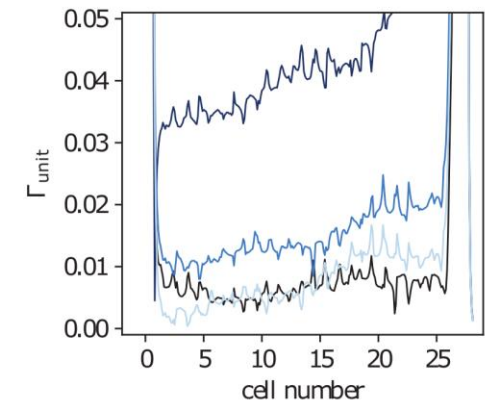
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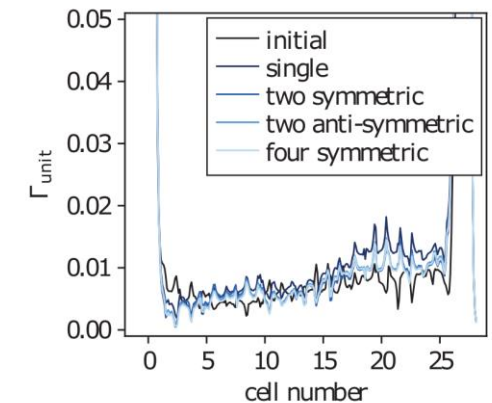
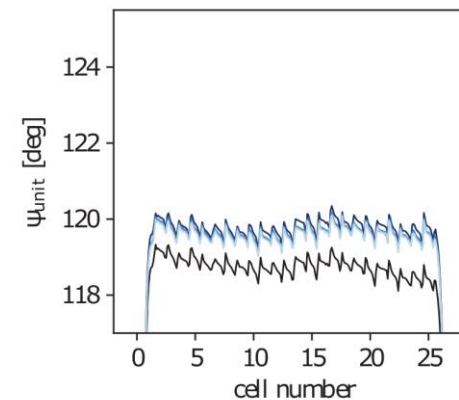


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- Phase advance  $\Psi_{\text{unit}}$  and internal reflections  $\Gamma_{\text{unit}}$  generally increases when accounting thermal conditions
- Flow rate  $\geq 3\text{l/min}$  required to reduce impact of RF heating on  $\Psi_{\text{unit}}$  and  $\Gamma_{\text{unit}}$
- Qualitative same RF results for different cooling paths

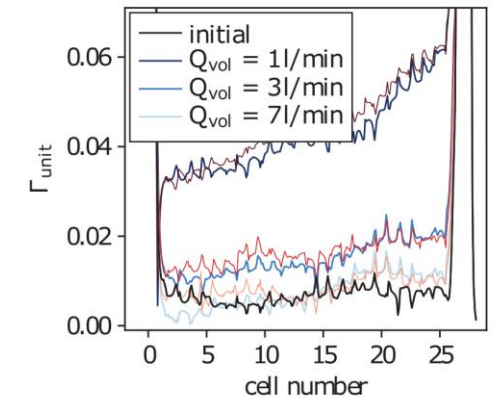
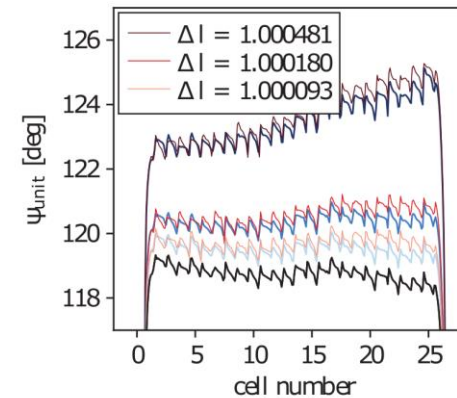
**TD26R05CC: 1kW** input RF power, **3l/min** water flow rate, **5W/(m<sup>2</sup>K)** air convective heat transfer coefficient,  $T_{\text{amb}} = 28\text{degC}$ ,  $T_{\text{inlet}} = 27\text{degC}$



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- Phase advance  $\Psi_{\text{unit}}$  and internal reflections  $\Gamma_{\text{unit}}$  generally increases when accounting thermal conditions
- Flow rate  $\geq 3\text{l/min}$  required to reduce impact of RF heating on  $\Psi_{\text{unit}}$  and  $\Gamma_{\text{unit}}$
- Similar results for different cooling paths (marginal impact)
- Qualitative same RF results for scaled geometry

**TD26R05CC: 1.5kW** input RF power, **var** water flow rate, **5W/(m<sup>2</sup>K)** air convective heat transfer coefficient,  $T_{\text{amb}} = 28\text{degC}$ ,  $T_{\text{inlet}} = 27\text{degC}$

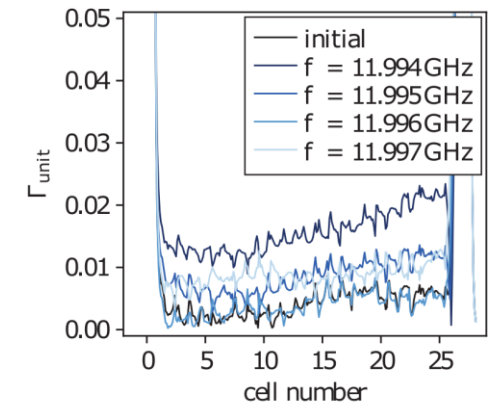
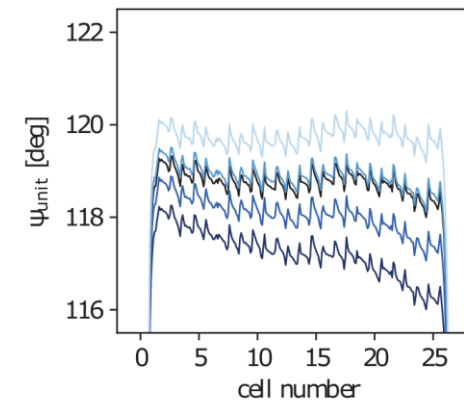


Relative length variation  $\Delta l$  is based on the variation of the cavity length (longitudinal change)

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- Frequency tuned by inlet temperature without compromising RF profiles

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Profiles of cell-to-cell phase and internal reflection **completely restored** at a frequency 2 MHz higher than by design

# Summary

- Heat concentration around irises despite of large thermal conductivity
- Single cooling circuit can result in few micron transverse center displacement
- Flow rates of at least 3l/min should be considered to reduce enhancement of internal reflections and cell-to-cell phase advance
- RF behavior of deformed structure well described by a scaled model (no mesh deformation required)
- Frequency can be tuned by inlet temperature without compromising RF profiles