



# Modelling of Flux Concentrators for Positron Sources

H. Bajas, Y. Zhao

# Outline

- Flux Concentrator in linear accelerators
- Objectives of the study
- Modelling of the geometry and the electrical circuit
- Recall of the model's outcome from last workshop
- Design proposal for the SuperKEKB e+ source
- Design optimization for the CLIC e+ source
- Conclusion

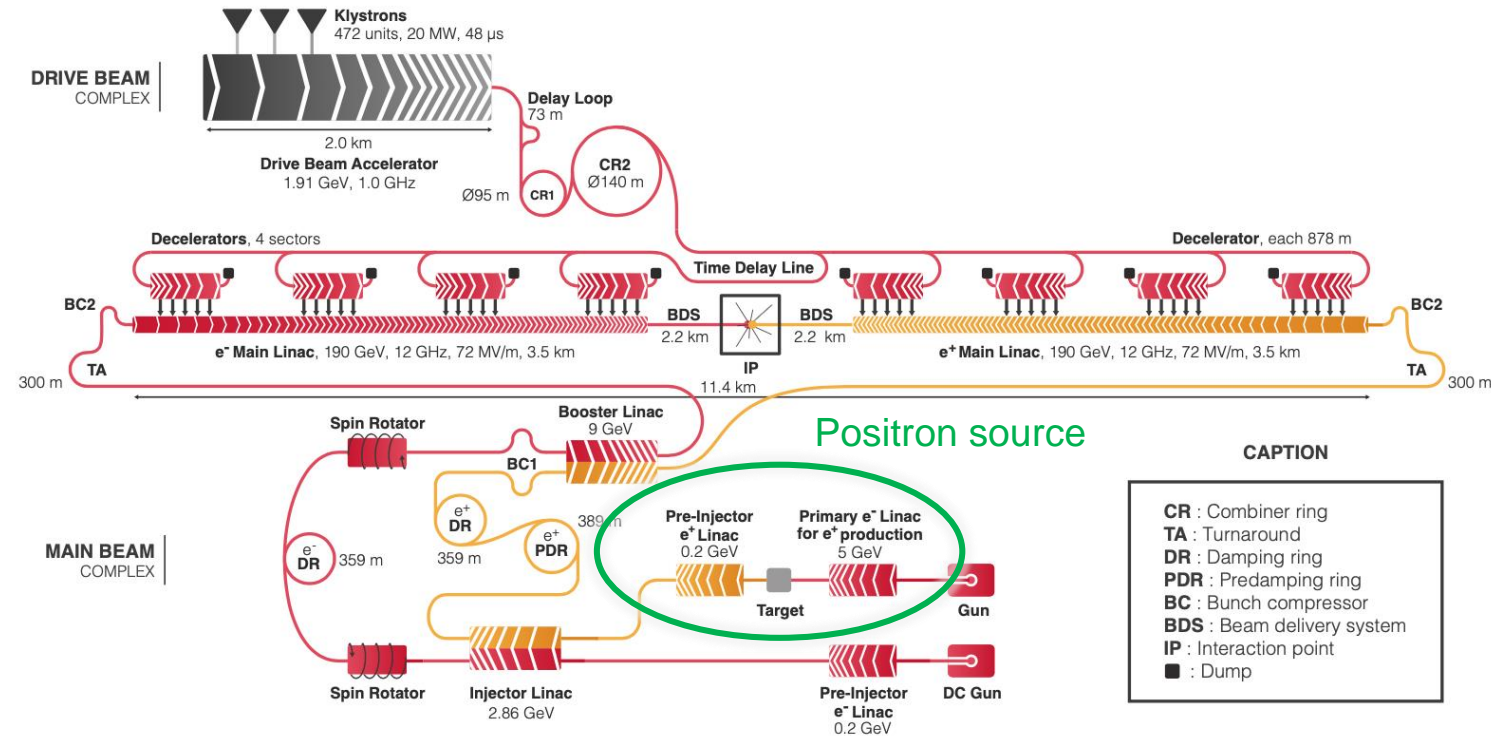
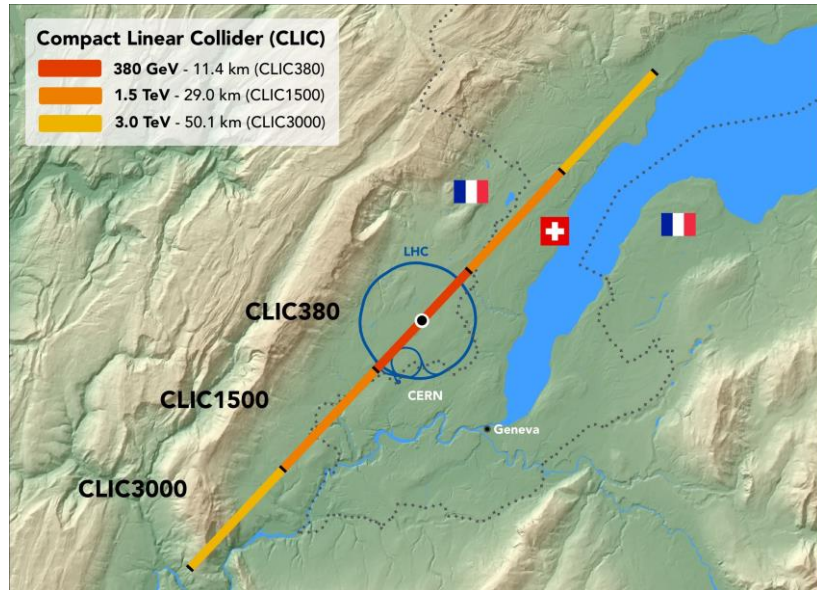
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# Flux Concentrator in linear accelerators

Future linear colliders, such as CLIC at CERN, would use both electrons and **positrons**. The **positron source** produces positrons from the collision of electrons on fixed target then introduced in the pre-injector.

The quality of the source is of prior importance for the luminosity of the machine.

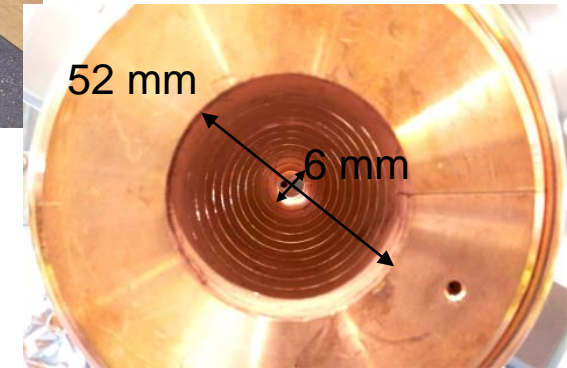
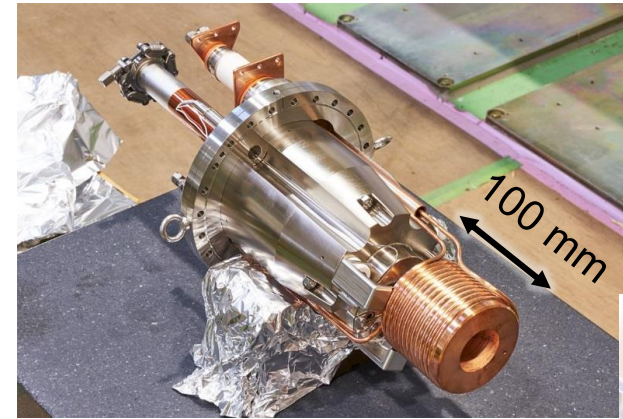
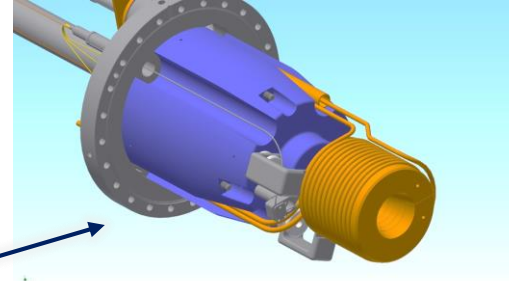
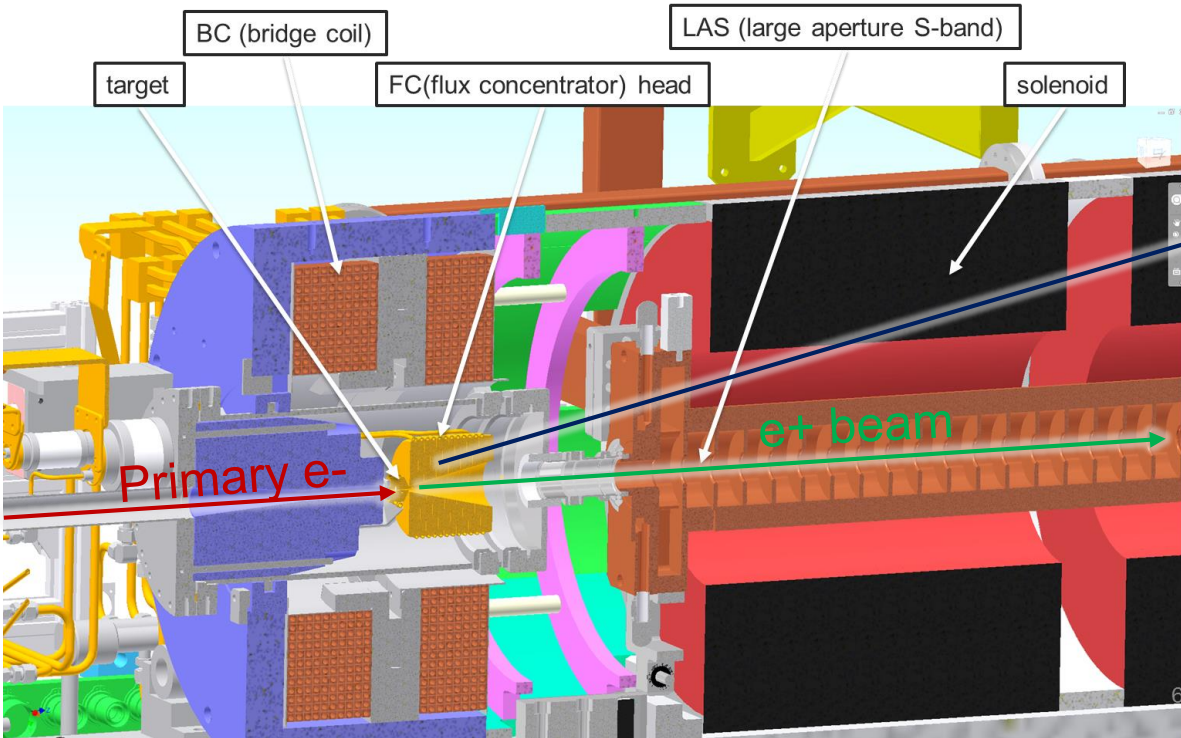


Steinar Stapnes, October 2019, Sendai  
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# Flux Concentrator in linear accelerators

At the SuperKEKB e+ source



Tapered 12-turn solenoid  
made of Copper (OFHC)

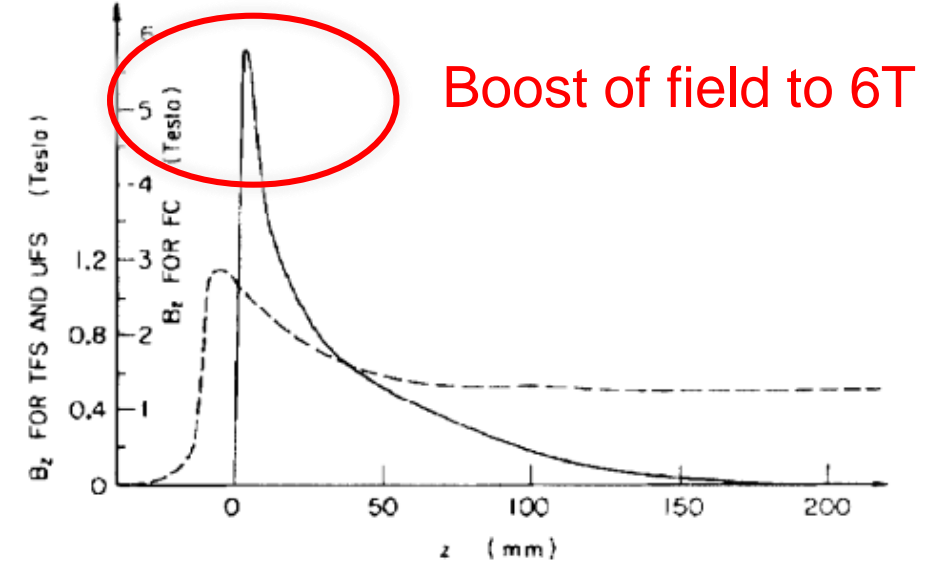
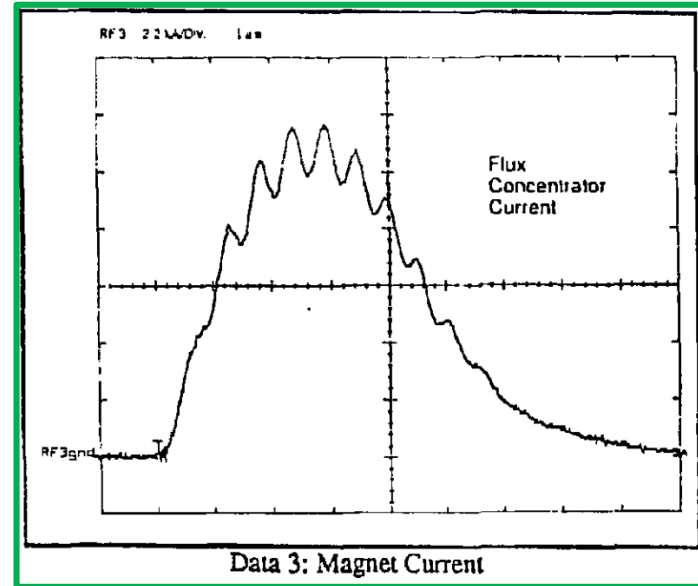
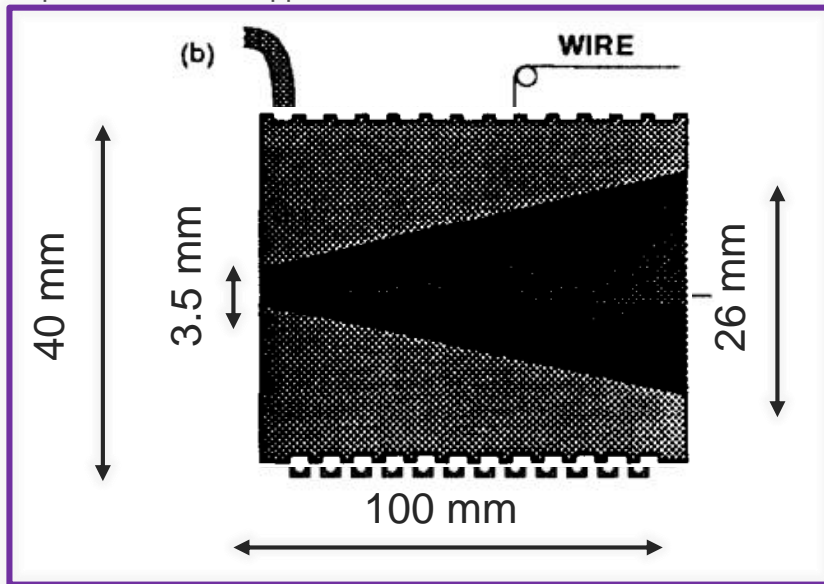
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# Working principle of a Flux Concentrator

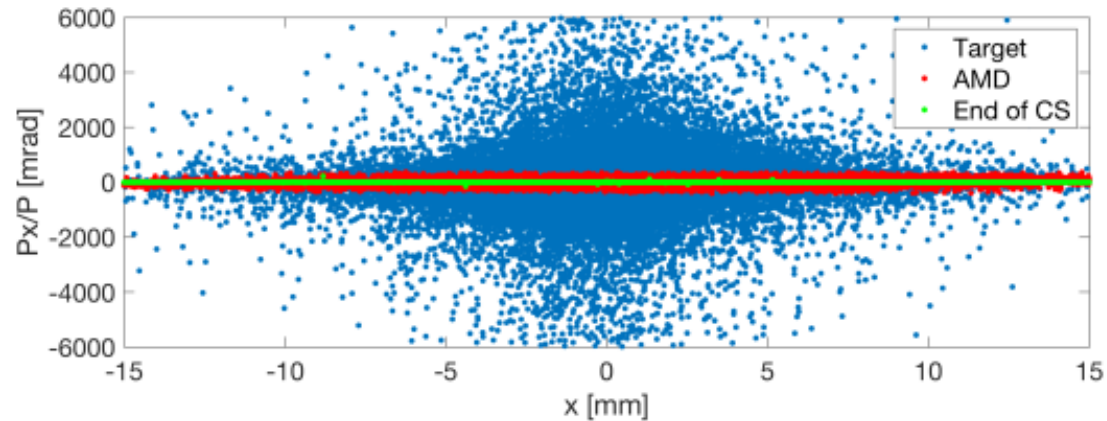
- Based on **old concept** used for several years at the **SLAC** positron source.
- **High current pulses (13 kA, 5 $\mu$ s)** produce **pulses of magnet field**.
- Axial field sharp rise ( $\sim 6$ T) at device entrance followed by a rapid decay to 0 T.

Tapered 12-turns Copper solenoid



# Working principle of a Flux Concentrator

Positron emittance at the exit of  
the target, the AMD and the capture section



Purpose of the Adiabatic Matching Device (containing the FC):

- Matching the  $e^+$  beam (with very large transverse divergence) to the acceptance of the pre-injector linac.
- Maximise the “so-called” positron yields:

$$\text{yield}_{e^+} = \frac{n_{e^+}^{\text{produced}}}{n_{e^-}^{\text{primary}}}$$



Courtesy I. Chaikovska October 2019, Sendai  
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# Objectives of the study

- To study in detail the **working principle** of an Adiabatic Matching Device Flux Concentrator (AMD FC) by the means of **electromagnetic transient models** using Opera<sup>®</sup> software.
- To validate the model by direct comparison to experimental data.
- To understand the phenomenology of the axial **field boost** from 2 to 6 T.
- To run **parametric study** in order to **optimize** future AMD FC design.
- To propose solution for KEK design and future FC at CERN.

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# Modelling of the geometry and the electrical circuit

Opera<sup>®</sup> allows linking the FE model to the circuit elements to impose flow of current (current supply, external resistor and winding elements)

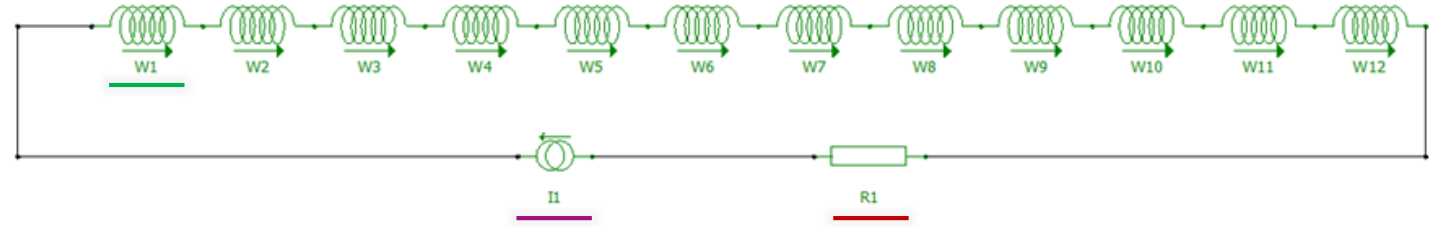
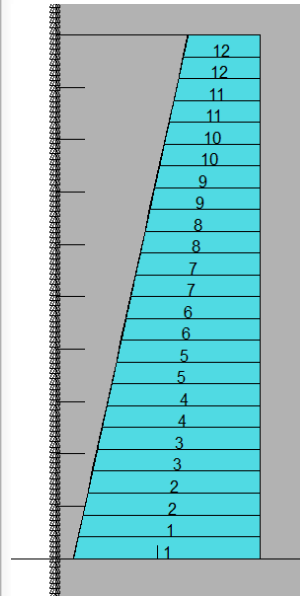
**Component Explorer**

- Voltage
- Winding
  - W1
  - W2
  - W3
  - W4
  - W5
  - W6
  - W7
  - W8
  - W9
  - W10
  - W11
  - W12

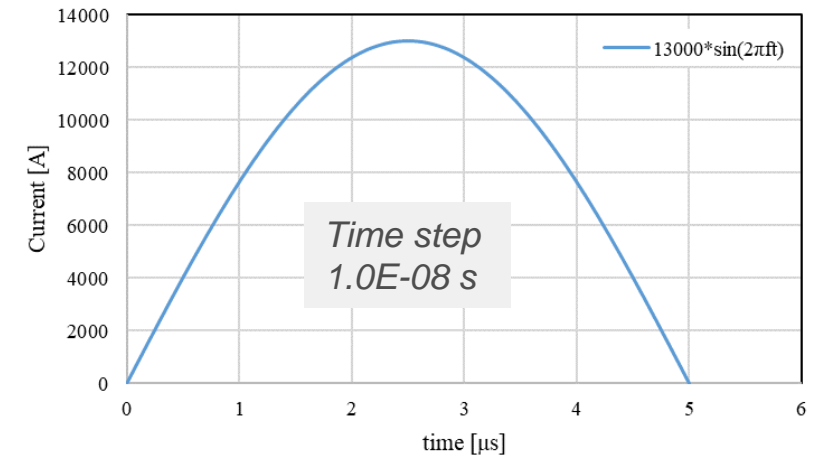
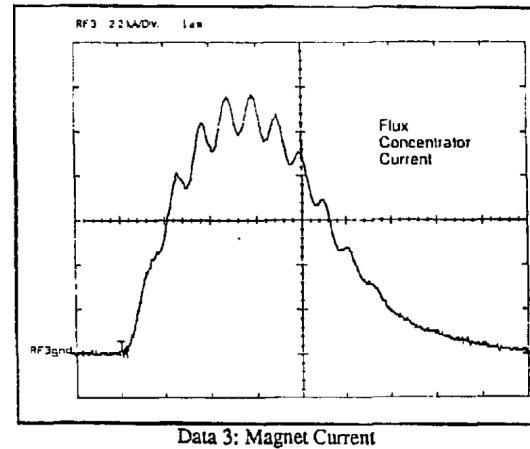
**Component Property**

Winding: W6

Property	Value
Name	W6
Conductor Set	6
Circuit type	Bulk Eddy Current
Resistance per U...	#copper_resistivity
Unit	Ω/m
Turns per condu...	1
Use model symmetry	No
Symmetry Factor	1
Voltage Probe Resist...	1
Unit	MΩ
Initial current	0
Unit	A
Notes	
Show label	Name only
Font	A [MS Shell Dlg 2, 8]
Colour	[0, 128, 0] (255)
Show Direction	Yes



The built-in circuit allows reproducing the experimental pulse of current.

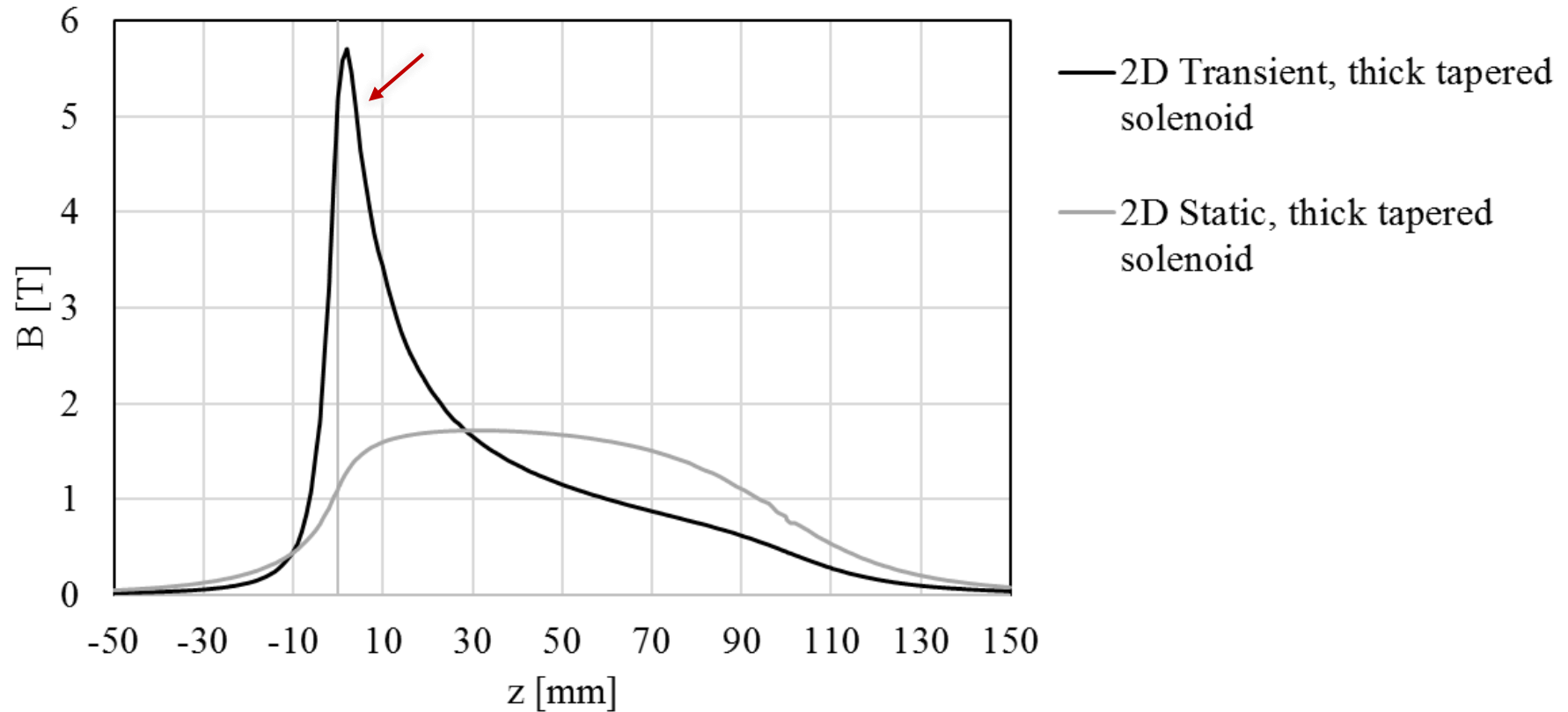


J. De Lamare, et Al. , "SLC Positron Source Flux Concentrator Modulator," SLAC-PUB-5472, May 1991.

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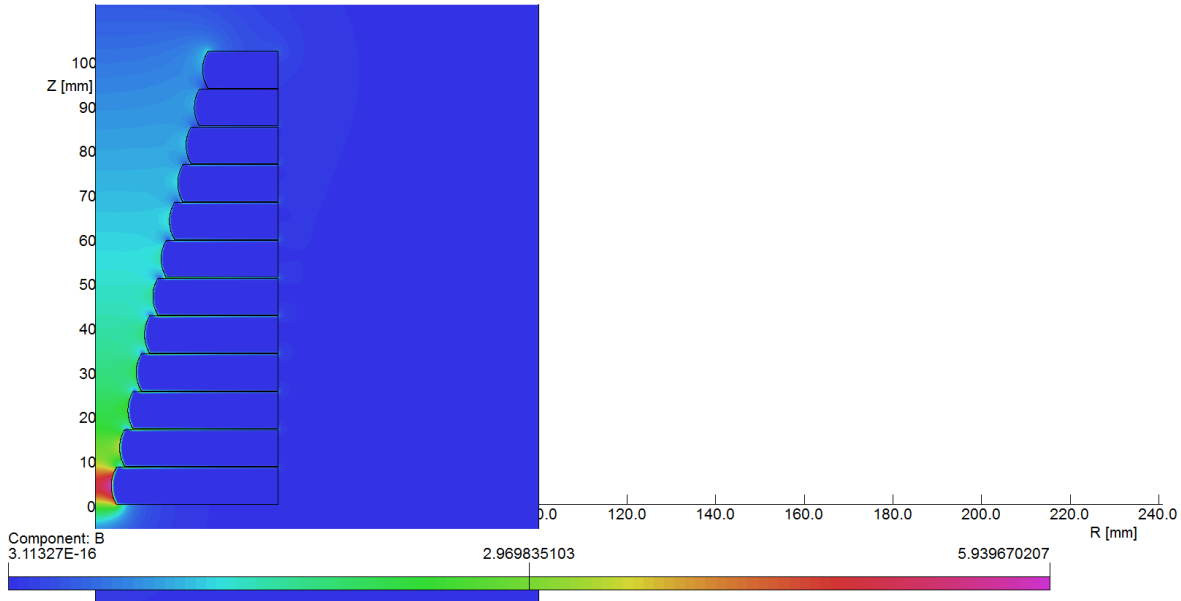
# The origin of the field boost



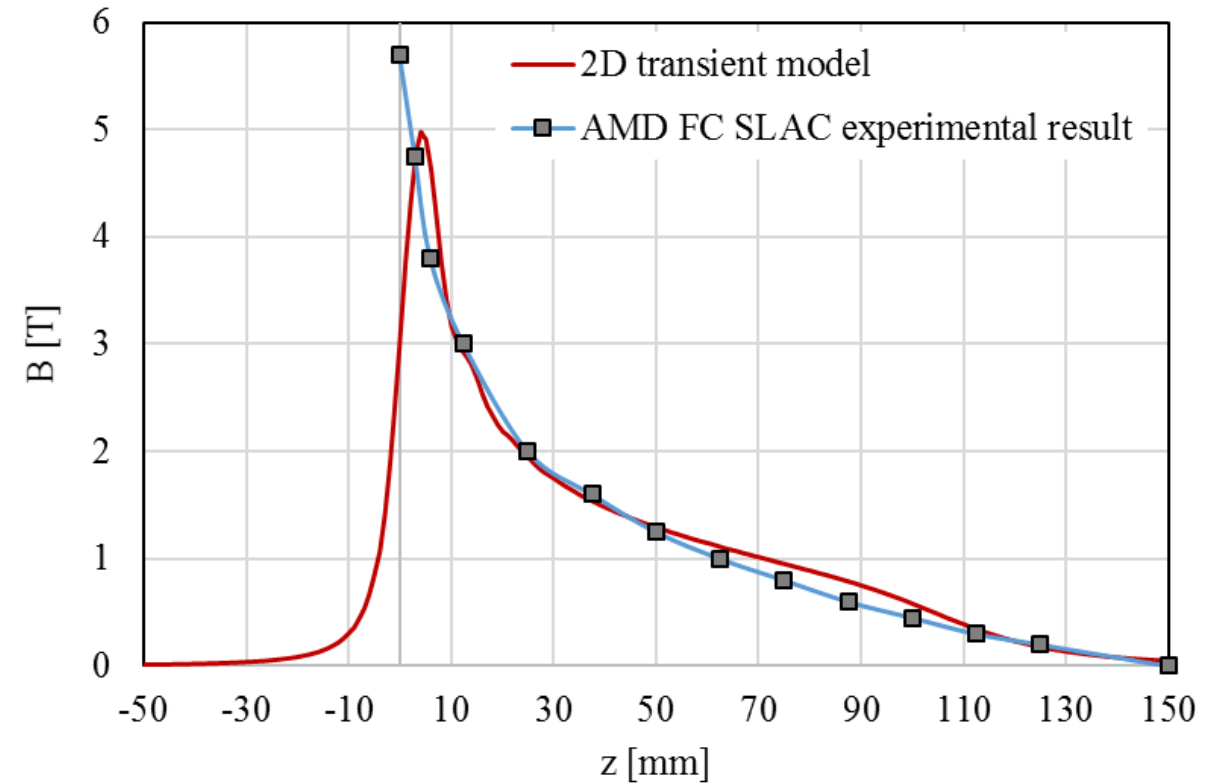
The **boost of field** only occurs for tapered coil in **transient mode** when both **skin effect** and **eddy current** occur.

<https://agenda.linearcollider.org/event/8217/>

# Comparison with experimental result: SLAC

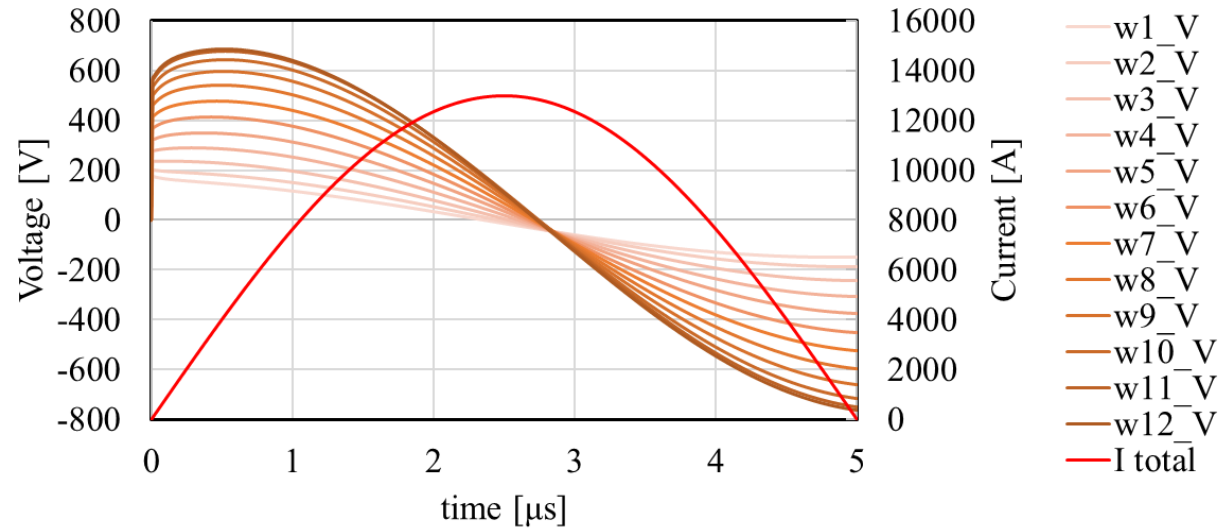


Solenoidal field map

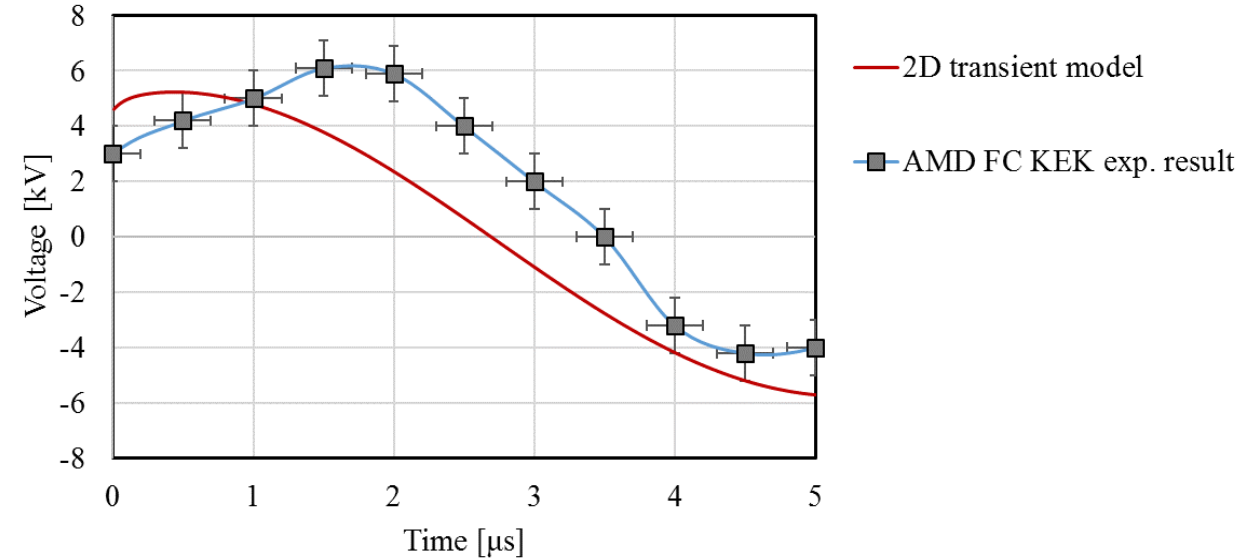


<https://agenda.linearcollider.org/event/8217/>

# Comparison with experimental result : KEK



Voltage across each turn

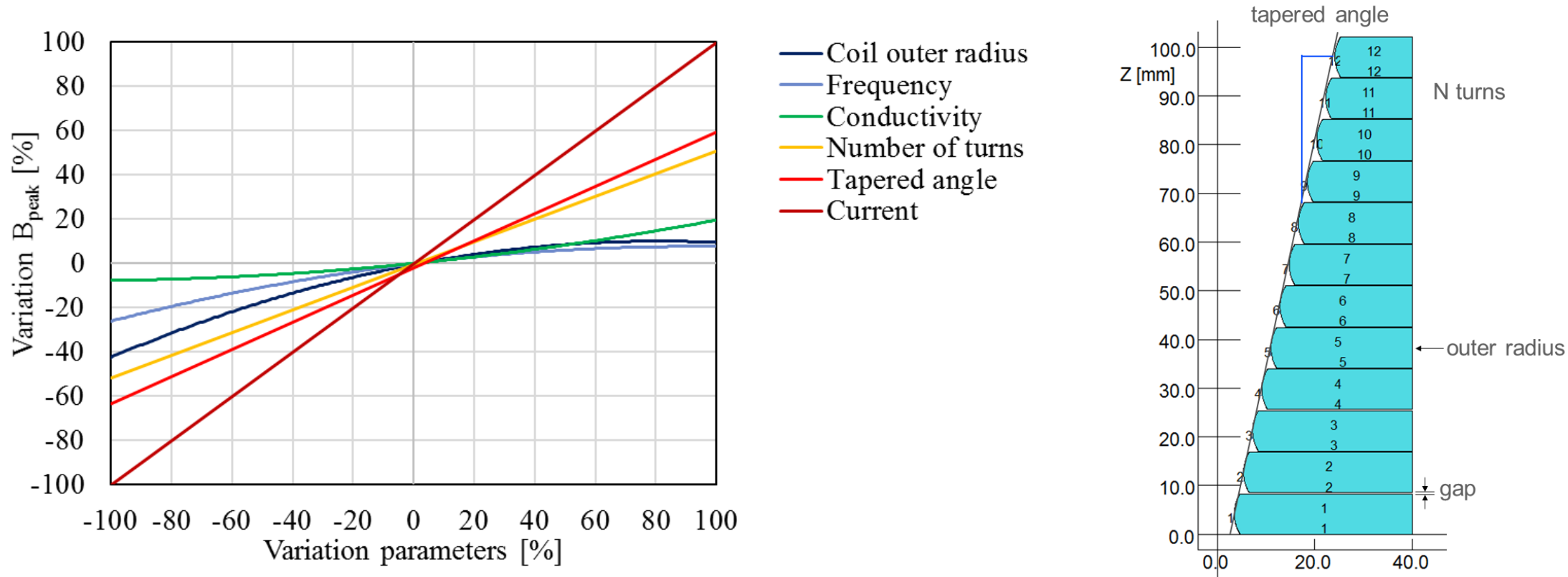


Voltage across the solenoid

<https://agenda.linearcollider.org/event/8217/>



# Parametric study for FC design optimisation



A **tool to optimise** FC's design.

In particular it is possible to **increase the gap between turns** compensating the loss of field.

<https://indico.cern.ch/event/879495/>

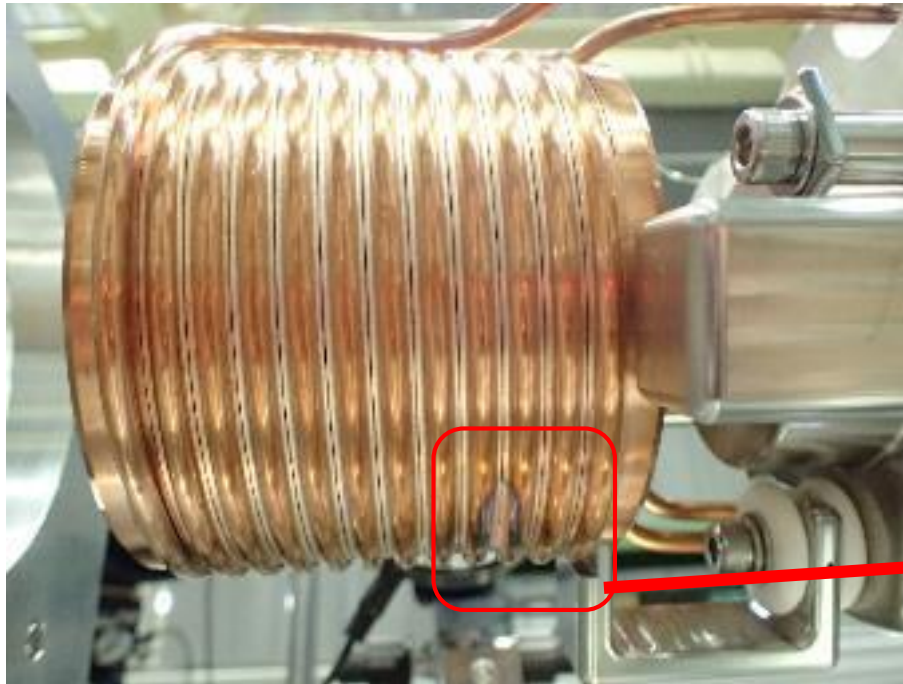
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# Dielectric breakdowns during the test of the KEKB FC

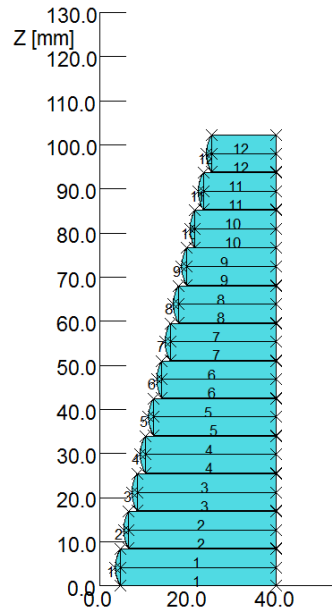
- Issue of **electrical arcing** between turns at full current discharge during FC test.

Flux Concentrator  
design from KEK



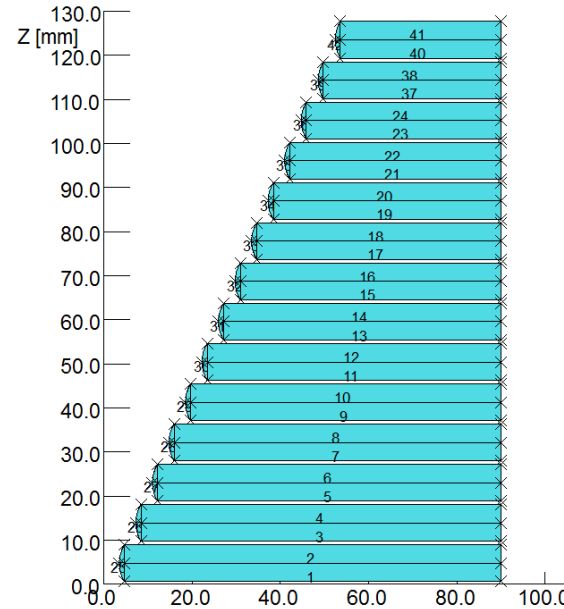
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# Modified design to cope with breakdown issue



## SLAC design

gap=0.2 mm  
 $\sigma=5.67 \cdot 10^7$  S/m  
 $R_o=40$  mm  
N=12 turns  
 $\gamma=0.255$   
f=100 kHz



## Modified design

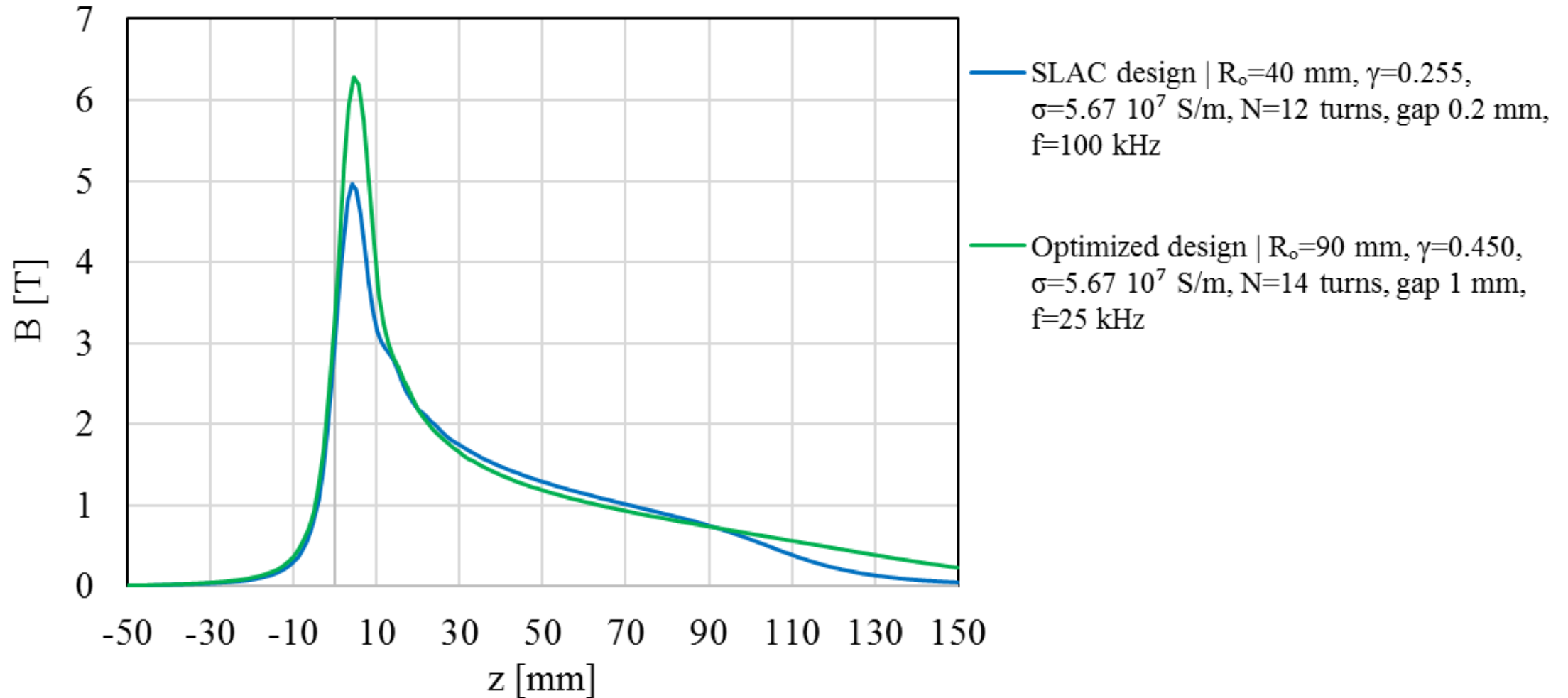
gap=0.8 mm  
 $\sigma=5.67 \cdot 10^7$  S/m  
 $R_o=90$  mm  
N=14 turns  
 $\gamma=0.450$   
f=25 kHz

The **gap** between turns is increased and the loss of field compensated with **2 extra turns** and larger **tapered angle**.

The voltage between turns is minimized using lower frequency and larger outer radius.

<https://indico.cern.ch/event/879495/>

# Expected results for the modified design

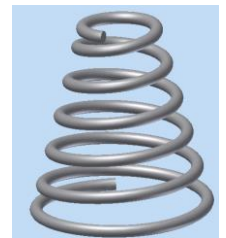
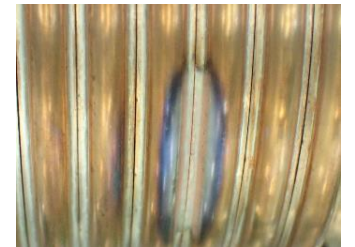
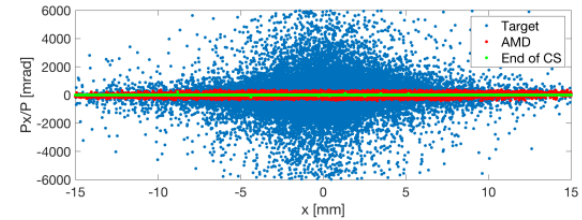


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# Design optimization for the CLIC e+ source

- Parameters to optimize:
  - To maximize:
    - the *positron yield* (purpose of the device)
  - To minimize:
    - the *total voltage* & the *inter-turn voltage* (power supply limitation & electrical breakdown)
    - the Lorentz forces (mechanical displacement, vibration)



# Design optimization for the CLIC e+ source

- OPERA computes: the field, the voltages and the Lorentz forces.
- The positron yield is computed using RF-track and GEANT4 by Yongke Zhao (many thanks!).

<https://indico.cern.ch/event/862915/>

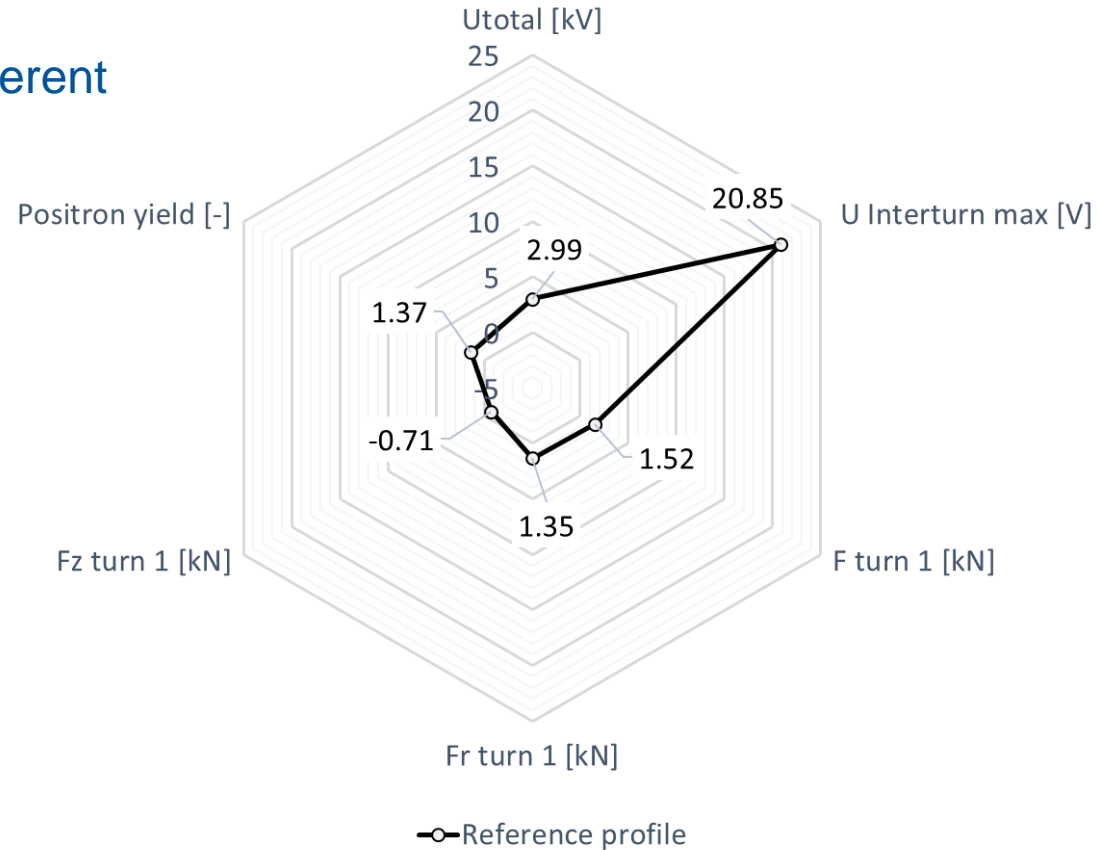


# Design optimization for the CLIC e+ source

SLAC design  
@ 25 kHz & 13 kA

Graphics containing the parameters to optimize.

Use of the radar plot to compare different design of FC.

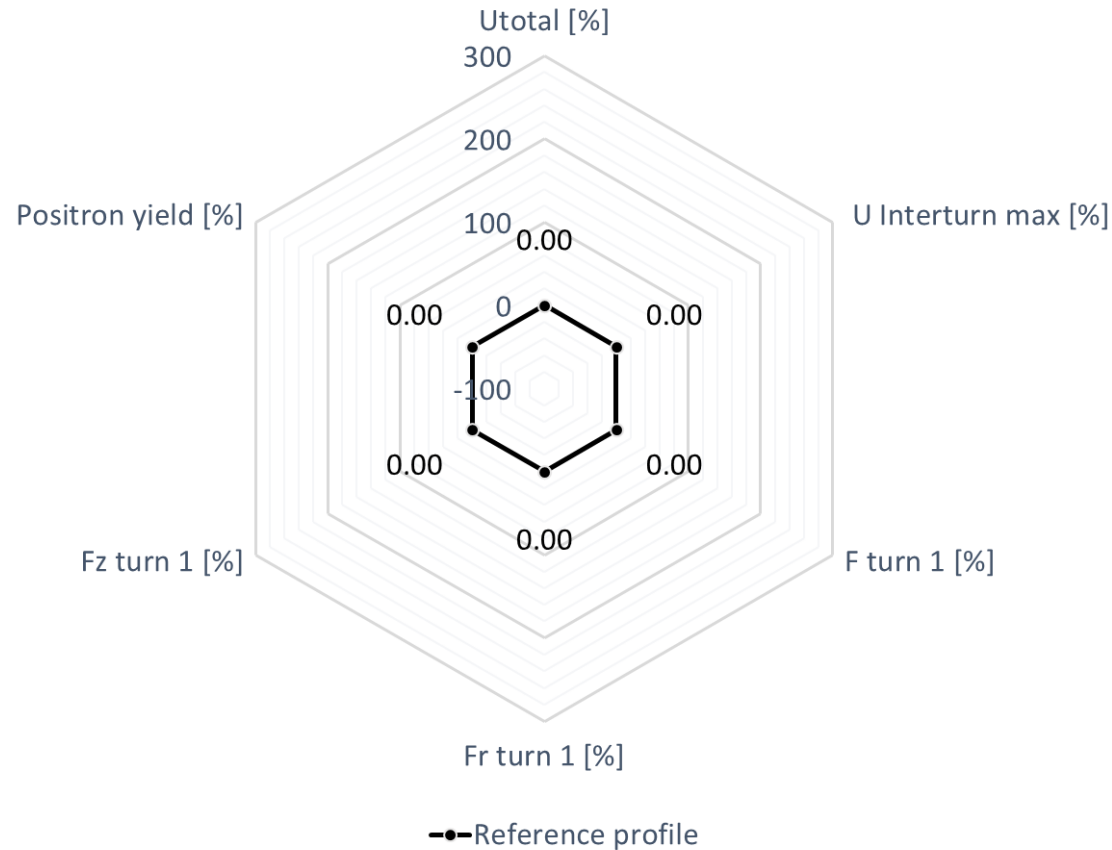


# Design optimization for the CLIC e+ source

Normalization of each parameter to its reference value:

$$Var [\%] = 100 * \frac{(V - V_{ref})}{V_{ref}}$$

SLAC design  
@ 25 kHz & 13 kA



# Design optimization for the CLIC e+ source

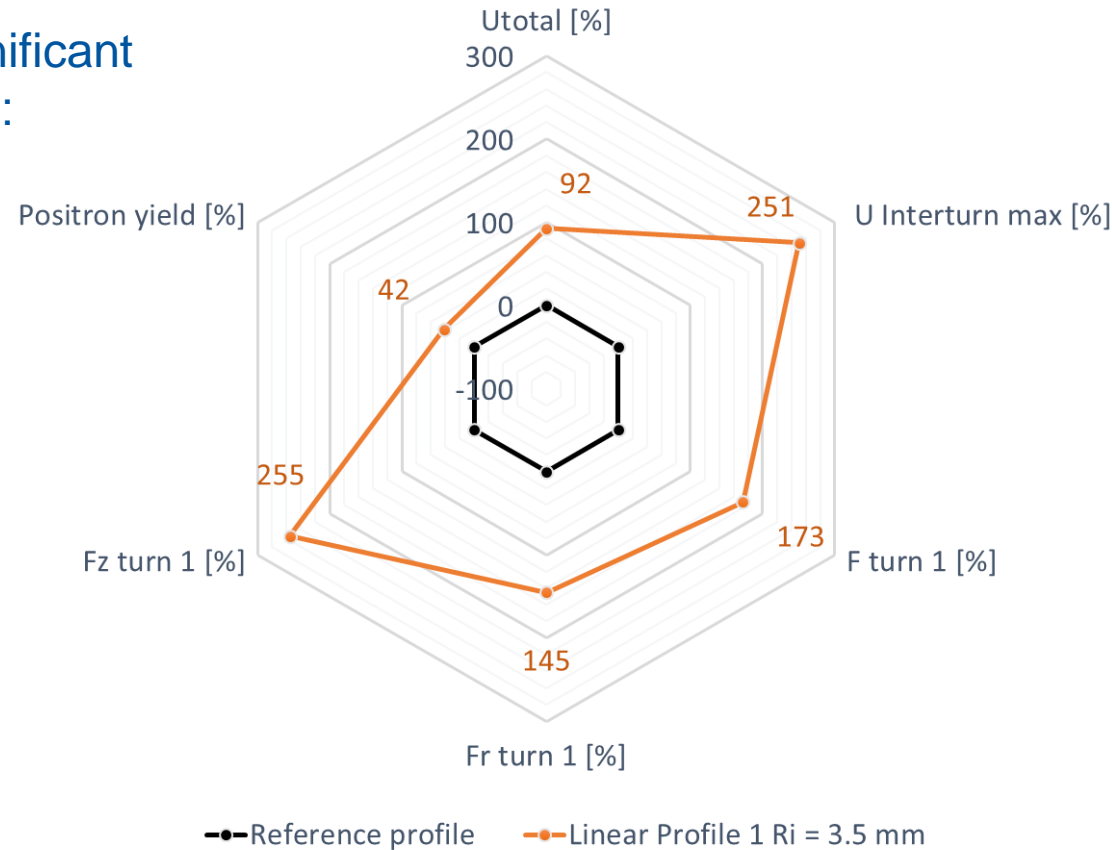
SLAC design (reference)  
@ 25 kHz & 13 kA

Vs.

**linear modified design**  
**@ 25 kHz & 13.8 kA**

The modified design induces a significant increase of each parameters' value:

- The yield increases by 42%
- The voltage increases by 92% (due to the gap increase and current increase)
- The forces get ~3 times higher



# Design optimization for the CLIC e+ source

SLAC design  
@ 25 kHz & 13 kA

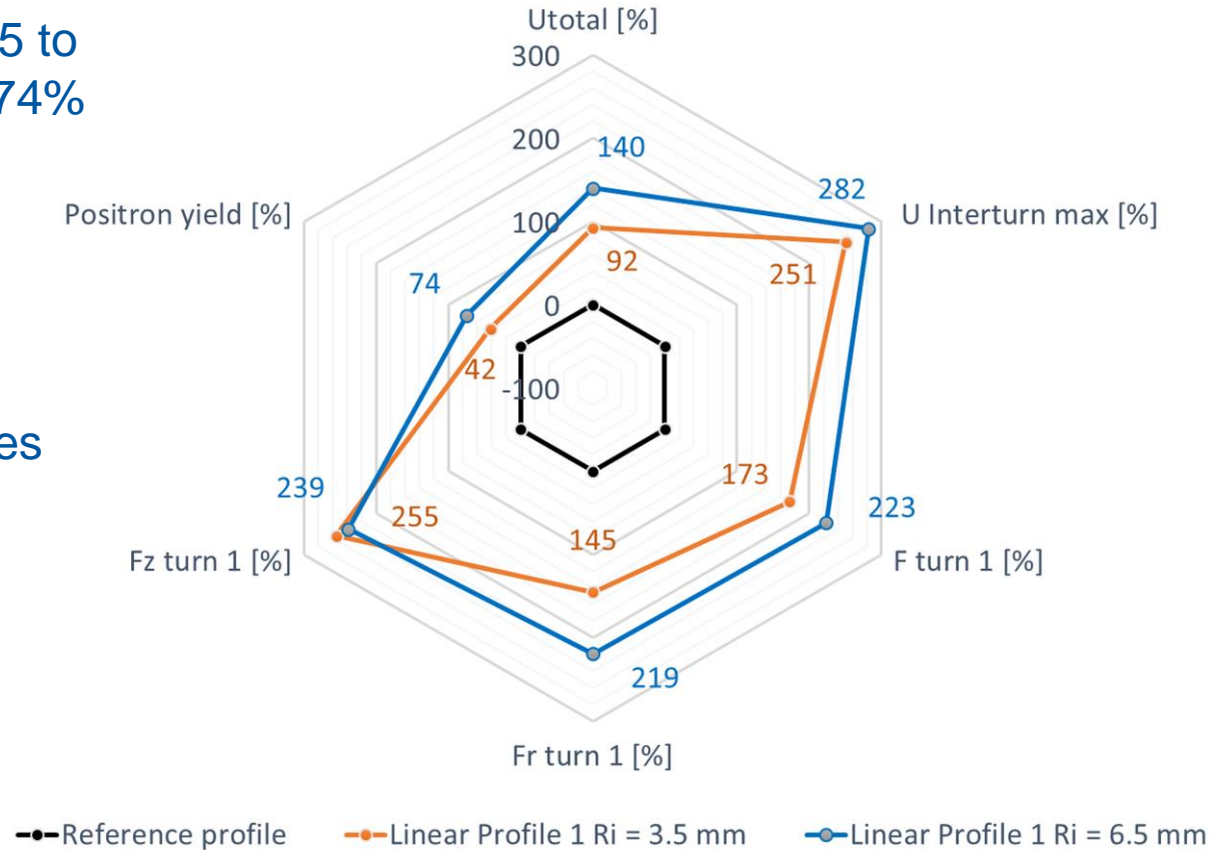
Vs.

linear modified design

Vs.

linear modified design  
with large aperture

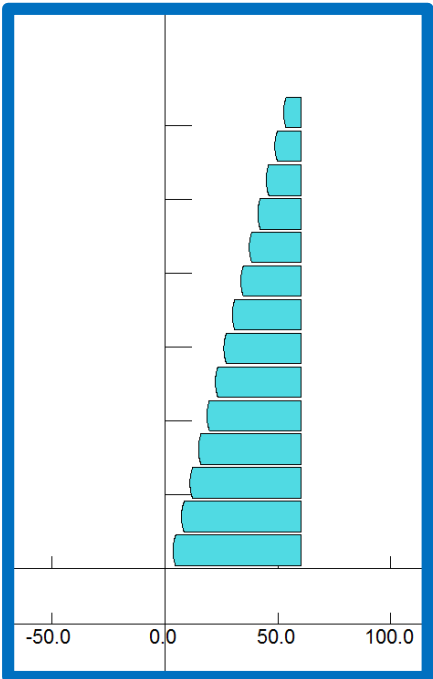
- Increasing the aperture from 3.5 to 6.5 mm increases the yield by 74% (from 1.37 to 2.39).
- Both voltages and Lorentz forces grow very fast!



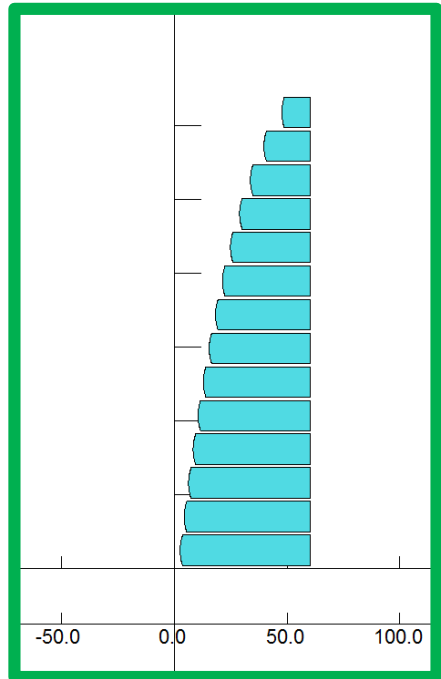
# Design optimization for the CLIC e+ source

- From linear to non-linear profile for the FC aperture:

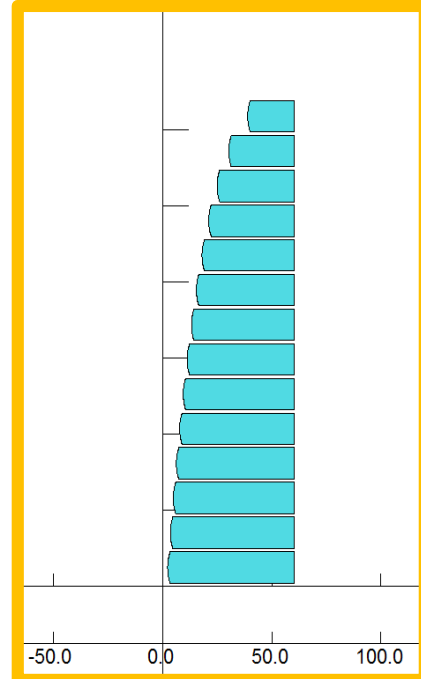
Linear



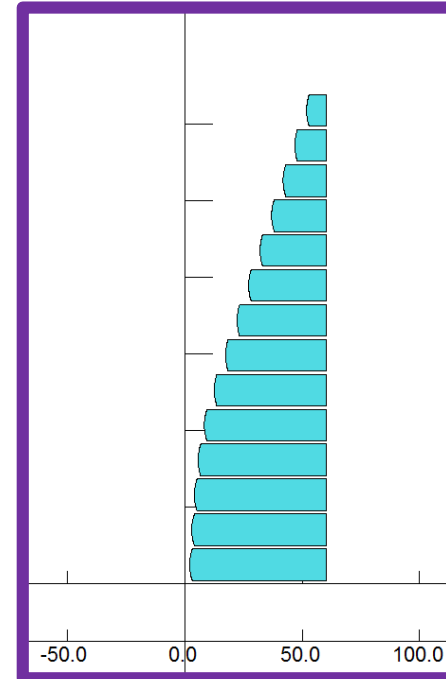
Concave downward (1)



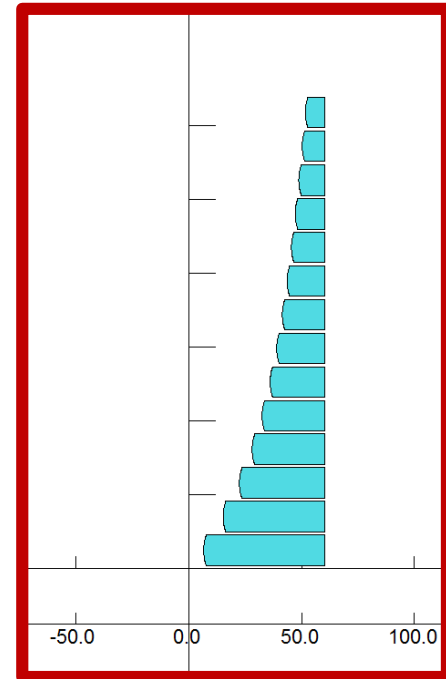
Concave downward (2)



Concave downward + linear (3)



Concave upward



How does the shape impact the parameters to optimize?

# Design optimization for the CLIC e+ source

SLAC design  
@ 25 kHz & 13 kA

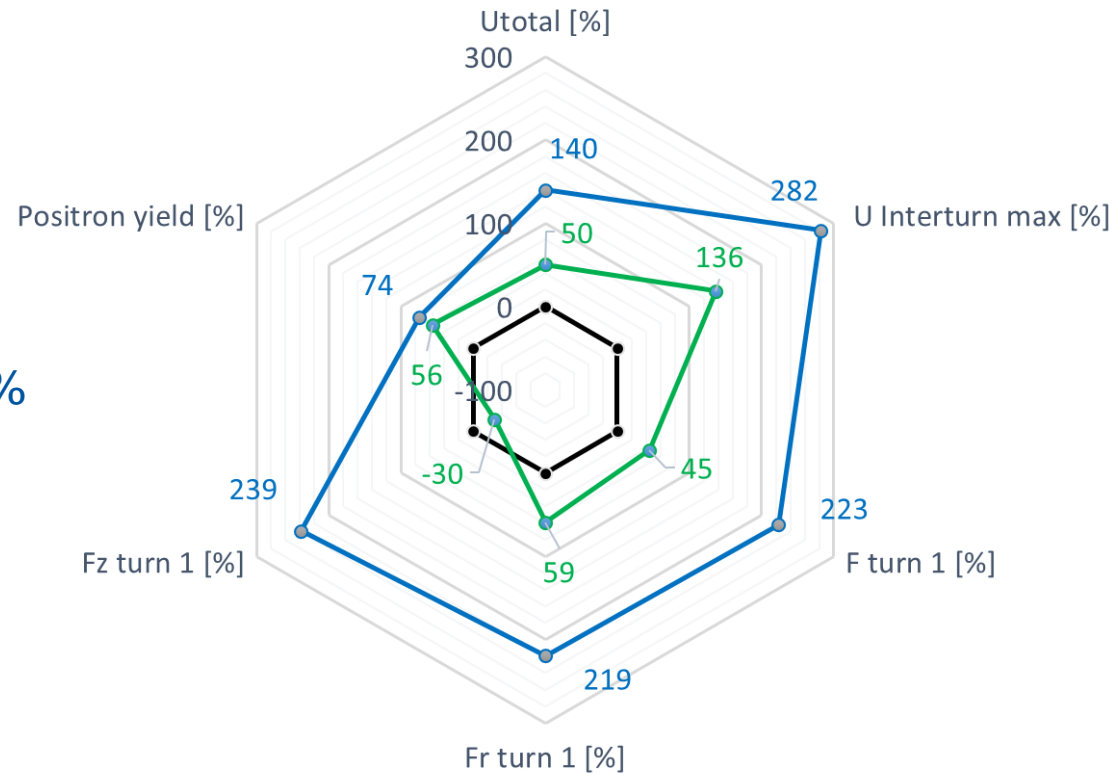
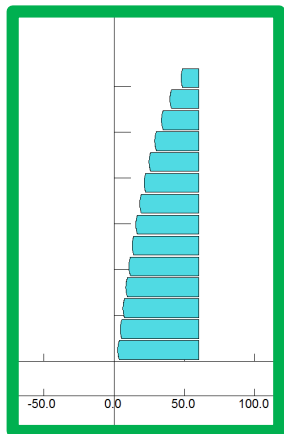
Vs.

**linear modified design  
with large aperture**

Vs.

**Non-linear design (1)  
Concave downward**

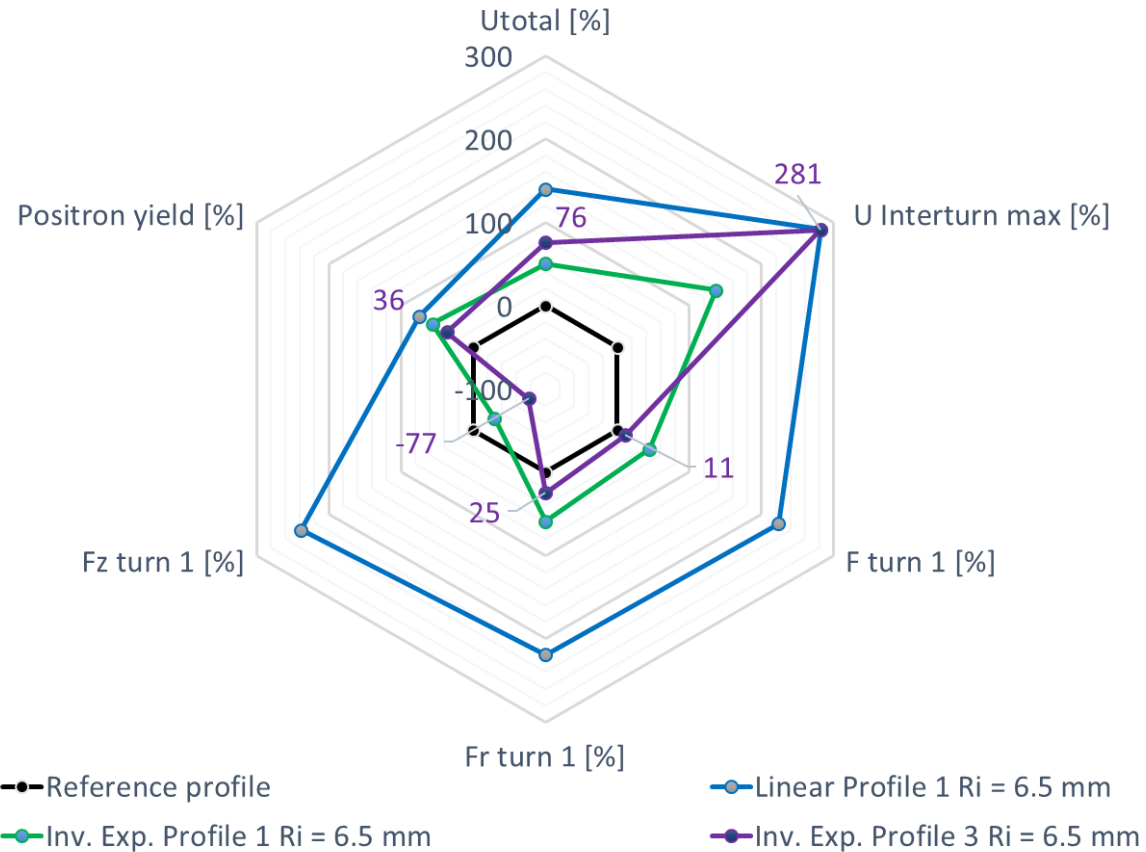
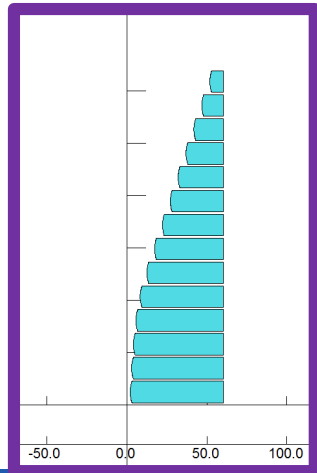
- The use of non-linear shape induces a dramatic drop of the voltages.
- The Lorentz forces decrease significantly.
- The yield get lower but is still 56% higher than the reference case.



● Reference profile    
 ● Linear Profile 1 Ri = 6.5 mm    
 ● Inv. Exp. Profile 1 Ri = 6.5 mm

# Design optimization for the CLIC e+ source

- Using more exotic shape allows to decrease the Lorentz forces.
- The yield gets lower though.
- The voltage gets higher.



SLAC design  
@ 25 kHz & 13 kA

Vs.

**linear modified design  
with large aperture**

Vs.

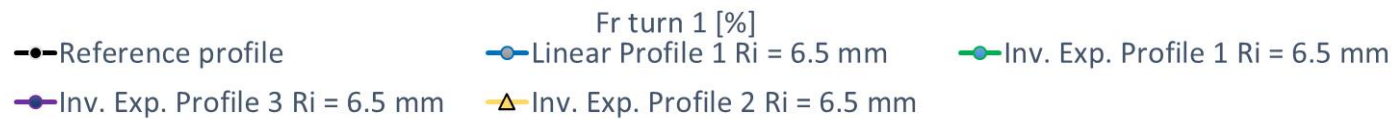
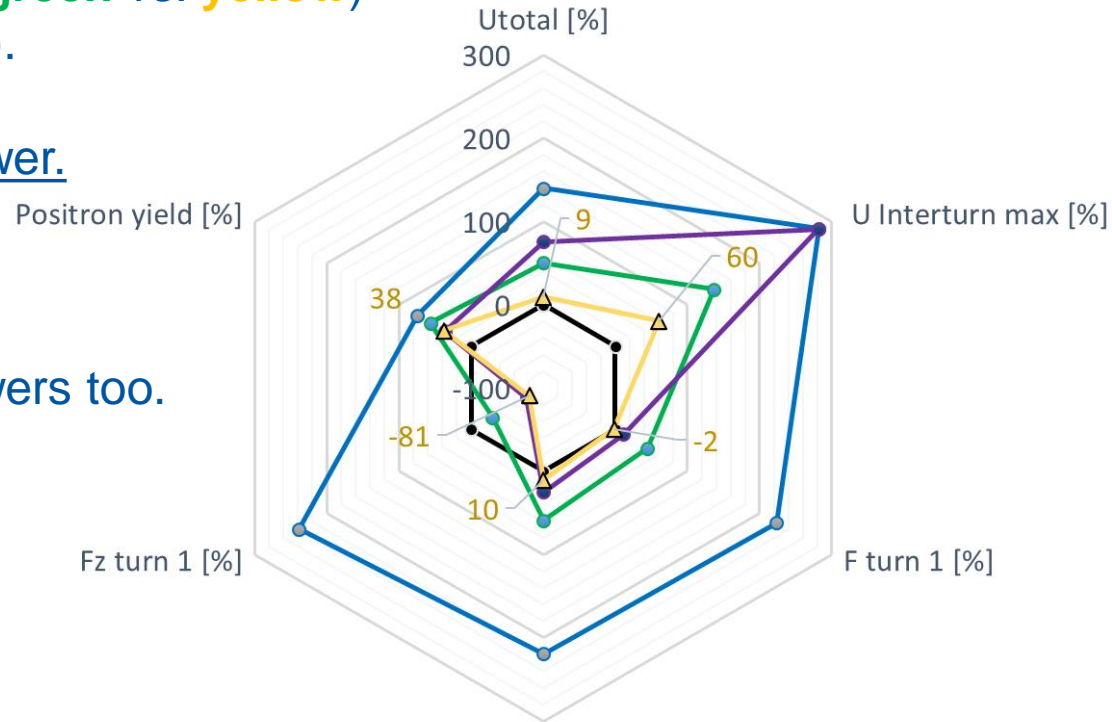
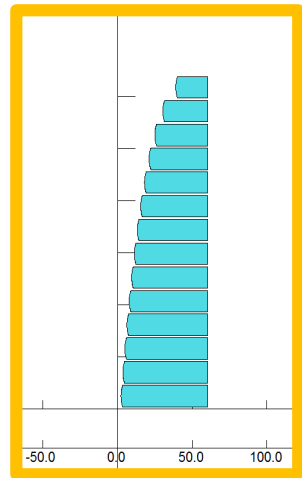
**Non-linear design (1)  
Concave downward**

Vs.

**Non-linear design (3)  
Concave downward + linear**

# Design optimization for the CLIC e+ source

- Adapting the non-linear shape (**green vs. yellow**) preserves the yield (38% higher).
- The voltages get significantly lower.
- The detrimental forces directed along the coil axis  $Z$  lowers too.



SLAC design  
@ 25 kHz & 13 kA

Vs.

**linear modified design  
with large aperture**

Vs.

**Non-linear design (1)  
Concave downward**

Vs.

**Non-linear design (3)  
Concave downward + linear**

Vs.

**Non-linear design (2)  
Concave downward**

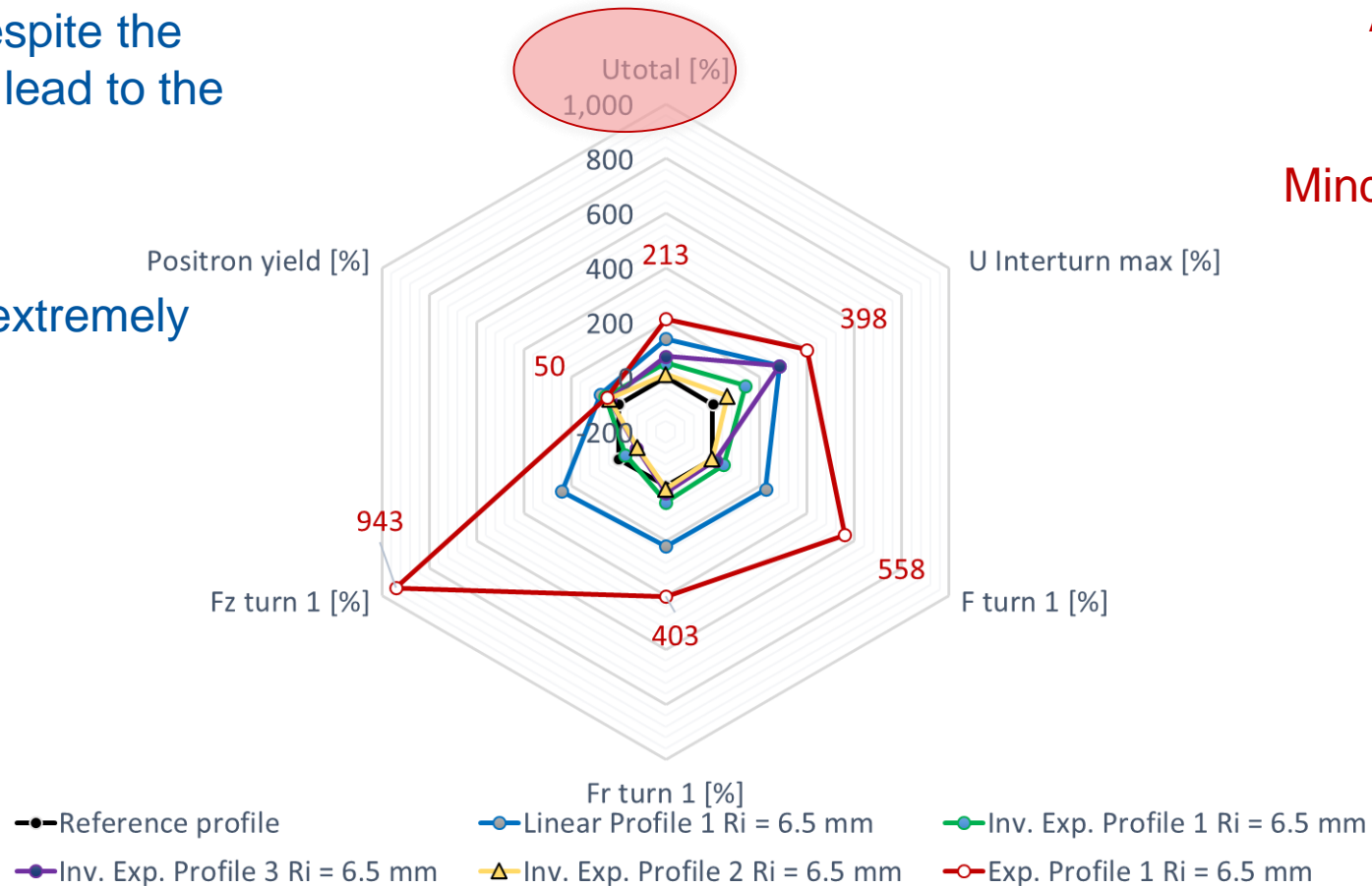
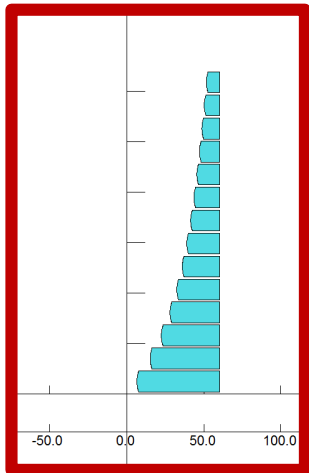


# Design optimization for the CLIC e+ source

- The upward concavity despite the highest peak field do not lead to the highest yield.
- Voltages and forces get extremely high.

Adding the upward concavity case

Mind the change of scale !!



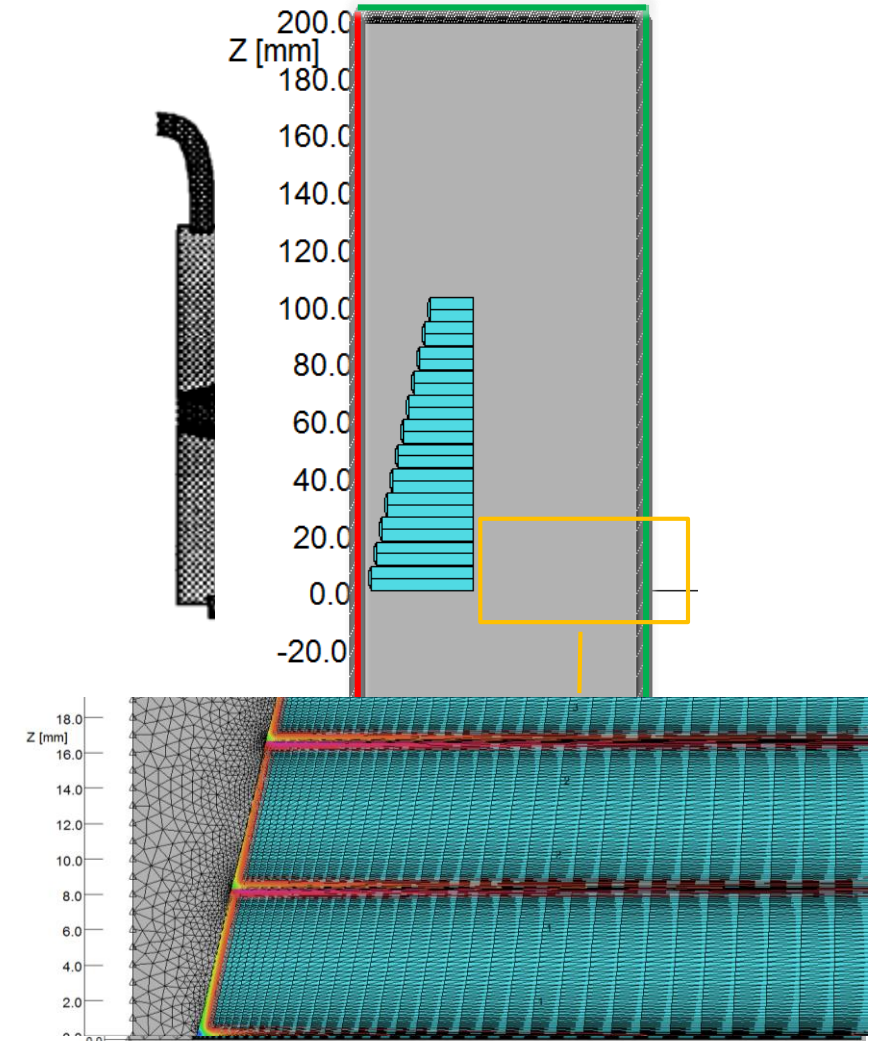
# Conclusion

- Construction of a transient electromagnetic model of Flux Concentrator using Opera<sup>®</sup> software.
- Validation of the model by direct comparison with available experimental data (current, voltage and magnetic field).
- Parametric study for optimization of the electromagnetic behavior (voltage and field) to cope with breakdown voltage issue.
- Export of 2D field maps as input for particles tracking software packages (GEANT4, RF-track) and positron yield computations.
- New design of the coil's geometry using non-linear profiles for coupled optimization: electromagnetic, mechanical (Lorentz forces) and optical behavior (positron yield).
- The optimization process lead to an interesting design that produces a better positron yield of 1.89 (38% gain) keeping low voltages (3kV, 10% extra) and lower forces (-81%  $F_z$ , -2%  $F_{total}$ ).



# Modelling of the geometry

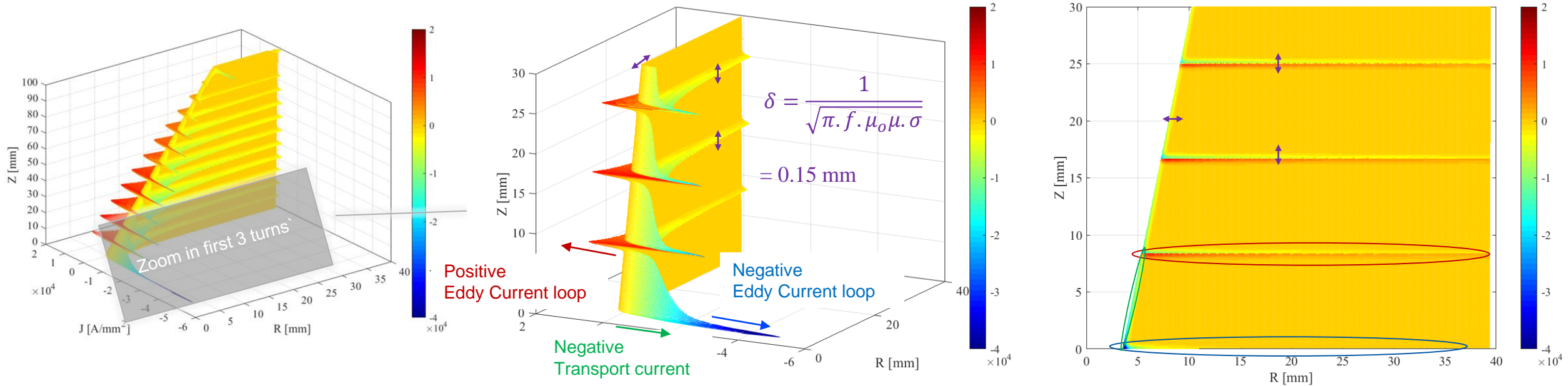
- 12-turn tapered solenoid (SLAC design)
- 2D model
- Axi-symmetric system
- Boundary conditions:
  - Tangential field for symmetry and far field
- Material properties
  - Conductivity with linear behavior (OFHC Copper)
- Regular mesh and mesh refinement:
  - quadrilateral Finite Element in conductor and Bias method
- Transient simulation:
  - Eddy Current and Skin effect



# Backup

# The origin of the field boost

## Tapered solenoid in transient



The pulse of current produces strong **eddy current loops** that circulate in opposite directions within each turn.

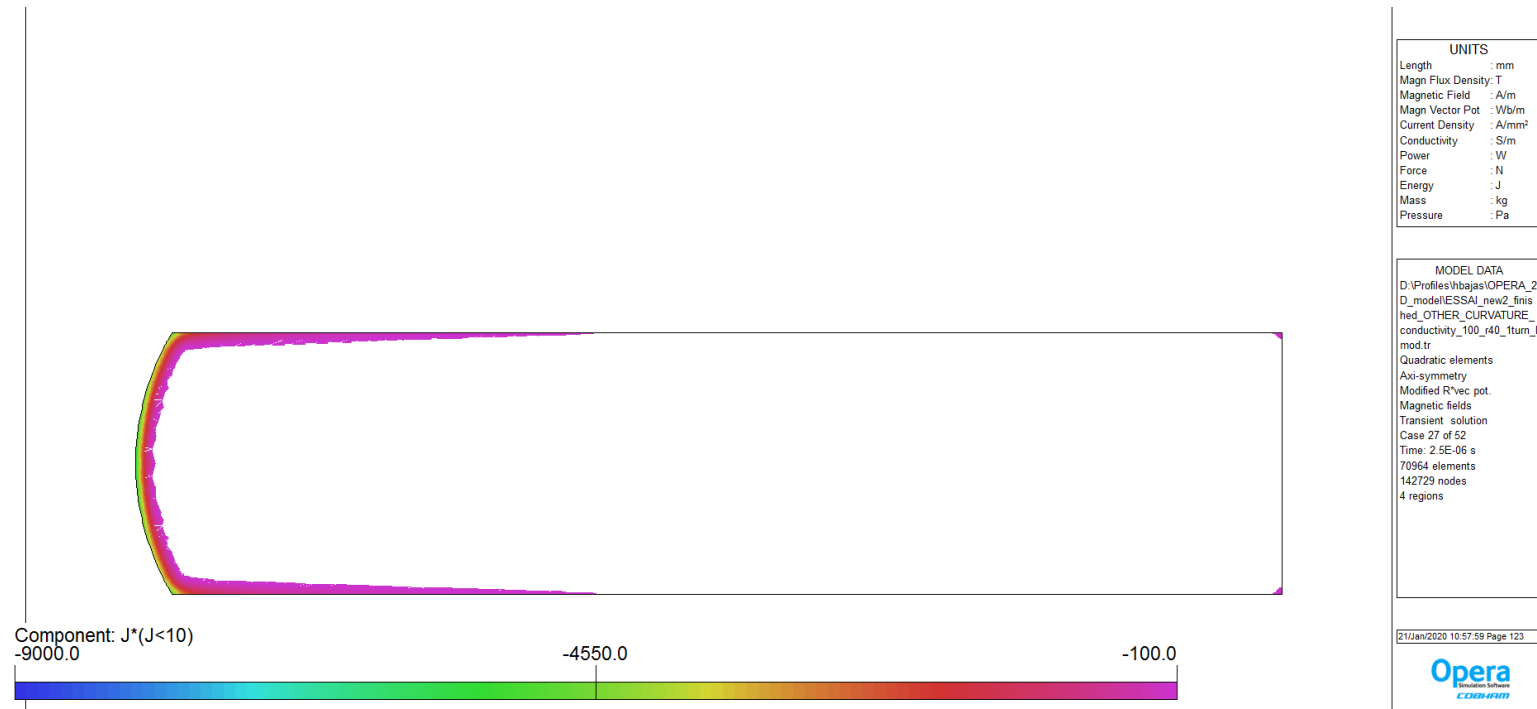
The current density concentrates at **the skin of the conductor**.

<https://agenda.linearcollider.org/event/8217/>

# The eddy currents depend on the adjacent turns

Let's model  
One-turn coil

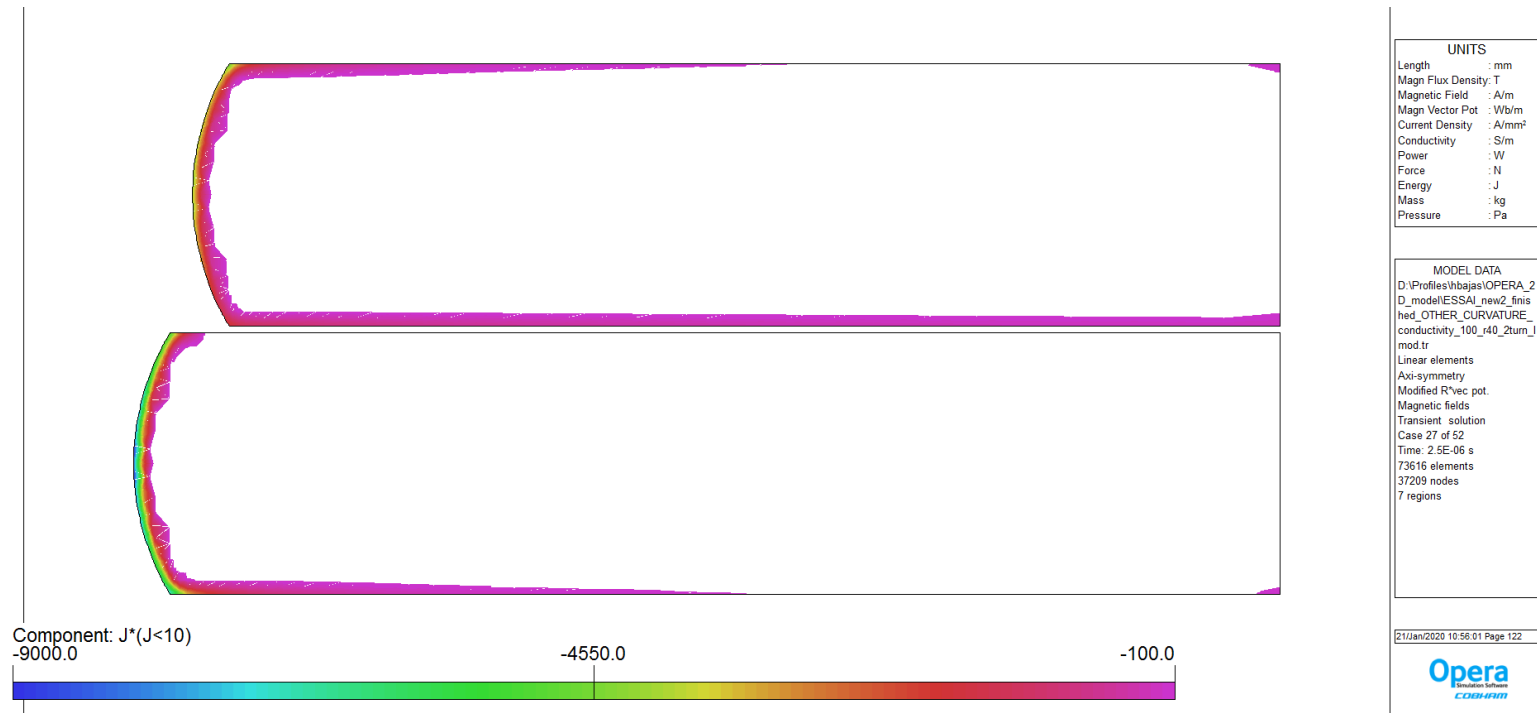
The current  
density is only  
negative



# The eddy currents depend on the adjacent turns

Let's model  
Two-turn coil

The current density  
is both positive &  
negative



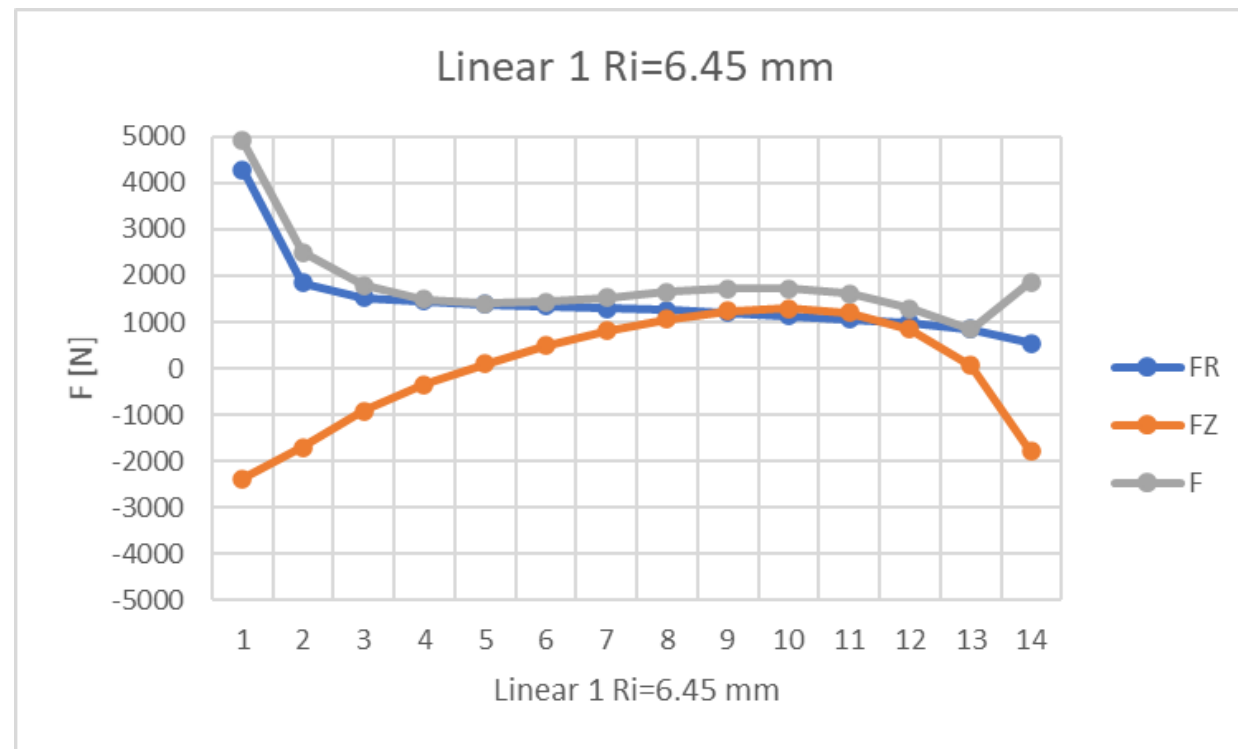


# Third run of optimisation

**The Lorentz force are now available as output data.**

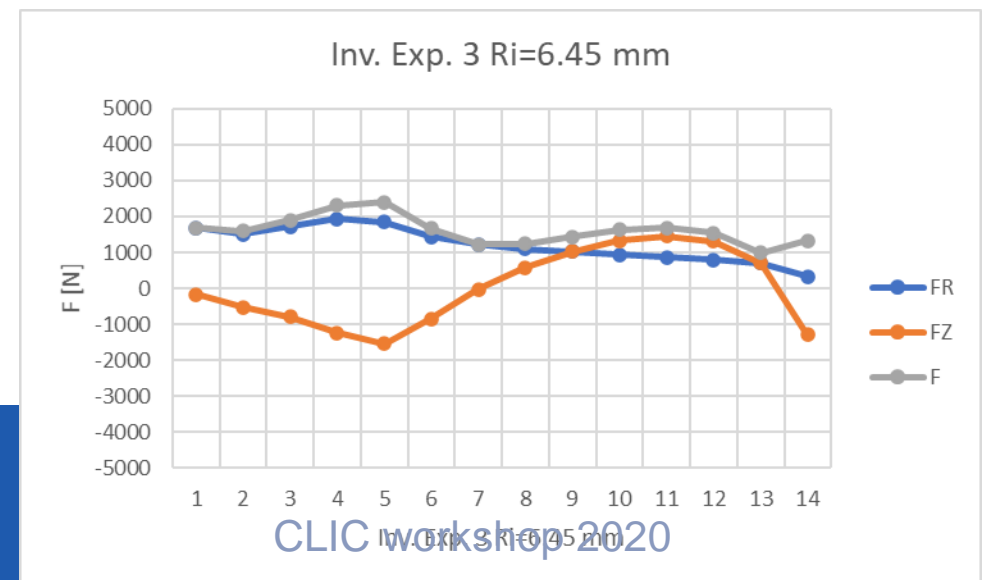
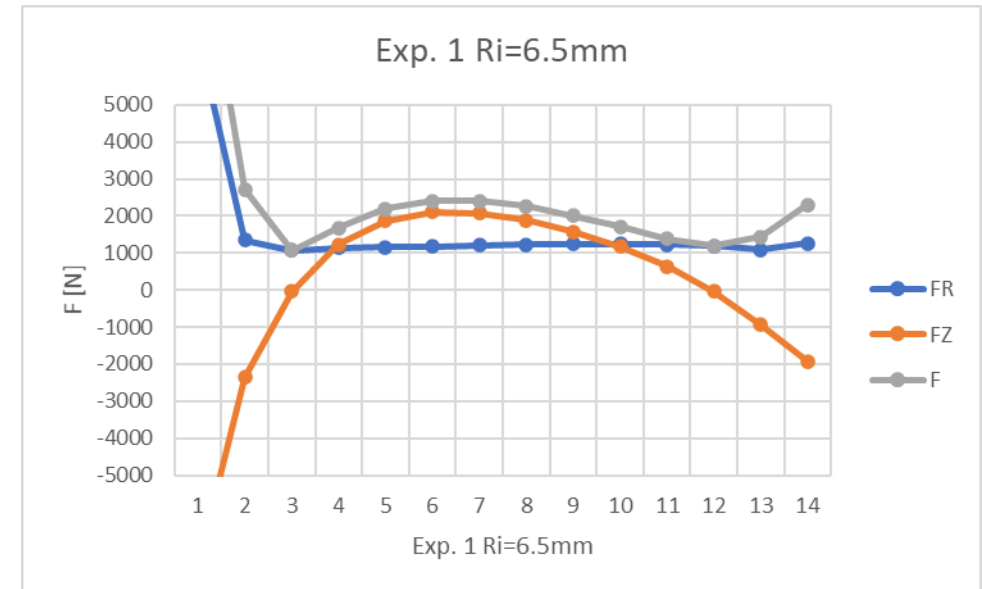
The forces are not only directed along the radius in the outward direction.

A significant compressive force applies to the FC along the solenoid axis.



The distribution of the force along and accross the coil is complexe and need further investigation.

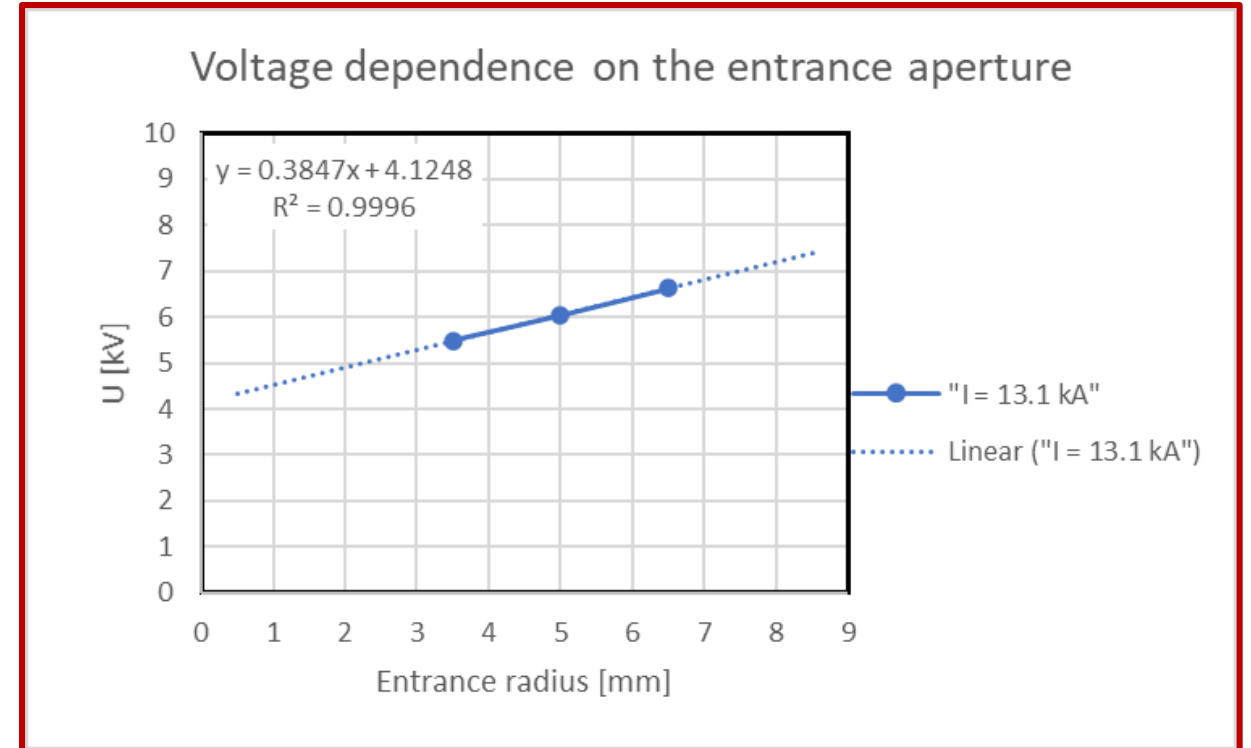
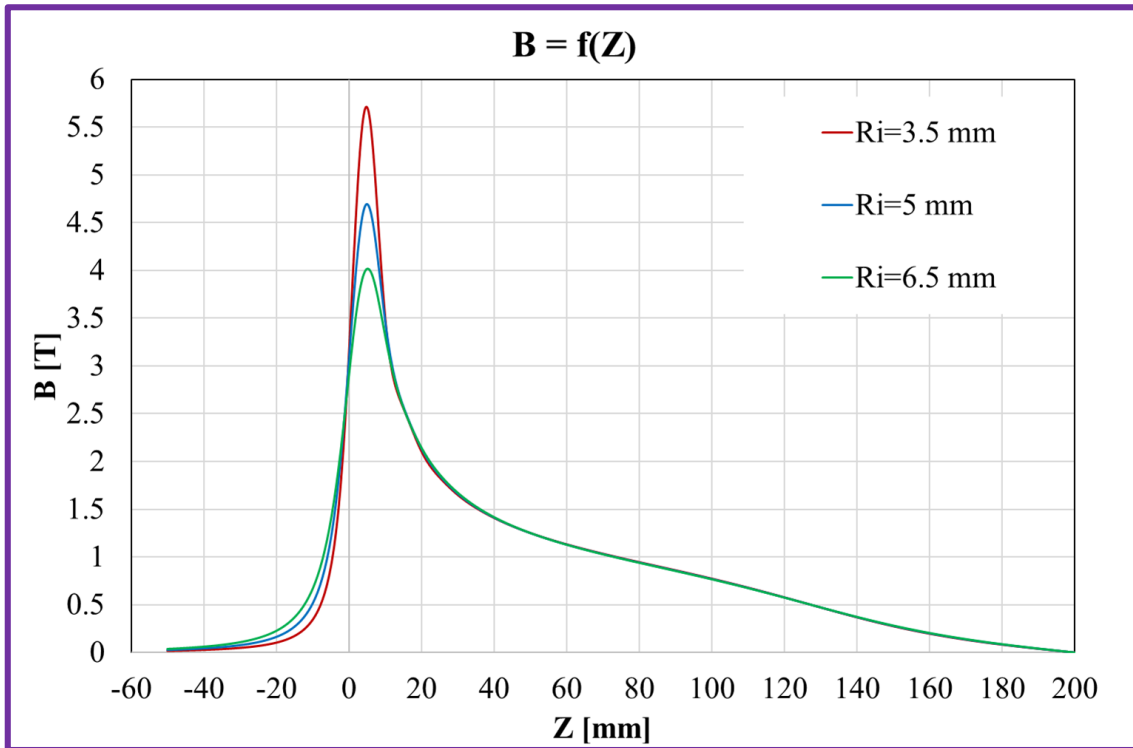
It changes a lot with the geometry.



# Design optimization for the CLIC e+ source

- Increasing the entrance aperture yields to higher positron but:
  - The field decreases with the aperture
  - The voltage increases with the aperture

R. H. Helm, SLAC, Report No. 4, August 1962.



# Design optimization for the CLIC e+ source

The shape of the FC profile significantly impacts the shape of the field distribution.

The downward concavity leads to:

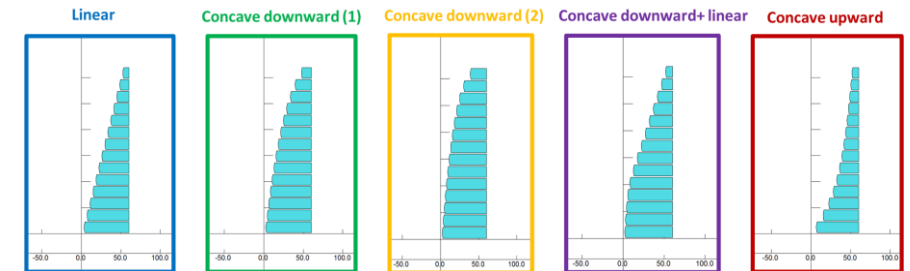
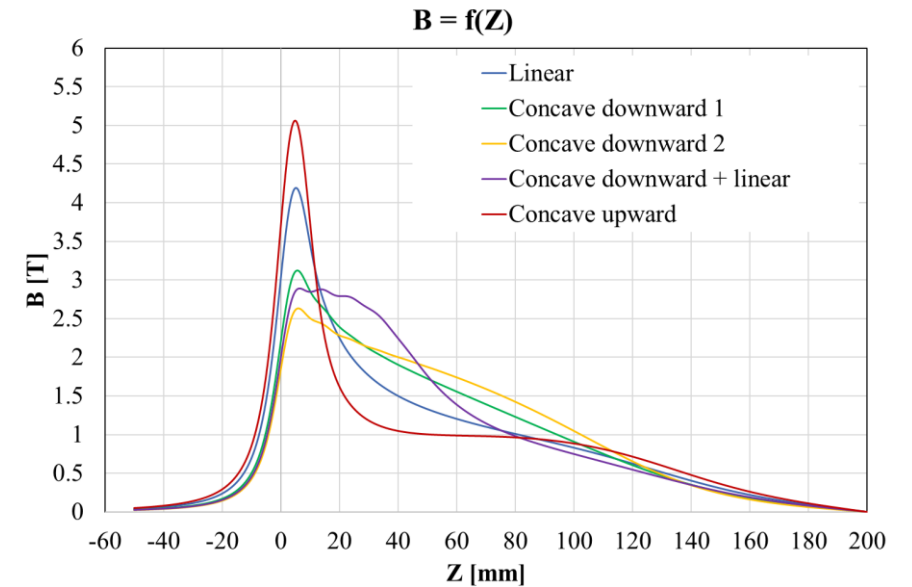
- a broad distribution in the low field domain ( $< 3T$ ) that extend to  $Z=50$  mm
- Small fringe field  $Z < 0$  mm

The upward concavity leads to:

- a “peaky” distribution in the high field domain ( $>4T$ )
- Larger fringe field

More complex shape:

- The field distribution can be more or less broad according to the design



What is a «GOOD FIELD DISTRIBUTION» in terms of positron yield?

# Design optimization for the CLIC e+ source

The voltage across the magnet is largely impacted by the coil design.

Still the tradeoff between Good Field Distribution and Voltage level should be done.

