New Horizons for TPCs, 5th to 9th of October 2020 Video workshop from Santiago de Compostella



Charge spreading with a Resistive-Capacitive coating

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Introduction to charge spreading

- Typical r.m.s. diameter of a Micromegas avalanche : 15 to 25 μm (dominated by diffusion in the amplification gap). This is much less than the pad width, typically 1-10 mm.
- A track segment usually hits only 1 pad (unless sufficient diffusion in the drift space)
- This leads to $w/\sqrt{12}$ resolution (870 μ m for 3mm pads, 2.9 mm for 10mm pads!)





Introduction to charge spreading

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- Need to spread the charge to share the signals between several pads
- This can be done with a resistive-capacitive continuous network.
- This also helps in protecting against sparks Charge spreading in TPCs

One way of analysing the charge spreading (assumes infinite and thin resistive layer on top of a dielectric) is to consider it as a 2D resistive-capacitive network (2D analog of a transmission line) obeying the 2D telegraphist equation.

$$\frac{\partial \rho}{\partial t} = \frac{1}{RC} \left[\frac{\partial^2 \rho}{\partial r^2} + \frac{1}{r} \frac{\partial \rho}{\partial r} \right] \Rightarrow \rho(r,t) = \frac{RC}{2t} e^{\frac{-r^2 RC}{4t}}$$

assuming rotation symmetry and $\rho \rightarrow 0$ at $r \rightarrow \infty$ boundary conditions . Solution : 2D gaussian charge distribution with $\sigma = \sqrt{(2t/RC)}$.

Typical spread is given for t~peaking time of the electronics (200 ns) The smaller RC, the larger the spread. Neighbouring pads see delayed and wider signals





Calculation of induced charge



W. Riegler

Specifications of T2K and ILC ERAM module

Doromotor	ERAM module for:				
Parameter	T2K	ILC			
Number of pads in Horizontal direction	36	72			
Number of pads in Vertical direction	32	24			
a (Horizontal length of Module)	40.2 cm	21.6 cm			
b (Vertical length of Module)	32.3 cm	16.8 cm			
w _x (Horizontal length of Readout pad)	11.18 mm	3 mm			
w _y (Vertical length of Readout pad)	10.09 mm	7 mm			
d ₁ (Distance b/w Resistive layer and Readout pads)	250 µm	125 µm			
d ₃ (Distance b/w Resistive layer and Mesh)	120 µm	120 µm			
R (Surface resistivity of Resistive layer)	400 kΩ/square	2.5 MΩ/square			
\mathcal{E}_1 (Permittivity of d 1 region)	$4 \times \mathcal{E}_0$	$4 \times \mathcal{E}_0$			
\mathcal{E}_3 (Permittivity of d 3 region)	\mathcal{E}_0	\mathcal{E}_0			

Induced charge

Assume a charge appears on the DLC surface at t=0 at point x_p , y_p and calculate induced charge at point x_0 , y_0 at time t The problem is similar to a critically damped membrane with fixed boundary on a rectangle.

$$Q^{ind}(x_0, y_0, t) = \Theta(t) \frac{16Q}{\pi^2} \sum_{\alpha=1}^{\infty} \sum_{\beta=1}^{\infty} \frac{\sin\left(\alpha \pi \frac{w_x}{2a}\right) \sin\left(\alpha \pi \frac{x_p}{a}\right) \sin\left(\alpha \pi \frac{x_0}{a}\right)}{\alpha} \frac{\sin\left(\beta \pi \frac{w_y}{2b}\right) \sin\left(\beta \pi \frac{y_0}{b}\right) \sin\left(\beta \pi \frac{y_0}{b}\right)}{\beta} h(k_{\alpha\beta}, t)$$
with $k_{\alpha\beta} = \pi \sqrt{\frac{\alpha^2}{a^2} + \frac{\beta^2}{b^2}}$ and
$$h(k, t) = \frac{\varepsilon_1 e^{-t/\tau(k)}}{\varepsilon_1 \cosh(kd_1) + \varepsilon_3 \coth(kd_3) \sinh(kd_1)} \qquad \tau(k) = \frac{R}{k} \left(\varepsilon_1 \coth(kd_1) + \varepsilon_3 \coth(kd_3)\right)$$
(1)
A full simulation is possible starting from this point charge solution

A full simulation is possible starting from this point charge solution, by adding :

- Electron ionization
- Avalanche creation, and its fluctuation
- lons going back to the mesh
- In a quasistatic way
- And convolute by electronics response

See D. Janssens, WG4 on Monday

W. Riegler

07/10/2020



T2K pads ~3 times wider than ILC and RC~3 times smaller

Q^{ind}(x, t) plots with varying Surface resistivity (R).



- Vary RC value by changing R.
- Lower RC implies more charge spreading.

S. Joshi

$Q^{ind}(x, t)$ plots with varying Insulation thickness (d₁).



- Vary RC value by changing C.
- Capacitive coupling of resistive foil to pad plane also varies, thus signal strength.



Induced Charge for 1D case

Edge effects

S. Joshi

Charge spreading varies as $1/\sqrt{RC}$: minimize RC to spread more.

However the signal is proportional to the relative capacitive coupling to pad wrt mesh : $Q^{ind} = Q_0 C_1 / (C_1 + C_3).$

This factor is between 0.67 and 0.80 for 120 μ m to 250 μ m insulator.

So there is a trade-off between spreading, sensitivity to small signals, and stability of operation if it is too close to the breakdown limit (this is not the case for ILC and T2K).

ILC module





Electron beam track taken at DESY Drift : 5 cm

T2K/ND280 module

(See talk by C. Giganti on Friday)







O. Pizzirusso, R. De Oliveira

Mesh

Photo-imageable film (for pillars)

DLC-coated kapton

Glue (prepreg)

Copper pad 35 μm

PCB

Resistive materials : surface resistivity



 $R = \rho L/S$

 ρ : bulk resistivity Metal : 10^{-6} - $10^{-5}~\Omega.cm$ Insulator >10^{17} $\Omega.cm$

R = ρ L/wt Flat layer: t small Square L=w Surface resistivity R= ρ/t Units : Ohm per square Materials : Ex: AlSi (Cermets), amorphous hydrogeneted silicon carbon-loaded kapton Si_xN_y Ruthenium oxyde Diamond-Like Carbon (DLC)

Thickness : 100 nm to few microns (even 50 μm for CLK)

We use 2.5 M Ω / \Box for ILC (3mm pads) and 200 k Ω / \Box

Measurement techniques

Cut a long band of resistive. Hold it both ends with conductive tape on an insulating surface, measure the resistance and divide by the number of squares L/w.

Or cut a square of resistive film and measure the resistance between 2 conductive lines

Circular probe

(for example ETS model 803B) Measure the resistance between 2 rings

 $\rho_{s} = \frac{(D_1 + D_2)}{(D_2 - D_1)} \pi R_m \text{ Ohms/sq}$

 D_1 = Outside Diameter of inner ring D_2 = Inner Diameter of outer ring R_m = Measured resistance in ohms 07/10/2020



CERN probe



Charge spreading in TPCs

What is DLC?

• Diamond-like Carbon

Diamond DLC Graphite Graphite Graphite Sp³ bounds Amorphous with H, both sp² and sp³

- Properties
 - Electric : resistive
 - Mechanical : hardness, anti-corrosion protection, solid lubricant
- Applications in MPGD
 - Charge spreading anode: deposited on an insulating substrate makes a continuous resistive-capacitive network, evenly spreading the charge, improving point resolution by allowing a barycenter between pads or strips
 - Anti-spark protection (O(1 to 10 or 100) M Ω/\Box). Needs several microns to get to low enough resistivity for T2K (400 Kohm/sq)
- Other applications
 - Fuel cell battery component

Two fabrication techniques for DLC

- Sputtering : use an argon plasma to vaporize a graphite target
 - BE-sput company in Kyoto (contact by Atsuhiko Ochi). Successfully produced resistivity in the range 0.4-several 10 Mohm per square.
 - Production also in USTC China (contact Yi Zhou)
- Plasma Assisted ion deposition : use a methane plasma in a high E field to deposit carbon on the substrate. Deposition rate 5-10 µ/hour. Need ~2 microns for 400 Kohm/sq (T2K requirement)
 - PAI company in Kyoto

With the PIA technique, bulk resistivity below 10⁻² Ω .cm requires temperatures in excess of 350 °C



Different sparking behaviours of standard and resistive detector:

Standard SLHC2(@10KHz):

Resistive R3(@wide beam,15KHz):



RATE CAPABILITY

Resistive layers slow down the detector, as the charge remains some time on the anode. They degrade slightly the rate capability.



Cluster size distributions

evolution with amplification voltage

T2K MM1-DLC2 (75µm+50) Cosmics





S. Hassani 07/10/2020

Pad Response function

2D distribution : Charge fraction vs Xpad-Xtrack

Fit a parameterization to the profile, for i

$$PRF(x, r, w) = \frac{\exp[-4\ln 2(1-r)x^2/w^2]}{1+4rx^2/w^2}$$

Use the Pad Response Function to obtain the track postion in each padrow from the charge fraction

Re-fit the track and iterate



 q_{i+}

Residuals of the fitted track (after iterations)



Take the geometrical mean between resolution including and excluding the hit in question to get an unbiased result

T2K beam test data



PRF Calibration column #24

M. Lehureaux

Fit to the profile using the ratio of 2 4th order Polynomials

Uniformity of the charge spreading

T. Ogawa ILC

Half width at half maximum of PRF over the module

150	1		1 1	1 1		I I	1 1		1 1	· 1	1.8 E
150	1.722	1.735	1.734	1.662	1.678	1.747	1.713	1.731	1.643	1.609	Ē
	1.717	1.747	1.754	1.712	1.718	1.762	1.752	1.769	1.652	1.613	<u> </u>
	1.692	1.739	1.738	1.707	1.704	1.737	1.739	1.754	1.640	1.605	L L
	1.677	1.724	1.721	1.688	1.697	1.713	1.723	1.748	1.660	1.630 _	1.75
	1.668	1.677	1.686	1.658	1.671	1.714	1.697	1.727	1.685	1.625	- -
5	1.666	1.642	1.661	1.663	1.667	1.702	1.690	1.696	1.681	1.629	0
	1.675	1.709	1.694	1.694	1.669	1.709	1.734	1.763	1.713	1.668	Ξ
Е	1.693	1.723	1.725	1.704	1.705	1.731	1.737	1.764	1.724	1.688	1.7 2
_	_ 1.711	1.729	1.726	1.714	1.682	1.732	1.738	1.758	1.713	1.697	.E
te	1.697	1.725	1.723	1.710	1.689	1.711	1.762	1.746	1.700	1.665	ä
а	1.698	1.726	1.732	1.709	1.677	1.715	1.764	1.768	1.710	1.671	Ë
⊒.	1.689	1.708	1.729	1.698	1.697	1.728	1.758	1.741	1.702	1.650	1 65 ×
y coord	1.699	1.703	1.707	1.681	1.689	1.708	1.739	1.736	1.700	1.663	20 °
	1.690	1.691	1.695	1.666	1.663	1.686	1.714	1.723	1.689	1.658	÷
	1.673	1.682	1.691	1.658	1.660	1.682	1.714	1.718	1.691	1.658	b)
	1.689	1.678	1.691	1.666	1.665	1.691	1.720	1.719	1.693	1.652	다. 두
	1.674	1.709	1.687	1.673	1.684	1.690	1.735	1.718	1.679	1.640	1.6 0
	1.675	1.679	1.671	1.668	1.669	1.684	1.728	1.712	1.653	1.636	≥
	1.691	1.673	1.662	1.655	1.661	1.670	1.714	1.708	1.646	1.626	<u> </u>
	1.673	1.648	1.648	1.638	1.639	1.672	1.703	1.685	1.636	1.629	<u>9</u>
	1.675	1.631	1.636	1.641	1.635	1.662	1.695	1.676	1.643	1.636	1.55 📥
	1.651	1.636	1.642	1.637	1.642	1.658	1.679	1.669	1.643	1.625	
	1.678	1.633	1.634	1.629	1.625	1.639	1.655	1.660	1.633	1.611	
0	1.658	1.592	1.594	1.582	1.578	1.629	1.639	1.637	1.573	1.585	
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$$\sigma = sqrt(2t/RC)$$

The PRF width is very uniform : 1.6 to 1.7mm

An RC map can be obtained from a fit to the waveforms (T2K)

The electronic response is fitted to the leading pad waveform, and RC is fitted to the convolution of the response by the expected signal shape in the two neighbouring pads. Note that both amplitude and time are sensitive to the track position (G. Collazuol).



RC(ns/mm2) map from analytical fit



Position resolution

T. Ogawa, S. Ganjour, ILC



Resolution at zero drift distance : 60 μ m with 3mm pads. Gain by a factor of 14 with respect to w/ $\sqrt{12}$!



Figure 9: The distributions of the spatial and z resolution for different drift lengths over all pad-rows in three modules with the track reconstruction using those modules.

dE/dx measurement



T. Ogawa



Mitigation of distortions

The ERAM scheme allows the mesh to be at ground, while the resistive coating is at a positive high voltage.

As the frames are necessarily grounded, this provides a much better equipotential surface at the endplate level.

As a consequence, distortions are suppressed by an order of magnitude.

This also brings a large flexibility as this allows to have a module at a different voltage, or even switched of, without affecting the neighbours.



Future

A Micromegas TPC with a resistive anode is one of the options of SAND (the DUNE near detector), surrounding a 3D Scintillator Tracker and centered on the beam axis, in the KLOE magnet.





Compared to T2K / ND280: Higher momentum beam and Hydrogen-rich target (no Fermi motion smearing) -> better space resolution and segmentation

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Conclusions

- The ERAM structure (Encapsulated Resistive Anode Micromegas) is a good way of improving
 - resolution and cost-effectiveness
 - detector stability
 - distortion mitigation
 - flexibility
- There are already several applications in progress of ERAM-equipped TPCs