



# Appendix C: A digression on costs and two case studies

Ezio Todesco

European Organization for Nuclear Research (CERN)

Lectures based on University of Milano Bicocca courses in 2016-2018  
Thanks to L. Bottura and G. de Rijk for proposing and supporting this initiative

*All the units will use International System (meter, kilo, second, ampere) unless specified*



# CONTENTS

- Previous digressions in these lectures
  - Appendix A: A digression on beam optics, from stable motion to chaos
  - Appendix B: A digression on Maxwell equations and scales in atomic physics
- Coming today and next week
  - Appendix C: A digression on costs, and two case studies
  - Appendix D: A digression on manufacturing techniques of magnet components

- Cost as enabling factor for technologies: two oversimplified cases
  - Power line
  - Large aperture solenoid (MRI-like)
- Two case studies
  - A conceptual design: a 640 T dipole as shown in Terminator III
  - A sensitivity analysis: how to squeeze some more field from LHC dipoles (Fresca dipole)

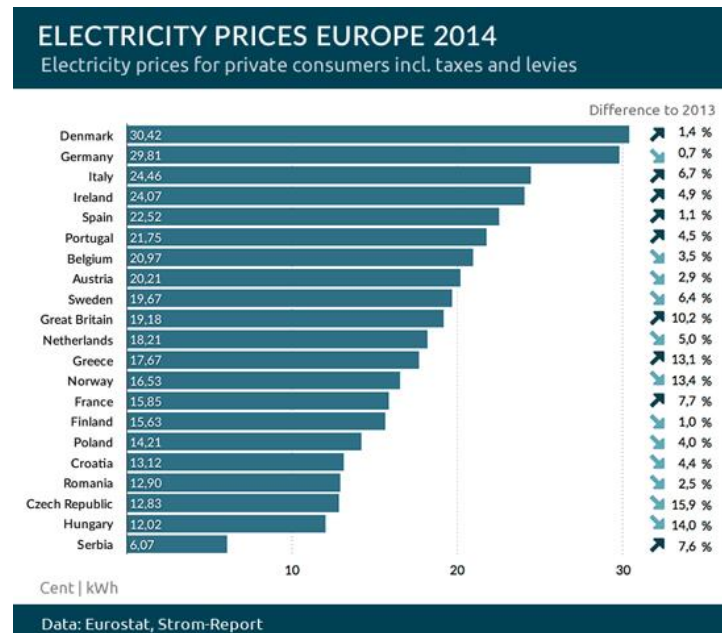
- If superconductivity exists and works, why do we still have resistive power lines ?



- Here we will address some issues related to costs using oversimplified models
  - Even though the simplifications we use are huge, one can learn something on cost as an enabling factor of a technology

# ENERGY PRICE

- Electricity is the most versatile form of energy in our society, easy to transport (but not to store)
- Prices of electricity for private use range between **0.1-0.3 \$/kWh**
  - 1 kWh = 1000 J/s × 3600 s = 3.6 MJ
  - One LHC dipole has 2 kWh stored energy



[from <http://strom-report.de/strompreise/#strompreise-europa>]

- A human being has a power of  $\sim 150$  W
  - At the gym, we can lift 15 kg in 1 s for 1 m:  $15 \times 9.8 \times 1/1 = 150$  W
  - Infact, in one day you have about 86 000 s, this means you produce/consume 12 MJ, that is 3 kcal (6 BigMac – 1.5 LHC dipole)



- Considering that a human being can make 150 W, in our society electricity price corresponds to paying  $\sim 3$  cents per hour a person ... that's cheap

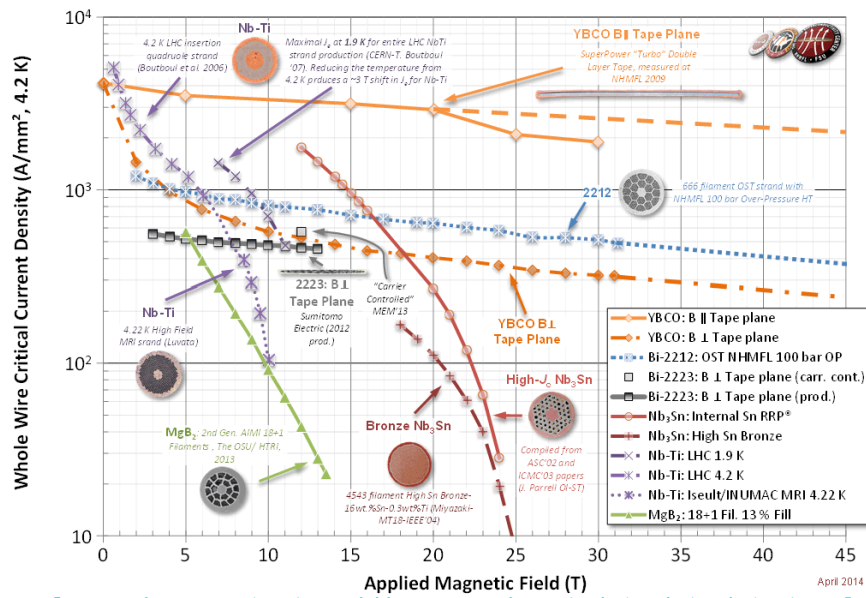
# ALUMINIUM VERSUS COPPER

- The two main conductors are **Al and Cu**
- Different features:
  - Density: 2700 kg/m<sup>3</sup> for Al, 8900 kg/m<sup>3</sup> for Cu
  - Cost: 1.5 \$/kg for Al, 4.5 \$/kg for Cu  
(source [www.metalprices.com](http://www.metalprices.com) )
  - Resistivity at 300 K:  $2.7 \times 10^{-8} \Omega \text{ m}$  for Al,  $1.7 \times 10^{-8} \Omega \text{ m}$  for Cu  
(many sources, see Y. Iwasa, “Case studies in superconducting magnets”, Springer, or J. Ekin, “Experimental techniques for low temperature measurements”, Oxford Univ. press)
  - What counts for electricity is the volume: the **difference in volumetric price is a factor ten in favor of Al**
  - That’s why **Al is used when large quantities** are needed (power lines)
  - The lower mechanical strength is compensated by adding some stainless steel
- Limits to current density
  - 1 A/mm<sup>2</sup> without active cooling
  - 5 A/mm<sup>2</sup> with cooling



# COST OF SUPERCONDUCTORS

- There are orders of magnitudes in the price of conductors and superconductors
- Price is a primary factor to enable a technological switch
  - Nb-Ti for accelerator magnets is 200 \$/kg
  - Nb<sub>3</sub>Sn lower cost is 800 \$/kg (low current density for ITER)
  - HTS are more than one order of magnitude w.r.t. Nb<sub>3</sub>Sn



[P. Lee famous plot, <http://fs.magnet.fsu.edu/~lee/plot/plot.htm> ]



# COST IN \$/kA m

- Price of superconductors is **also given in \$/kA m**
  - At the end, this is what is interesting to make power lines or magnets (Ampere turns)
  - One has to associated a current density  $j$
- Example of Nb-Ti,  $j = 500 \text{ A/mm}^2$ 

$$P_{kAm} = P_{kg} \frac{\rho}{j \left[ \text{A} / \text{mm}^2 \right]} 10^{-3}$$
  - To carry 1 kA one needs  $2 \text{ mm}^2$
  - One meter of this wire has a volume of  $2 \times 10^{-6} \text{ m}^3$
  - For Nb-Ti it has a weight of 12 g, and a cost of 2.4 \$/kA m
- Example of Al, 1 kA can be carried out by  $1000 \text{ mm}^2$ 
  - One meter of this wire has a volume of  $10^{-3} \text{ m}^3$
  - For Al it has a weight of 2.7 kg, and a cost of 4.0 \$/kA m
- For Nb-Ti, the 500 times larger ability of carrying current density is more than compensating the 200 times larger price

# EXAMPLE: A POWER LINE

- What **counts is the price per kA m**, and Nb-Ti is cheaper than Al
  - Notwithstanding the much larger price (200 \$/kg versus 1.5 \$/kg), the current density is more than 100 times larger and therefore in terms of material is competitive
  - Much higher prices for other materials must be compensated by a corresponding increase in the current density, and today this is not the case for Nb<sub>3</sub>Sn or HTS
- For a power line there are two additional factors
  - **Losses on large distances can be reduced to very small fraction** of total energy by using a higher voltage
    - Infact, losses are dominated by the last kilometer distribution, that are at lower voltage
  - Superconductivity would require diffused cryogenic installations whose cost is non negligible

# EXAMPLE: A POWER LINE

- Let us consider a **power line of 100 km carrying 100 MW**
  - We will show that losses can be made negligible
- Overhead power lines rated according to the voltage
  - Low voltage below 1 kV
  - Medium voltage 1 – 70 kV urban and rural areas
  - High voltage 70-230 kV
  - Ultra-high voltage over 230 kV up to 800 kV
- High voltage means low current, and low losses
  - Note that we make a DC example, even though power lines are AC
  - With 500 kV, one needs to carry 200 A :  $500 \times 1000 \times 200 = 100 \text{ MW}$
  - Assume a conductor with  $0.1 \text{ A/mm}^2$  (to minimize losses)
  - $2000 \text{ mm}^2$  needed, corresponding to  $200 \text{ m}^3$  of conductor
  - Resistivity is  $2.7 \times 10^{-8} / 2 \times 10^{-3} \times 10^5 = 1.35 \Omega$
  - Losses are  $R I^2 = 1.35 \times 200^2 = 54 \text{ kW}$  **less than 1 per mil of the 100 MW**

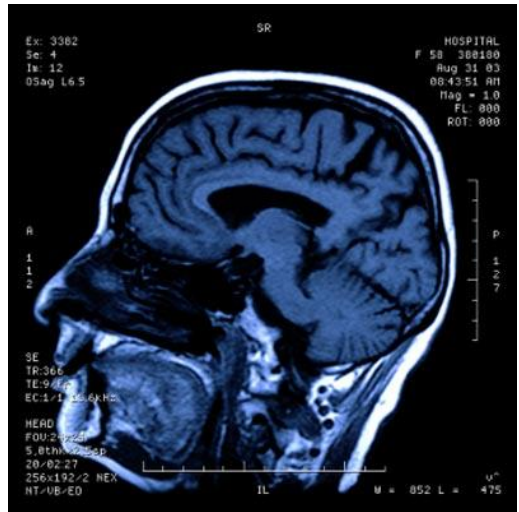


## EXAMPLE: A POWER LINE

- Losses are **dominated by the last km of the power line**, where the high voltages cannot be used
- Even though resistive losses cannot be a cost driving factor, there are several other aspects that can push for some specific applications of superconductivity to power lines
  - In particular large current densities of superconductivity allow much more **compact devices** – this can be an enabling factor for cases in which space has a large cost: for instance underground power line in dense metropolis
  - See for a review on possible advantages [H. Thomas, et al. “Superconducting transmission lines” \*Renewable and Sustainable Energy Reviews\* 55 \(2016\) 59-72](#)
- The compactness of superconductivity makes it an interesting option for all applications where weight/space has a large cost: for instance the motor windings in wind turbines, see [A. B. Abrahmsen, et al. “Large superconducting wind turbine generators” \*Energy Procedia\* 24 \(2012\) 60-67](#)

- Cost as enabling factor for technologies: two oversimplified cases
  - Power line
  - Large aperture solenoid (MRI-like)
- Two case studies
  - A conceptual design: a 640 T dipole as shown in Terminator III
  - A sensitivity analysis: how to squeeze some more field from LHC dipoles (Fresca dipole)

- Let us consider a MRI (Magnetic Resonance Imaging) magnet with 1 m diameter, 2 m long, 4 T operational field



- We assume is a vertical dipole (not a solenoid) to use our formulas for accelerator magnets

$$B = 6.9 \cdot 10^{-4} w(mm) j(A/mm^2)$$

- Therefore for 4 T, with 5 A/mm<sup>2</sup> we need a coil width of  $w=1200$  mm
- Let us consider an aperture  $r=500$  mm



# EXAMPLE: A MRI MAGNET

- $B=4 \text{ T}$        $j= 5 \text{ A/mm}^2$        $r= 500 \text{ mm}$        $w=1200 \text{ mm}$

- Conductor volume  $V=11 \text{ m}^3$        $V = L \frac{2}{3} \rho (w^2 + 2rw)$

- Let us assume a cable surface  $A$  with  $N$  turns

- Total length of conductor is

$$l_c = 4LN$$

- Resistance is

$$R = \frac{r}{A} l_c$$

$$V = A l_c$$

- Dissipated power is

$$P = RI^2 = \frac{r}{A} l_c j^2 A^2 = r l_c j^2 A = r j^2 V$$

- Let us take copper to minimize losses:  $P=1.7 \times 10^{-8} \times (5 \times 10^6)^2 \times 11 = 4.6 \text{ MW}$



## EXAMPLE: A MRI MAGNET

- Summary of the resistive magnet: operational current of  $5 \text{ A/mm}^2$ 
  - Large coil thickness of 1200 mm
  - Volume of coil is  $11 \text{ m}^3$ , this gives 100 tons of Cu and **450 k\$ of material**
- Dissipated power is 4.6 MW, assuming a 50% availability during the year (5000 hours) this makes 23 GWh, for a cost **of 4.5 M\$/y**
- Let us make a further attempt to optimize:
  - We divide by 3 the current density, and by 10 the dissipated power
  - Current density is  $1.6 \text{ A/mm}^2$ , coil thickness goes to 3800 mm, total size of the magnet is 8 m – pretty large
  - **Operational cost is 0.45 M\$/y**
  - But copper volume is  $75 \text{ m}^3$ , **3 M\$ cost for the conductor only** ... not to speak about the large infrastructure



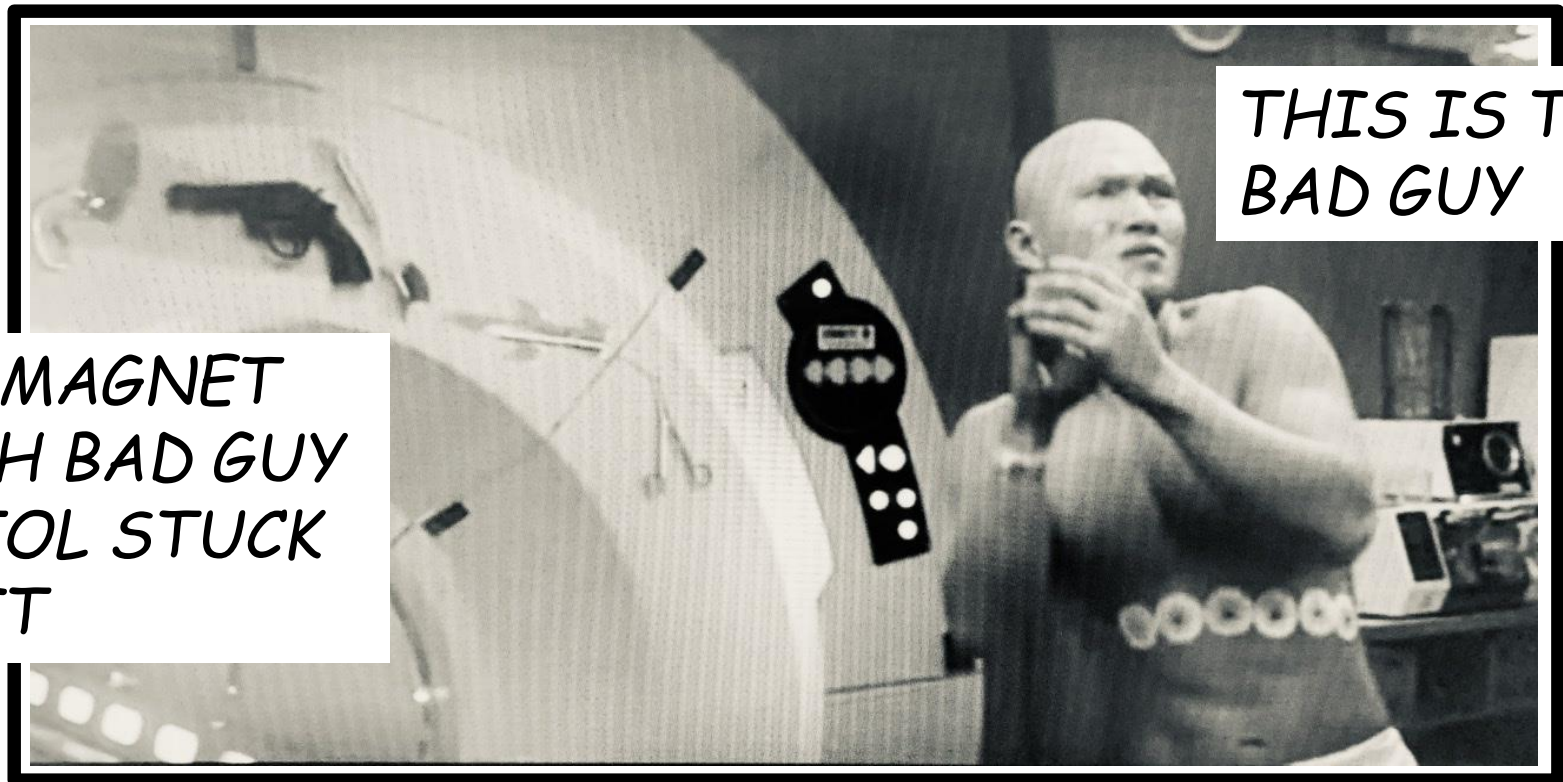


## EXAMPLE: A MRI MAGNET

- Let us explore the superconductive option with Nb-Ti
- We can have  $400 \text{ A/mm}^2$ , i.e. produce the 4 T field **with only 15 mm coil width**
  - The total volume is  $0.065 \text{ m}^3$ , for a superconductor mass of 500 kg
- In case of Nb-Ti this **is 100 k\$ of material**
  - Cheaper than copper, even in the  $5 \text{ A/mm}^2$  option
  - But operational cost only related to cryogenics (local in this case, ie close to the magnet – one does not need to cool a 100 km line), instead of 4 M\$/year
  - ...
- Once more, cost is critical !
  
- An essential feature of superconductivity is the ability to use very high current density without paying the associated losses

# TALKING ABOUT MRI ...

- James Bond switching on and off an MRI magnet during a fight
  - Die another day(L. Tamahori, Eon productions, 2002)
  - Well, MRI do not switch on and off in a fraction of second ...



THIS IS THE  
BAD GUY

MRI MAGNET  
WITH BAD GUY  
PISTOL STUCK  
ON IT

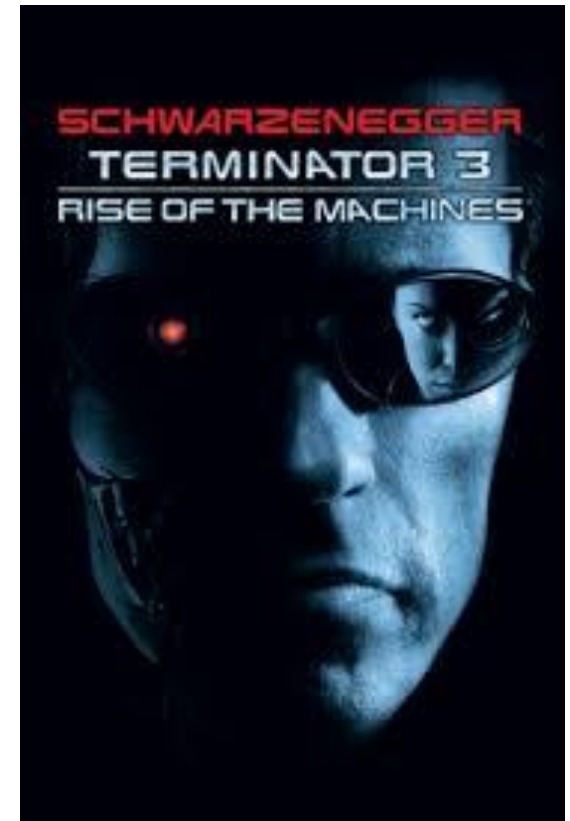


# SOMETHING MORE FROM HOLLYWOOD

- The man with golden gun (G. Hamilton, Eon productions, 1974)
  - James Bond explaining to the M. Scaramanga how solar energy can be stored in superconducting magnets operating in liquid helium
  - Well, magnetic field is not the best place to store energy ...
- Live and let die (G. Hamilton, Eon productions, 1973)
  - James Bond using a magnetic watch to open a closet and to unzip the clothes of a spy
  - Well, I let you make the computations...
- X-Men 2 (B. Singer, 20<sup>th</sup> Century Fox, Marvel ent. et al, 2003)
  - Magneto escaping from his plastic prison using the iron in the blood of the guard
  - I'm not able to comment this ...
- At the end, the accelerator shown in Terminator is not one of the most impossible devices ...

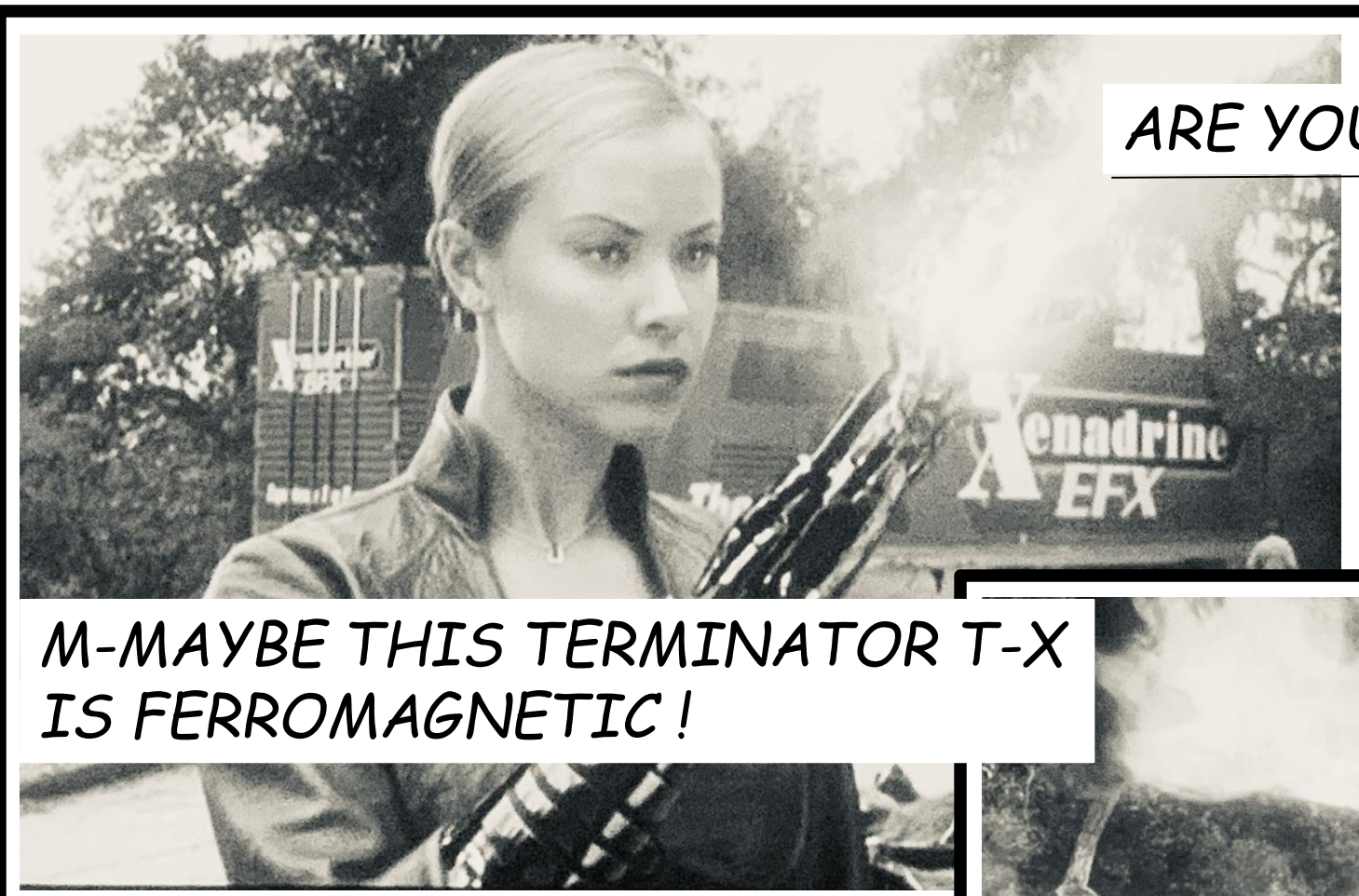
# A FEW WORDS ON THE MOVIE

- Terminator: the rise of the machines (J. Mostow, Intermedia and C2 pictures, 2003)
  - Third episode of the Terminator saga
- Three main elements
  - Human beings losing control over machines
    - Golem (Jewish tradition, around 1500)
    - Frankenstein (M. Shelley, 1818)
    - Matrix (L. Wachowski and L. Wachowski, 1999)
  - Enhanced human beings, or human-like machines
    - ... in the cyberpunk tradition
      - Blade Runner (R. Scott, 1982)
      - Robocop (P. Verhoeven, 1987)
  - Travelling in time
    - The time machine (H. G. Wells, 1895)
    - La jetée (C. Marker, 1962)
    - Back to the future (R. Zemeckis, 1985)
    - 12 monkeys (T. Gilliam, 1995)





# TERMINATOR III DIGEST



ARE YOU KIDDING ?!

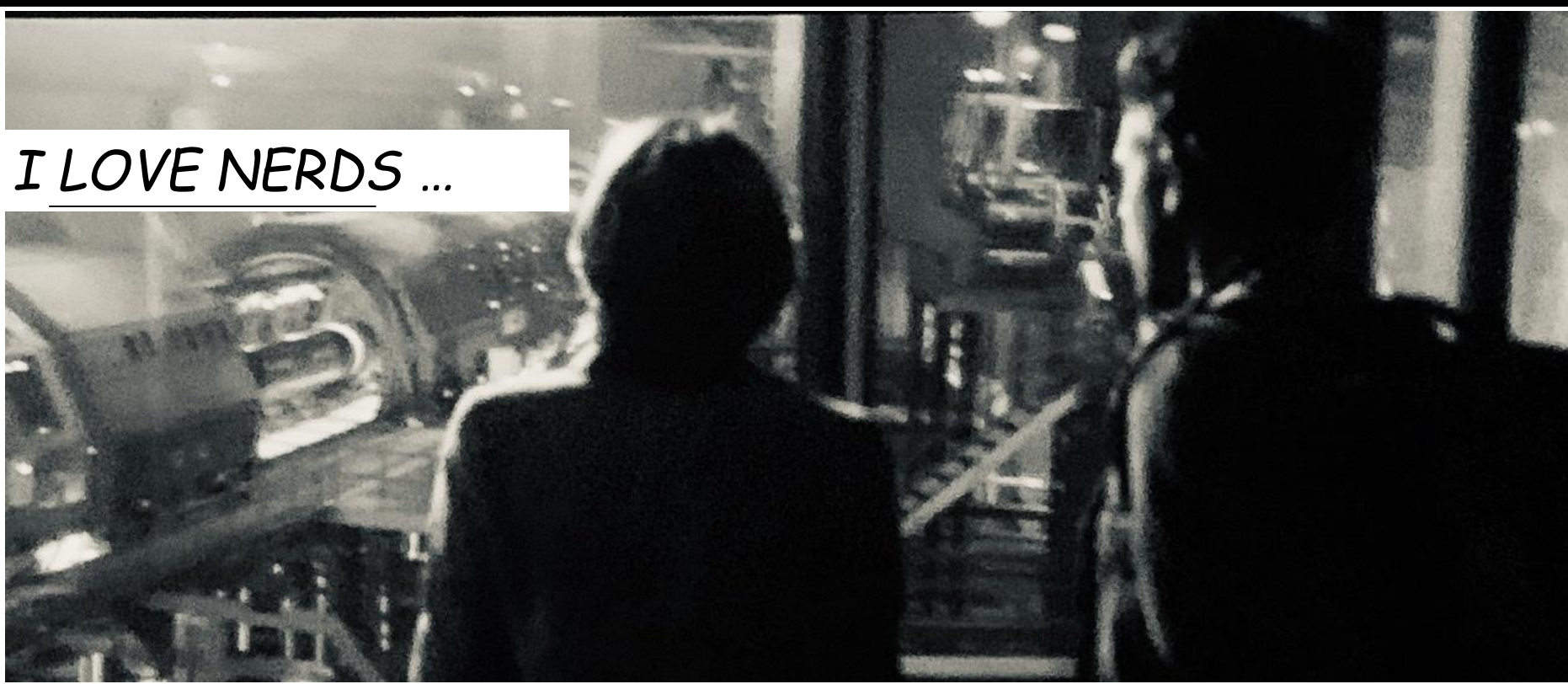
M-MAYBE THIS TERMINATOR T-X  
IS FERROMAGNETIC !



# TERMINATOR III DIGEST

*A 5.76 TeV ACCELERATOR!! WITH THIS SIZE  
THE MAGNETS SHOULD MAKE 600 T!*

*I LOVE NERDS ...*





LET'S RAMP THE MAGNETS:  
THE TERMINATOR WILL STICK  
ON THEM AS A SOUVENIR  
ON THE FRIDGE!

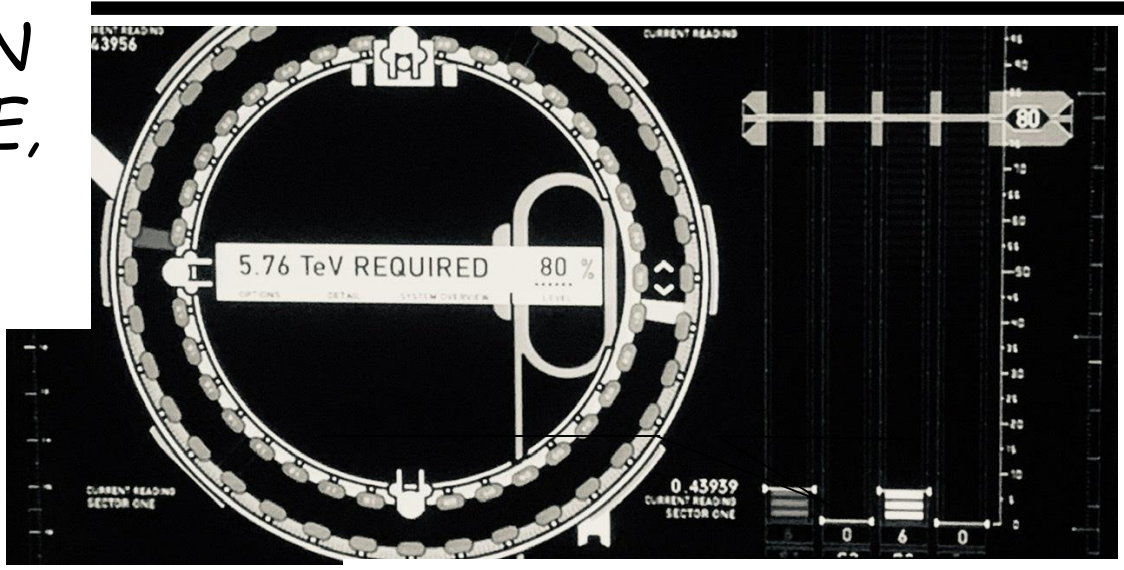
THIS WOULD NEVER  
WORK IN THE LHC ...





# TERMINATOR III DIGEST

*BABY, NOT MORE THAN 80% OF SHORT SAMPLE, I WOULD PREFER NO QUENCHES ...*



**BEGINNING OF RAMP !**





# TERMINATOR III DIGEST



# TERMINATOR III DIGEST





.... IT WORKS !!!

DIE YOU \*\*\*\*\* ...





# MAGNETIC FIELD AND CURRENT DENSITY ESTIMATE

- Curvature radius of the order of 30 m (circumference of 200 m)
- Energy is 5760 GeV  
(see Unit 1)
  - Field required is  $5760/9=640$  T
- Magnet length is much shorter than in LHC (2 m)
- Magnet cryostat has the same size of LHC (1 m)
  - Not clear if this is a collider (double aperture) or a single aperture
    - We assume it is a single aperture with 50 mm aperture (25 mm radius)
  - Magnet size cannot be larger than 800 mm (diameter)
  - Coil width cannot be larger than 250 mm, so let us assume a  $w=0.25$  m (a very large coil width)
  - This leaves 125 mm for the mechanical structure

$$E[GeV] = 0.3 \times B[T] \times \rho[m]$$



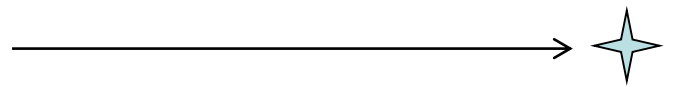
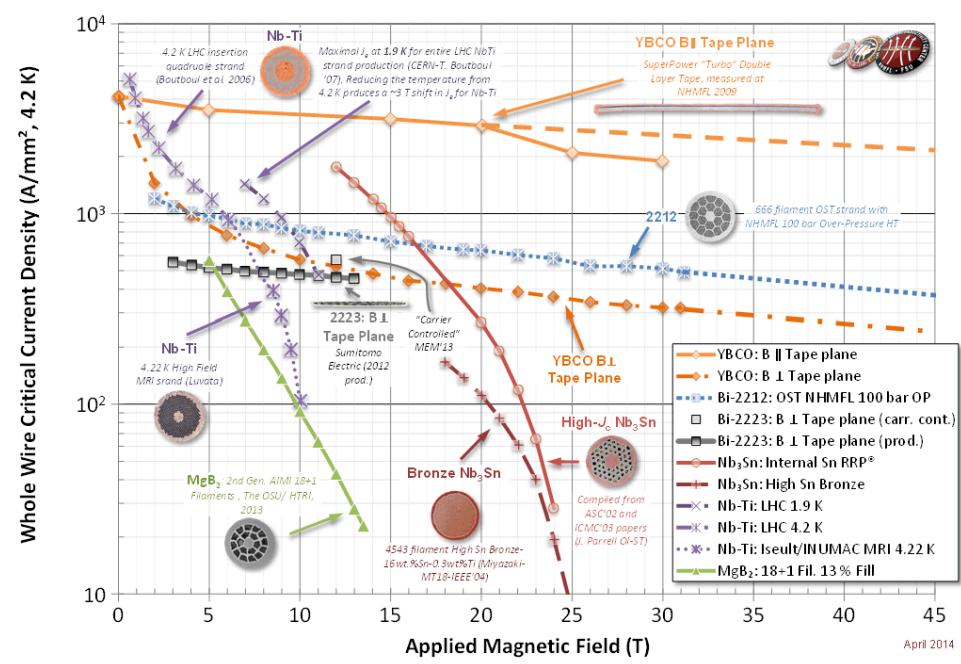
# MAGNETIC FIELD AND CURRENT DENSITY ESTIMATE

- 640 T given by 250 mm coil width  $B_1 = 6.9 \times 10^{-4} w [\text{mm}] j [\text{A/mm}^2]$   
(see Unit 4)
  - In the LHC we have 30 mm coil width and 400 A/mm<sup>2</sup>, giving 8 T
  - We need to increase 80 times the field, we increase 8 times the coil length, so the current density must increase by a factor 10
  - Overall current density is 4000 A/mm<sup>2</sup>
  - We are a factor ten above typical values in accelerator magnets
- Iron cannot help much ...
  - With  $r=25$  mm,  $w=200$  mm if we place the iron directly in contact with the coil we have  $R_I=225$  mm and the field enhancement due to iron is
  - $(25 \times 225) / 225^2 = 11\%$
  - (See Unit 9)
  - At these field it is totally saturated ... let us neglect its contribution



# MAGNETIC FIELD AND CURRENT DENSITY ESTIMATE

- Field of 640 T, coil width of 250 mm
  - Current density of 4000 A/mm<sup>2</sup>
  - At 80% of short sample, therefore conductor should have 5000 A/mm<sup>2</sup> overall current density at 800 T
  - 15000 A/mm<sup>2</sup> superconductor current density at 800 T, assuming 1/3 of sc (see Unit 5)



This way



640 T

- Accumulation of stress in the midplane

(see Unit 10)

$$S_q(\text{MPa}) = \frac{j(A/\text{mm}^2)B(T)r(\text{mm})}{2000}$$

- On the border of the aperture:  $\sigma_\theta = 4000 \times 25 \times 640 / 2 = 32 \text{ GPa}$
- Using the Fessia-Regis corrective factor,

$$S_{q\text{max}} = \frac{jBr}{2} \max_{0 < x < w} \frac{2(r+x)^3 + r^3 - 3(r+x)^2(r+w)}{3wr(r+x)}$$

- We get to 4.5 times larger value, i.e. 150 GPa

- Stress in the radial direction

- It is about 1.5 times the magnetic pressure
- $\sigma_r = 1.5 \times 640^2 / 2 / (4\pi 10^7) = 240 \text{ GPa}$

- Therefore the superconductor should be able to withstand order of 250 GPa, without degradation

- ... and the structure as well



# COIL ENERGY DENSITY AND PROTECTION

- Estimate of stored energy
  - 640 T over an aperture of 25 (aperture)+125 (half coil width) mm
  - 23 GJ, or 12 GJ/m (it is 0.5 MJ/m in the LHC dipoles)
  - Coil area of  $0.31 \text{ m}^3$
  - Energy density of  $70 \text{ GJ/m}^3 = 70 \text{ J/mm}^3$   
(see Unit 12 and 13)
  - Protection limit given by coil enthalpy is  $0.5 \text{ J/m}^3$  so this is impossible unless extracting 99.5% of the energy



- So let us consider the energy extraction

- Short magnet of 2 m length – stored energy of 23 GJ
  - (this is 23 times the energy of all the 1232 LHC dipoles !)
- Assume a very large cable, 30 mm width, 3 mm thickness
  - This has 90 mm<sup>2</sup>, with 4000 A/mm<sup>2</sup> current density, so the magnet current is 360 kA, and inductance is  $2 \times 23\,000 / 360^2 = 0.35$  H

$$\Gamma(T_{\max}) \equiv A^2 v \int_{T_0}^{T_{\max}} \frac{c_p(T)}{\rho_{Cu}(T)} dT$$

- What is the  $\Gamma(T_{\max})$  of a cable with 90 mm<sup>2</sup> surface?

- Let us scale the plot, multiplying  $10^{17}$  for the  $(90 \times 10^{-6} \text{ m}^2)^2$  and taking half of Cu
- This gives  $\Gamma(T_{\max}) = 400 \text{ MA}^2 \text{ s}$
- Condition for protection is

$$G(300K) > G_q = \frac{U}{R_d} = \frac{UI_0}{V_{\max}}$$

- Therefore the resistance should be  $R_d > U/\Gamma(300K) = 23 \times 10^9 / 400 \times 10^6 = 60 \text{ } \Omega$
  - So to have energy extraction the magnet should withstand
- $$V_{\max} = R_d I_0 = 60 \times 360 \text{ kV} = 22 \text{ MV}$$



# COIL ENERGY DENSITY AND PROTECTION

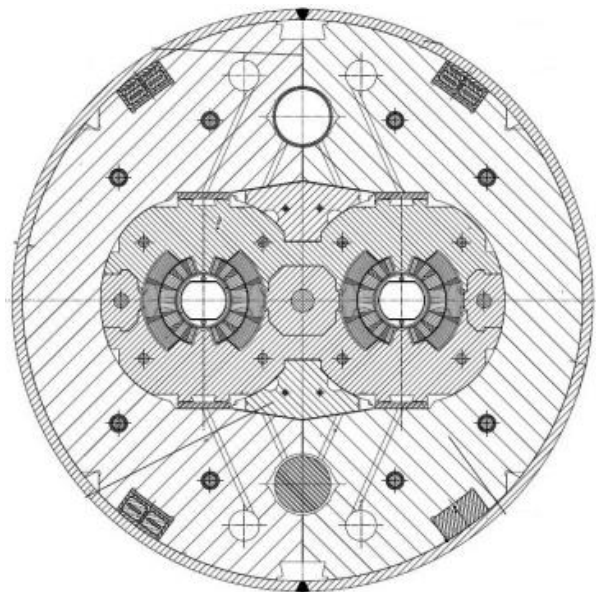
- An alternative path for protection
  - How about developing an electromagnetic coupling with the structure so that the whole magnet takes the heat ?
  - The magnet volume is  $2 \times 0.4^2 \times \pi = 1 \text{ m}^3$
  - Therefore the energy density is  $23 \text{ GJ/m}^3 = 23 \text{ J/mm}^3$
  - Still too large ... no way



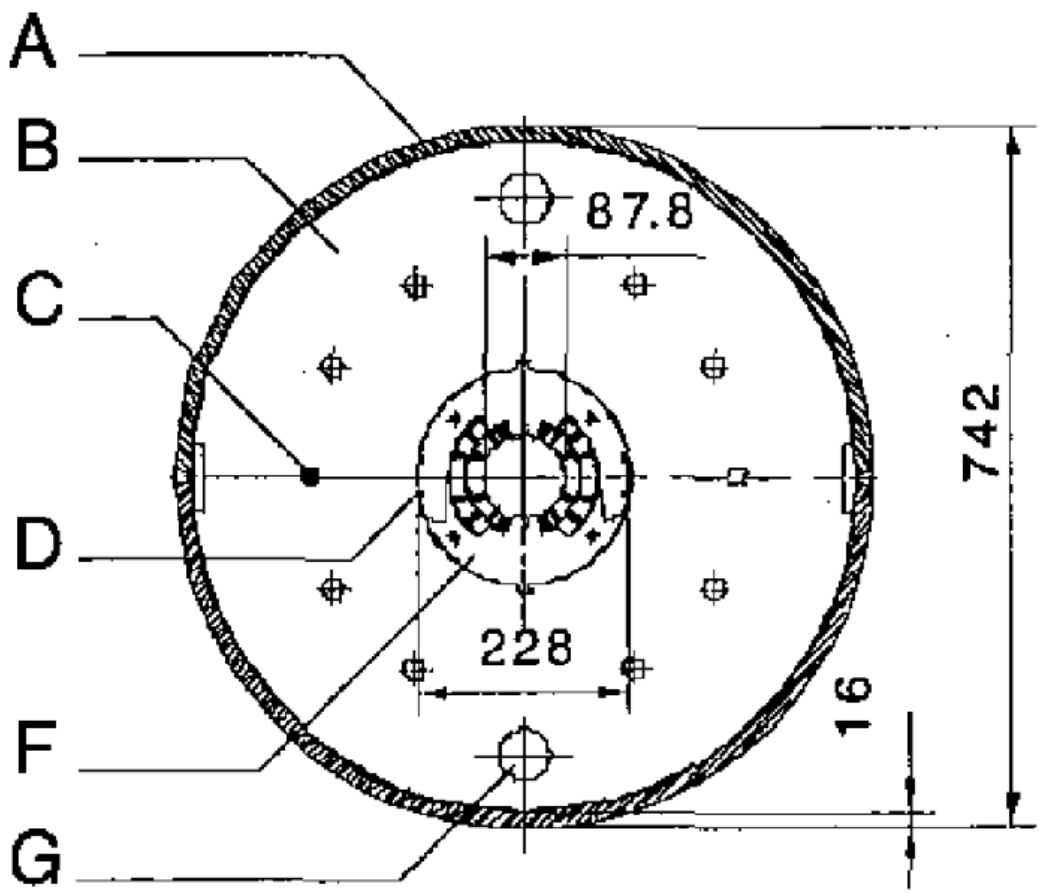
- Summary of the requirements
- Conductor
  - Current density in the superconductor:  $>15000 \text{ A/mm}^2$  at 800 T
  - Filament size:  $5 \mu\text{m}$  (scale with inverse of current density)
  - Cable with  $<5\%$  degradation at 250 Gpa
- Structure
  - Structure able to withstand 250 GPa, with a thickness of 125 mm
- Protection
  - Development of insulation able to withstand 50 MV, occupying not more than 20% of the coil volume

- Cost as enabling factor for technologies: two oversimplified cases
  - Power line
  - Large aperture solenoid (MRI-like)
- Two case studies
  - A conceptual design: a 400 T dipole as shown in Terminator III
  - A sensitivity analysis: how to squeeze some more field from LHC dipoles (Fresca dipole)

# LHC DIPOLE VERSUS FRESCA DIPOLE



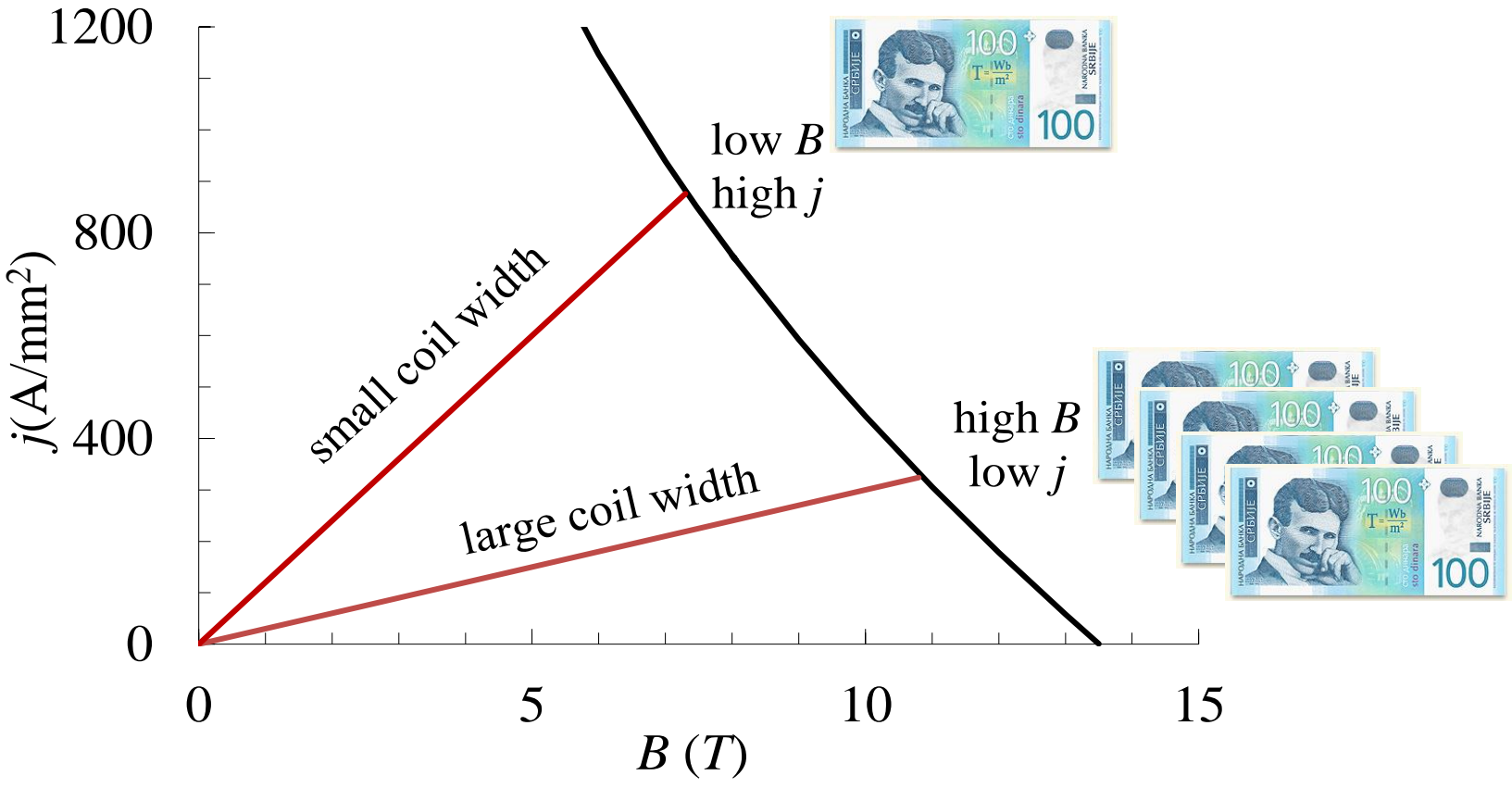
LHC main dipole  
 (R. Perin, D. Leroy, S. Russenschuck  
 D. Perini, P. Fessia, et many al.)



- |                       |            |                        |
|-----------------------|------------|------------------------|
| A) Shrinking Cylinder | B) Yoke    | C) Alignment Key       |
| D) Collar Key         | F) Collars | G) Heat Exchanger Hole |

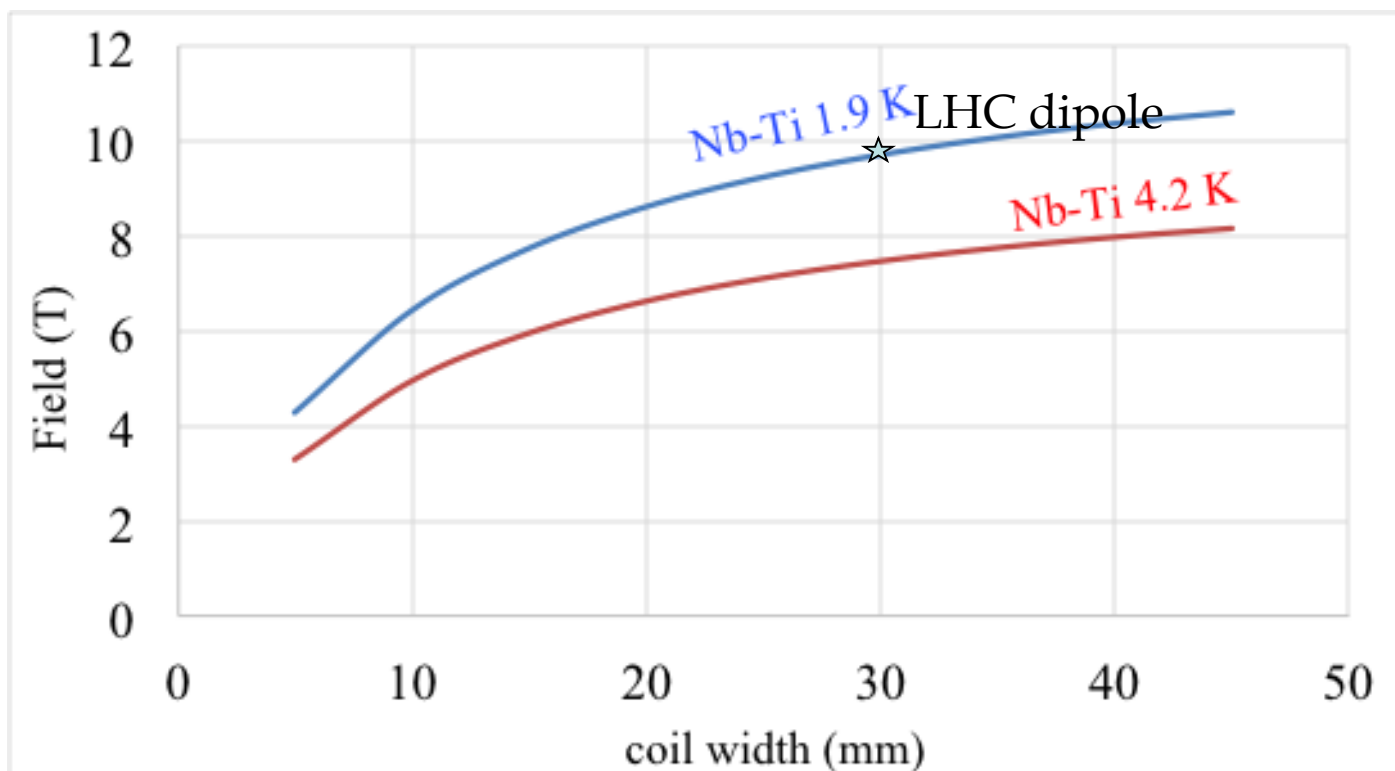
Fresca dipole (G. Spigo, D. Leroy, A. Verweij)

- As quoted in Unit 8, the short sample field versus the coil width has an implacable law, that make the last teslas very expensive



# HOW TO SQUEEZE MORE FIELD FROM THE LHC DIPOLES

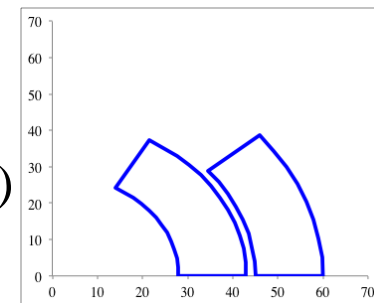
- LHC dipole, with its 30 mm coil width and 9.7 T short sample field, is considered to be the ultimate field reachable with Nb-Ti
  - However, the world record for accelerator like dipoles belong to Fresca – that managed to squeeze few more tenths of tesla out of Nb-Ti



# HOW TO SQUEEZE MORE FIELD FROM THE LHC DIPOLES

- Here we will discuss the use of the sensitivity equation applied to the LHC dipoles, in the direction pursued by Fresca dipole
- We start with the LHC dipole

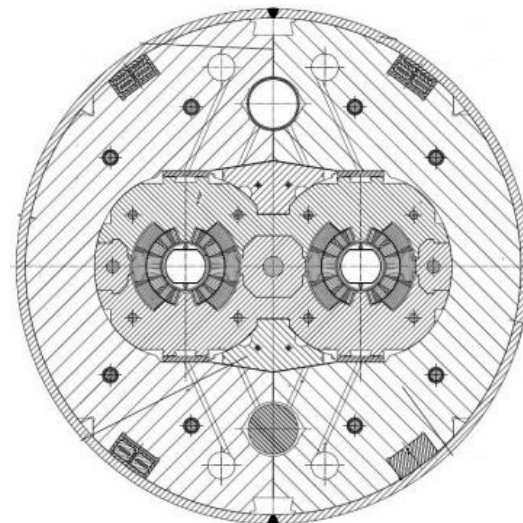
- Aperture 28 mm
- Coil width: two layers of 15.4 mm width insulated cable
- Insulated cable surface: 33.24 mm<sup>2</sup> (inner) 26.78 mm<sup>2</sup> (outer)
- Turns: 15 (inner layer), 25 (outer layer)



- Equivalent coil width (ignoring grading)

- Equation given in Unit 8, slide 18
- $A=4 \times 15 \times 33.24 + 4 \times 25 \times 26.78$
- $w_{eq} = 26.9 \text{ mm}$

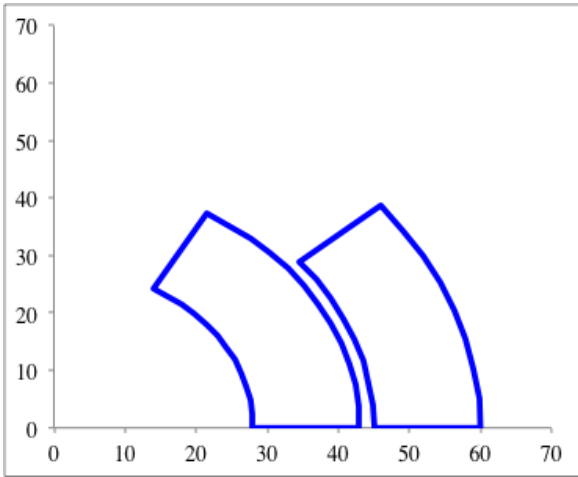
$$w_{eq} = r_{CC} \sqrt{1 + \frac{3A}{2\rho r^2}} - 1 \frac{\ddot{\theta}}{\dot{\theta}}$$





- Here we will discuss the use of the sensitivity equation applied to the LHC dipoles, in the direction pursued by Fresca dipole
- We start with the LHC dipole
  - Aperture 28 mm
  - Coil width: two layers of 15.4 mm width insulated cable
  - Insulated cable surface: 33.24 mm<sup>2</sup> (inner) 26.78 mm<sup>2</sup> (outer)
  - Turns: 15 (inner layer), 25 (outer layer)
  - Grading: 33.24/26.78=1.24 (25% larger current density in the outer layer)
- Equivalent coil width (including grading)
  - Equation given in **Unit 8, slide 18**
  - $A=4 \times 15 \times 33.24 + 4 \times 25 \times 26.78 \times 1.24$
  - $w_{eq}=29.6$  mm

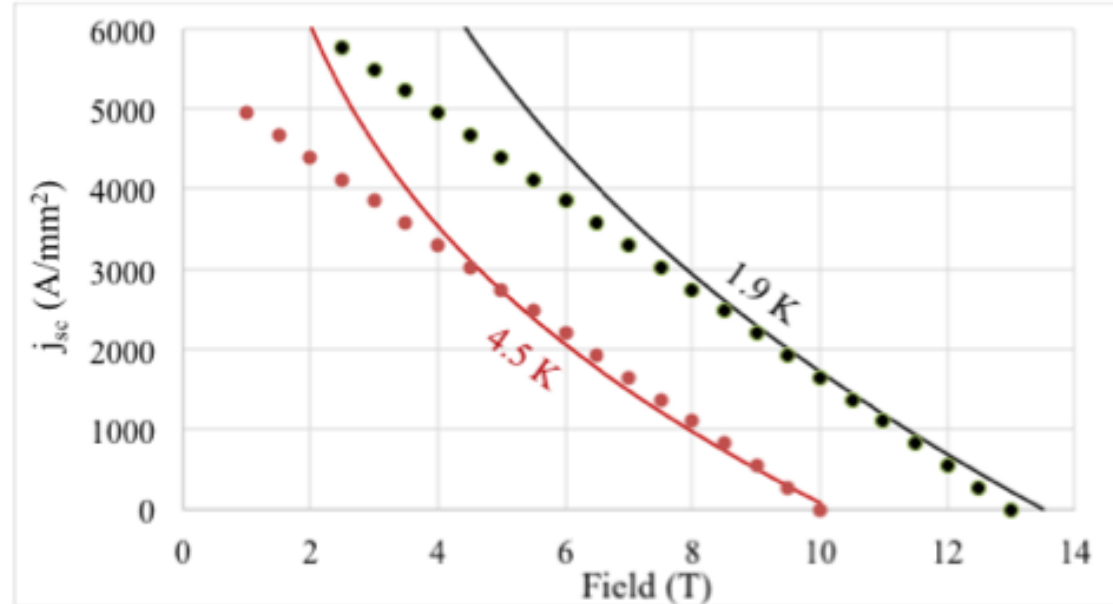
$$w_{eq} = r_c \sqrt{1 + \frac{3A}{2\rho r^2}} - \frac{\rho}{\delta}$$



# HOW TO SQUEEZE MORE FIELD FROM THE LHC DIPOLES

- Critical surface parameters (Unit 8, slide 6)
  - Slope of the critical surface at 1.9 K:  $s=550 \times 10^6 \text{ A/m}^2/\text{T} = 550 \text{ A/mm}^2/\text{T}$
  - Linear approximation of critical field at 1.9 K:  $b(1.9 \text{ K})=13 \text{ T}$

$$j_{sc,c}(B) = s(b(T) - B),$$





# HOW TO SQUEEZE MORE FIELD FROM THE LHC DIPOLES

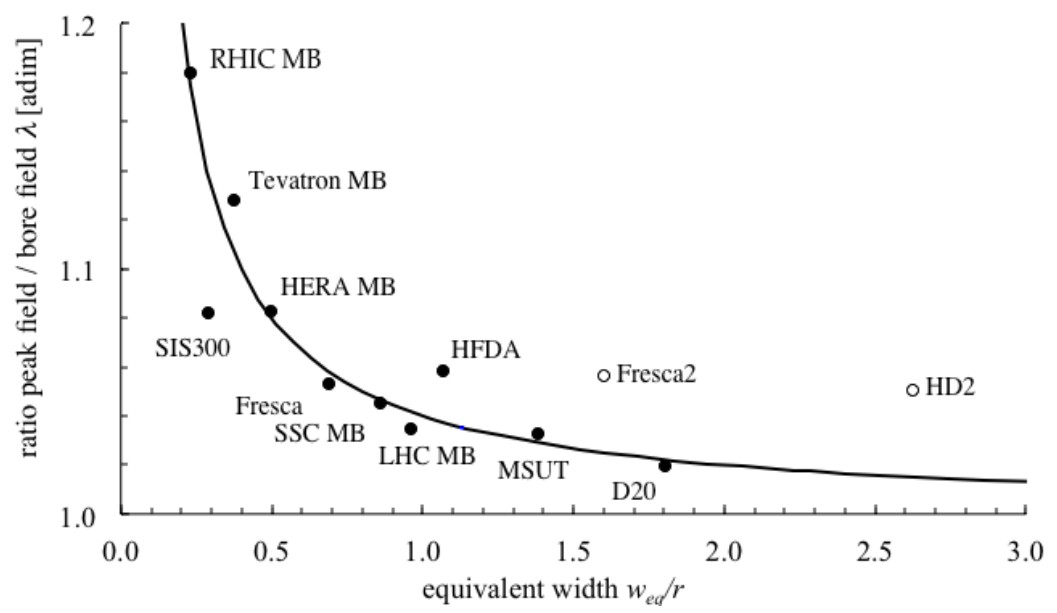
- Fraction of superconductor in the insulated cable (Unit 8, slide 8)
  - $v$ : ratio between area of superconductor and area of insulated cable
  - Inner cable: 28 strands, 1.065 mm diameter, 1.65 Cu/No\_Cu – this gives  $A_{sc}=28 \times 1.065^2 \times 4 / \pi / (1 + 1.65) = 9.41 \text{ mm}^2$
  - Inner cable insulated surface  $33.24 \text{ mm}^2$
  - Fraction of superconductor:  $9.41 / 33.24 = 0.24$
  
  - Outer cable cable: 36 strands, 0.825 mm diameter, 1.95 Cu/No\_Cu – this gives  $A_{sc}=36 \times 0.825^2 \times 4 / \pi / (1 + 1.95) = 6.52 \text{ mm}^2$
  - Outer cable insulated surface  $26.78 \text{ mm}^2$
  - Fraction of superconductor:  $6.52 / 26.78 = 0.28$



# HOW TO SQUEEZE MORE FIELD FROM THE LHC DIPOLES

- Guess of ratio between peak field and bore field (Unit 8, slide 8)
  - $\lambda = 1 + 0.04 \times 28/29 = 1.039$
  - Therefore, peak field is 4% larger than bore field

$$/(w, r) \sim 1 + \frac{ar}{w_{eq}}$$



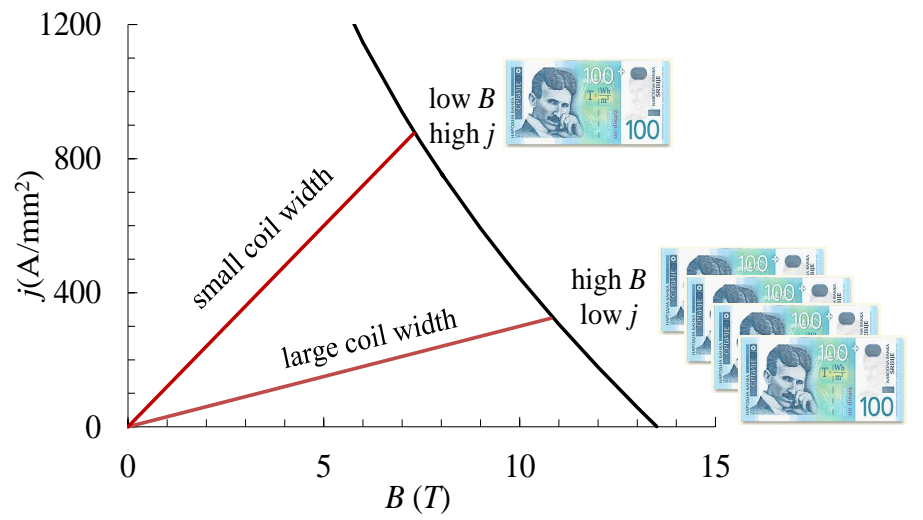


# HOW TO SQUEEZE MORE FIELD FROM THE LHC DIPOLES

- Short sample estimate, no iron (Unit 8, slide 11, 12 and 24)
  - Estimate of the factor  $X$
  - Where  $\gamma_c = 6.6 \times 10^{-7}$  T/A/m
  - $X = 6.6 \times 10^{-7} \times 0.28 \times 550 \times 10^6 \times 0.030 = 3.04$
  - As we knew, we are in the regime of large coils
  - $B_{ss} = 13 \times 3.04 / (1 + 1.04 \times 3.04) = 9.50$  T

$$X \propto g_c k s w$$

$$B_{ss} = b \frac{X}{1 + / X}$$







# HOW TO SQUEEZE MORE FIELD FROM THE LHC DIPOLES

- Short sample estimate, with iron (Unit 8, slide 11, 12 and 24)

- $r$ : aperture radius
- $w$  coil width
- $R_I$ : radius of iron (obviously,  $R_I$  must be smaller than  $r+w$ )

- Increase of transfer function due to iron: 
$$\frac{\Delta B_1^{iron}}{B_1} = \frac{m-1}{m+1} \frac{(r+w)r}{R_I^2} \approx \frac{(r+w)r}{R_I^2}$$

- Therefore for LHC dipole (neglecting saturation)

- Radius of iron is 98 mm
- $\Delta B_1/B_1 = (28+31) \times 28 / 98^2 = 0.17$
- Therefore increase of 17% of field due to iron

$$X \equiv g_c k_s w \left( 1 + \frac{\Delta B_1}{B_1} \right)$$

- Recomputing  $X$  including this increase:

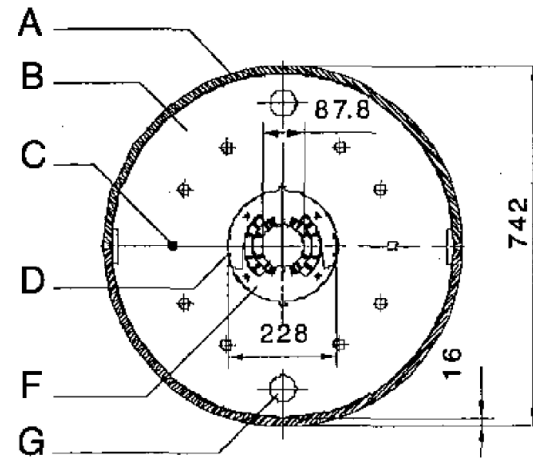
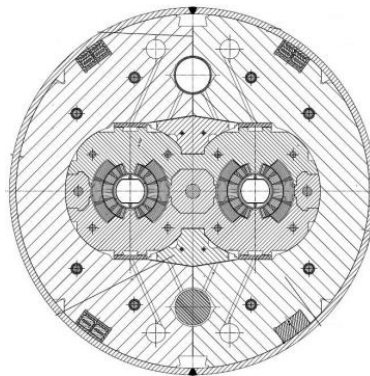
- $X = 6.6 \times 10^{-7} \times 0.28 \times 550 \times 10^6 \times 0.030 \times 1.17 = 3.56$

- And new short sample field is

- $B_{ss} = 13 \times 3.56 / (1 + 1.04 \times 3.56) = 9.84 \text{ T}$  (9.7 T computed with proper codes)

- Three main changes

- Bare cable width is increased from 15.1 mm to 16.74 mm (+10.9%)
  - This increase reflects in the short sample with a factor  $1/(1+\lambda X)=1/4.8$  (see Unit 8, slide 29) , therefore we gain 1.9% in short sample
- Aperture is increased by nearly a factor two (from 28 mm to 43.9) – therefore ratio peak field/bore field improves from 1.039 (LHC dipole) to  $\lambda=1+0.04\times 43.9/35=1.050$ 
  - This increase reflects in the short sample with a factor  $X/(1+\lambda X)=3.6/4.8$  (see Unit 8, slide 29) , therefore we lose 0.8% in short sample
- Iron contribution increases from 0.17 to 0.26
- $\Delta B_1/B_1=(43.9+33)\times 43.9/114^2=0.26$



- New estimate

- Equivalent coil width increases by 11% (15.1 mm to 16.7 mm bare cable, projected to equivalent coil width from 29.6 mm to 32.8 mm)
- Iron contribution increases from 0.17 to 0.26

$$\Delta B_I/B_I = (43.9+33) \times 43.9 / 114^2 = 0.26$$

$$X \equiv g_c k_{sw} \left( 1 + \frac{DB_1}{B_1} \right)$$

- $X = 6.6 \times 10^{-7} \times 0.28 \times 550 \times 10^6 \times 0.033 \times 1.26 = 4.23$
- Ratio peak field/bore field gets worse from 1.040 (LHC dipole) to  $\lambda = 1 + 0.04 \times 43.9 / 35 = 1.050$

- And new short sample field is

- $B_{ss} = 13 \times 4.23 / (1 + 1.05 \times 4.23) = 10.11 \text{ T}$  (10.15 T computed with proper codes)

- Therefore, with a 10% increase in the width, and the enhanced contribution of iron, the final increase of the short sample field is 2.5%

- **Price is an important** variable in the applications of superconductivity (as in most applications)
  - Price per volume of superconductors is **300 times** larger than Al for Nb-Ti, and much larger for Nb<sub>3</sub>Sn and HTS
- The main atout of superconductivity is to carry large current densities, and therefore provide compact devices, without having to pay for dissipated power
  - From 1-5 A/mm<sup>2</sup> to 100-500 A/mm<sup>2</sup> – it is a factor 100
    - **For Nb-Ti, the larger current density roughly compensates the higher price**
    - **So the price per kA m is comparable**
- Why 100-500 A/mm<sup>2</sup> and not more ?
  - Limits in the critical surface, instabilities (already shown) plus stresses induced by Lorentz forces in magnets and protection

- With this range of prices and properties (current densities), **superconductivity can replace resistive devices** in some cases
  - Power lines: when compact devices are needed (example, **power lines in metropolis**, where the size becomes an issue)
  - Motors: when compact devices are needed (when **weight is an issue**)
  - For high field magnets, superconductivity allows not only to have compact devices but also **saving on operational costs**
    - NMR (Nuclear Magnetic Resonance) is a spectroscopy method to method to probe matter: physics, chemistry, material science, biology
    - MRI (Magnetic Resonance Imaging) is a special case of NMR, applied to biology
    - Accelerator magnets



900 MHz NMR magnet of 21.2 T

# CONCLUSIONS

- We discussed the possibility of building a 600 T magnet as shown in a blockbuster science fiction movie
  - Using the equations derived for **magnetic design, mechanical structure and protection** we outlined the directions to explore to get to this target
- We showed how to use the equations discussed for the magnetic design to get a few more tenths of tesla in Nb-Ti magnets with two layers coils, showing how Fresca managed to break the 10 T barrier
  - This is another application of the analytical approach, that can be used to make accurate **sensitivity analysis containing an “insight”** on the main mechanisms