

DFH Detail Design Review Cables, splices and instrumentation

J. Fleiter and A. Ballarino on behalf of WP6a

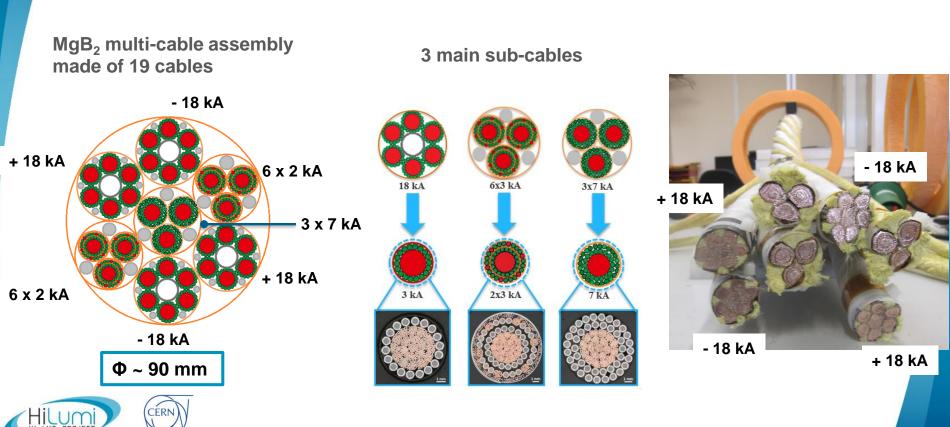


Outline

- MgB₂ and HTS cables
- Routing of cables
- Splices geometry and fix point
- Dielectric insulation requirements
- Instrumentation (Vtaps and temperature)



MgB₂ cables of IT Sc Link

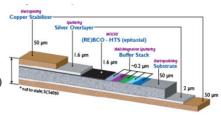


HTS cables of IT Sc Link

- HTS cables will operate between 50 K and 20 K with field ~ 1 T
- HTS cables made from REBCO tapes (4 mm x 0.1 mm)
- HTS tapes helically wound around a multi strand core 11 mm OD to form 3 kA sub cables.
- Sub cables insulated with Kapton tapes, (11.5 mm OD)
- Six sub-cables assembled to form the 18 kA cables (40 mm OD)
- Two 3 kA sub-cables for the trims circuits (arranged in six around 1)
- Orbit corrector cable made of a single sub cable (arranged by groups of four)









18 kA HTS cable (wo final insulation)

MgB₂/HTS splices

- HTS/MgB₂ splice will be performed by soldering (Sn-Pb or Sn-In)
- Sub-cables will be spliced in equipotential to allow current redistribution
- Splices dimensions:
 - 18-14 kA 300mm x 70 mm x 60 mm
 - 2 kA trim 300 mm x 20 mm x 45 mm
 - 2 kA 650 mm x 20 mm x 30 mm
 - **0.6 kA** 300 mm x 20 mm x 30 mm

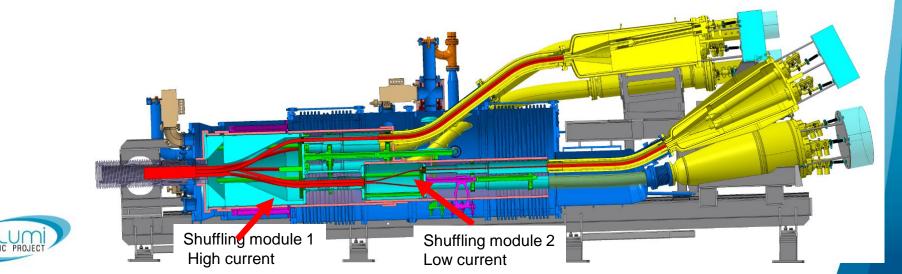


 MgB₂/HTS splices will be fix points. Splice will be encapsulated in insulated structure allowing GHe convection and rigid contact with the He sleeves (see next slides) providing sufficient dielectric insulation.



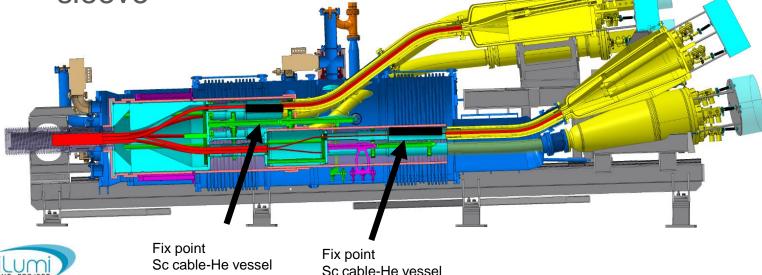
From DSH each MgB₂ cable is routed to its current leads via shuffling modules

- DFHx equipped with two shuffling modules (high and low current)
- DFHm equipped with only one shuffling module
- S-bend of Sc cable in shuffling module and till the leads designed to accommodate differential thermal shrinkage
- Routing of MgB₂ and HTS cables respect the minimum bending radius.



Fix points at splice location

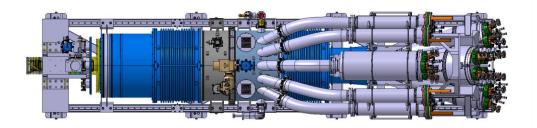
- Each MgB₂/HTS splice will be a fix point
- Splice will be encapsulated in insulating material that allow He flow, sufficient arc length and longitudinal contact with sleeve

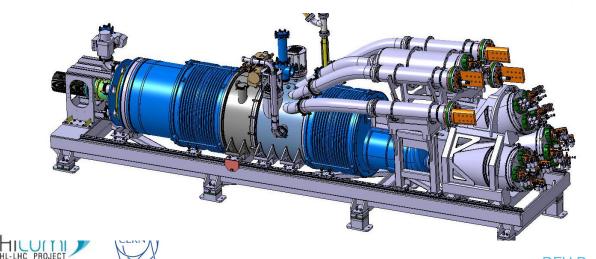


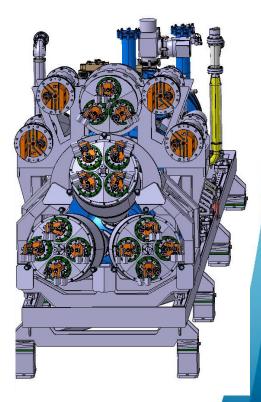
Lorentz forces on cable in DFH

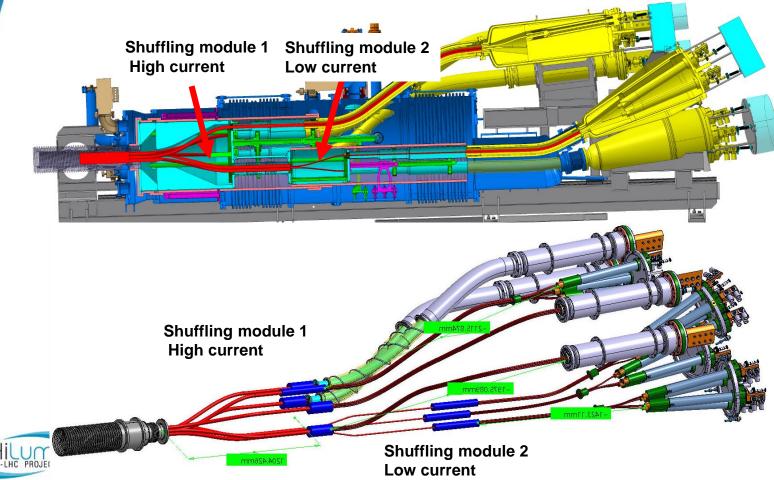
- Cables are maintained together in the Sc Link assembly via the structure of the cable
- In the shuffling modules, cables maintained in place via adapted mechanical structure
- Typical forces:
 - 650 N/m for 2x18 kA @ 100 mm
 - 8 N/m for 2x2 kA @ 100 mm
 - 72 N/m for 2 and 18 kA @ 100 mm
- Length of shuffling module is about 600 mm



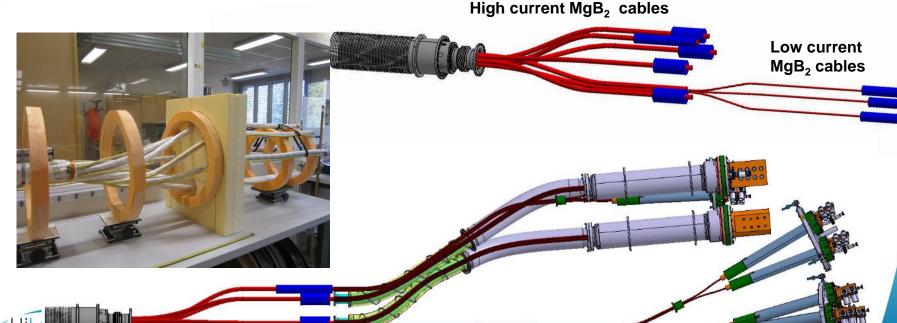


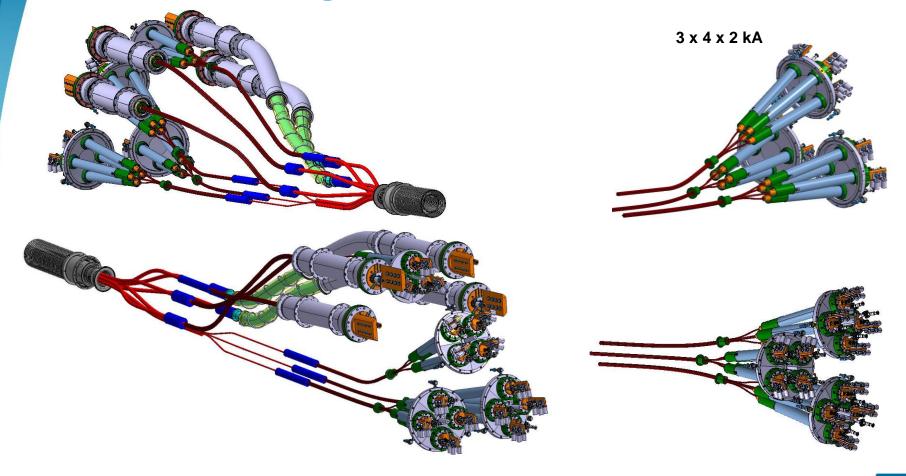


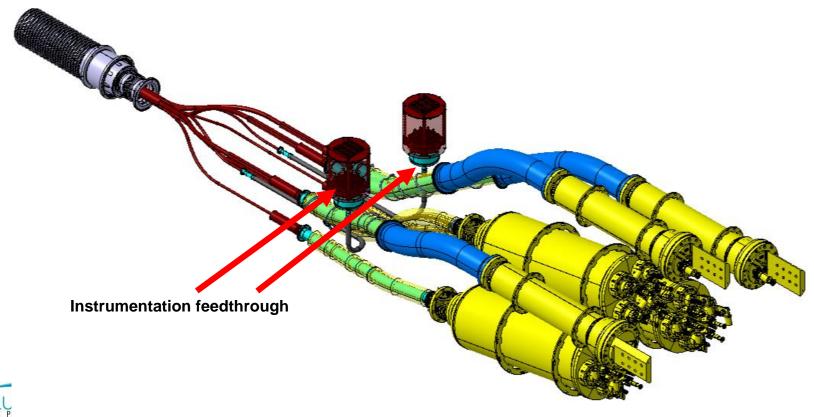


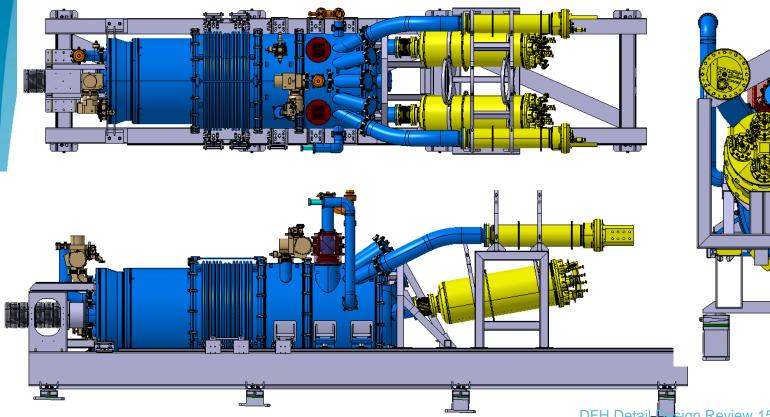


Phase of MgB₂ cable entering DFH selected during assembly=>pre defined routing





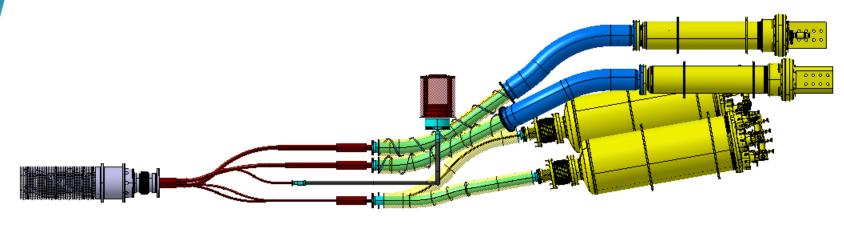


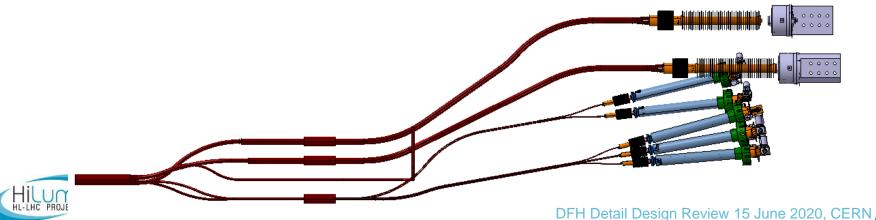


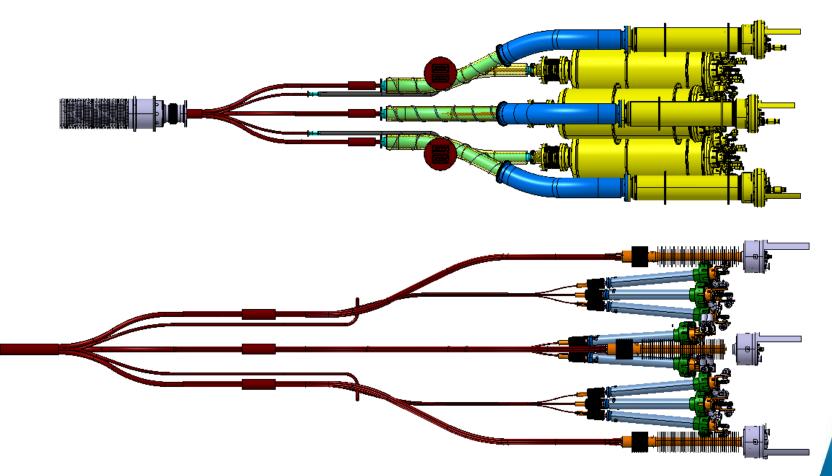
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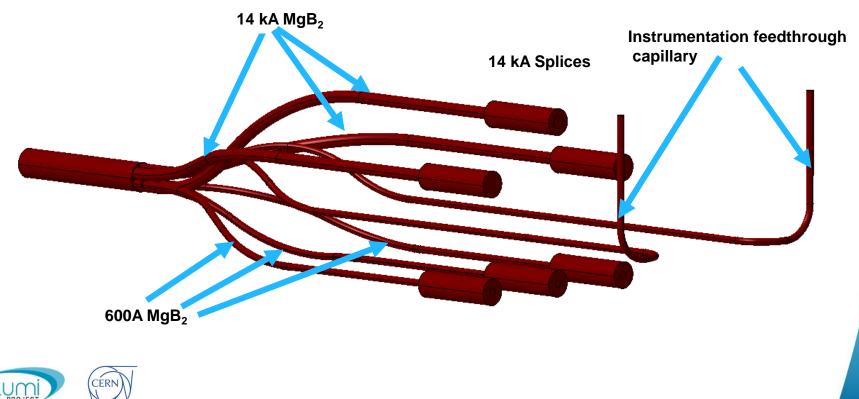
- 2 x14 kA (and 1 spare)
- 8 x 600 A











Cryogenic instrumentation of DFH

- Wiring of cryo Instrumentation of DFH routed via DFH feedthrough
- No routing of cryo instrumentation of DFX and current leads via the DFH
- For the prototype DFH, the temperature of each splice monitored thanks to Cernox sensor embedded in Cu matrix of the splice
 - 19 active Thermal transducers for DFHx
 - 10 active Thermal transducers for DFHm
- Temperature of GHe monitored
 - 1 active Thermal transducers for DFHx
 - 1 active Thermal transducers for DFHm
- Each active temperature sensor has a spare
- 1 He pressure gage, external to He tank for DFHx and DFHm
- Each Cernox (4 xCu AWG 32 (EDMS 320597)) is cabled till the feedthrough on the same connector has the Vtaps of its circuit in similar way as for current leads of LHC
- > 160 wires at DFHx feedthrough for cryo instrumentation

88 wires at DFHm feedthrough for cryo instrumentation

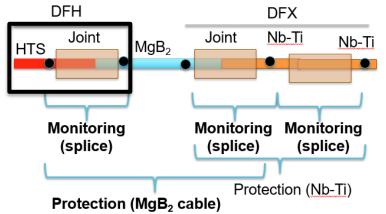
DFH Instrumentation for circuit protection

Each circuit branch will be equipped with voltage taps:

- 1 pair within the DFH cold mass to monitor the MgB₂/HTS splice
- 1 pair routed via the DFH to monitor the MgB₂ cable
- 1 pair to protect the HTS cable (routed at current lead)
- 1 pair to protect the Cu HEX of the leads (routed at current lead)
- One spare for each of the above
- \rightarrow 8 wires per circuit branch to route out from the DFH

¹ Axon HH2619, EDMS 2030599

- 152 Vtaps for DFHx
- 80 Vtaps for DFHm
- Wire for voltage taps:Polyimide insulated Cu wire, AWG 26 (used for magnet instrumentation) ¹
- Design of feedthroughs is considering the different electric potential of the circuits (during operation and insulation tests) EDMS 1821907



A. Ballarino, Requirements for the protection of the Sc-links components, Indico 643197

EDM3 1821		VALIDITY APPROVED					
Rating (kA)	Worst case voltage to ground during operation (V)	comp	ice tests of onents und (V)	Insulation test voltage of system to ground (V)		Leakage current per component (µA)	Test duration (s)
		RT	NOC	RT	NOC		
18	900	4600	2300	460	1080	≤10	30
7	900	4600	2300	460	1080	≤10	30
2	540	3160	1580	316	648	≤10	30
0.2	540	3160	1580	316	648	≤10	30
0.12	40	1160	580	220	360	≤10	30
0.035	900	4600	2300	460	1080	≤10	30



Conclusions

- Routing of MgB₂ and HTS cables respect their minimum bending radius and allow to cope with thermal contraction
- MgB₂/HTs splice are fix points

Cryo instrumentation in DFH:

- 40 Temp probes in DFHx, 22 in DFHm
- All wiring of Temp probes routed at feedthrough of DFH
- 1 pressure transducer per DFH
- Instrumentation for Electrical Protection
 - 8 Vtaps per branch of circuit: 152 Vtaps (DFHx) 80 Vtaps (DFHm)
 - All wiring of above listed Vtaps routed at feedthrough of DFH
 - Design of feedthroughs is considering the different electric potential of the circuits (EDMS 1821207)





Thanks for your attention





Additional slides



HV Levels - Triplets

 EDMS NO.
 REV.
 VALIDITY

 1821907
 2.0
 APPROVED

Rating (kA)	Worst case voltage to ground during operation (V)	Acceptance tests of components to ground (V)		Insulation test voltage of system to ground (V)		Leakage current per component (µA)	Test duration (s)
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RT = Room Temperature $(20 \pm 5 °C)$

NOC = Nominal Operating Conditions. For all WP6s components, it corresponds to GHe at RT and 1.30 ± 0.05 bar



Thermalization of Splices

Splices thermalized by forced GHe convection

- For the high current circuits (18 kA and 13 kA), each splice is in hydraulic series with its HTS cable and Current Lead. So splice mass flow rate is ~1 g/s
- For the low current circuits (2-7 kA) 3-4 splices are regrouped in same He piping and put in hydraulic series with their relative currents leads (semi-series configuration).
- Series and semi series configuration flow assure weighted balanced flow and controlled heat exchange
- ΔT<1 K between GHe and 18 kA splice at nominal flow and current (with safety margin on splice resistance)
- The helium gas temperature has limited influence on the ΔT between gas and splice surface
- T_{GHE} has direct influence on Tsplice
- Pressure drop in the splice piping < 5 mB at nominal (flow, Temp and pressure)

 Series and semi series configuration flow assure sufficient cooling of splices

Precoverv 300K 1.0 g/s 0.9 g/s 3x0.11 g/s P_{DFH}, T_Ghe *ṁ*_{Sc link} GHe by pass 4x0.11 g/s 18 kA Splice temperature vs T GHe and splice 30.0 resista $T_{splice} = 16 - 15.5 K$ for: • $\dot{m} = 0.7 - 1.1 \, g/s$ ₹5.0 R_{18kA}=4.2 nΩ T_{GHF}=15K atinre 0.0 tiemper .0 . 0.011Ce — - Reg=4.2nΩ Lsplice=220 mm, TgHe=10K - - - - Reg=8.3nΩ Dea=20mm TgHe=15K Reg=16.7nΩ 5.0 mass flow around one splice $\frac{1}{2}$ DFH Detail Design Review 15 June 2020, CERN