

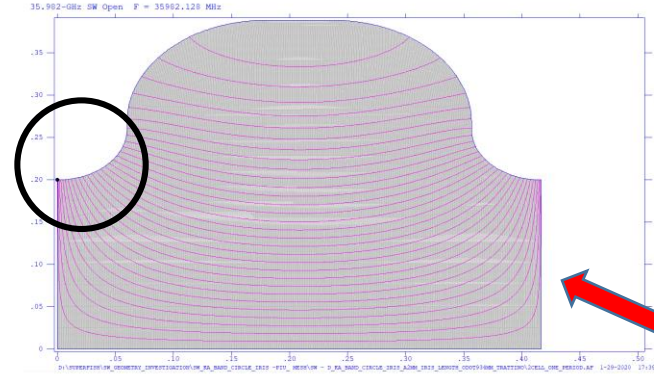
Investigations on the Standing Wave Ka-Band linearizer with a 2 mm iris radius

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On behalf of Compact Light XLS project

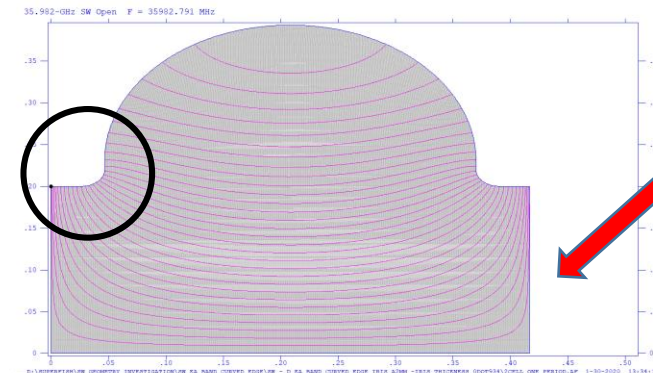
Simulated geometries profile of the Standing Wave Ka-Band structure

1) Rounded iris

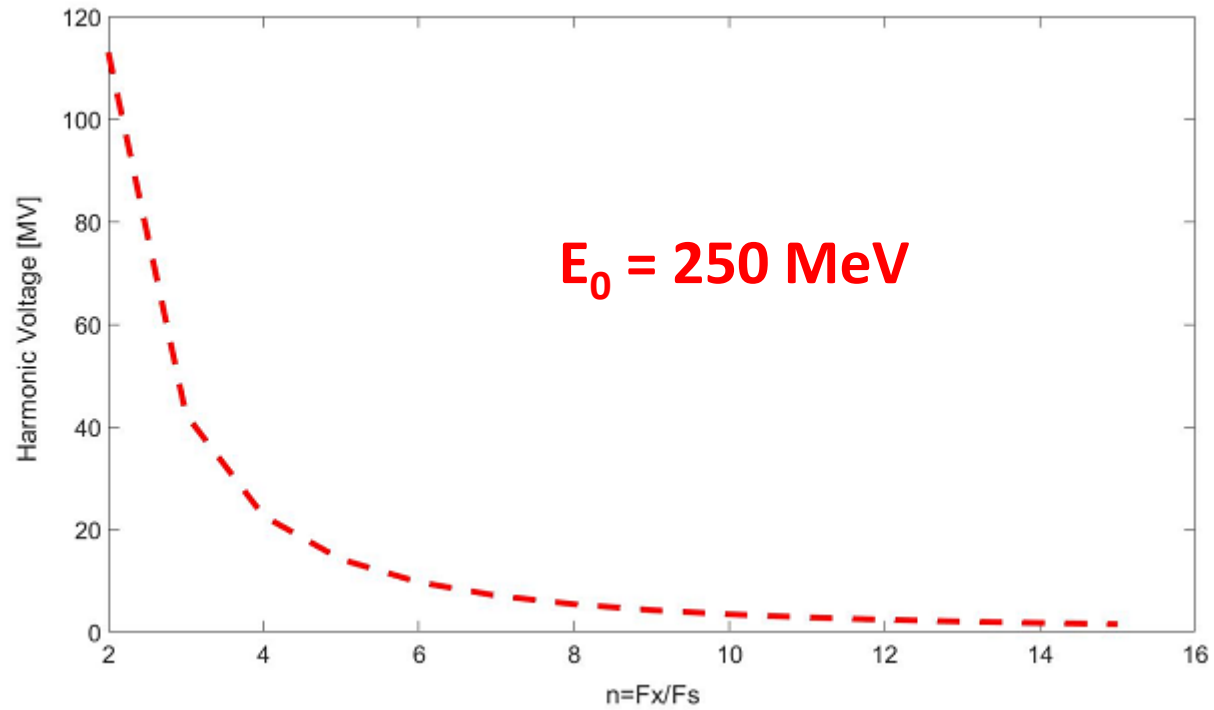


2 mm iris radius

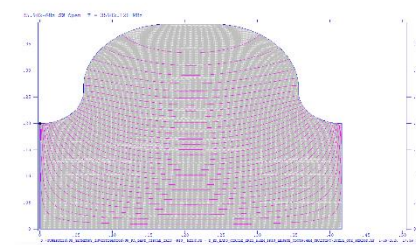
2) Iris fillet with 0.2 mm radius



Harmonic Voltage (according to P. Emma paper)



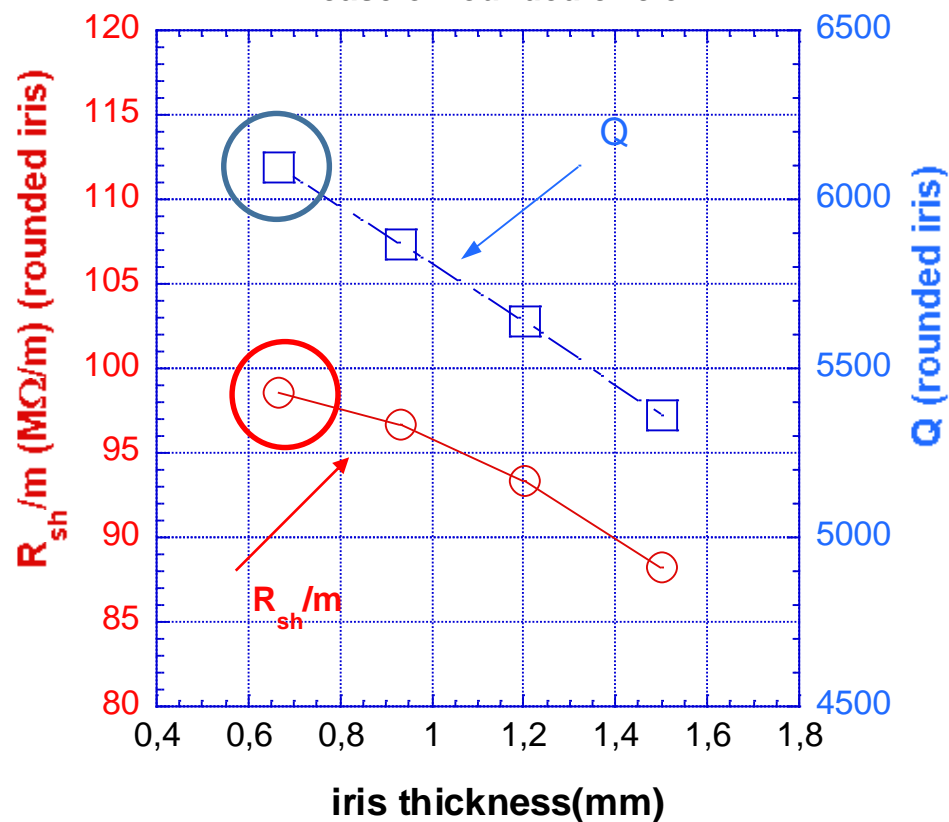
Shunt impedance and quality factor Q as function of the iris thickness



Rounded iris

Rounded iris with a 2 mm iris radius

Shunt impedance R_{sh}/m and unloaded quality factor Q as function of the iris thickness with an 2 mm iris radius at the operating frequency $F = 35.982$ GHz in case of rounded circle

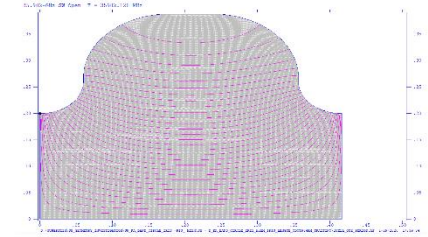


With a $h = 0.667$ mm iris thickness

- $R_{sh}/m \sim 99$ M Ω /m
- $Q \sim 6100$

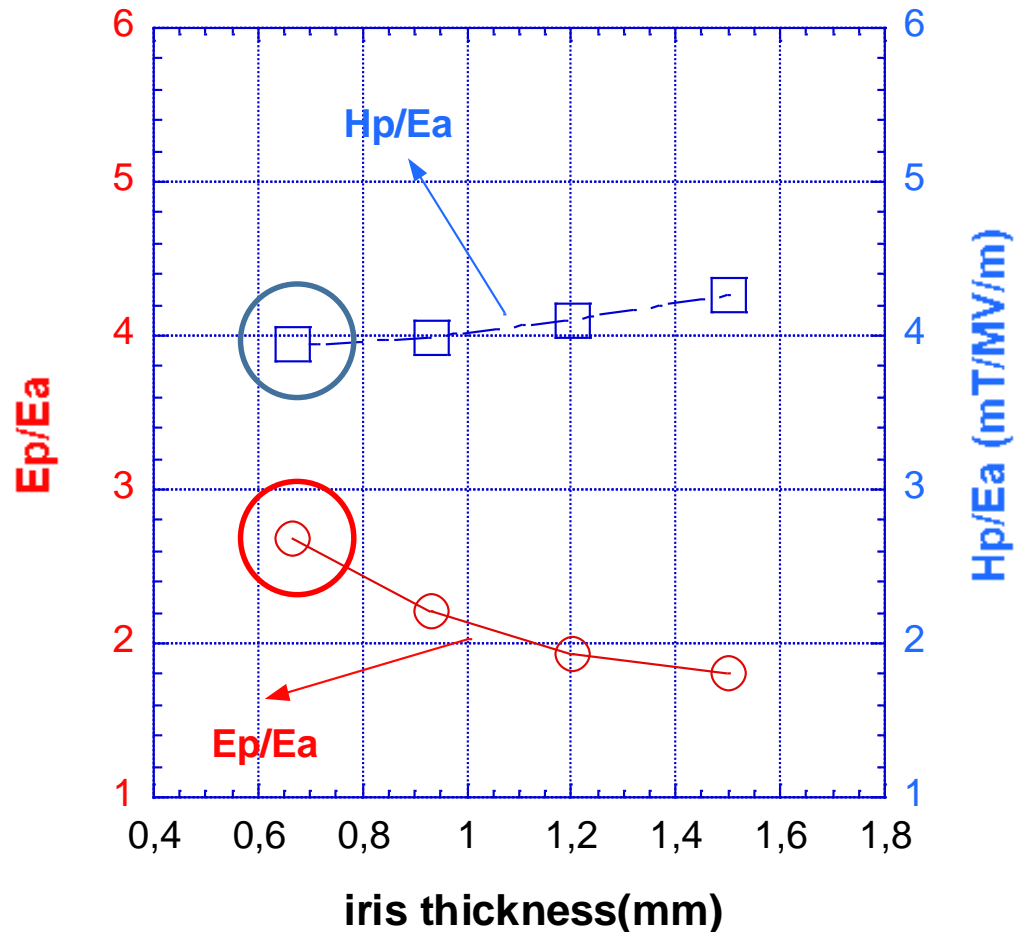
E_p/E_a and H_p/E_a as function of the iris thickness

Rounded iris with a 2 mm iris radius



Rounded iris

E_p/E_a and H_p/E_a as function of the iris thickness
at $F = 35.982$ GHz in case of rounded iris



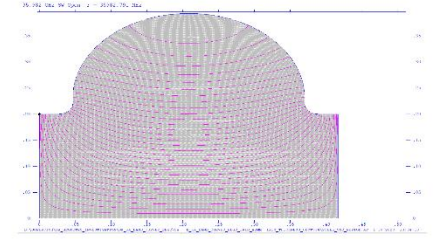
With a $h = 0.667$ mm iris thickness

$E_p/E_a \sim 2.67$

$H_p/E_a \sim 3.95$

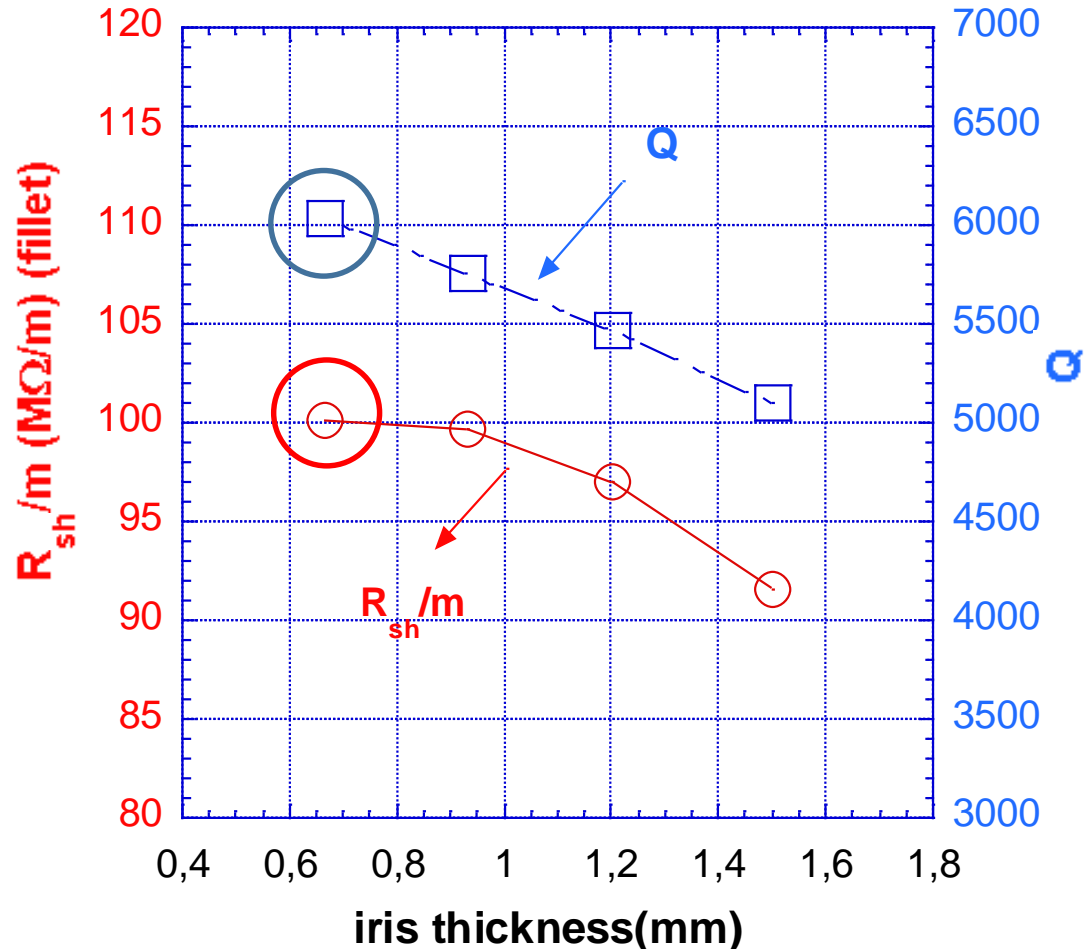
Shunt impedance and quality factor Q as function of the iris thickness

2 mm iris radius and a 0.2 mm Fillet radius



Fillet iris

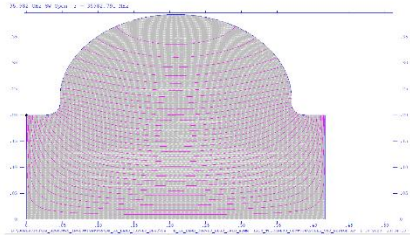
Shunt impedance R_{sh}/m and unloaded quality factor Q as function of the iris thickness with a 2 mm iris radius at the operating frequency $F = 35.982$ GHz in case of fillet shape with 0.2 mm radius



With a $h = 0.667$ mm iris thickness

- $R_{sh}/m \sim 100$ MΩ/m
- $Q \sim 6030$

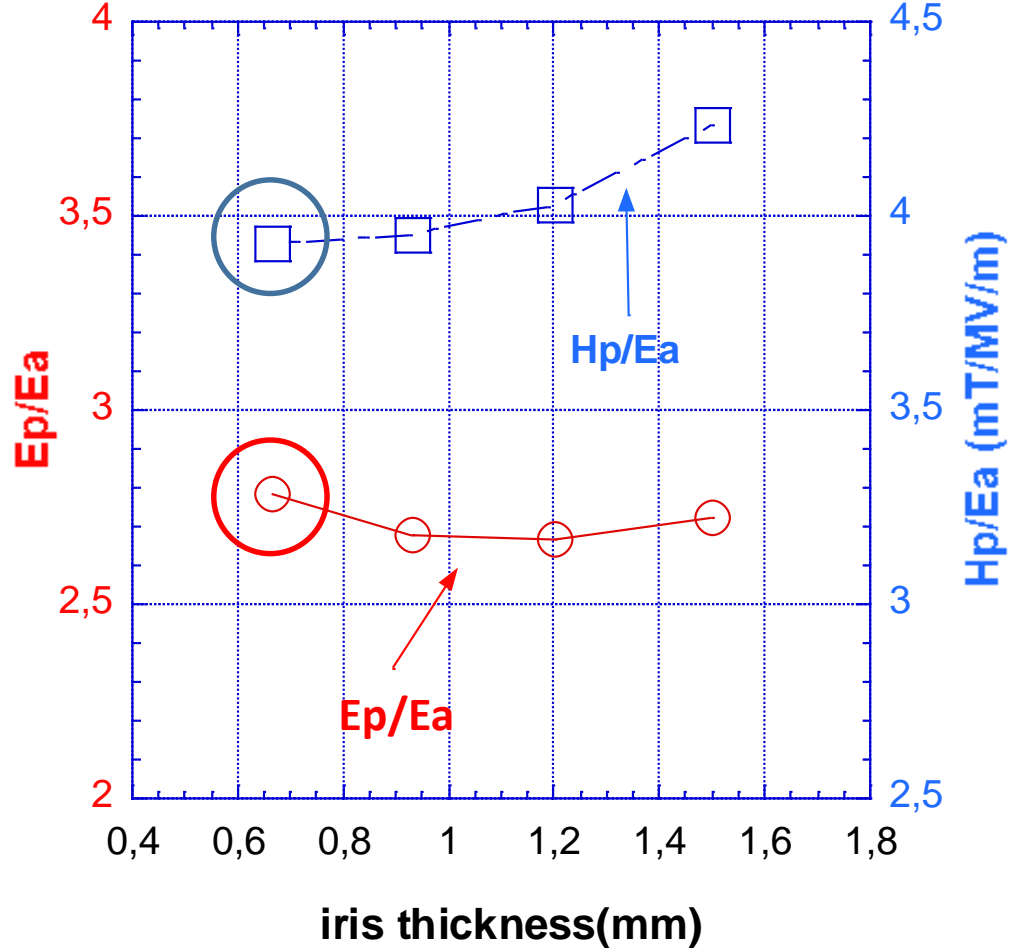
Ep/Ea and Hp/Ea as function of the iris thickness



Fillet iris

2 mm iris radius and a 0.2mm Fillet radius

Ep/Ea and Hp/Ea as function of the iris thickness with a 2 mm iris radius at F = 35.982 GHz in case of fillet shape with 0.2 mm radius

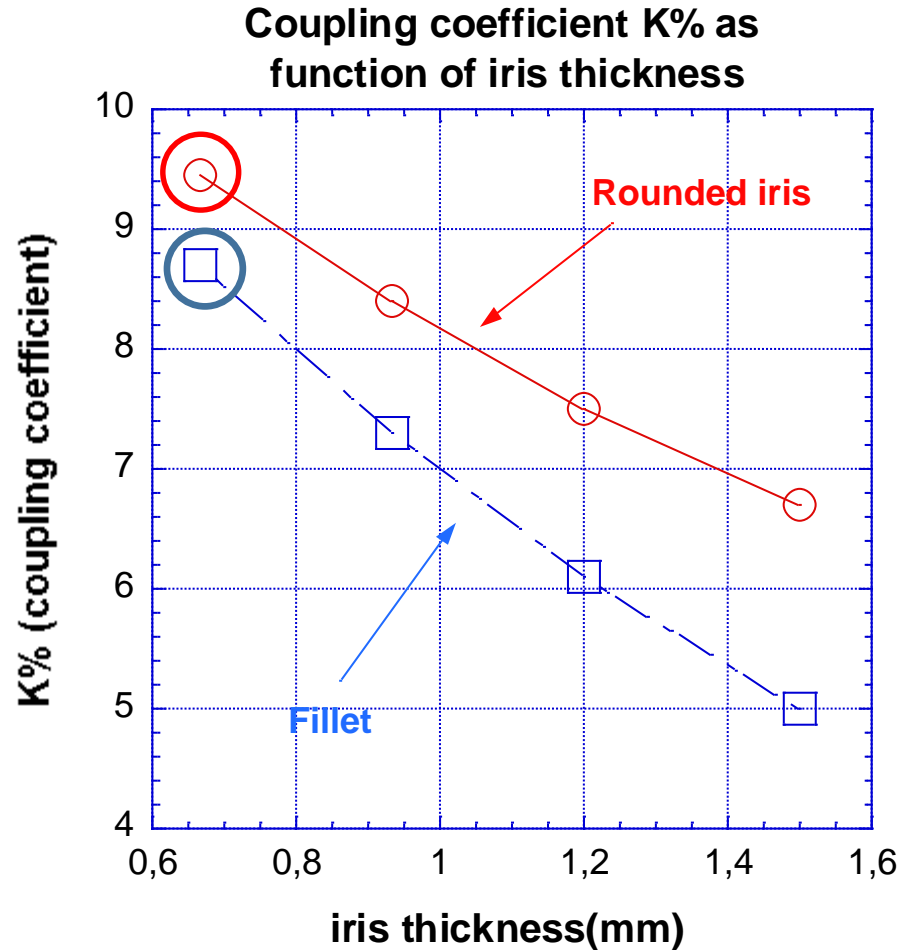


With a h = 0.667 mm iris thickness

Ep/Ea ~ 2.78

Hp/Ea ~ 3.93

Cell to cell coupling coefficient as function of the iris thickness



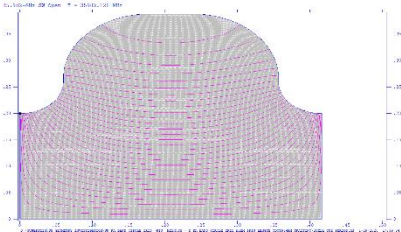
With a $h = 0.667$ mm iris thickness

**Rounded iris $K = 9.5 \%$
(cell to cell coupling coefficient)**

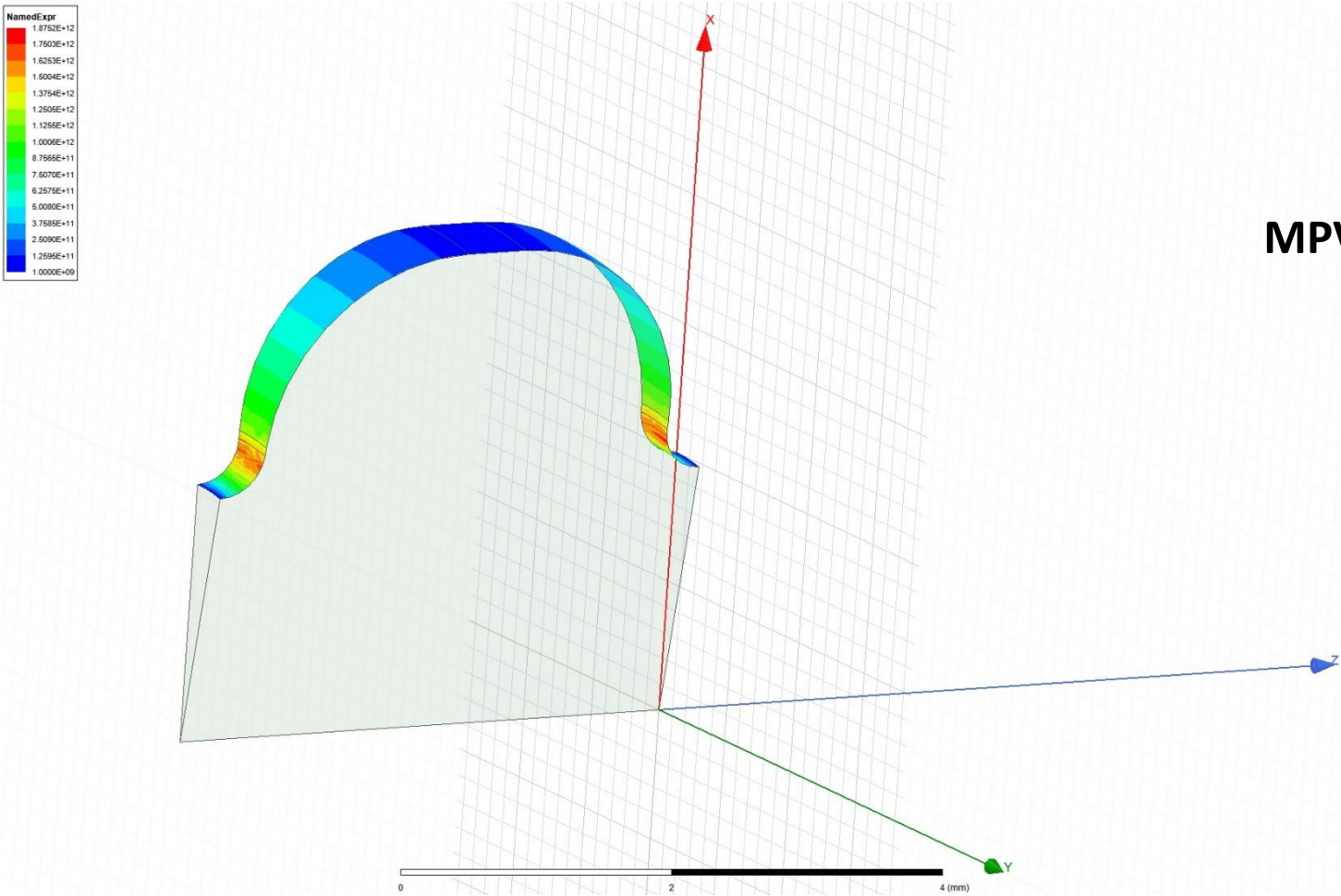
**Fillet iris $K = 8.7 \%$
(cell to cell coupling coefficient)**

Modified Poynting vector at Eacc = 70 MV/m

Rounded circle with a 2 mm iris radius and 0.667 mm thickness radius



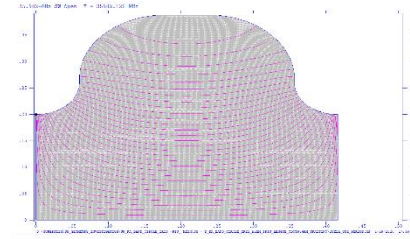
Rounded iris



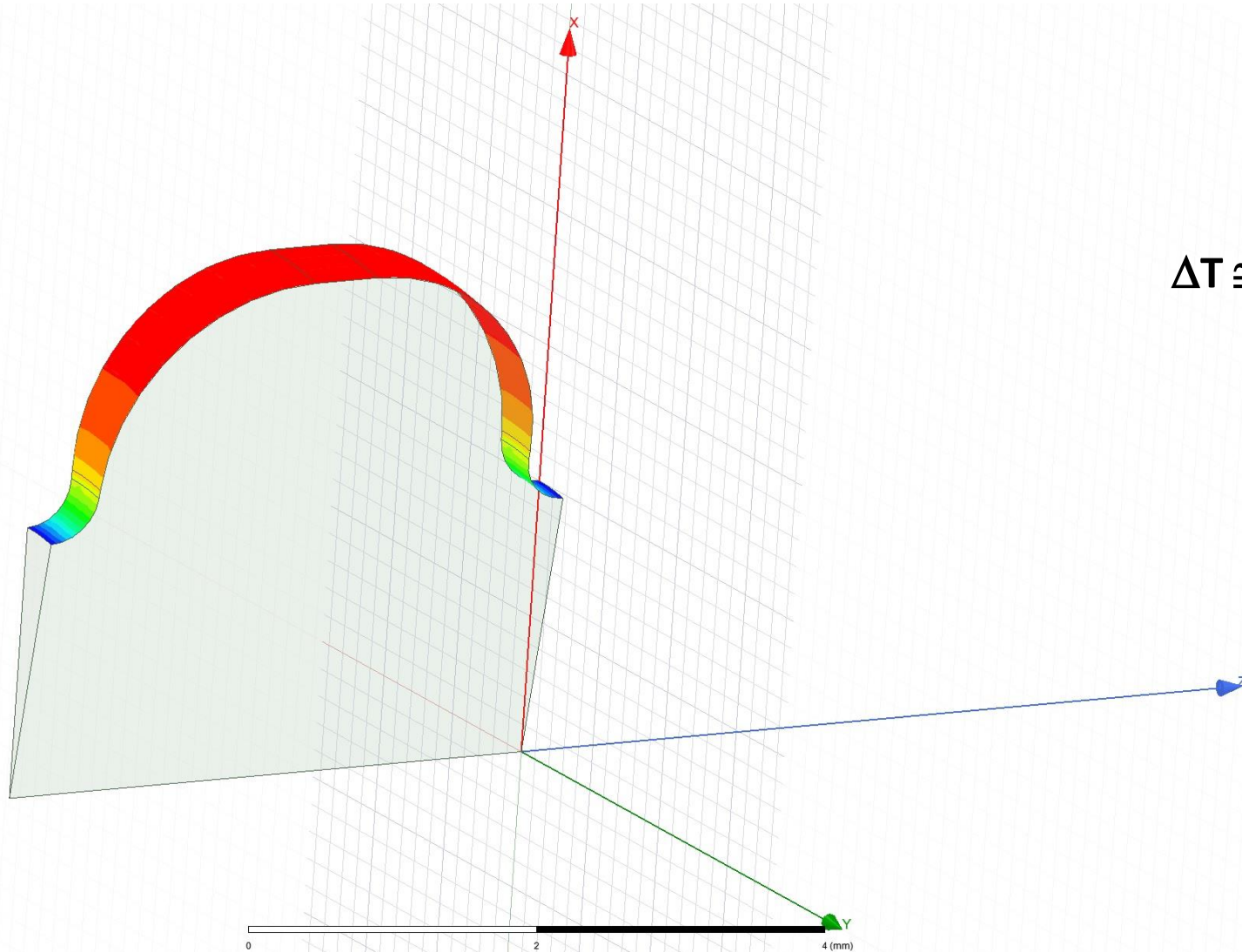
$MPV \cong 1.88 \text{ MW/mm}^2$

Pulse Heating at 70 MV/m@50 ns

Rounded circle with a 2 mm iris radius and 0.667 mm thickness radius



Rounded iris



$\Delta T \cong 7.50 \text{ } ^\circ\text{C}$

Modified Poynting Vector and pulse heating with a 2 mm iris radius and rounded iris (iris thickness 0.667 mm)

Eacc (MV/m)	EF (MV/m)	HF (MA/m)	Modified Poynting Vector (MW/mm ²)	Pulse Heating (Celsius °C)
35	93.65	0.11	0.47	1.87
70	187.53	0.21	1.88	7.50

K = 9.5 % (cell to cell coupling coefficient)

Modified Poynting Vector and pulse heating with a 2 mm iris radius and fillet iris (iris thickness 0.667 mm)

Eacc (MV/m)	EF (MV/m)	HF (MA/m)	Modified Poynting Vector (MW/mm ²)	Pulse Heating (Celsius °C)
35	93.65	0.10	0.43	1.57
70	187.53	0.20	1.72	6.29

K = 8.7 % (cell to cell coupling coefficient)

Conclusions

Assuming a 8 cm structure length, 5 MW matched input power, $R_{sh} \sim 100 \text{ M}\Omega/\text{m}$ we obtain an average accelerating Electric Field $E_{acc} \sim 80 \text{ MV/m}$

Gyroklystron gives $P = 3 \text{ MW}$ (Cern – England) and by using the SLED we are able to get $P = 12 \text{ MW}$

In all cases the modified Poynting vector and the pulse heating are well below the safety thresholds

The circulator has to be designed !

Cryostructure

At 77 Kelvin degree with a 2.2 enhancement factor (From J. Rosenzweig) the shunt impedance is estimated to be $R_{sh} = 220 \text{ M}\Omega/\text{m}$.

With $P = 3 \text{ MW}$ we are able to get an average electric field $E_{acc} \sim 91 \text{ MV/m}$ by assuming a 8 cm structure length

Thank you very much for your attention !