

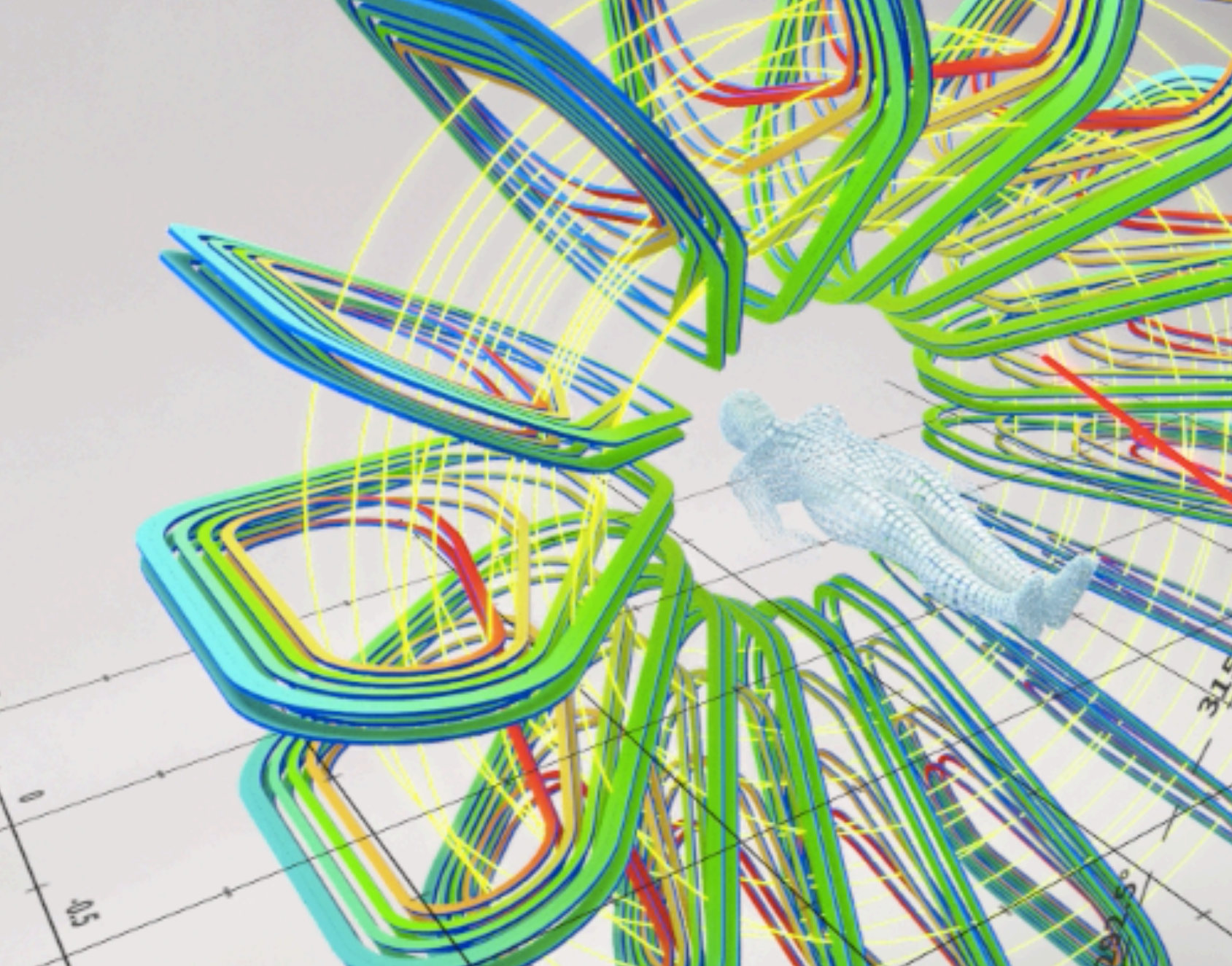


HTS Demonstrator Mechanics

GaToroid Project

Jérôme Harray

February 7, 2020



GaToroid Project

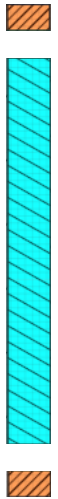
- **Demonstration of HTS technology**
- **Development of a prototype in scalable conditions**
- **Coil box design to freeze magnet nominal position**
- **Bolt stress state assessment**

Contact modeling

	Gap open/ close?	Sliding allowed?
Bonded	No	No
Frictionless	Yes	Yes, $\mu = 0$
Frictional	Yes	Yes, $F_{sliding} > F_{friction}$

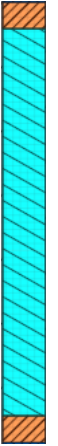
Pole - contact

- Contact between the **pole** & **1th tape stack** → **frictionless**
- Pre-constraint check-point → **pressure inspection**
- Pole material → pre-constraint strategy with $\alpha_{pole} < \alpha_{rim}$



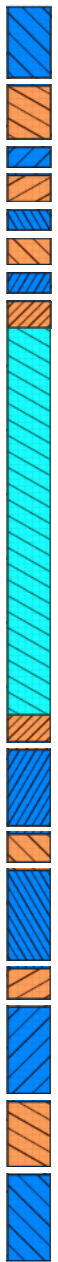
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Windings - contact

- If resin assumed as **non-structural** → **frictional** contact $\mu = 0.3$
- If resin keeps components altogether → **bonded** contact
- **Contact stress magnitude** to keep the contact between components
- Warnings: **linear** model → **dynamic** effects & **crack** propagation dismissed



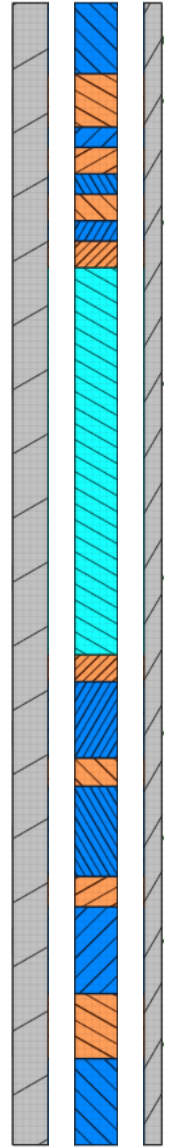
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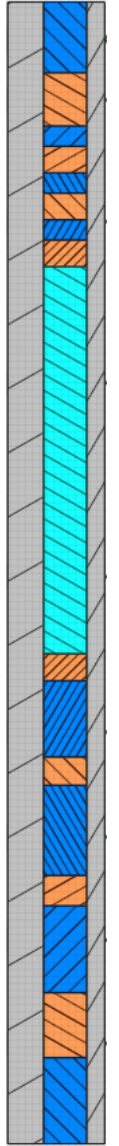
Coil box - contact

- Contact mainly subjected to **shear** from **contraction** & **Lorentz forces**
- Assumed all-time as **frictional** with $\mu = 0.3$



Coil box - contact

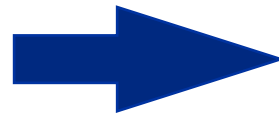
- Contact mainly subjected to **shear** from **contraction** & **Lorentz forces**
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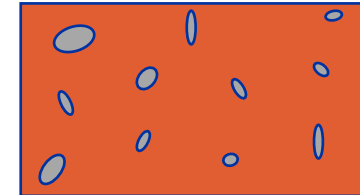
Isotropic tape model

- Tape material composition: 70% SS & 30% Cu
- HTS cable with **insulation** composition: 19% SS & 81% Cu
- **Stacked** layout → **anisotropic** ~ orthotropic
- Lack of data → material model **simplification**

Anisotropic



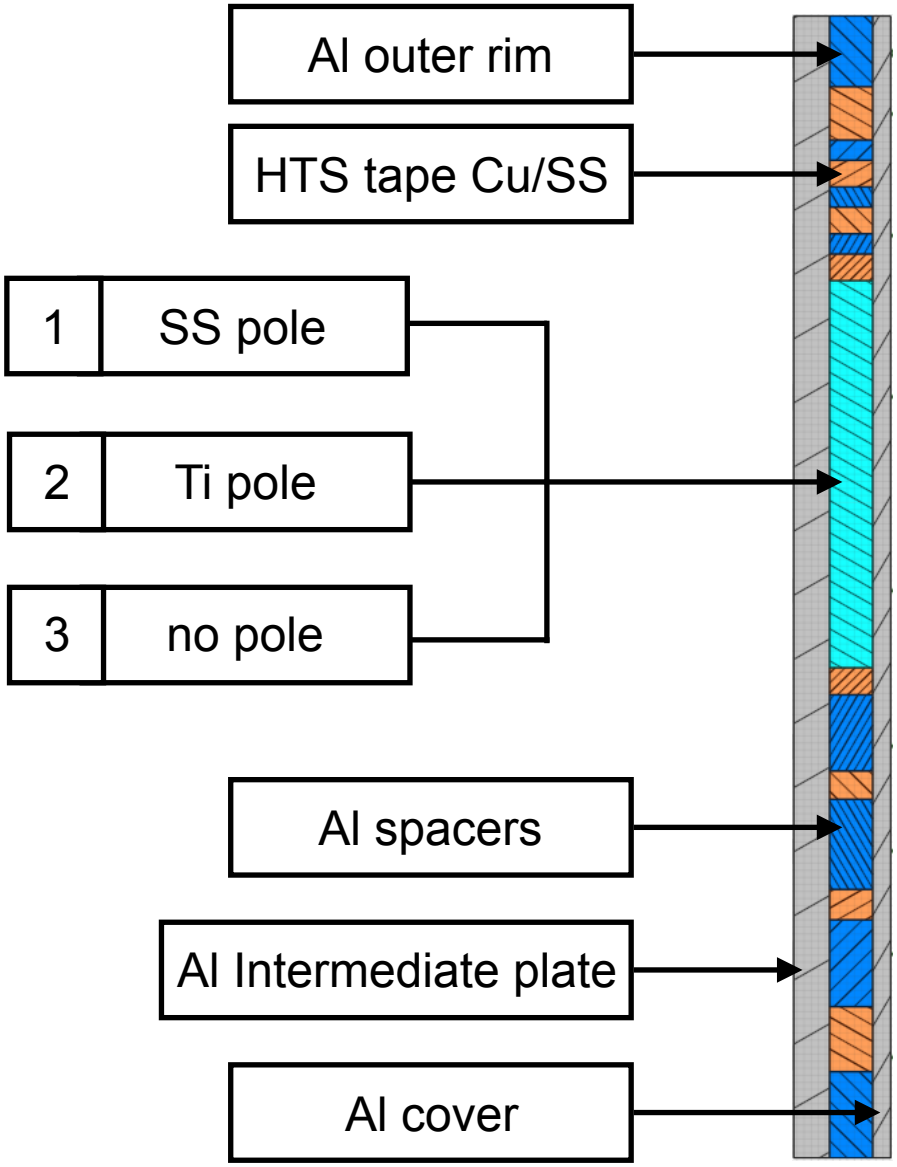
Isotropic



Material configurations

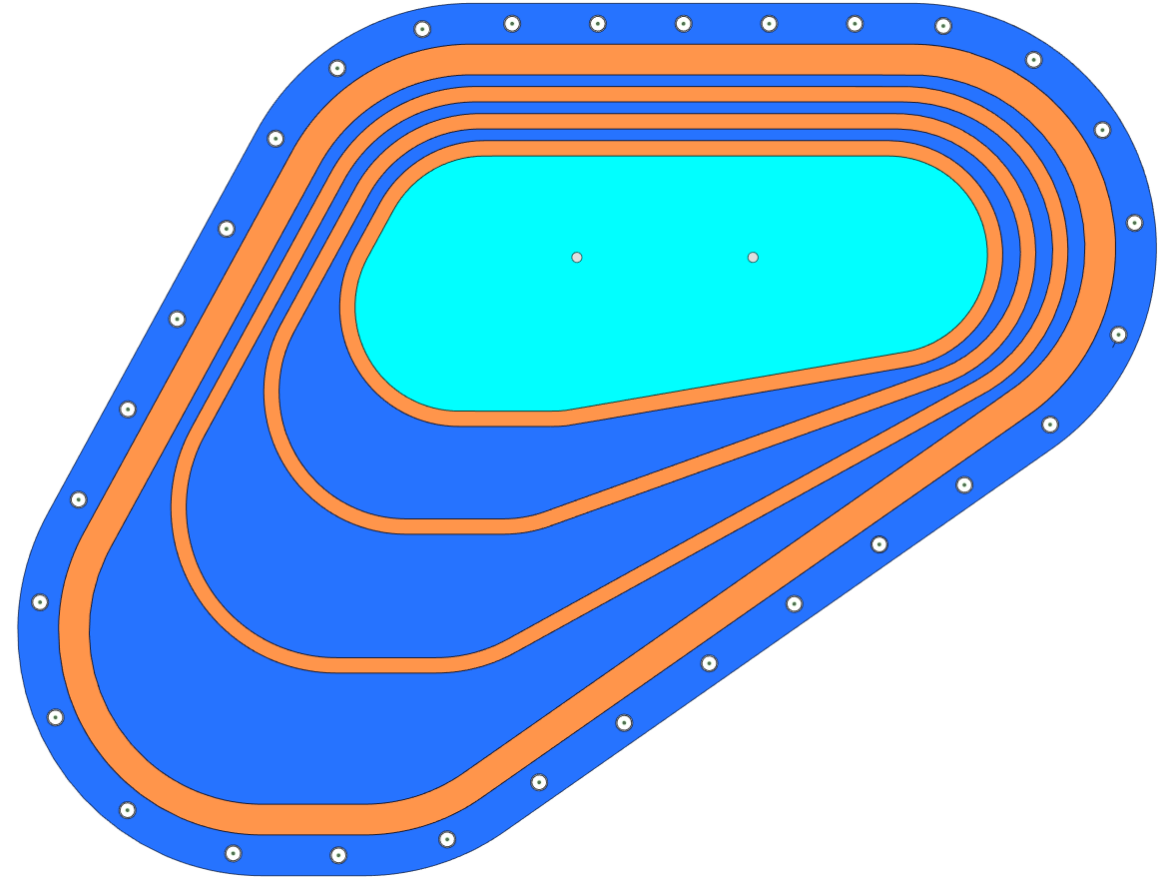
- Use of **Aluminium** for **structural** components
- Different **pre-constraint** strategies:
 1. Stainless Steel pole
 2. Titanium pole
 3. No pole

	Al	SS	Ti	HTS mixture
α [C ⁻¹]	1,44E-05	9,9E-06	5E-06	1,10E-05



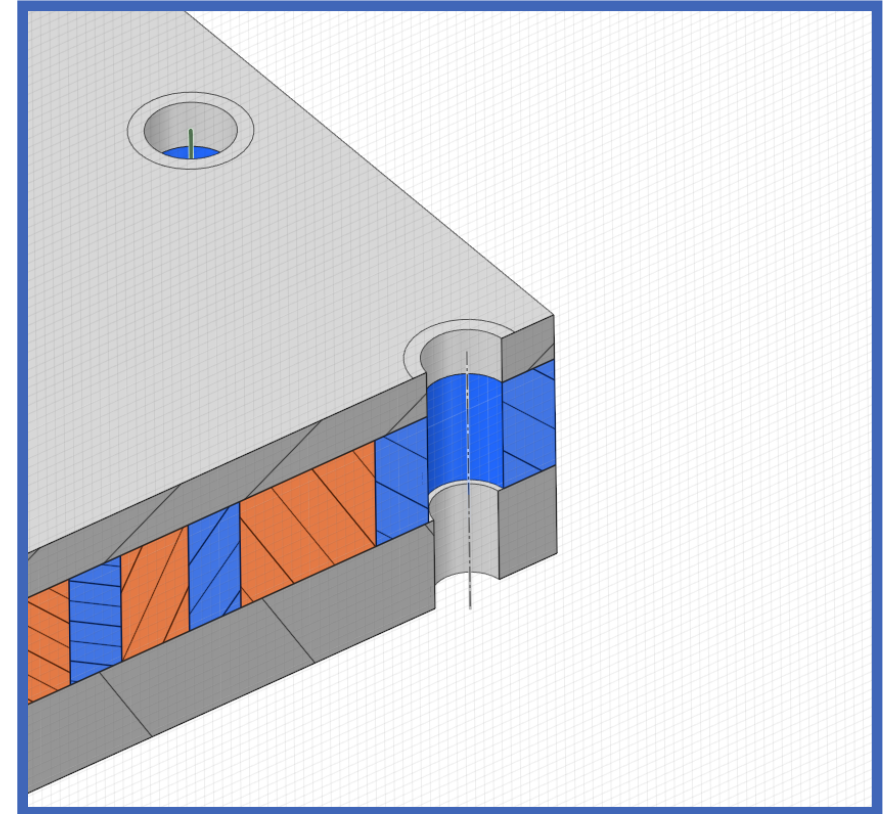
Bolts - layout

- **30 x M8 bolts** equally spaced along outer rim
- Pole falsely fixed at its centre
- Spacers **unpinned** in nominal conditions
- **Fixed spacers** configuration inspected

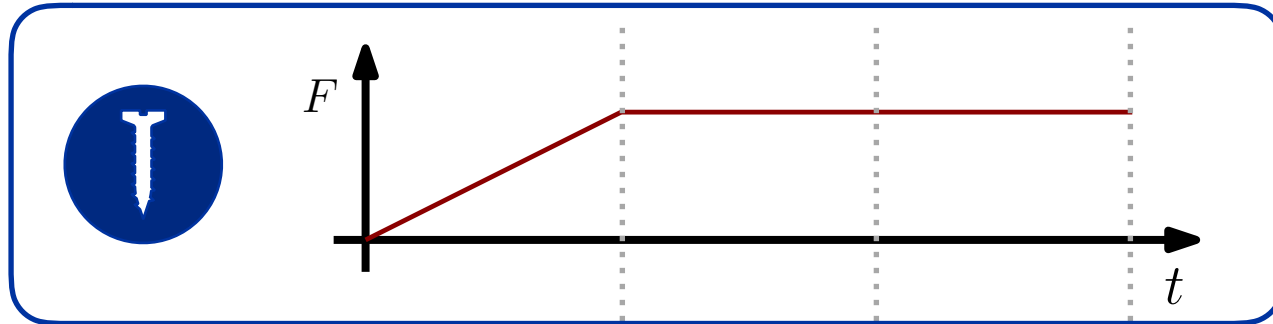


Bolts - modeling

- Load transmission
 - **Thread** in intermediate plate
 - **Head** surface on cover plate
- Bolt body simplified as **body line**
- **Pretension** applied on body line

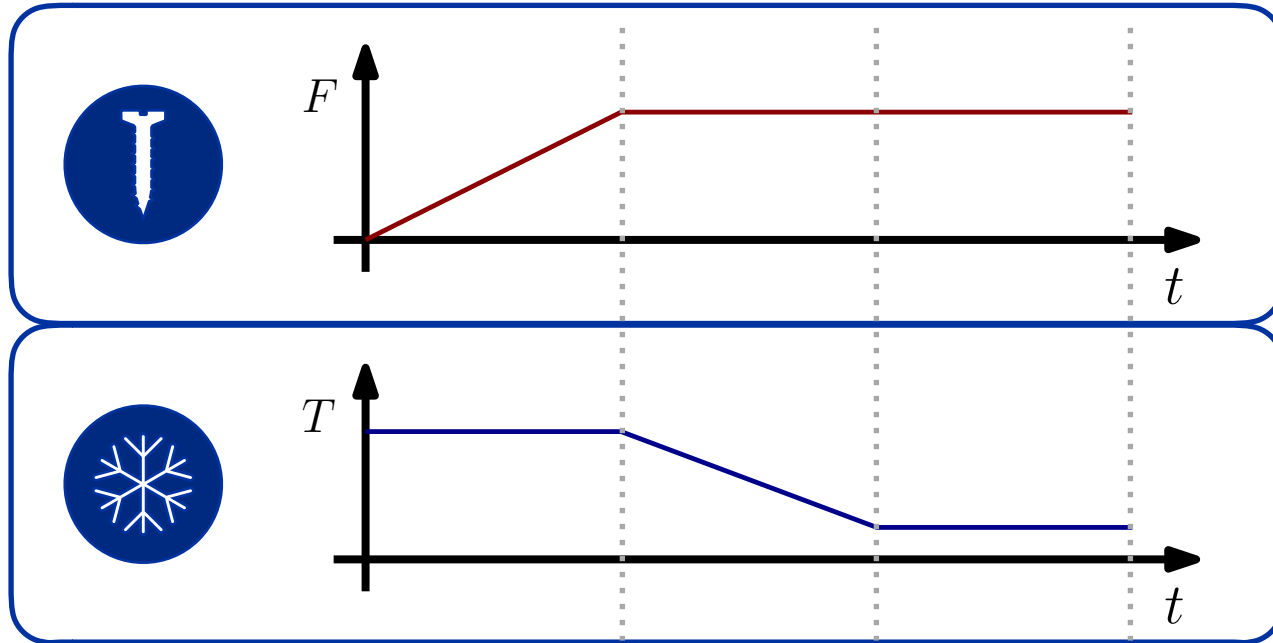


Multi-step static analysis



(1) Bolt pretension

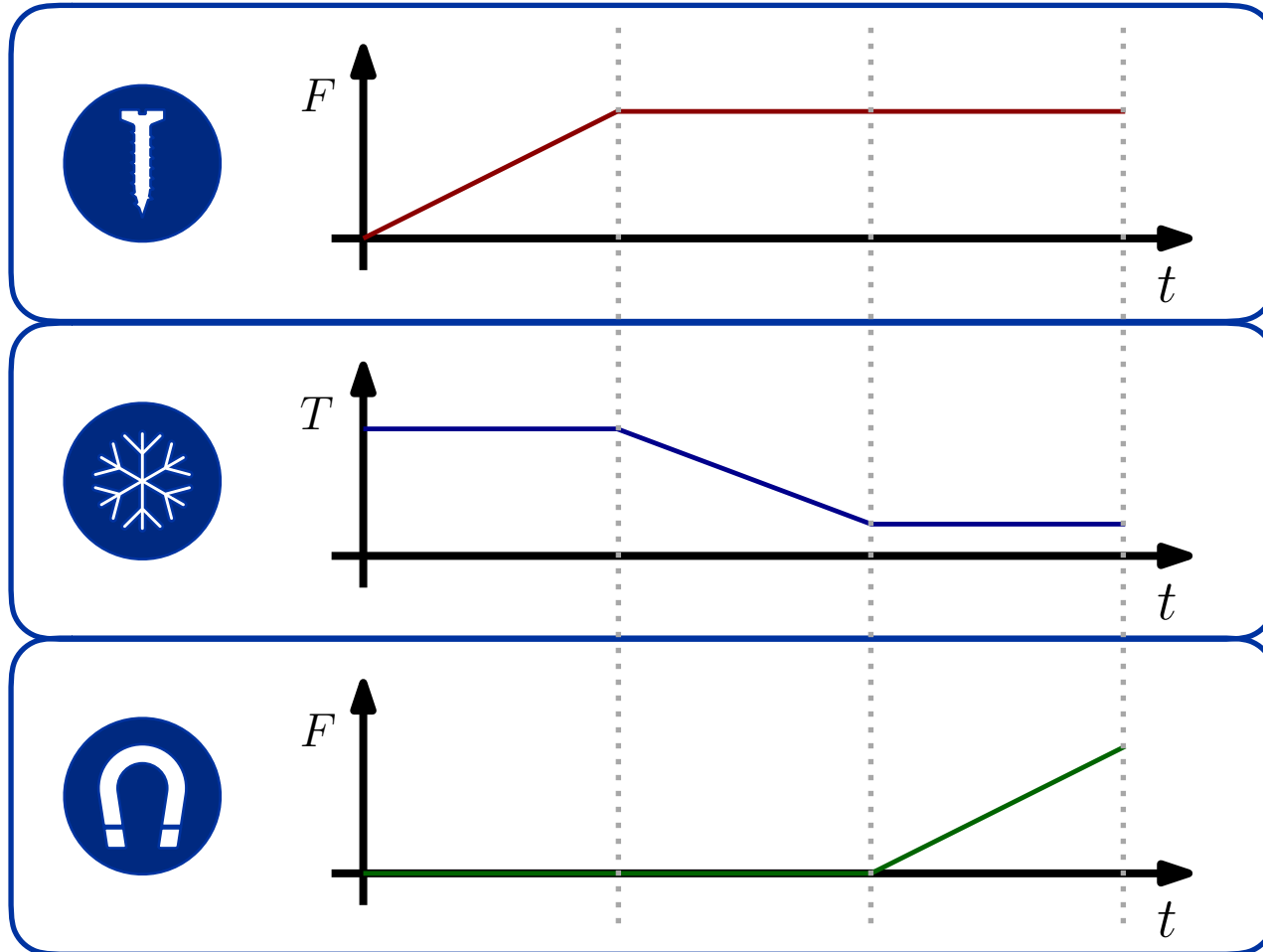
Multi-step static analysis



(1) Bolt pretension

(2) Cool-down

Multi-step static analysis



(1) Bolt pretension

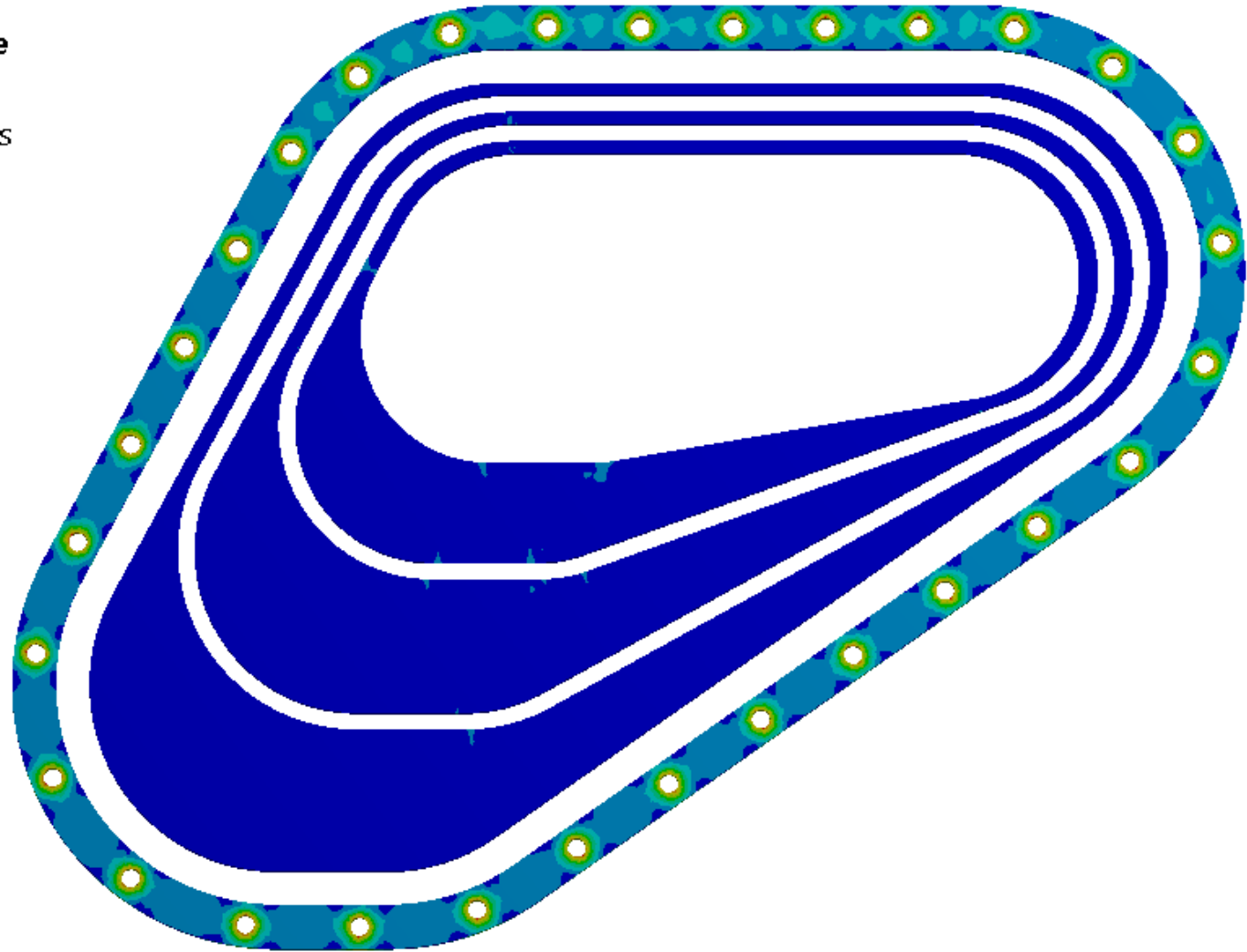
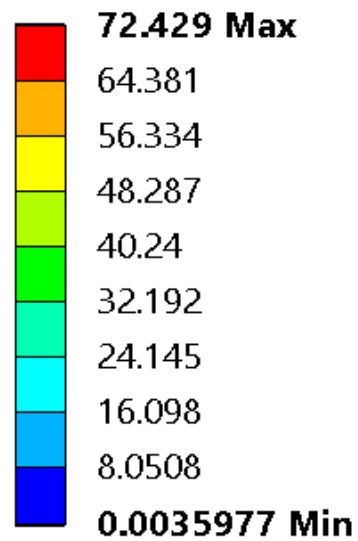
(2) Cool-down

(3) Lorentz forces

Results

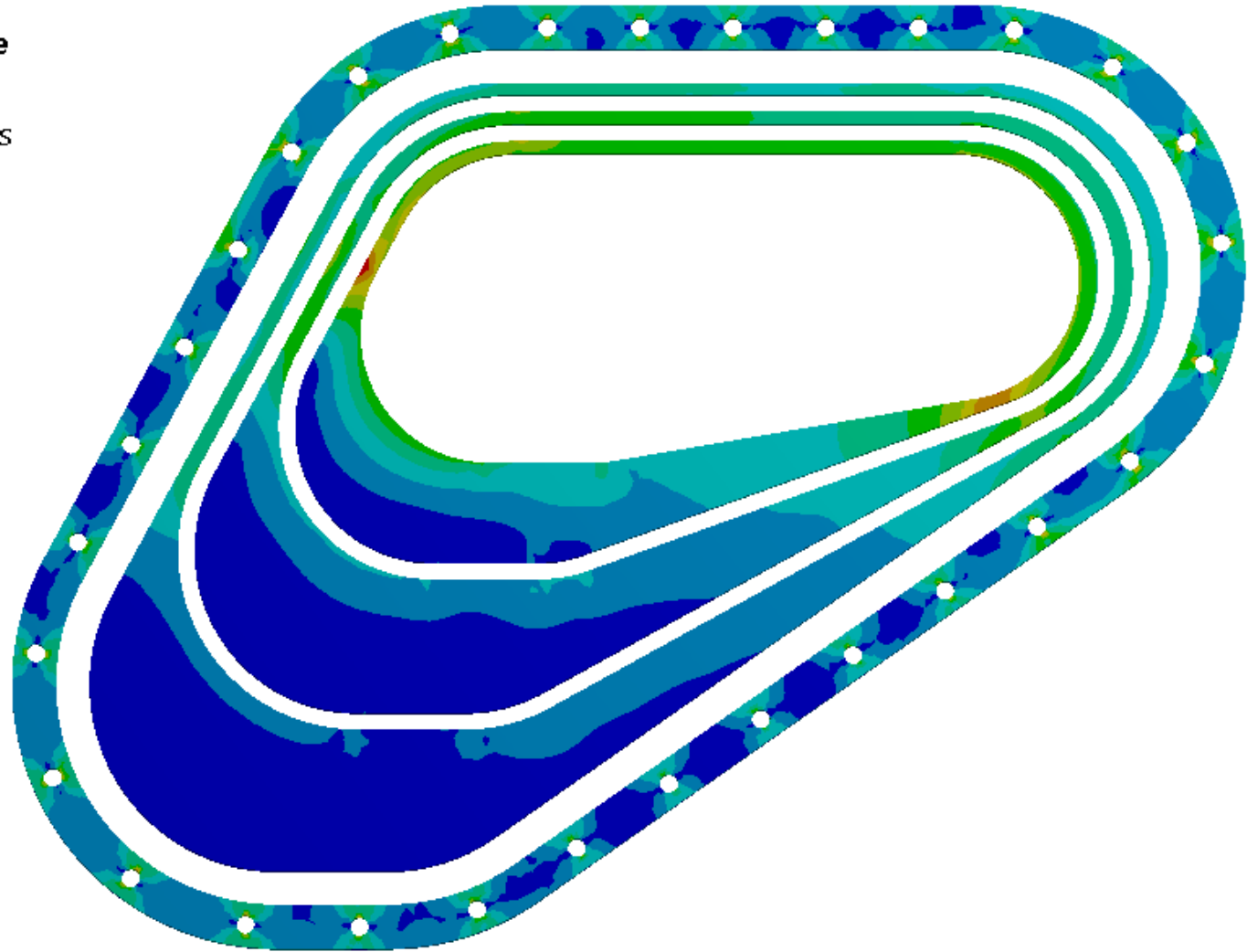
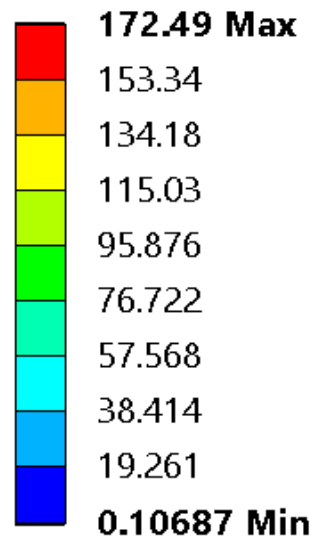
Spacers - equivalent stress (1)

C: coil friction - pole SS - coarse
Equivalent Stress - spacers
Type: Equivalent (von-Mises) Stress
Unit: MPa
Time: 1
07/02/2020 13:32



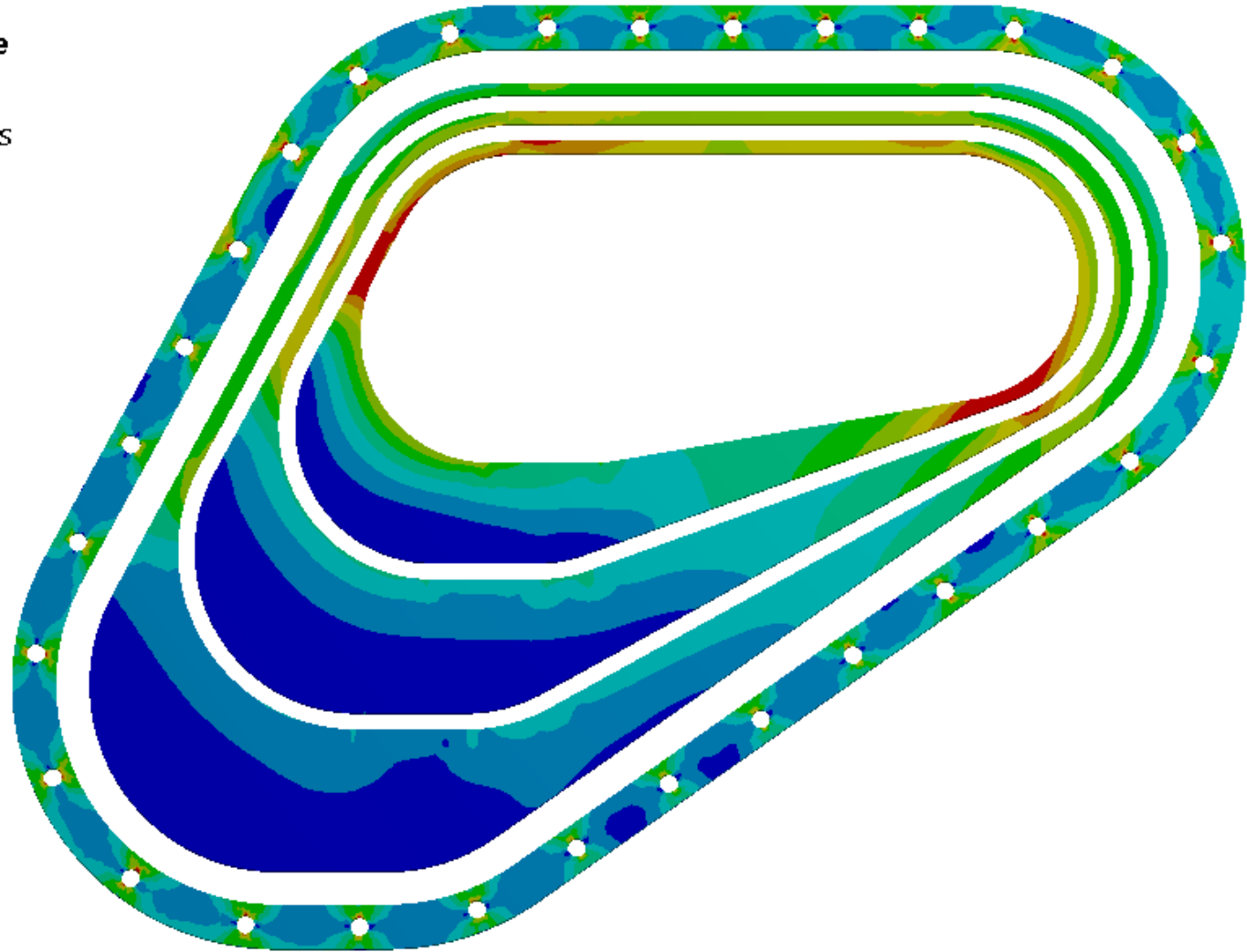
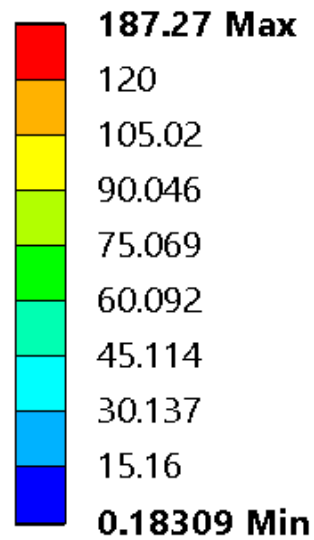
Spacers - equivalent stress (2)

C: coil friction - pole SS - coarse
Equivalent Stress - spacers 2
Type: Equivalent (von-Mises) Stress
Unit: MPa
Time: 2
07/02/2020 13:33



Spacers - equivalent stress (3)

C: coil friction - pole SS - coarse
Equivalent Stress - spacers 3
Type: Equivalent (von-Mises) Stress
Unit: MPa
Time: 3
07/02/2020 13:34



Coils - equivalent stress (1)

C: coil friction - pole SS - coarse

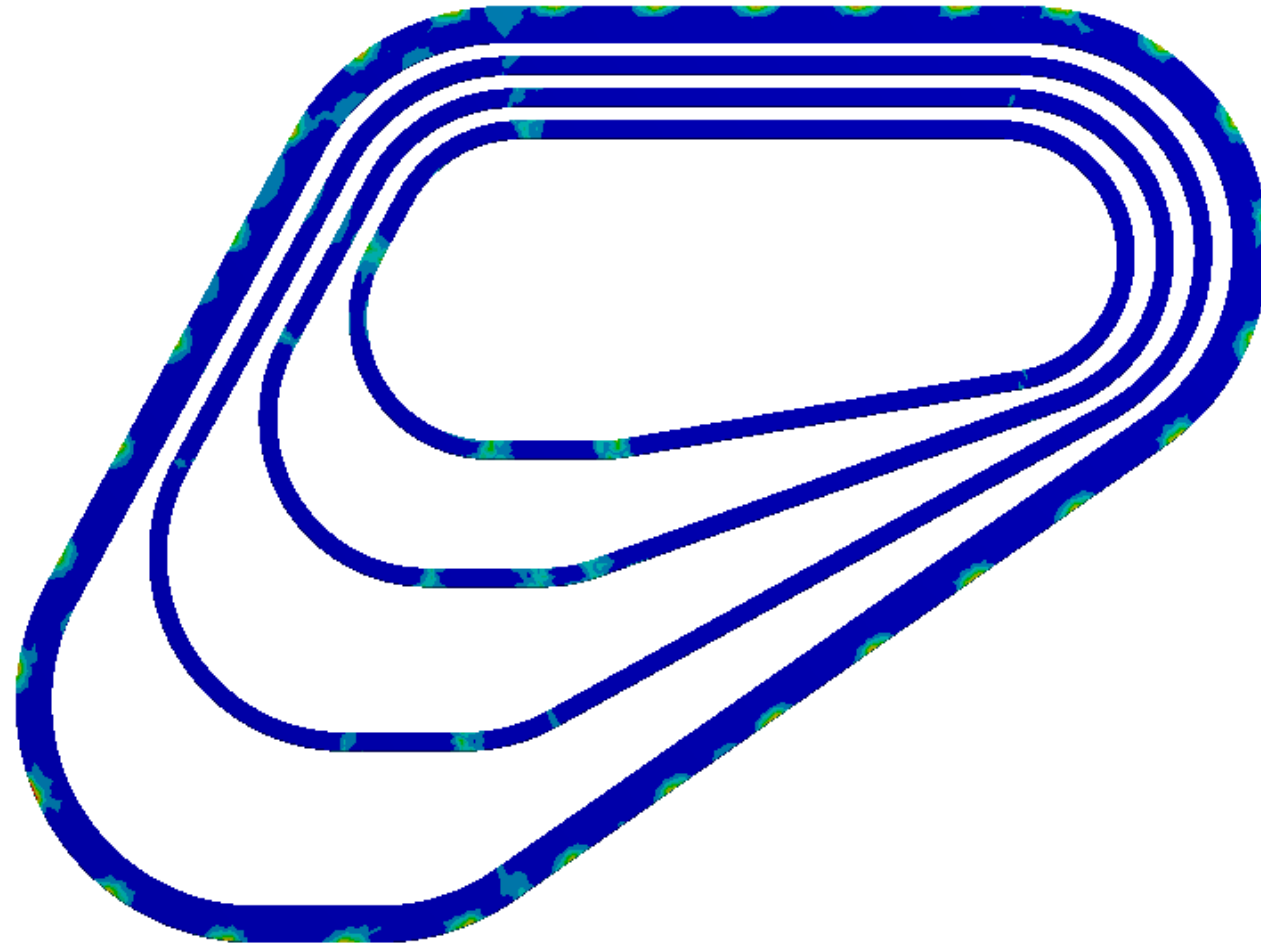
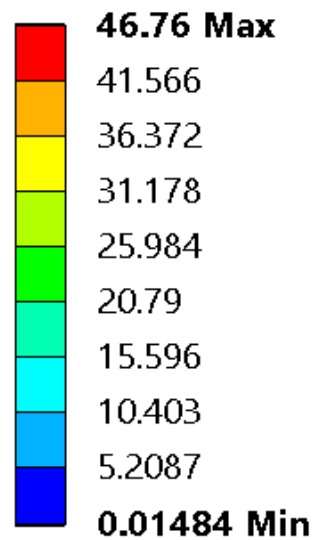
Equivalent Stress - coil

Type: Equivalent (von-Mises) Stress

Unit: MPa

Time: 1

07/02/2020 13:34



Coils - equivalent stress (2)

C: coil friction - pole SS - coarse

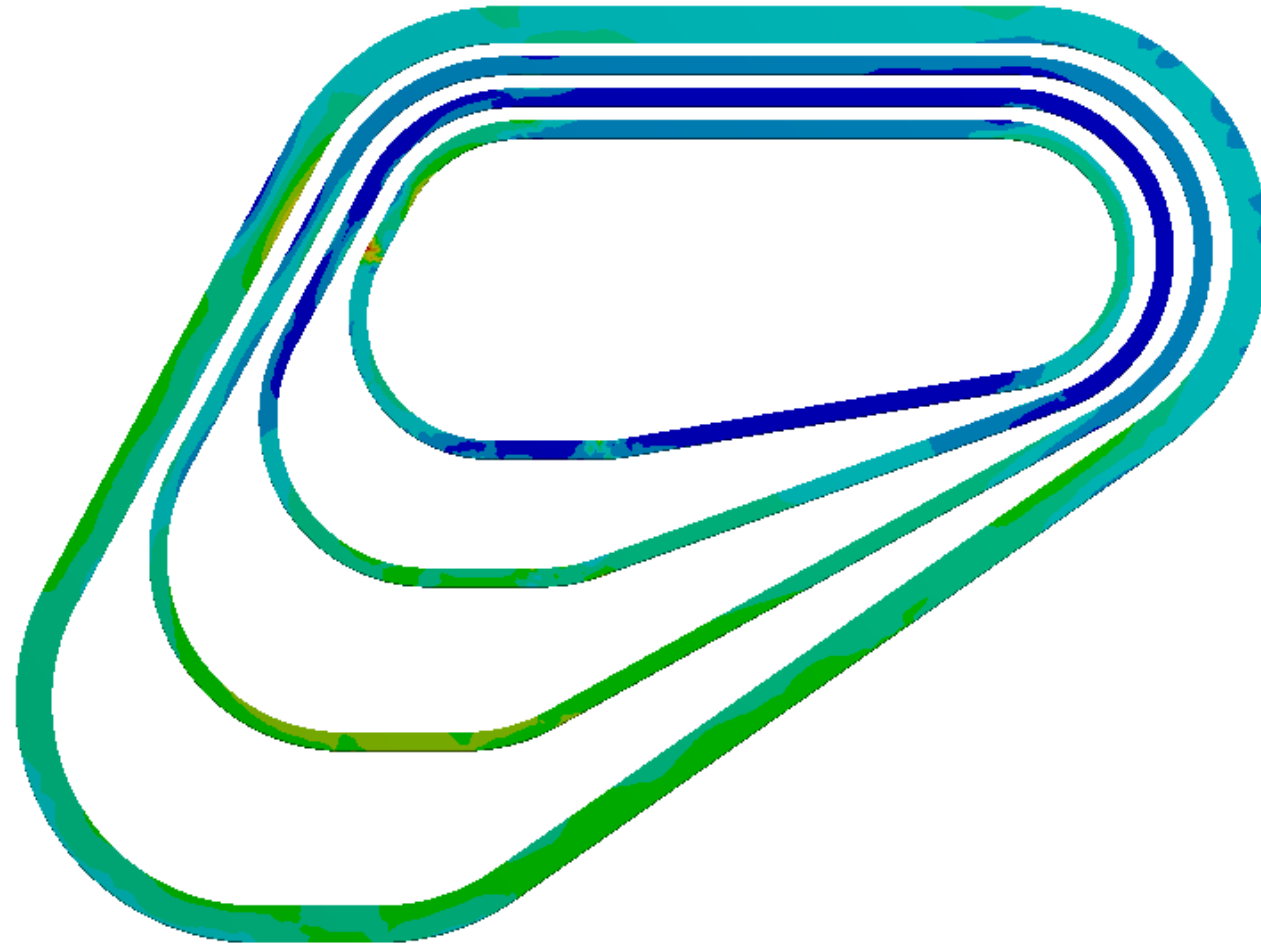
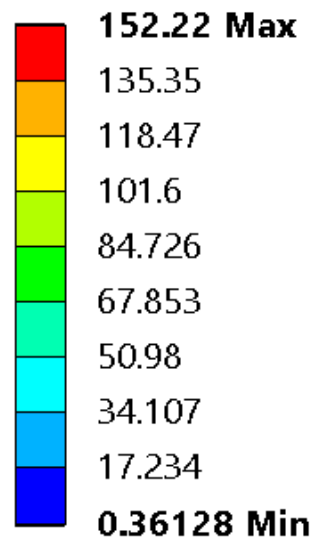
Equivalent Stress - coil 2

Type: Equivalent (von-Mises) Stress

Unit: MPa

Time: 2

07/02/2020 13:34



Coils - equivalent stress (3)

C: coil friction - pole SS - coarse

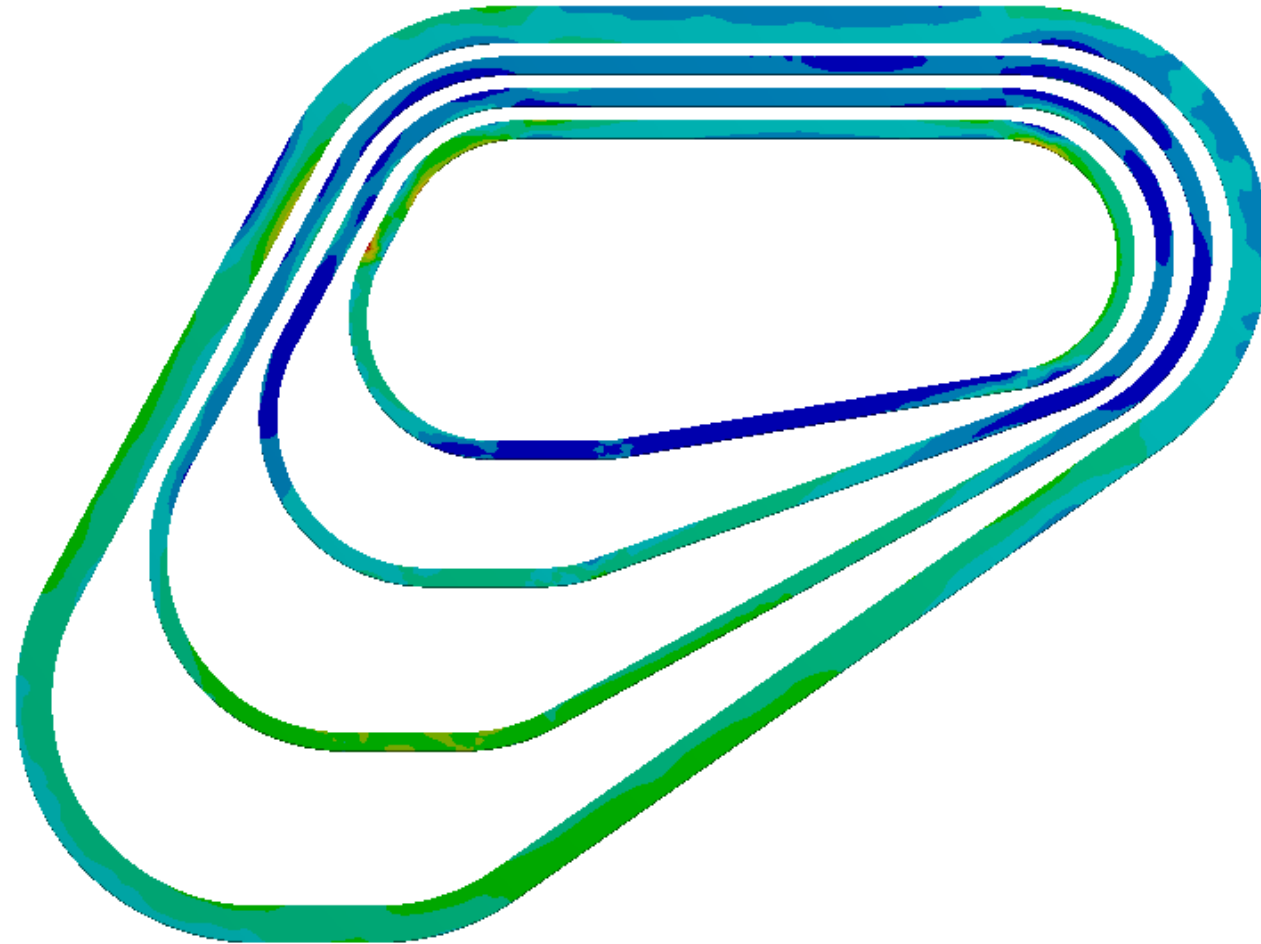
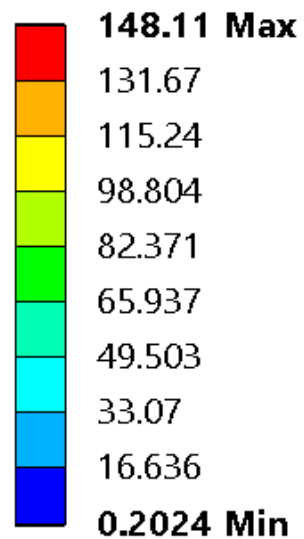
Equivalent Stress - coil 3

Type: Equivalent (von-Mises) Stress

Unit: MPa

Time: 3

07/02/2020 13:35



Bolts - bending moment

C: coil friction - pole SS - coarse

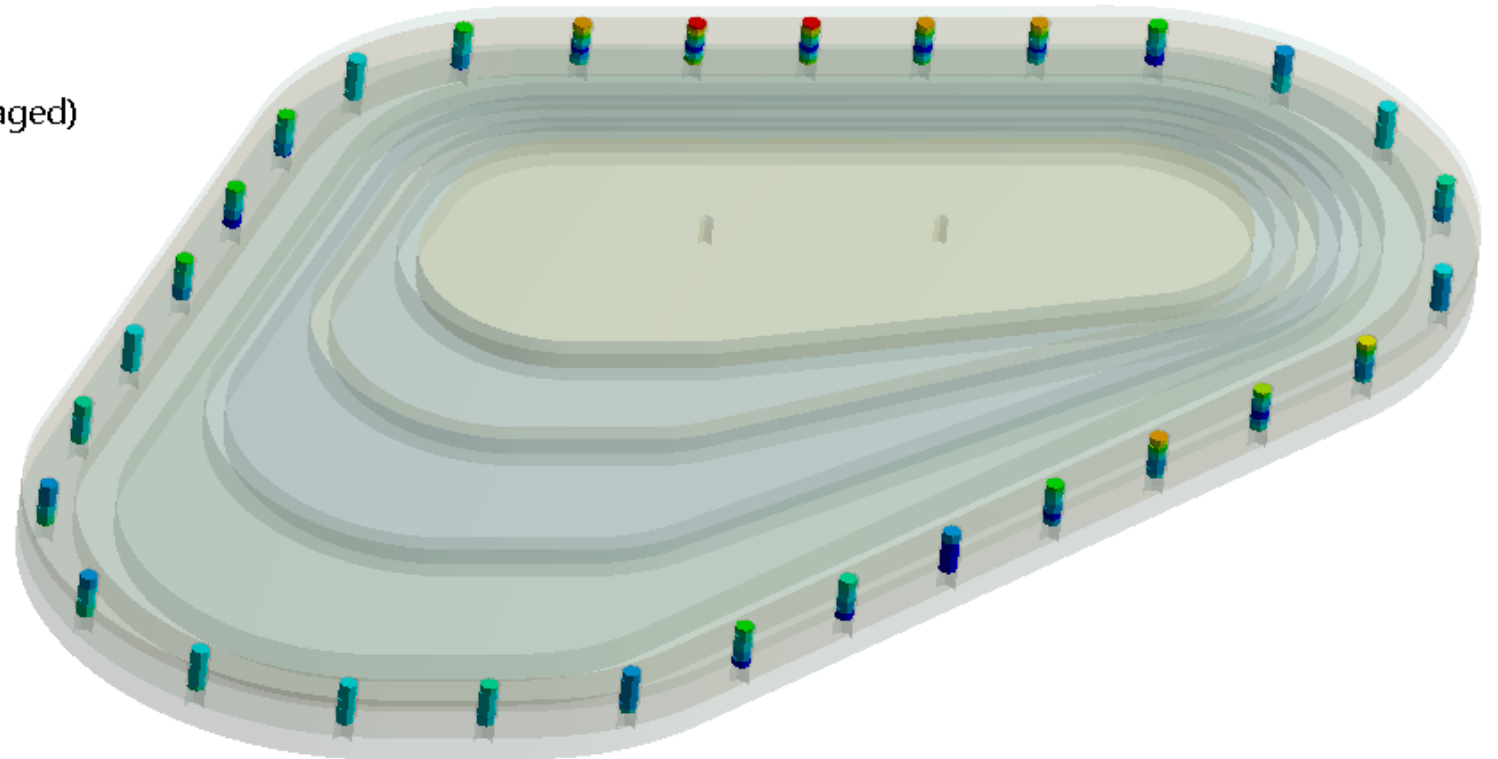
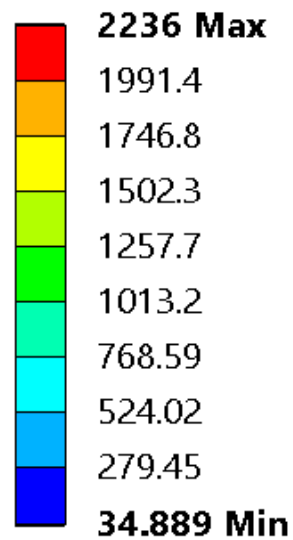
Total Bending Moment 3

Type: Total Bending Moment (Unaveraged)

Unit: N·mm

Time: 3

07/02/2020 13:52

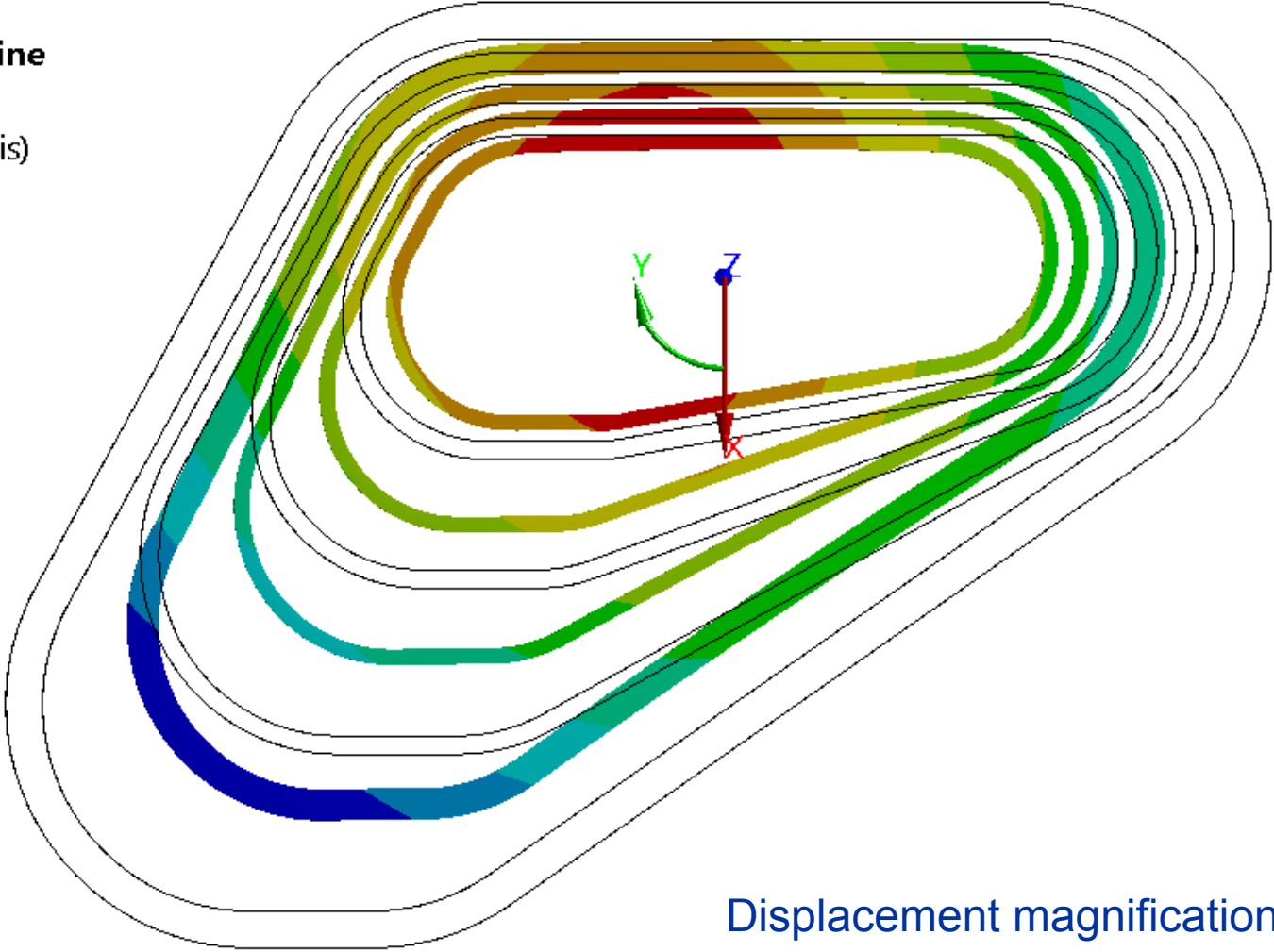
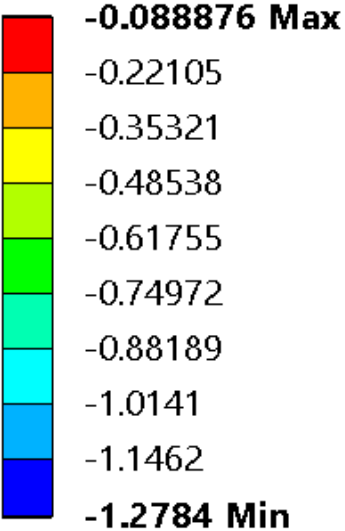


Equivalent stress computation:

$$\sigma_{red,B} = \sqrt{\sigma_{zb,max}^2 + 3(k_t \cdot \tau_{max})^2}$$

Radial displacement - bonded - SS pole

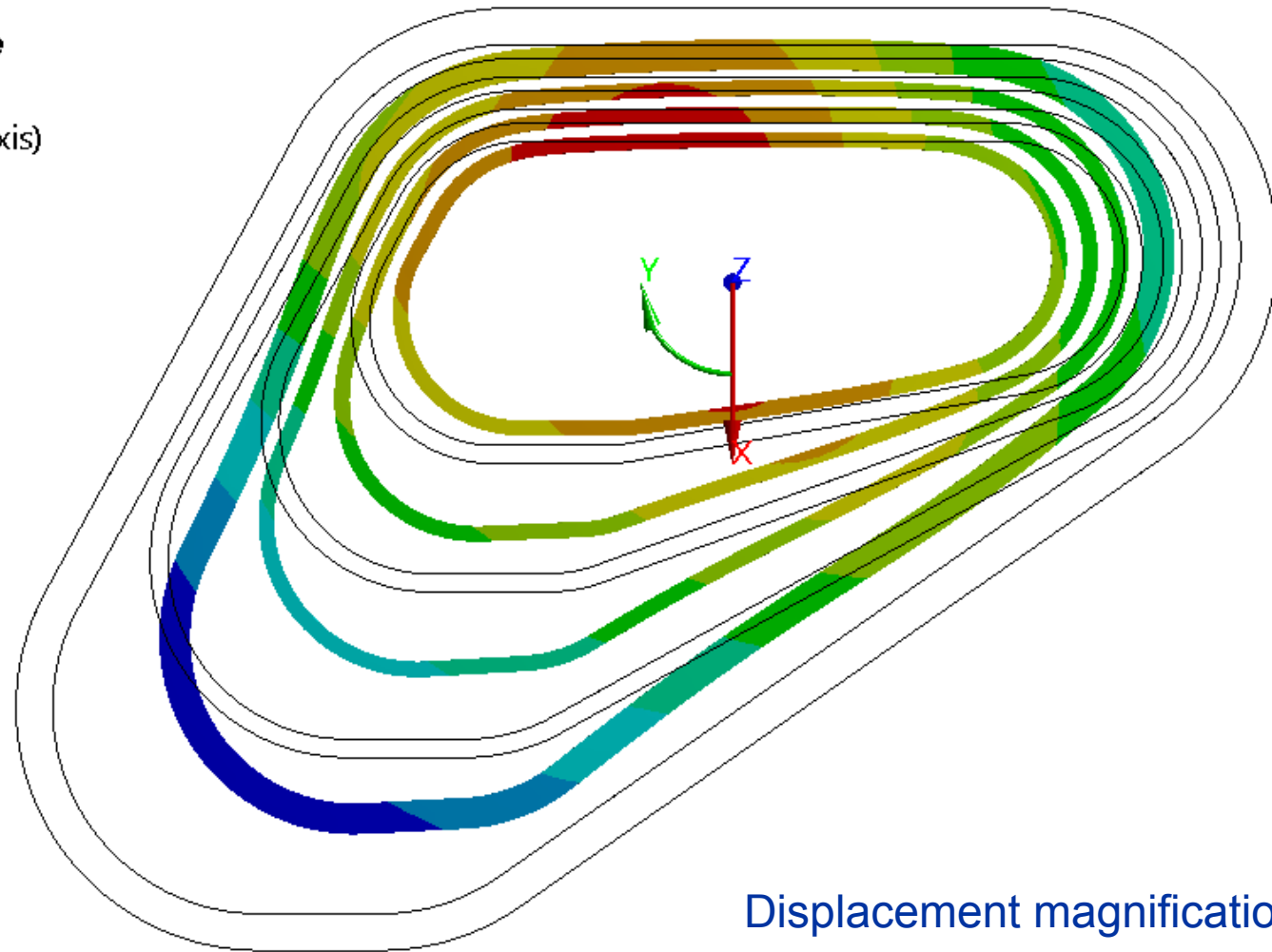
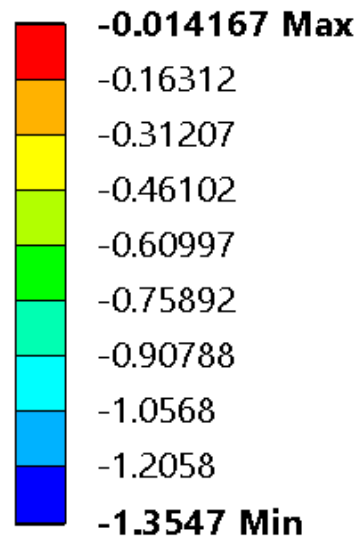
B: coil bonded - pole SS - futur fine
Directional Deformation
Type: Directional Deformation(X Axis)
Unit: mm
Polar centre
Time: 3
07/02/2020 17:57



Displacement magnification factor: 50

Radial displacement - frictional - SS pole

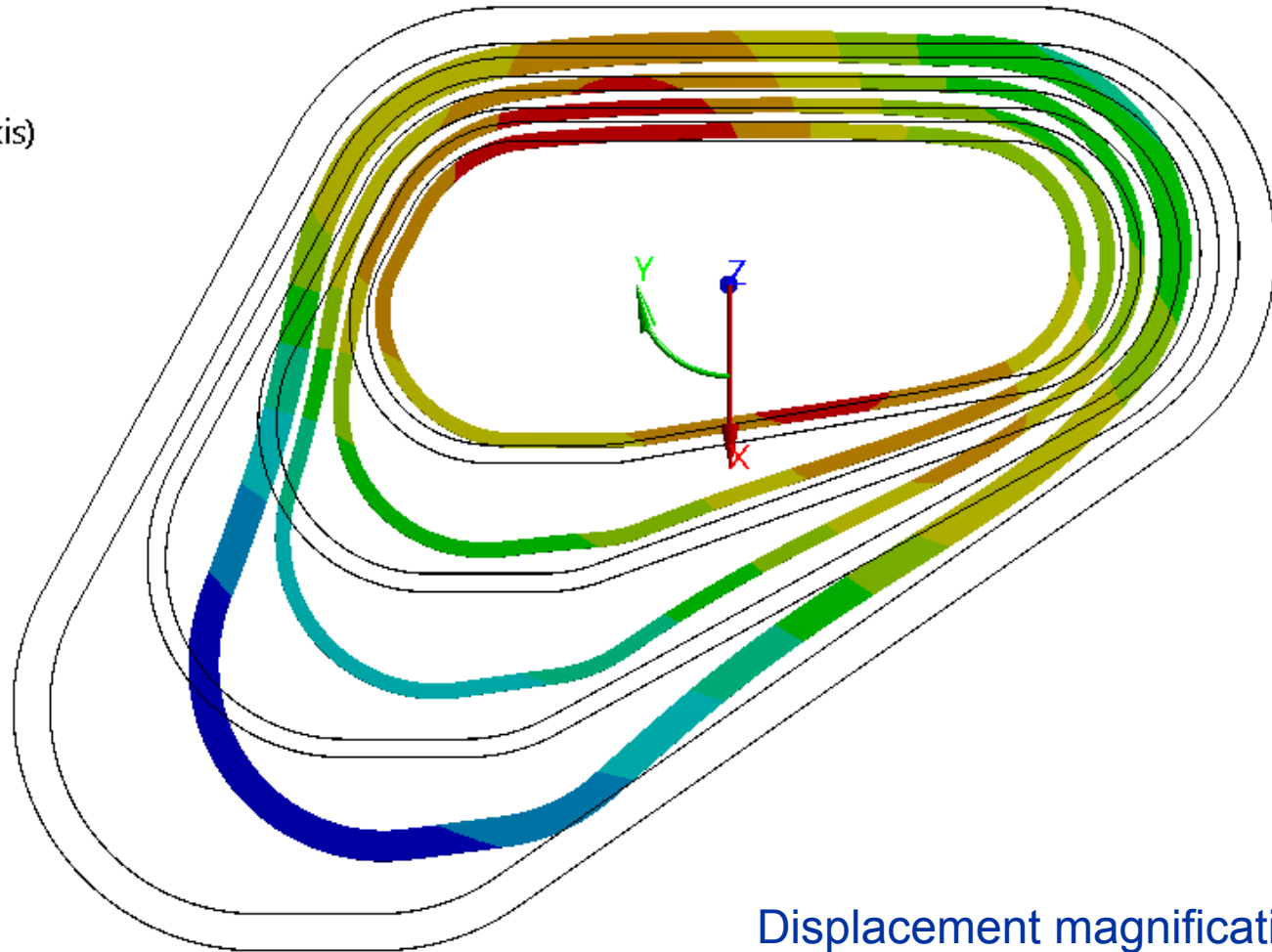
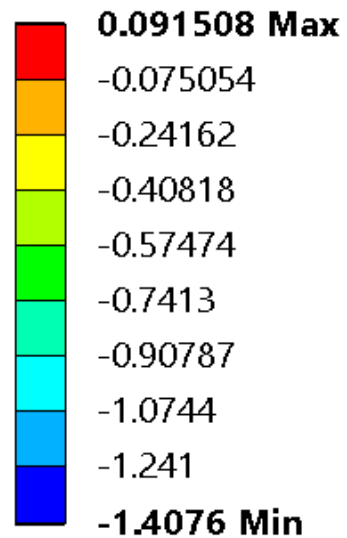
C: coil friction - pole SS - coarse
Directional Deformation 2
Type: Directional Deformation(X Axis)
Unit: mm
Polar centre
Time: 3
07/02/2020 17:57



Displacement magnification factor: 50

Radial displacement - frictional - Ti pole

D: coil friction - pole Ti - coarse
Directional Deformation 2
Type: Directional Deformation(X Axis)
Unit: mm
Polar center
Time: 3
07/02/2020 17:57



Displacement magnification factor: 50

Radial displacement - frictional - no pole

E: coil friction - no pole - coarse

Directional Deformation 2

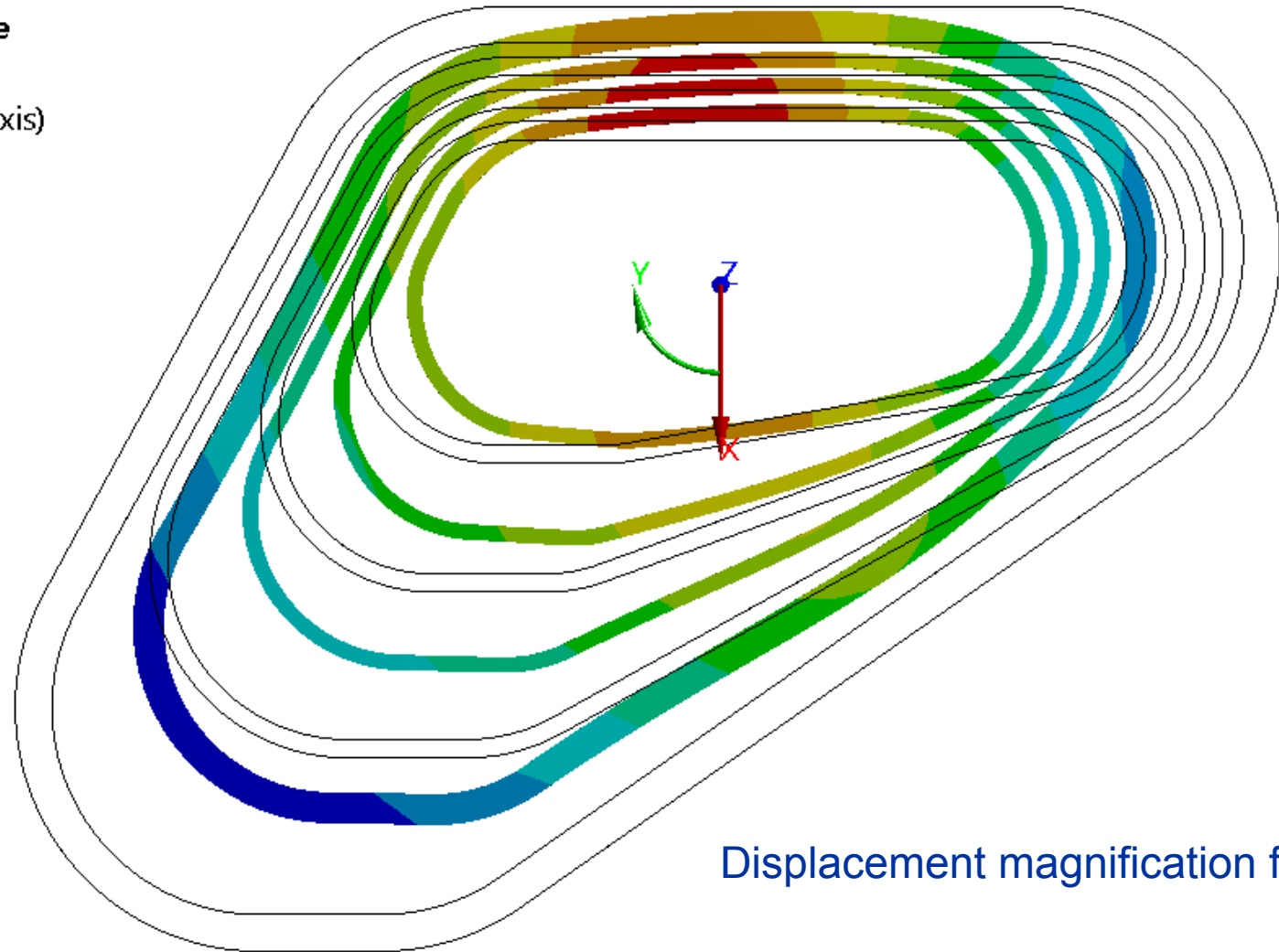
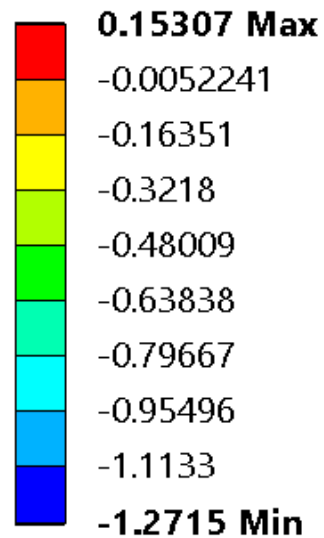
Type: Directional Deformation(X Axis)

Unit: mm

Polar centre

Time: 2

07/02/2020 17:56



Displacement magnification factor: 50

Configuration comparison

		Coil frictional SS pole	Coil bonded SS pole	Coil frictional Ti pole	Coil frictional No pole
Coils	Mean stress [MPa]	38	40	66	39
	Max stress [MPa]	148	117	324	97
	Max displacement [mm]	1.45	1.37	1.61	1.37
Spacers	Mean stress [MPa]	49	53	67	45
	Max stress [MPa]	187	207	303	183
Bolts	Safety factor	1.62	1.63	1.64	1.62
Pole	Mean pressure [MPa]	6	12	29	
	Max pressure [MPa]	86	111	140	

Take-home message

- Stress state mainly lead by the **cool-down**
- **Preload** seems introducing unreasonably **high-stress** level
- **Stiffness** of spacers overestimated by omitting **grade jumps**
- Shear stress at **contact interfaces** ~ 20 MPa \rightarrow **resin cannot withstand contact**
- Future investigation of configurations with **less preload** \rightarrow spacers in SS



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