



# Simulations of the HL-LHC octagonal beam screens: effect of shape and weld

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Acknowledgments: N. Kos, E. Métral, G. Rumolo, B. Salvant

# Overview

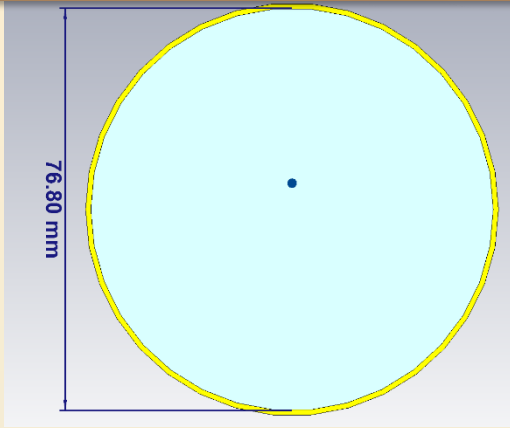
- Model
- Definition of the factors
- Simulation results
- Summary table

# Overview

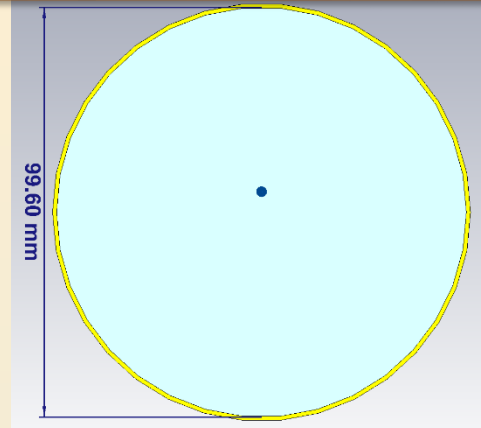
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# CST model

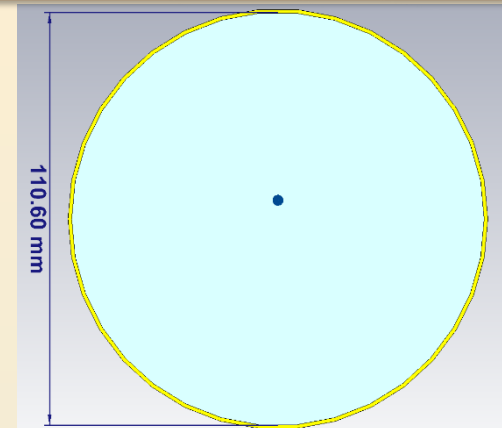
BS\_88(D2): reference



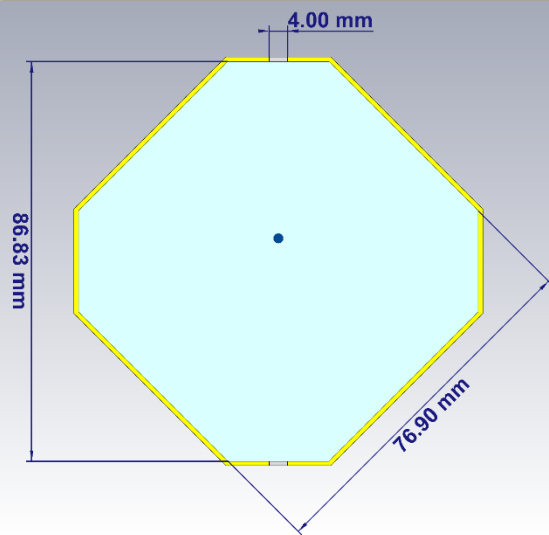
BS\_101(Q1): reference



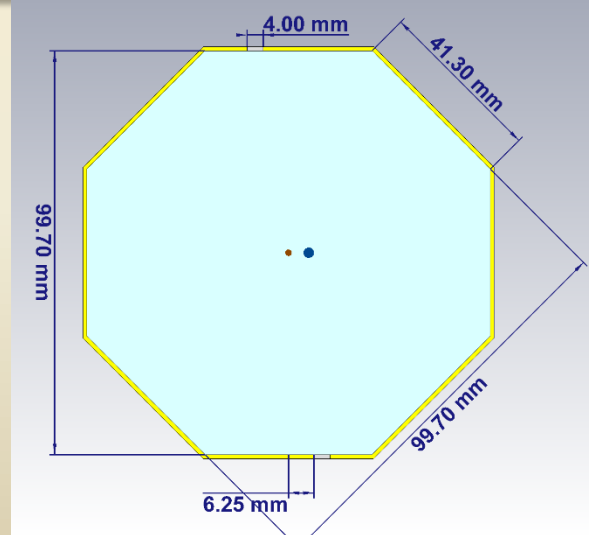
BS\_121(Q2-Q3-CP-D1):reference



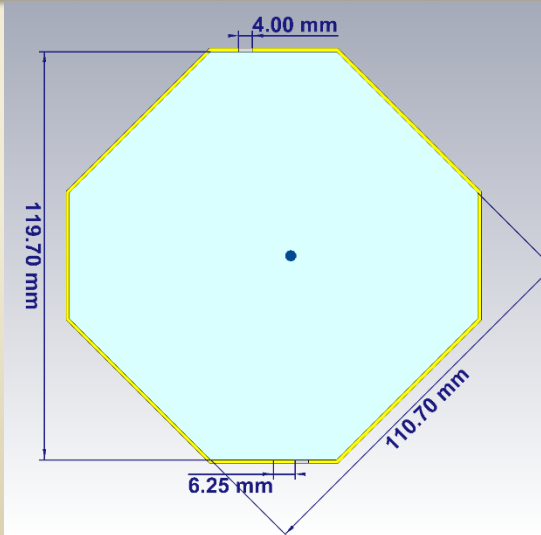
BS\_88(D2): realistic



BS\_101(Q1): realistic



BS\_121(Q2-Q3-CP-D1):realistic



$$\rho_{Cu} = 7.55 \times 10^{-10} \Omega m$$
$$\rho_{SS} = 6.0 \times 10^{-7} \Omega m$$

$$\rho_{Cu} = 2.65 \times 10^{-9} \Omega m$$
$$\rho_{SS} = 7.2 \times 10^{-7} \Omega m$$

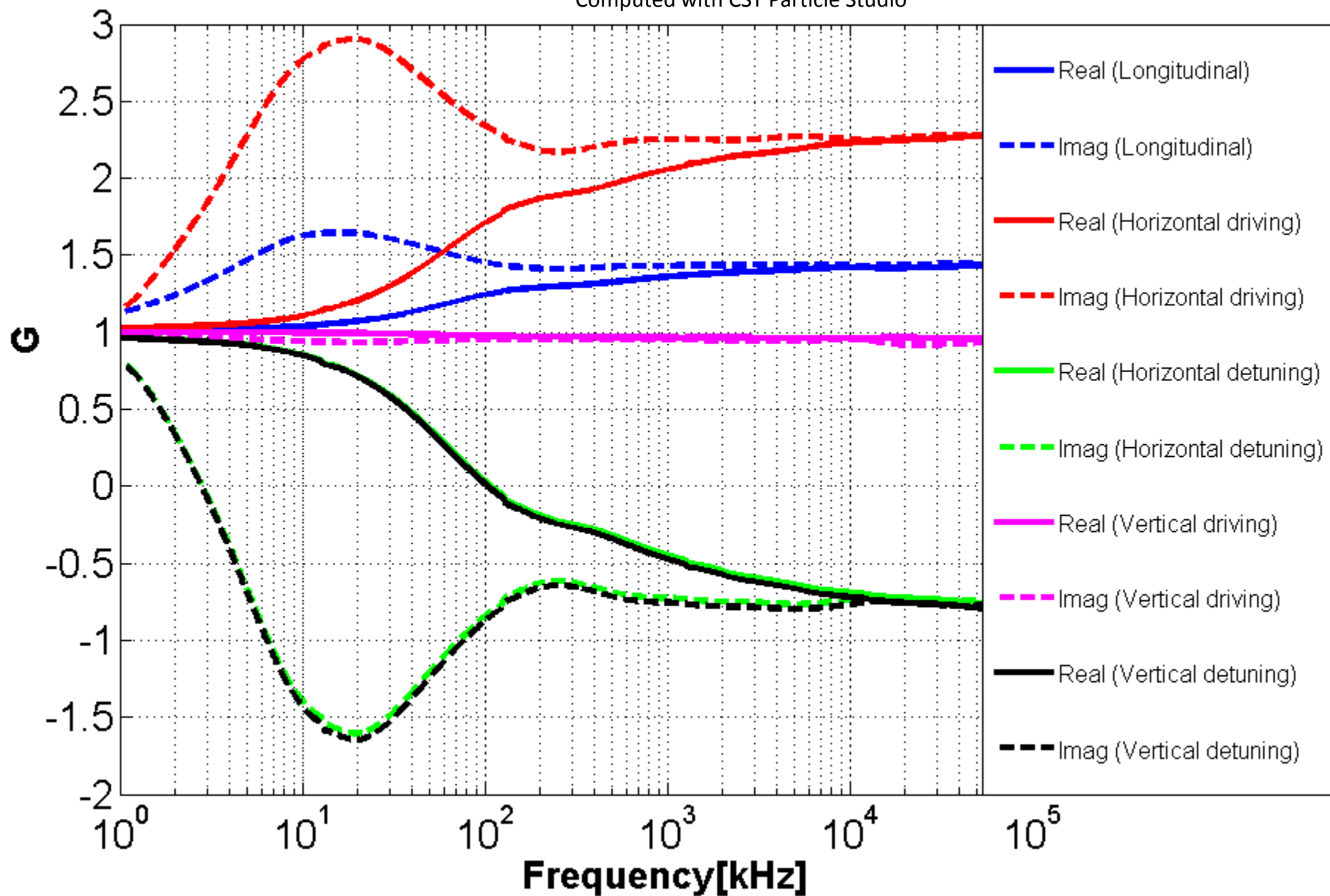
$$\rho_{Cu} = 2.65 \times 10^{-9} \Omega m$$
$$\rho_{SS} = 7.2 \times 10^{-7} \Omega m$$

# Overview

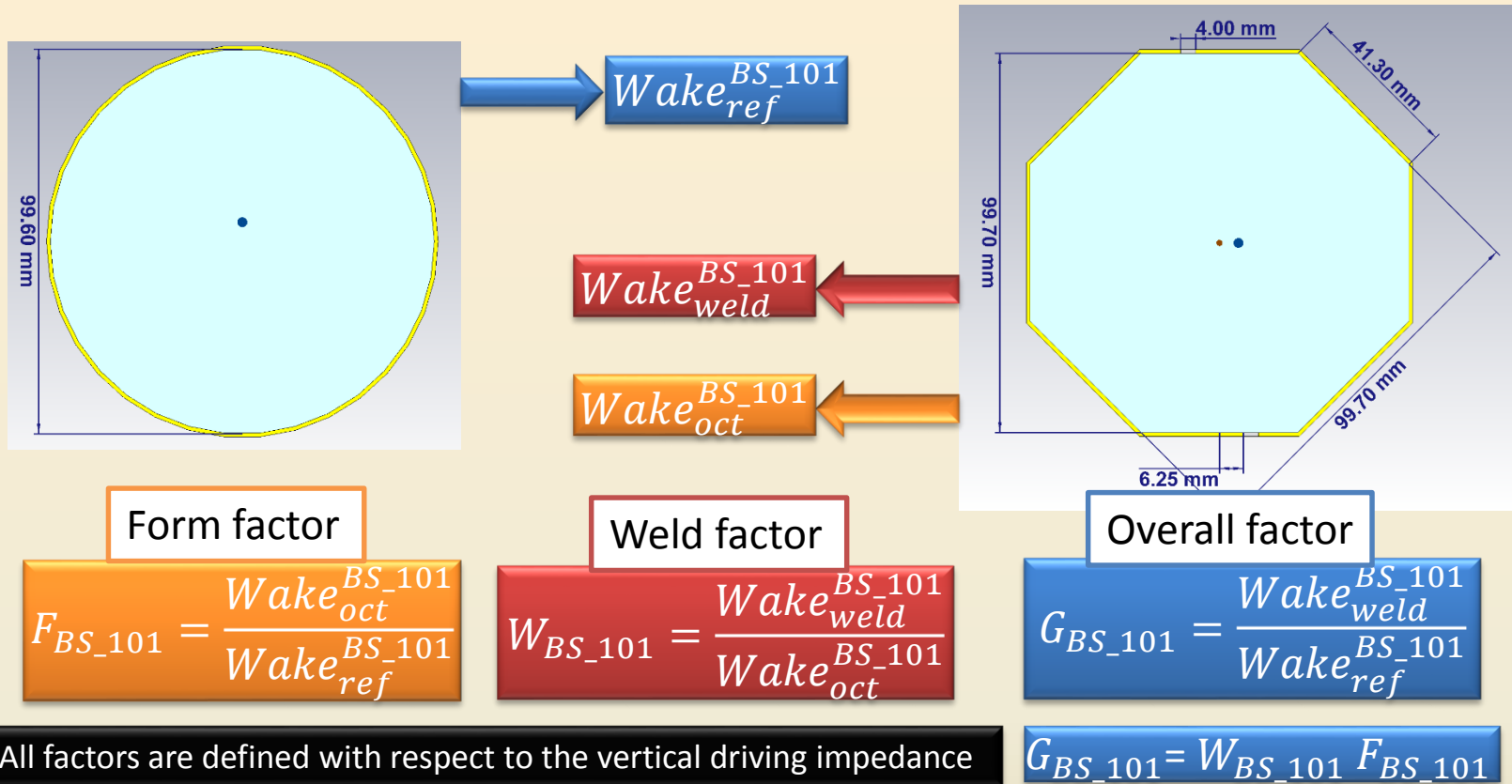
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# The LHC beam screen: effect of the weld

Computed with CST Particle Studio



# Definition of the form and weld factors



S. Heifets, A. Wagner, B. Zotter. *Generalized Impedances and Wakes in Asymmetric structures*

Generalized expansion of transverse wake/impedance at the first order

$$W_x(s) = c_{10} + x_0 c_{11} + 2x c_{20} - y_0 d_{11} - 2y d_{20}$$

$$W_y(s) = -d_{10} - x_0 d_{11} - 2x d_{20} - y_0 \bar{c}_{11} - 2y c_{20}$$

Constant terms

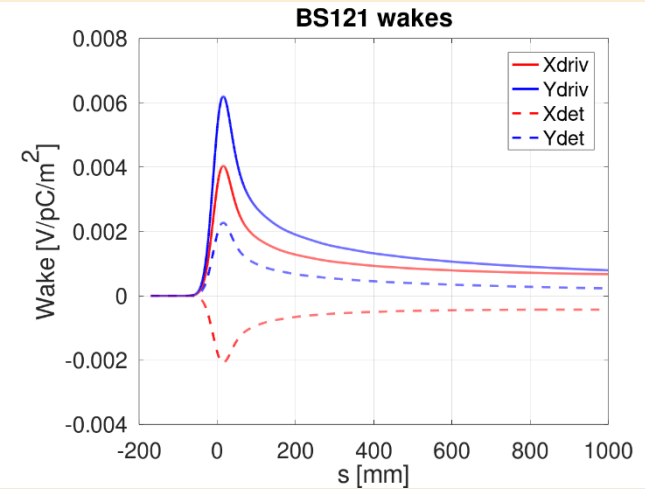
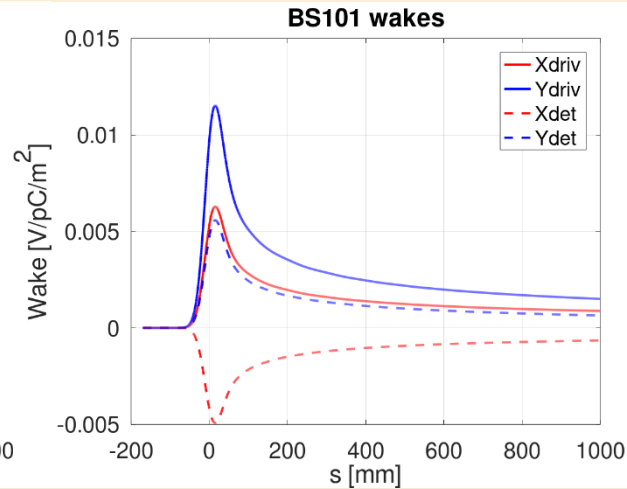
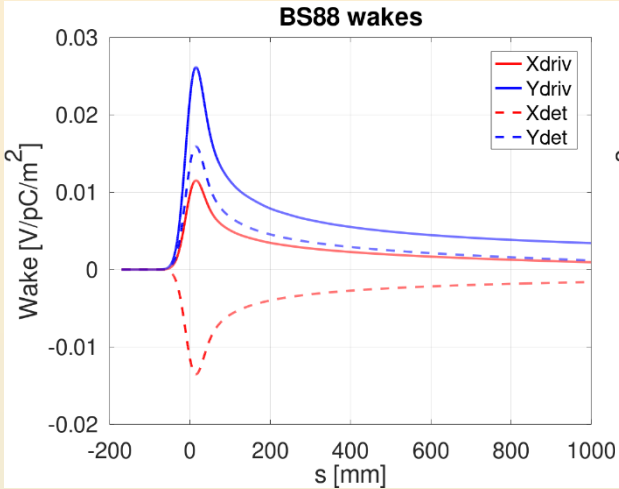
Coupling terms

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# Simulation results

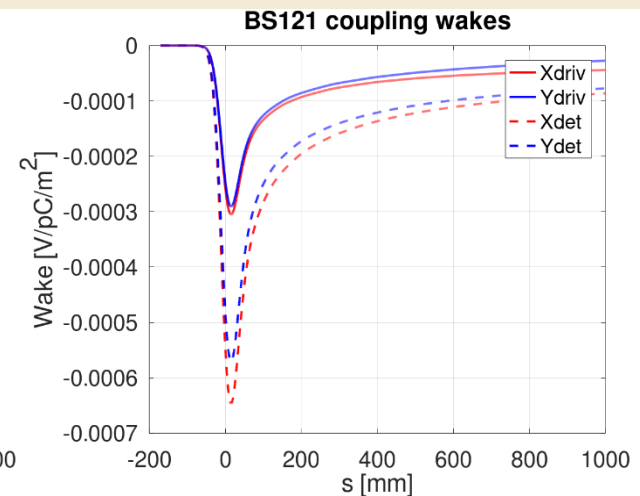
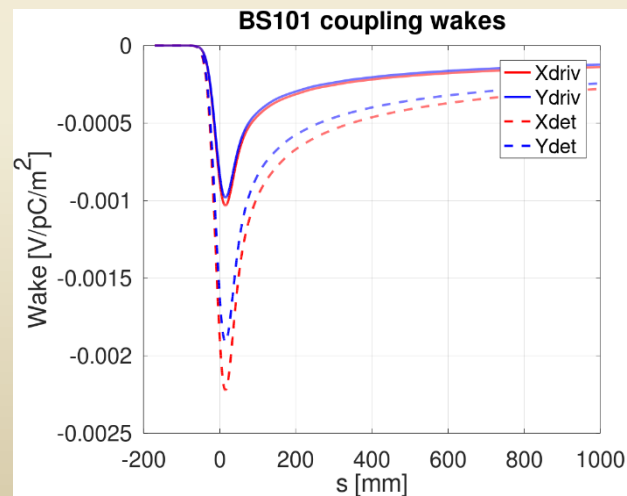


$$c_{10} + x_0 c_{11} + 2x c_{20} - y_0 d_{11} - 2y d_{20}$$

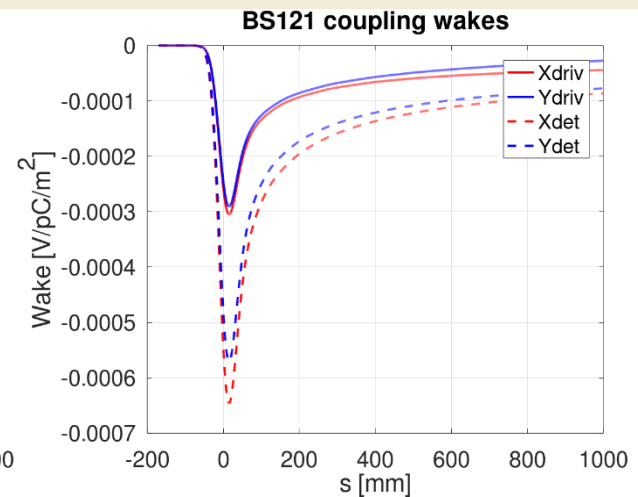
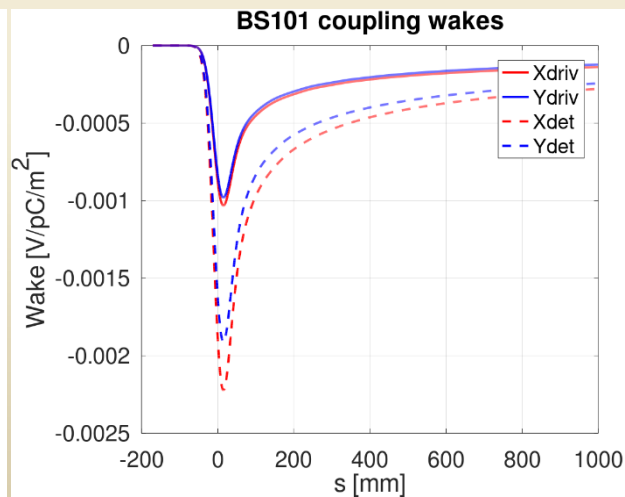
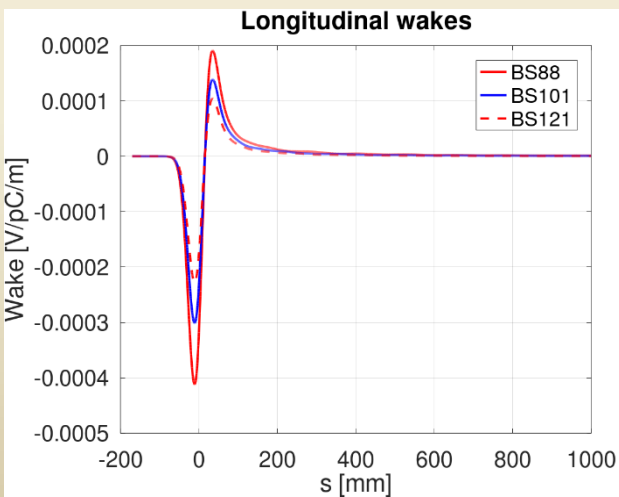
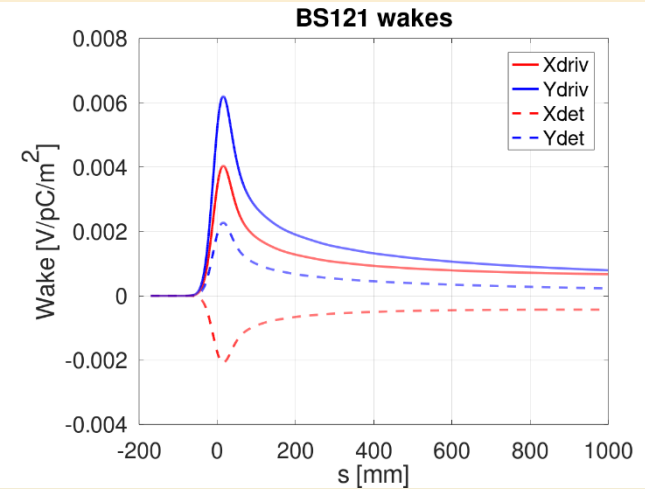
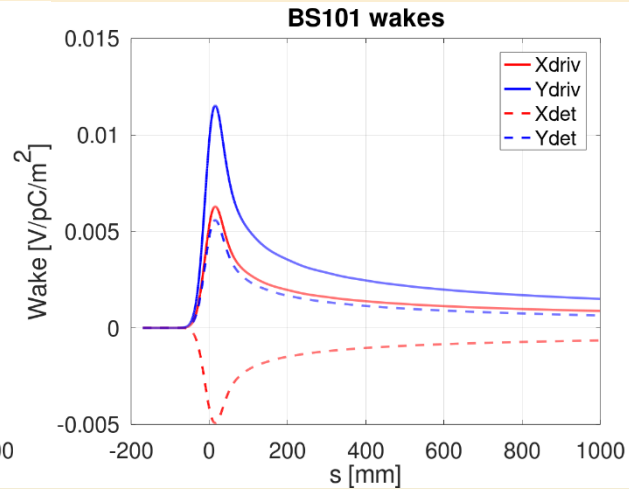
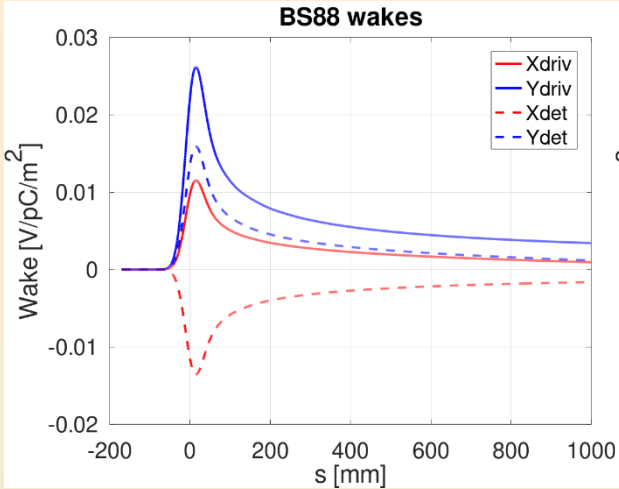
$$-d_{10} - x_0 d_{11} - 2x d_{20} - y_0 \bar{c}_{11} - 2y c_{20}$$



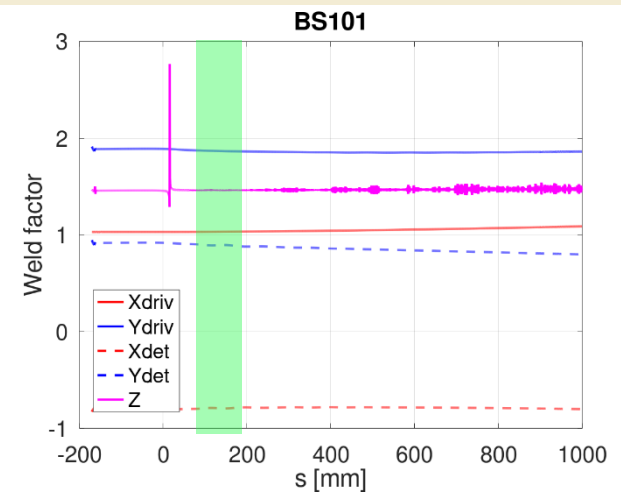
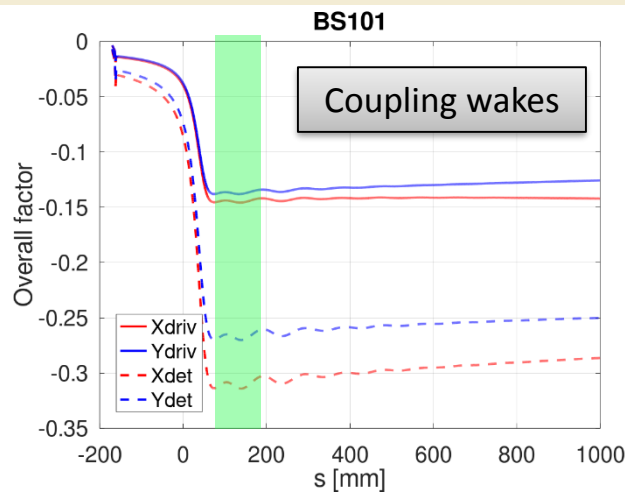
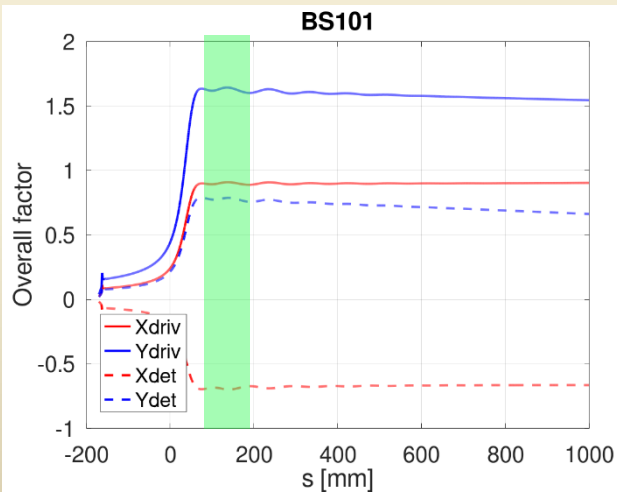
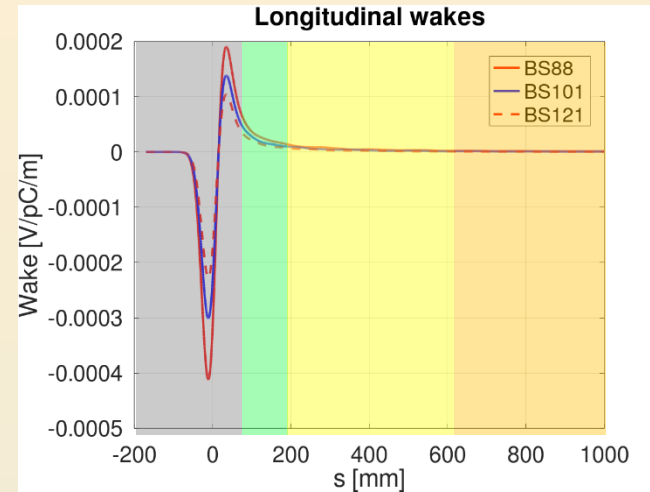
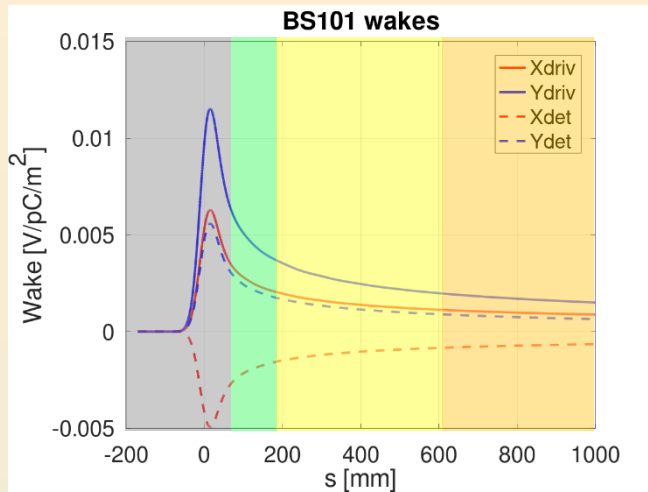
Coupling terms are all negatives  
Xdriv=Ydriv and Xdet=Ydet



# Simulation results



# Simulation results



Factors are defined in the green area where the simulation is expected to have the higher reproducibility

Weld factors are more accurate since are obtained using exactly the same discretization of the domain of calculus

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# Summary table of all factors

Factor	BS88	BS101	BS121
Wxdriv	0.98966	1.032	1.0172
Wydriv	2.2307	1.8726	1.5425
Wxdet	-1.1364	-0.79581	-0.51968
Wydet	1.3255	0.89992	0.55881
Wz	1.6343	1.4569	1.2853
Gxdriv	0.72855	0.89452	0.8587
Gydriv	1.6422	1.6231	1.3022
Gxdet	-0.83659	-0.6898	-0.43872
Gydet	0.97578	0.78005	0.47175
Gz	1.5942	1.36	1.0738
Gcxdriv	-	-0.14438	-0.063557
Gcydriv	-	-0.1368	-0.060006
Gcxdet	-	-0.31057	-0.13479
Gcydet	-	-0.26701	-0.11903

# Summary table of all factors: enforcing impedance symmetries

Factor	BS88	BS101	BS121
Wxdriv	0.98966	1.032	1.0172
Wydriv	2.2307	1.8726	1.5425
Wxdet	-1.2309	-0.84787	-0.53924
Wydet	1.2309	0.84787	0.53924
Wz	1.6343	1.4569	1.2853
Gxdriv	0.72855	0.89452	0.8587
Gydriv	1.6422	1.6231	1.3022
Gxdet	-0.90619	-0.73493	-0.45524
Gydet	0.90619	0.73493	0.45524
Gz	1.5942	1.36	1.0738
Gcxdriv	-	-0.14059	-0.0618
Gcydriv	-	-0.14059	-0.0618
Gcxdet	-	-0.28879	-0.12691
Gcydet	-	-0.28879	-0.12691

Known symmetries

Coupling terms  
 $X_{driv} = Y_{driv}$  and  $X_{det} = Y_{det}$   
 Detuning terms  
 $X_{det} = -Y_{det}$

Average between the  
two numerical factors



Enforcing symmetries

# Conclusions

- Form factors with respect to the circular reference shape used in the present impedance model have been calculated
- The effect of the weld has been evaluated and expressed in terms of a weld factor.
- The coupling terms have been also estimated
- Time (frequency) dependent weld factors could be obtained using the simulation scaling technique if there is a strong interest in this sense.

**Thank you for your attention**