
Superconducting materials for the magnetic confinement coils

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ITER Organization/MCD/EVDA

Magnet Section/ CSSP Group

EASISchool3 Summer School

09 October 2020

“The views and opinions expressed herein do not necessarily reflect those of the ITER Organization”

content

Magnetic confinement

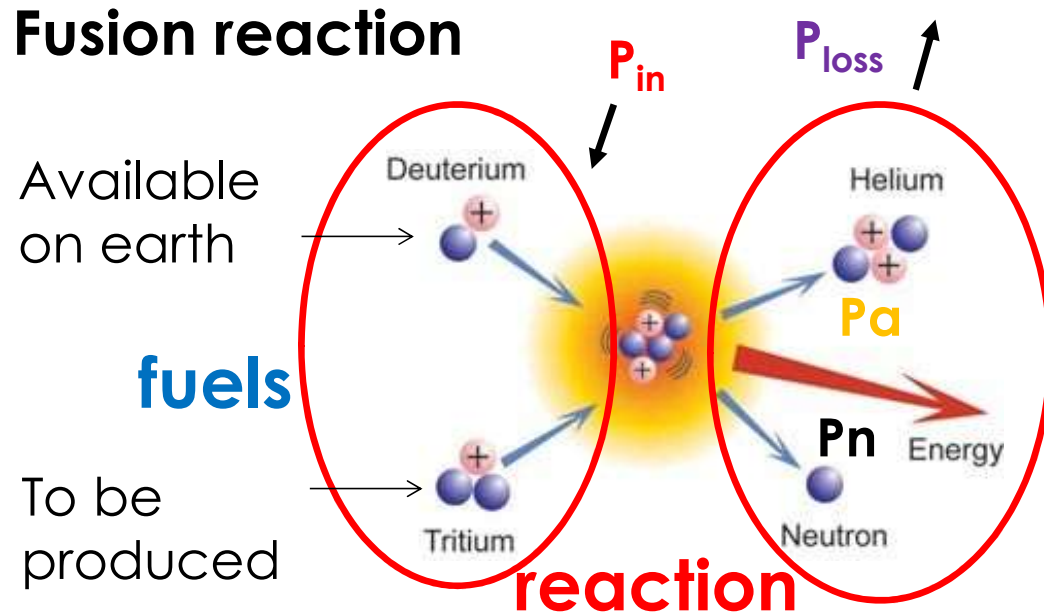
ITER magnet system

ITER superconductors

Manufacturing status

Magnetic confinement

Fusion reaction



Independant travel of charged particles:

→ **plasma** required

Issues:

- electrostatic repulsion
- energy losses P_{loss}

$$P_{fus} = P_{\alpha} + P_n$$

distribution:

$$P_{\alpha} \sim 20\%$$

$$P_n \sim 80\%$$

fusion products

Q energy gain

$$Q = P_{fus} / P_{in}$$

$Q = 1$ breakeven

$$Q = \infty \text{ Ignition} \quad \tau_E = W / P_{loss}$$

τ_E energy confinement time



Hans Bethe
(1906 - 2005)
Nobel Prize of Physics 1967

Magnetic confinement

Lawson criterion (1955)

Plasma energy balance: $dW/dt = 0$

Density (n) x confinement time (τ_E) x temperature (T)

$$n \cdot \tau_E \cdot T > 10^{21} \text{ (keV} \cdot \text{s} \cdot \text{m}^{-3}\text{)}$$

Fusion routes

Inertial fusion (sun)

High density

$(10^{27} \cdot \text{m}^{-3})$

Low temperature (1.5 keV)

Magnetic fusion (ITER)

Low density ($10^{20} \cdot \text{m}^{-3}$)

High temperature (10 keV)

Energy confinement time 3 s

$n \cdot \tau_E \cdot T = 3 \cdot 10^{21}$

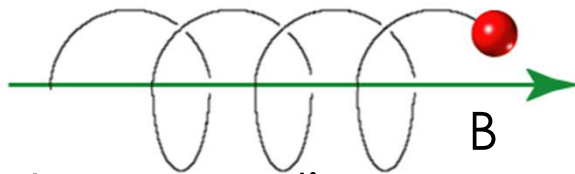


John D. Lawson
(1923-2008)

Magnetic confinement

Magnetic configurations

linear configuration

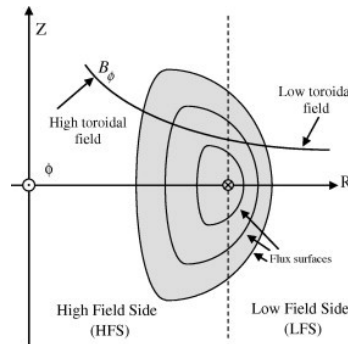
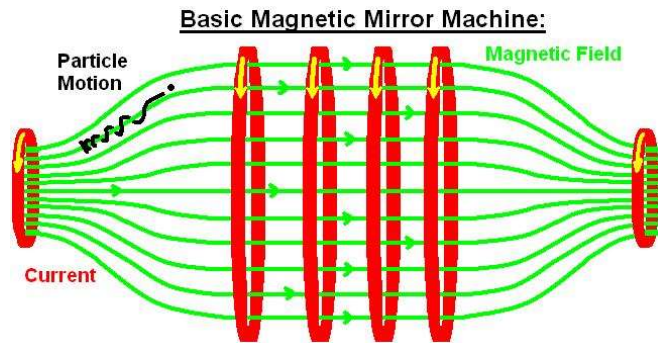
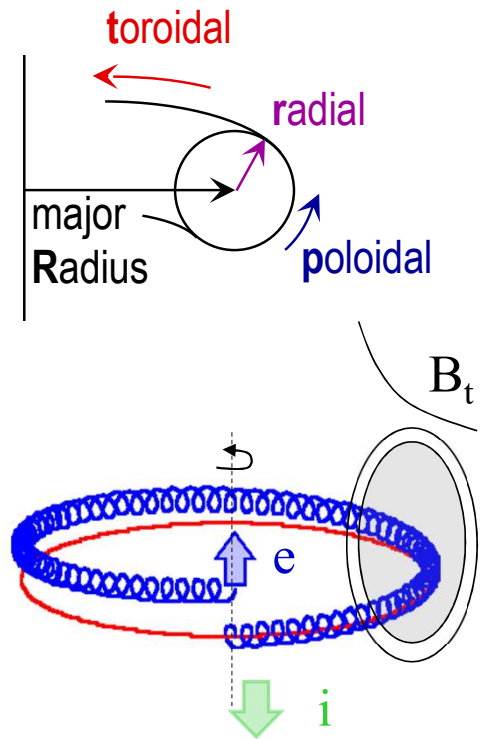


Larmor radius:
 $r_L = m \cdot v_{\perp} / q \cdot B$

toroidal configuration



Magnetic torus



Toroidal Field varies in $1/r$

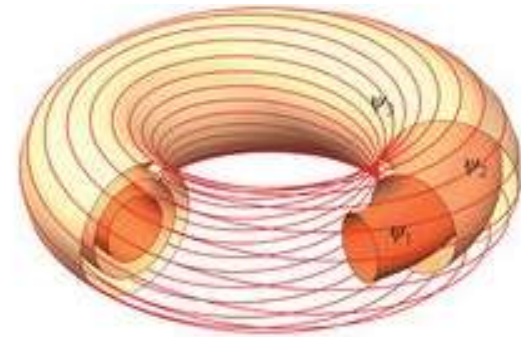
Issue: losses at the ends

Issue: vertical drift of particles

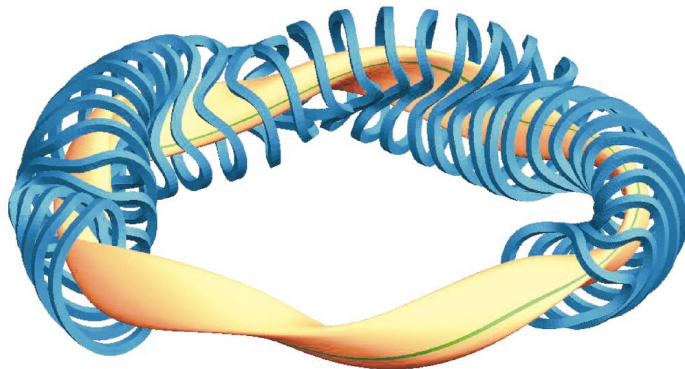
Magnetic confinement

Helical magnetic configurations

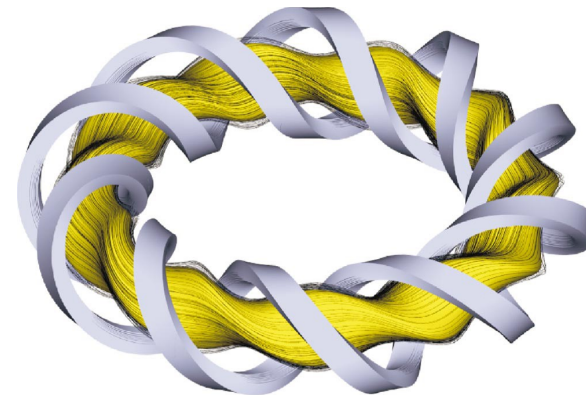
The magnetic field lines form a series of nested magnetic surfaces.
Charged particles remain trapped within magnetic surfaces



How to achieve it?



stellarator



heliotron

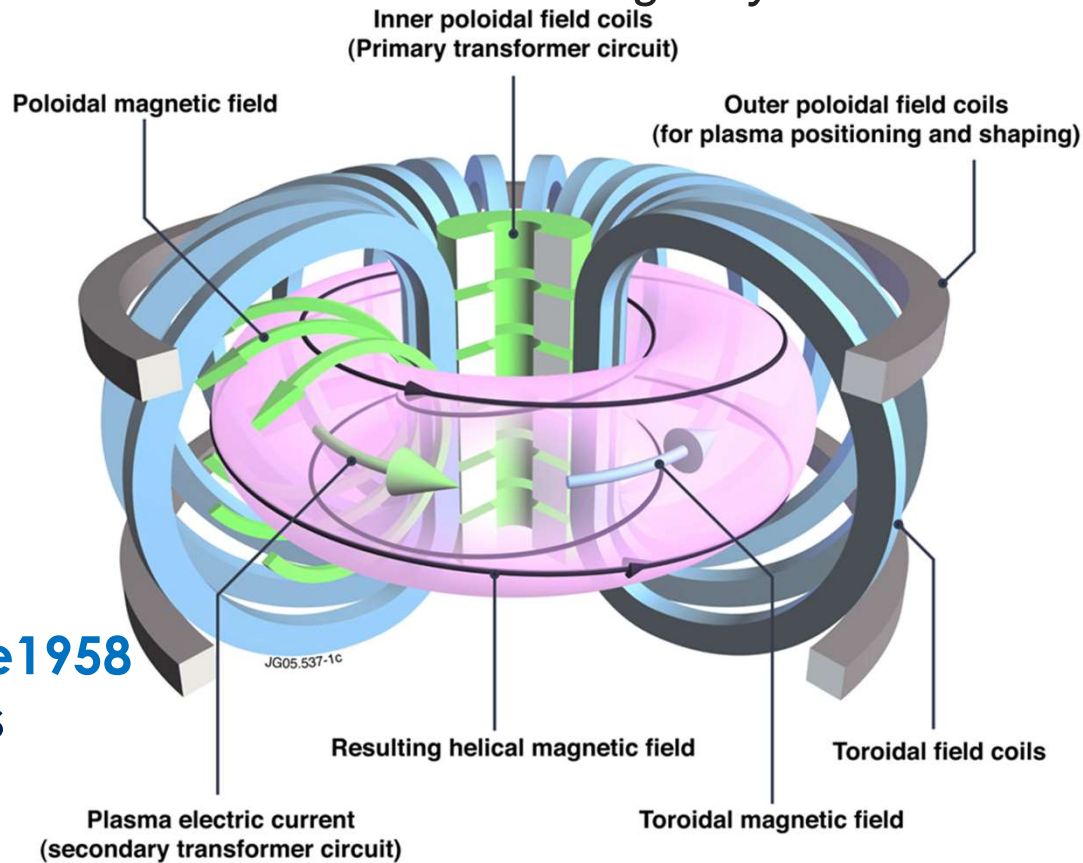
Magnetic confinement



Igor Kurtchatov
(1903-1960)

Geneva
Conference 1958
Researches
opening

Tokamak design (1958) *toroidalnaia kamera s magnitnymi katushkami*

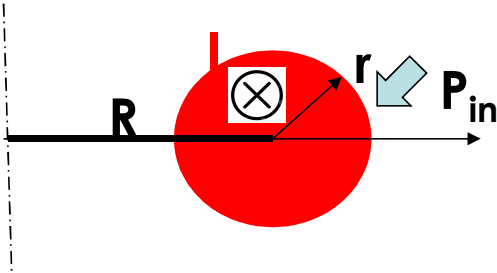


Lev A.
Artsimovitch
(1909-1973)

Novosibirsk
Conference 1968
 $T_e > 1 \text{ keV}$
 $\tau_E > 10 \text{ ms}$

Magnetic confinement

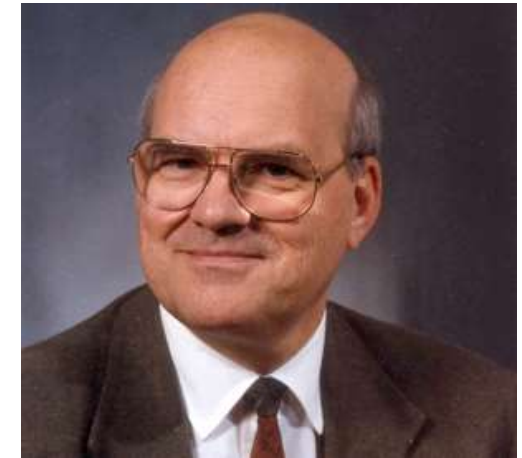
The tokamak route



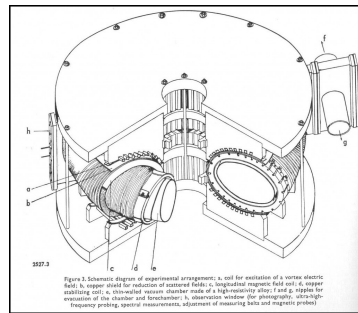
$$\tau_E \propto I_p R^2 P_{in}^{-2/3}$$

T1 (Moscow):	1958
T3 (Moscow):	1968
TFR (Fontenay-aux-Roses):	1973
JET (Culham):	

- commissioning: 1983
- 1st DT exp. 1991
- 2nd DT exp. 1997
- **3rd DT exp. 2020 ?**



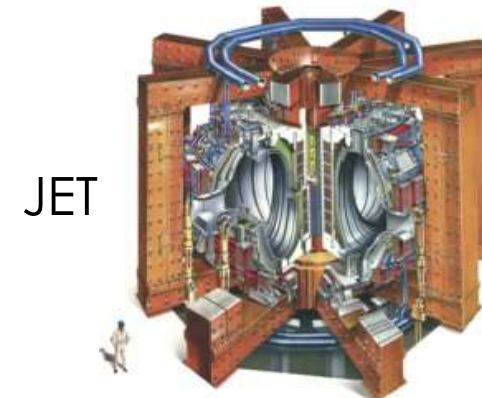
Paul-Henri Rebut
(1935-)



T1



TFR



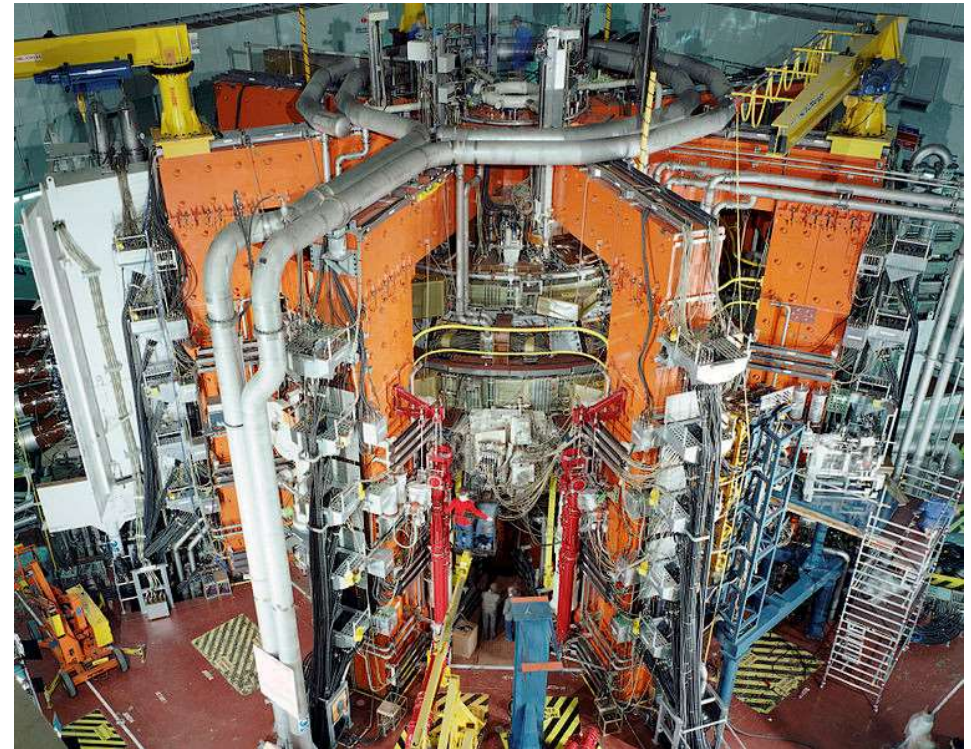
JET

Magnetic confinement

Copper magnets

Production of magnetic fields in tokamaks was first achieved using copper magnets.

JET electric power supply: **400 MW**
→ motor generator **flywheels** required



JET European tokamak(Culham)

→ **issue: electrical energy consumption**

Magnetic confinement

Superconducting magnets

The construction of magnets using superconducting materials allowed a considerable reduction of the needed electrical power for production of magnetic fields and long pulses.

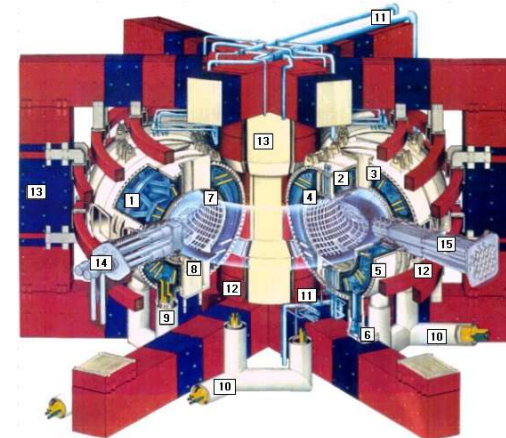


Robert Aymar
(1936 -)

T7 (**NbTi**, Moscow): 1979
Tore Supra (**NbTi**, Cadarache): 1988
T15 (**Nb₃Sn**, Moscow): 1988

Tore Supra TF electrical power: **1 MW**

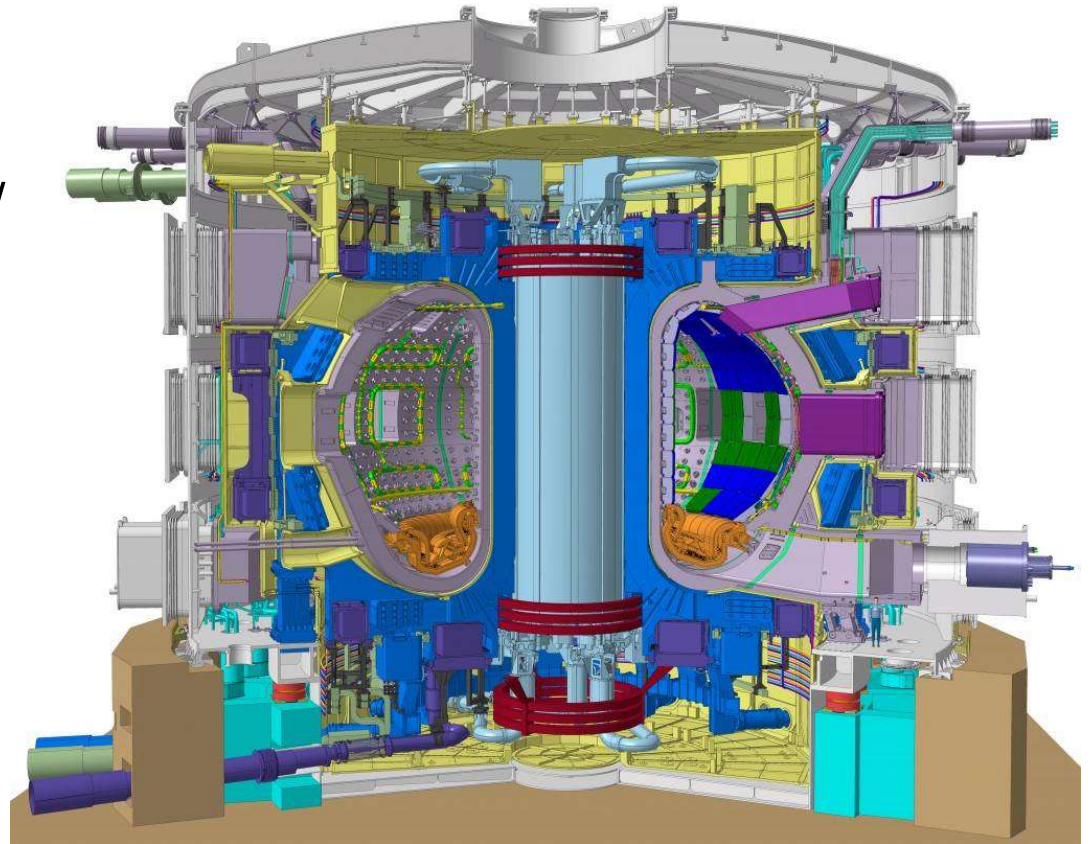
Tore
Supra



Magnetic confinement

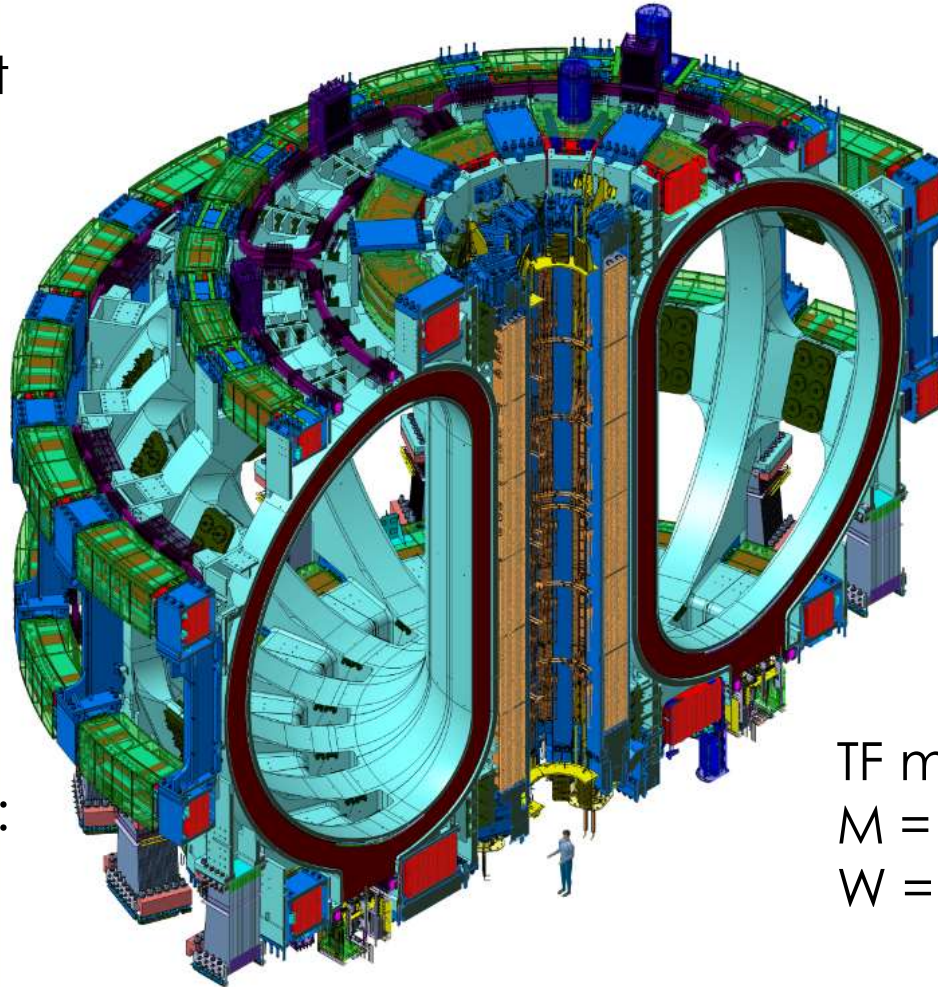
ITER design

Fusion power	500 MW
Energy gain	$Q \geq 10$
Inductive discharge	≥ 400 s
Large plasma radius	6.2 m
Small plasma radius	2.0 m
Plasma current	15 MA
Toroidal field	5.3 T



ITER Magnet System

PF magnet
 $M = 2746 \text{ t}$
 $W = 10 \text{ GJ}$
(17 MA)

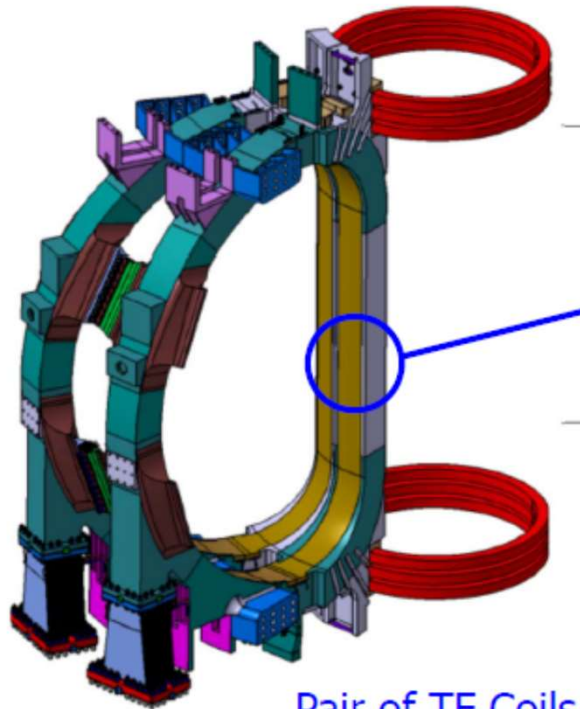


Total mass:
 $10\,360 \text{ t}$

TF magnet
 $M = 5373 \text{ t}$
 $W = 41 \text{ GJ}$

ITER Magnet System

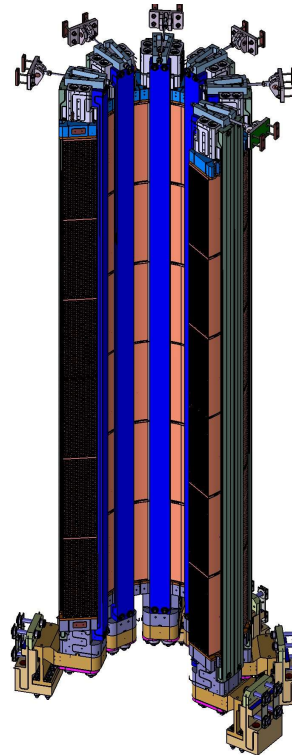
18 TF coils



Pair of TF Coils

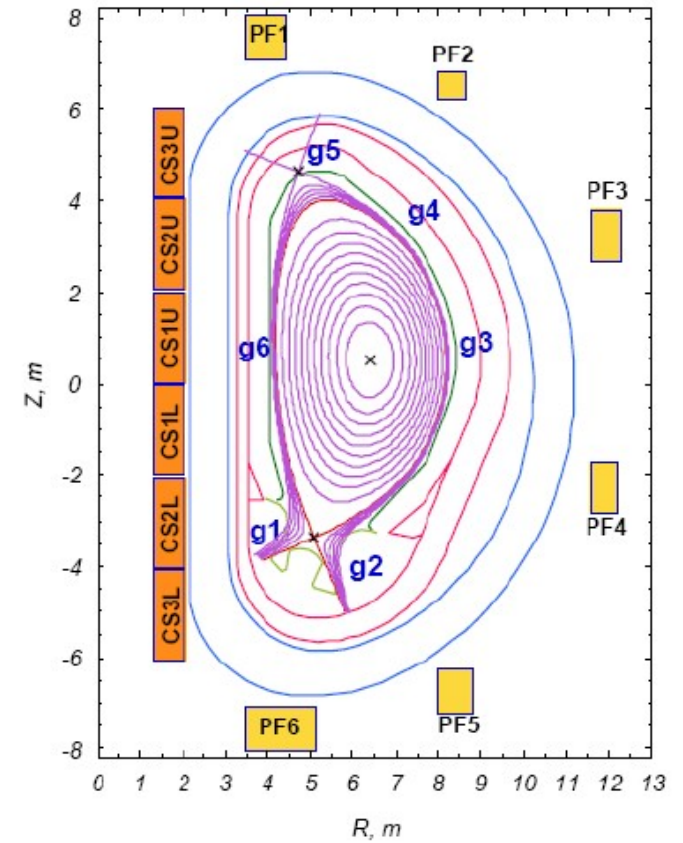
current capacity
 $I = 9.1 \text{ MA/coil}$

6 CS coils



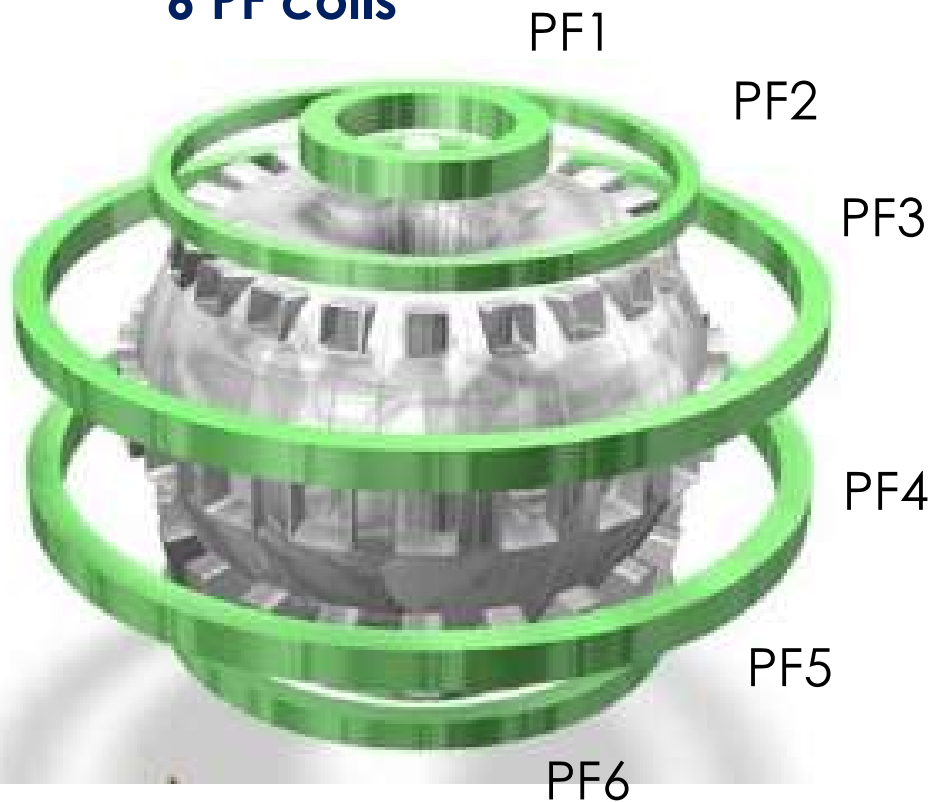
current capacity
 $I = 22.2 \text{ MA/coil}$

Poloidal cross-section



ITER Magnet System

6 PF coils

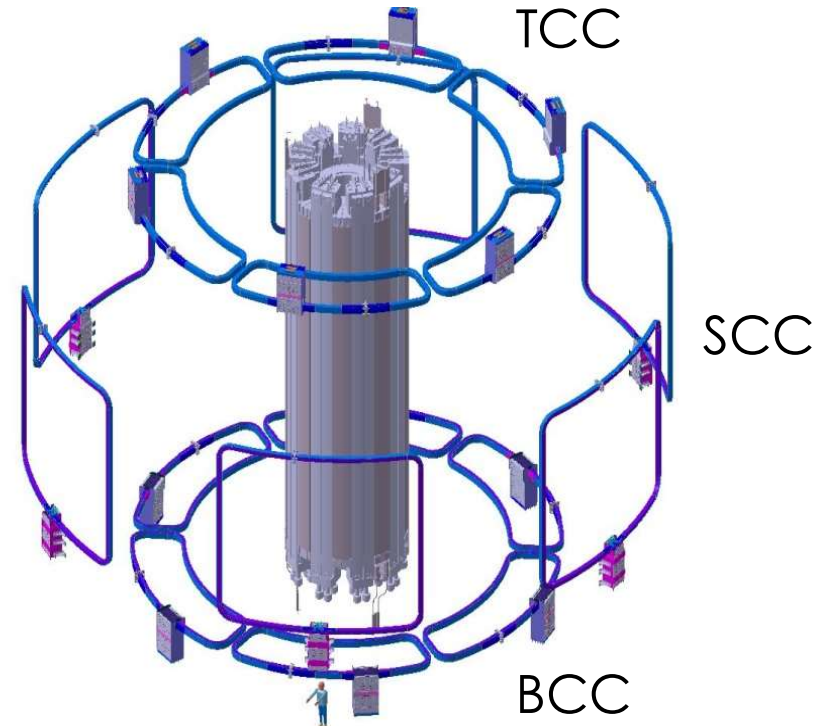


current capacity

$I = 55.8 \text{ MA}$

$(\text{PF1} + \text{PF2} + \text{PF3} + \text{PF4} + \text{PF5} + \text{PF6})$

18 Correction coils



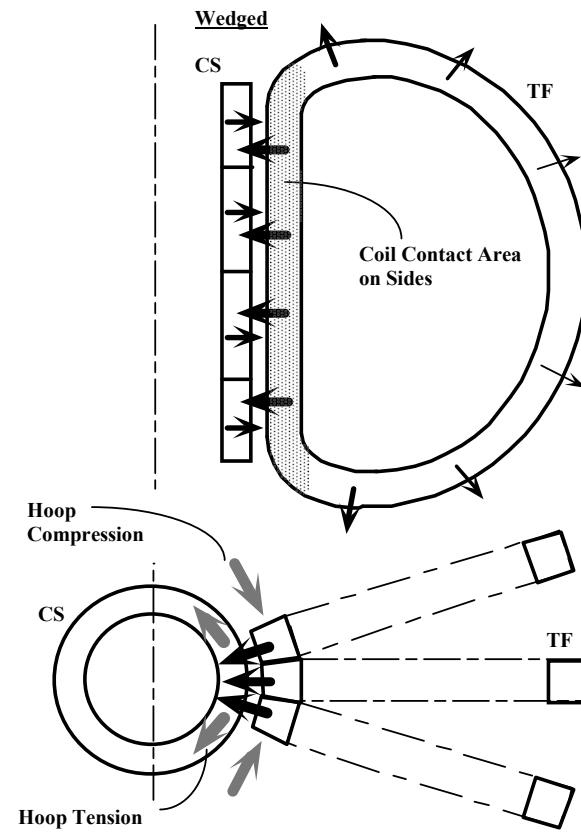
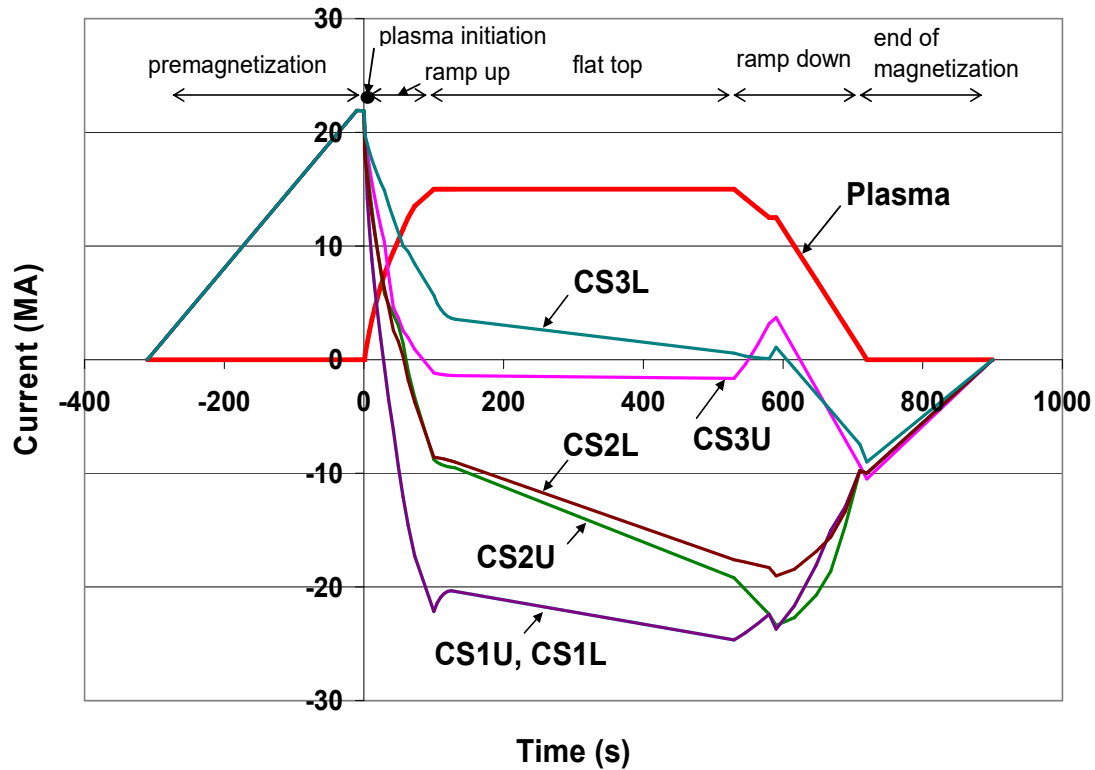
current capacity

$I = 0.32 \text{ MA/BCC TCC coil}$

$I = 0.20 \text{ MA/SCC coil}$

ITER Magnet System

Plasma operation



ITER Superconductors

Conductor design

Conductor current is determined by the maximum allowable voltage to discharge the coils

$$U = L \, di/dt$$

Discharge time constant: 11 s

→ **high current conductor required**

TF coil: 134 turns x **68 kA** = 9.1 MA/coil

CS coil: 556 turns x **40 kA** = 22.2 MA/coil

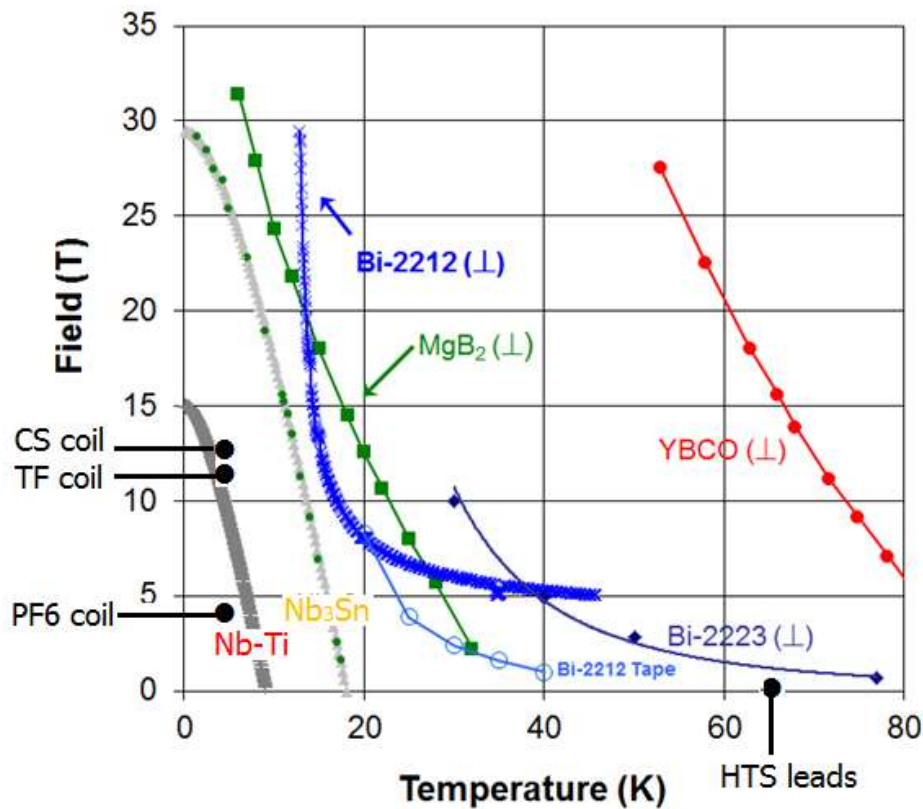
Maximum voltage

30 kV test voltage for CS coils

→ **high voltage insulation materials required**

ITER Superconductors

Superconducting materials



CS coils

$B_{max} = 13 \text{ T}$

→ **Nb₃Sn**

TF coils

$B_{max} = 11.8 \text{ T}$

→ **Nb₃Sn**

PF coils

$B_{max} = 6.4 \text{ T}$

→ **NbTi**

Correction Coils

$B_{max} = 6 \text{ T}$

→ **NbTi**

Feeders

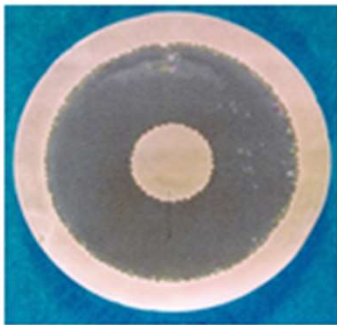
$B_{max} = 3.5 \text{ T}$ → **NbTi**

Current leads $B_{max} = 0.065 \text{ T}$ → **Bi2223**

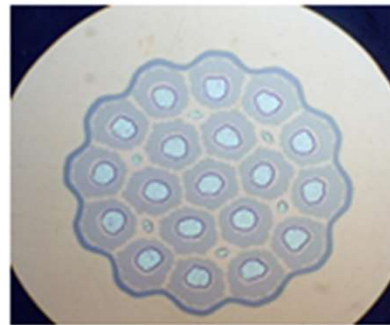
ITER Superconductors

Superconducting wires

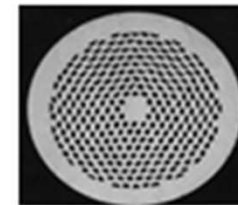
- For practical applications, the superconductor is subdivided into **fine filaments**, which are **twisted together** and **embedded in a low-resistivity matrix** of normal metal (e.g., pure OFHC Cu for Nb-Ti and Nb₃Sn, Ag or Ag–Au for HTS).
- The superconducting multifilament composites are manufactured under the form of **wires** (with an outer diameter of ~1 mm) or **tapes**.



Nb–Ti Wire for ITER



Nb₃Sn Wire for ITER



BSCCO 2212 Wire

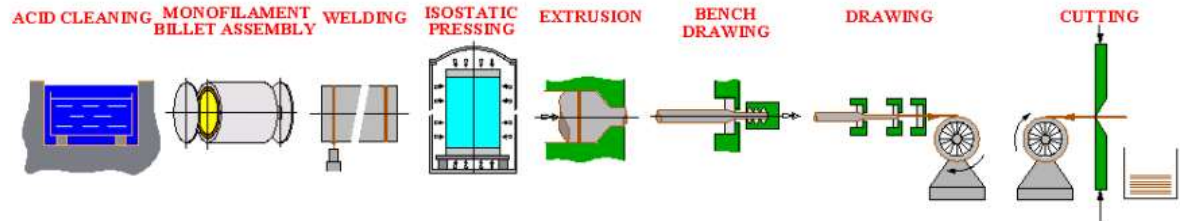


BSCCO 2223 Tape

ITER Superconductors

Industrial manufacture of supraconducting wires

A superconducting wire is made of superconducting **filaments** embedded into a copper matrix.

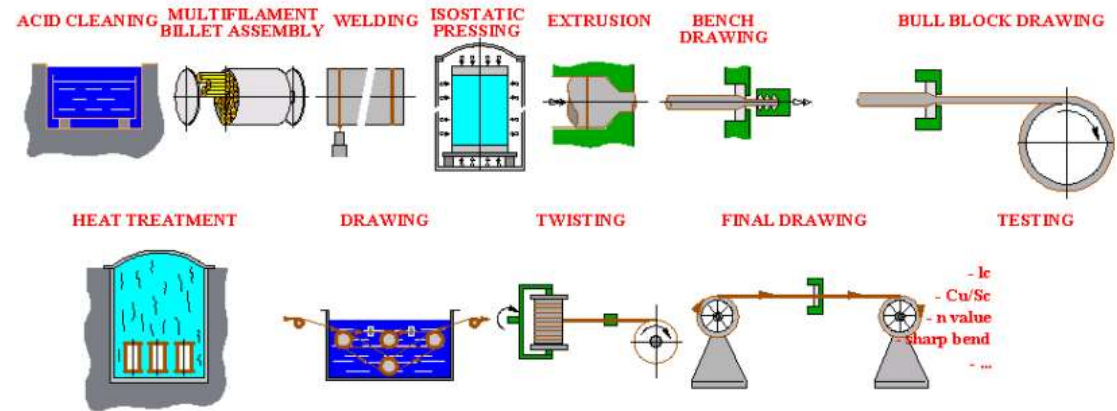


Monofilamentary step

The manufacture is performed in two steps:

- a **monofilamentary step**
- a **multifilamentary step**

→ **multifilamentary twisted composite wire**
(l ~ km, \varnothing ~mm)



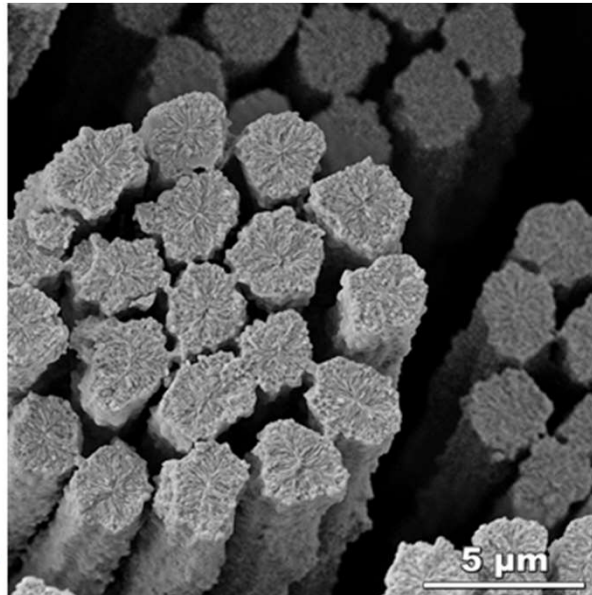
Multifilamentary step

ITER Superconductors

Multifilamentary twisted composite wire

CSJA2
HFZ

The Nb₃Sn fractures at the grain boundaries and thus we see the grain structure across the filaments.



 Peter J. Lee &
Carlos Sanabria

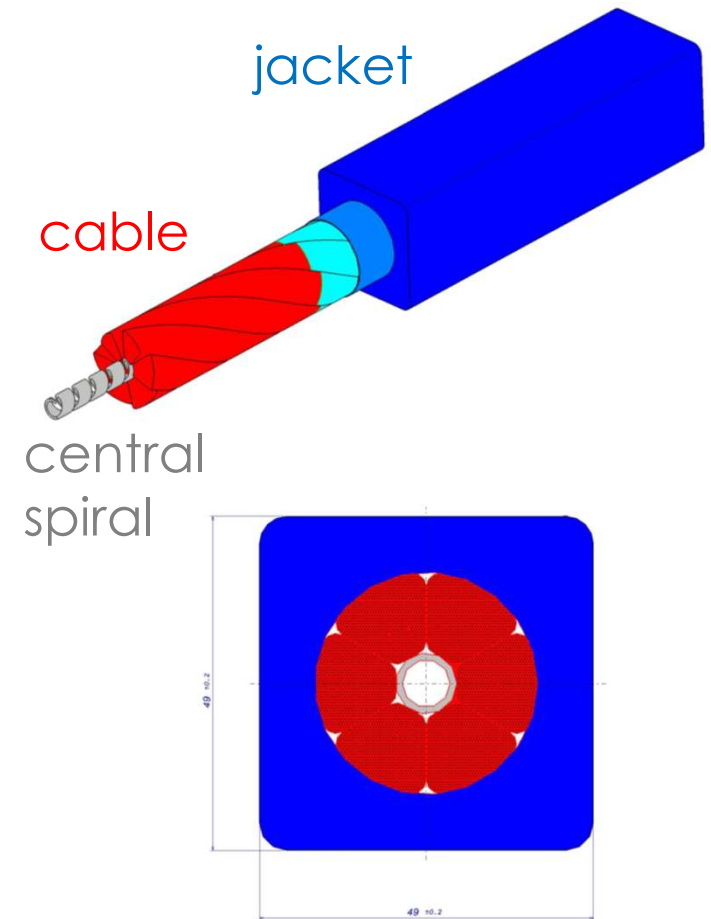
23

Deep Zoom into ITER CS conductor put together by Carlos Sanabria and Peter Lee, FSU

ITER Superconductors

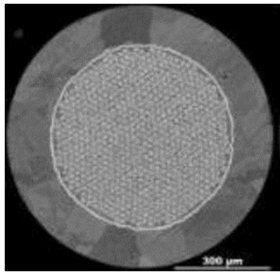
Cable-in-conduit conductors

- a cable-in-conduit conductor allows achieving **high transport current**, by twisting together into a cable **several hundreds** of strands contained in a steel pipe internally cooled by a flow of supercritical helium
- in a **dual channel** cable-in-conduit conductor, a central channel is managed along the conductor axis

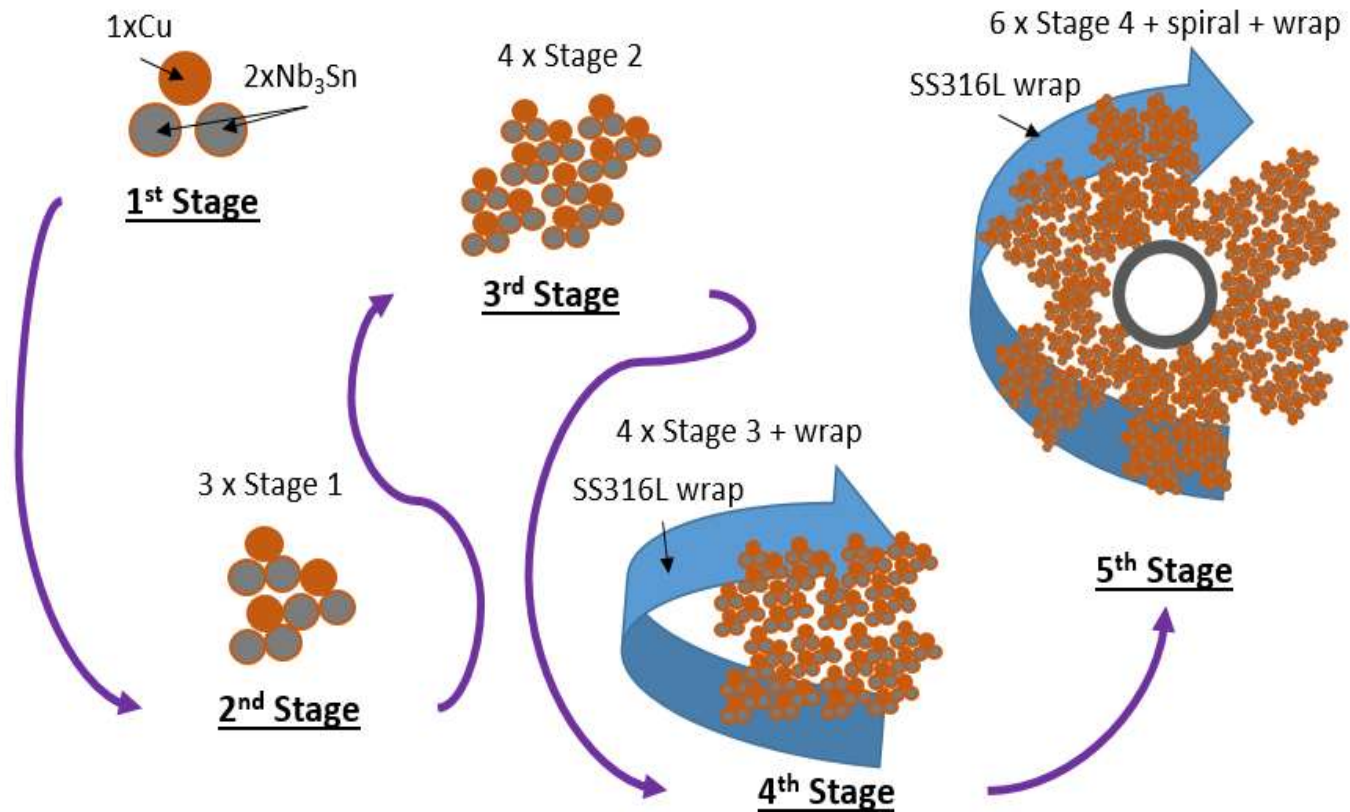


ITER Superconductors

Multistage twisted cables



Strand cabling is performed in a multistage process

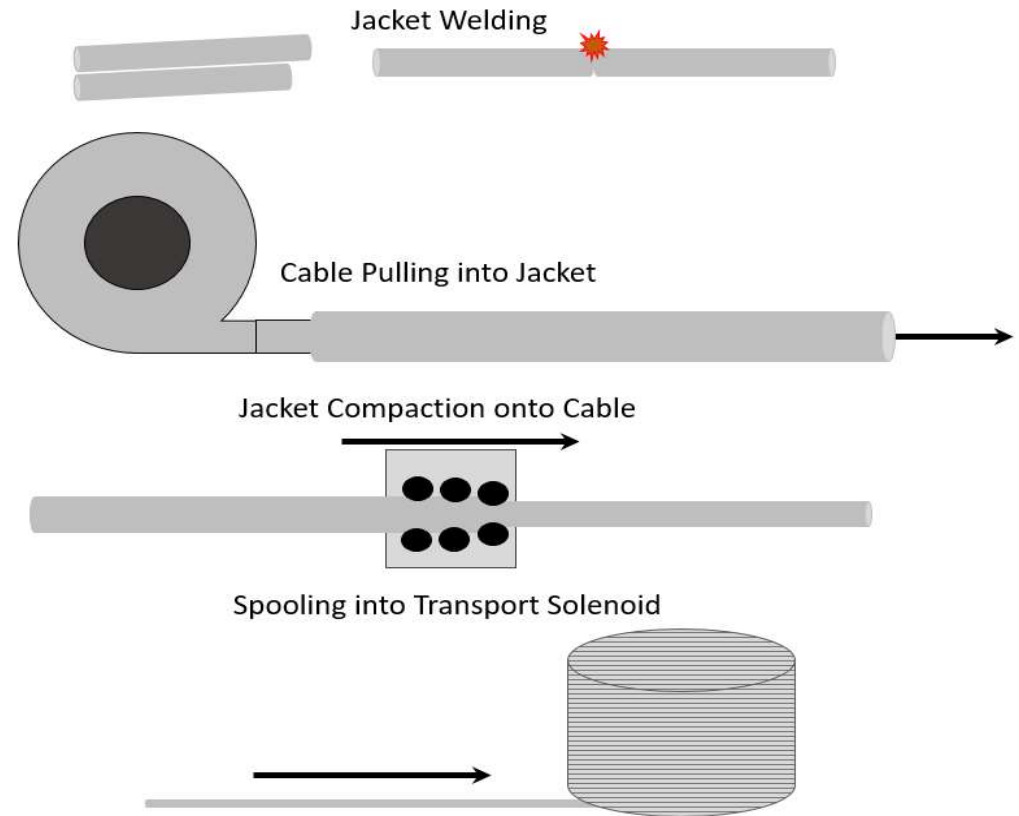


ITER Superconductors

Cable jacketing

Cable jacketing is performed in 3 steps:

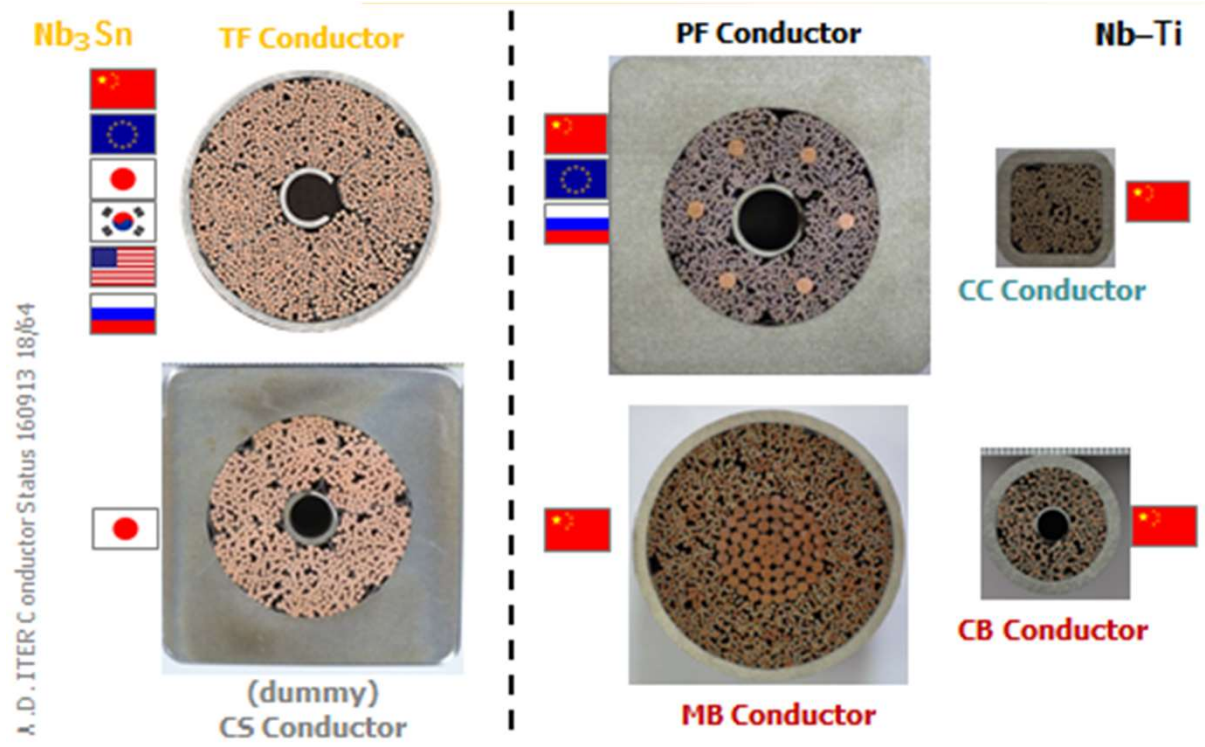
- Jacket manufacture
- Cable pulling through
- Jacket compaction



ITER Superconductors

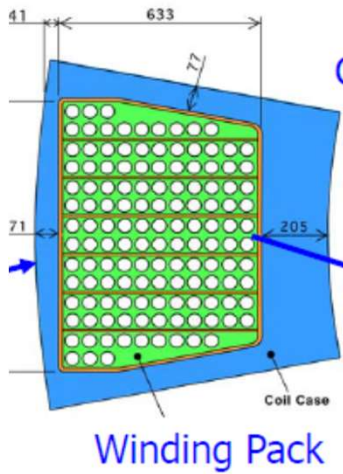
ITER Conductors

Cable-in-conduit ITER conductors cooled by supercritical He flow at 4.5 K



ITER Superconductors

Nb₃Sn coils



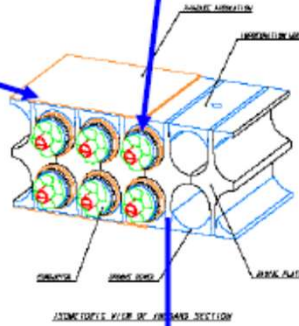
Stainless Steel
Radial Plate

TF coils

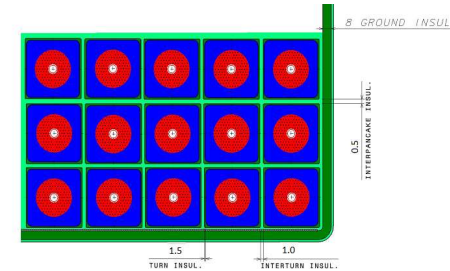
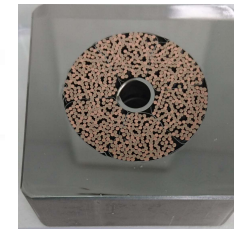
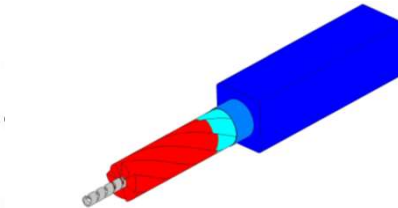
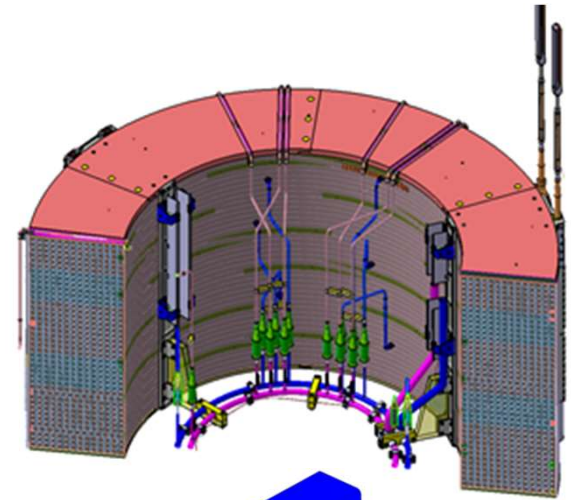
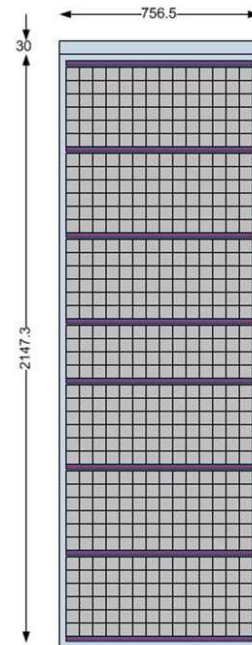
CIC
Conductor



Nb₃Sn Rope-
Type Cable



CS coils

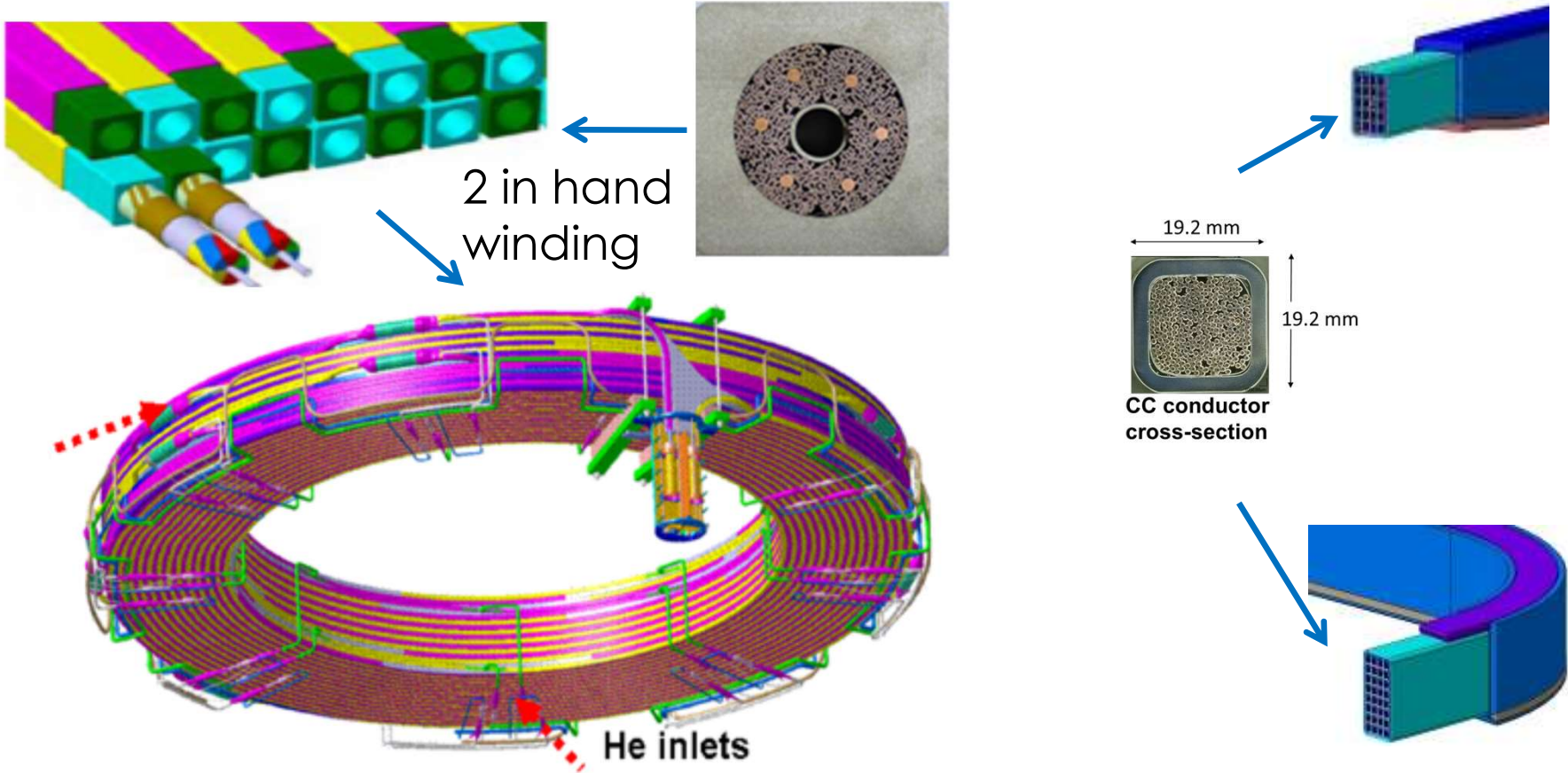


ITER Superconductors

NbTi coils

PF coils

Correction Coils



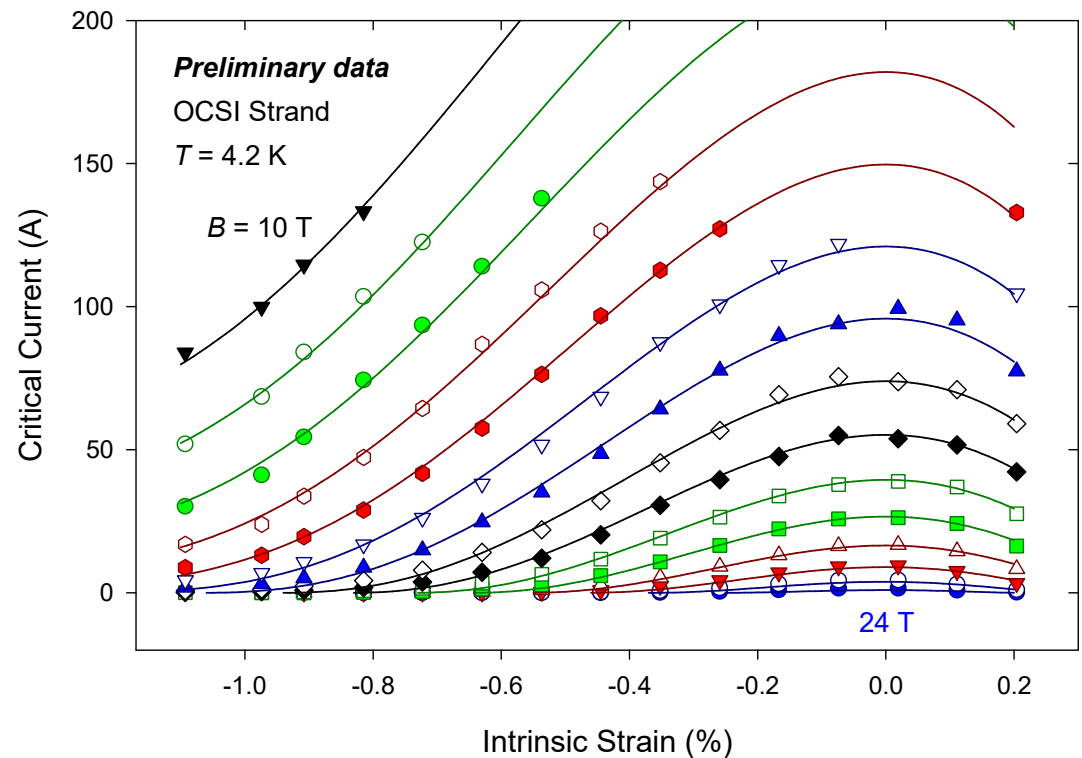
ITER Superconductors

Nb₃Sn critical current strain dependence

Nb₃Sn critical current is highly sensitive to applied **strain**

→ **selection of wind and react process to minimize applied strain**

- Winding
- Reaction heat treatment (650C, 200 h)
- Turn insulation



Manufacturing status

Nb₃Sn industrial production

- TF and CS strand productions are completed with **over 500 tons (~7800 billets and 100,000 km) for TF** and **~170 tons for CS.**
- It is the **largest Nb₃Sn strand production** ever and has called for a significant worldwide production **ramp up.**
- Pre-ITER world production was estimated at **~15 t/year**; it has been steady for the last five years at **~100 t/year.**

Data Compiled by D. Kaverinas of 31 May 2017 (ITER-CT)

- Nb₃Sn for TF: **~100% complete.**

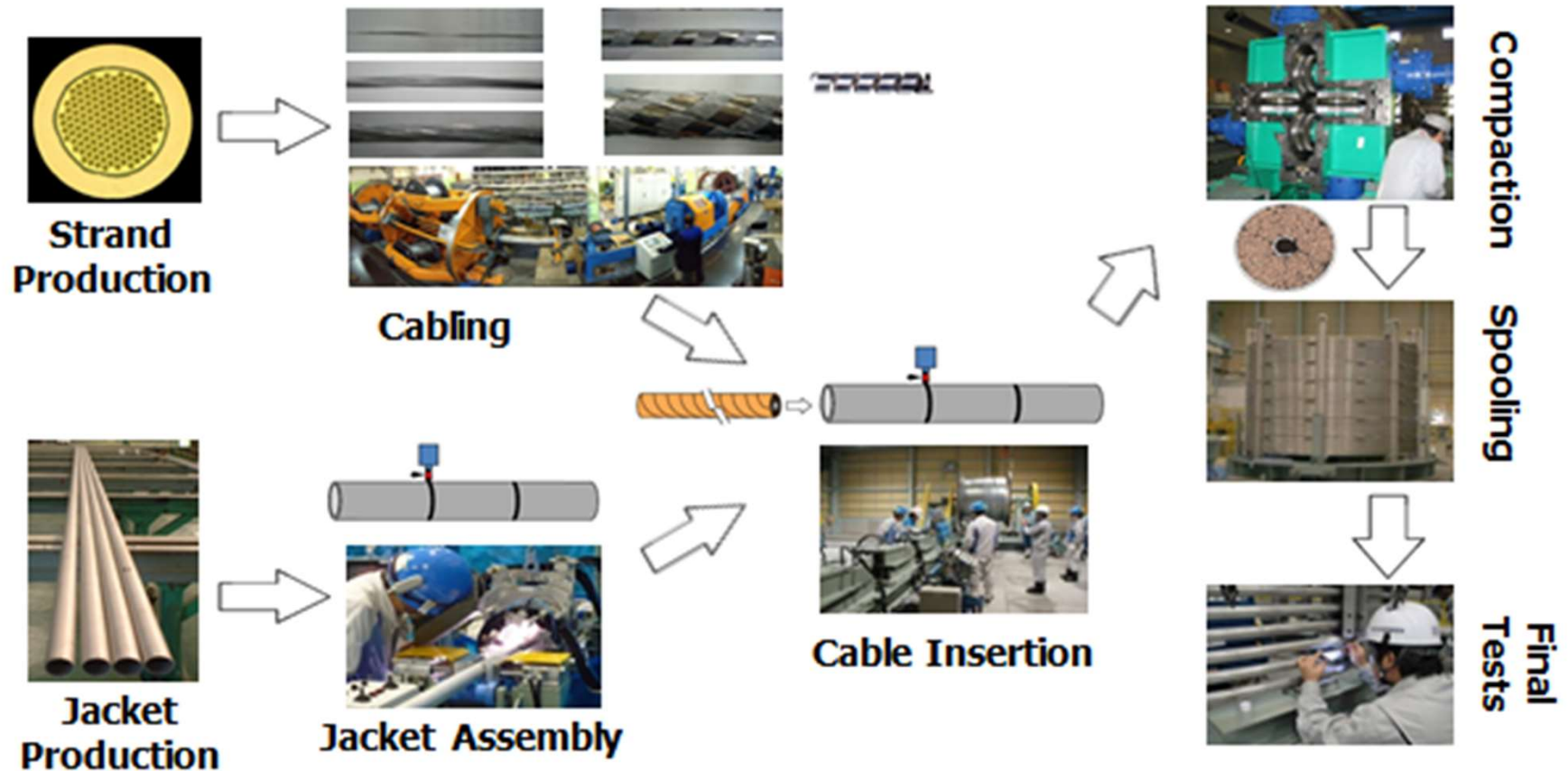


- Nb₃Sn for CS: **~100% complete.**



Manufacturing status

Conductor manufacture is complete



Manufacturing status

TF coils



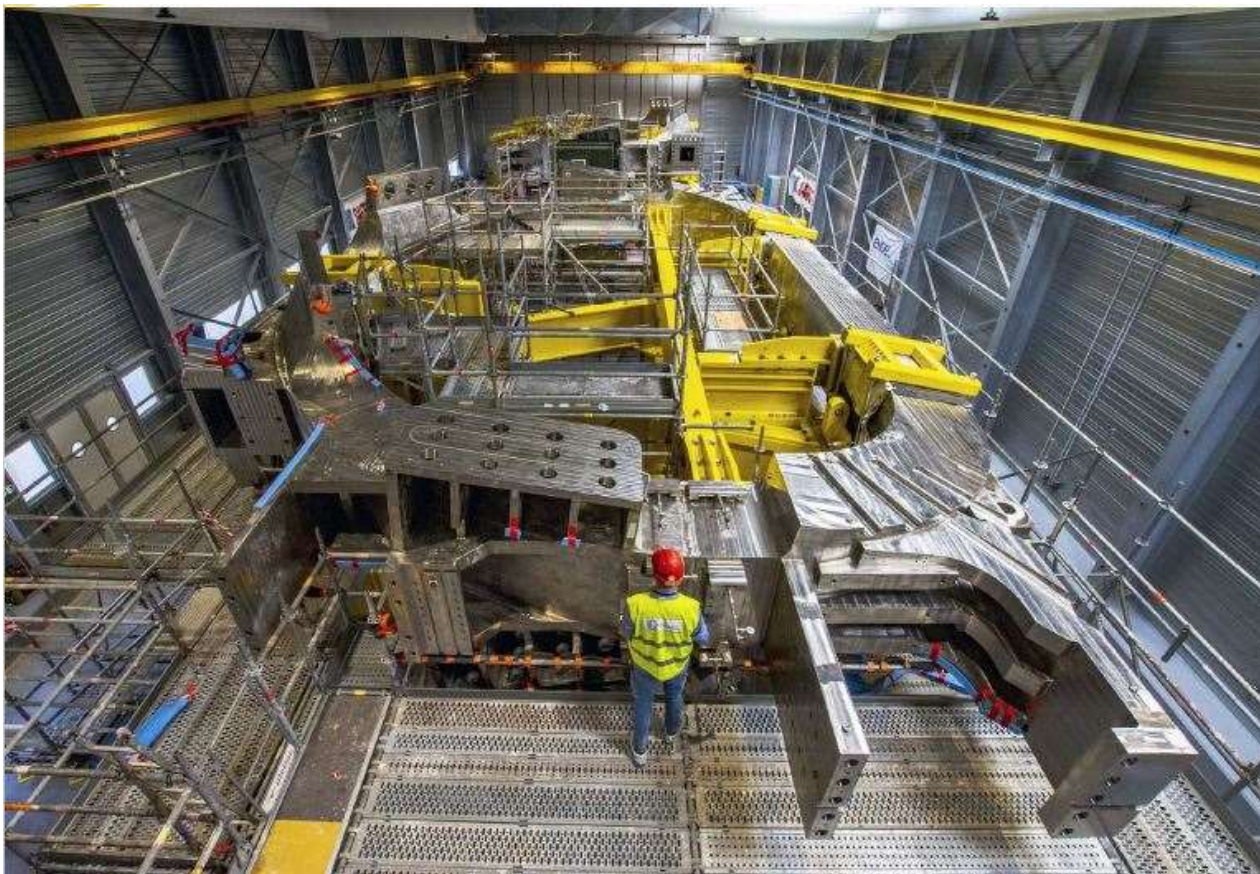
First TF winding-pack before resin impregnation



First TF case before assembly with winding-pack

Manufacturing status

TF coils



First TF coil delivered to ITER

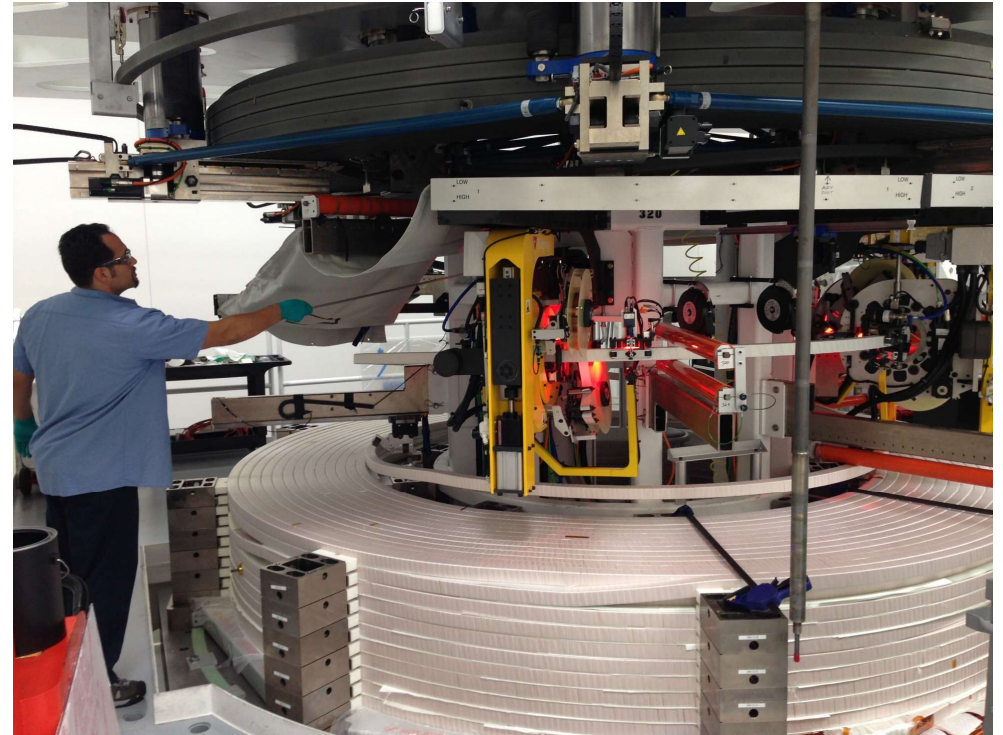
Manufacturing status

CS coils



Courtesy GA

CS Module heat treated



Courtesy GA

CS Module mock-up turn insulation application

Manufacturing status

CS coils



Courtesy GA

CS Module 1 ground insulated



Courtesy GA

CS Module 1 cold testing

Manufacturing status

PF coils



Courtesy F4E

PF4 2nd double pancake winding



Courtesy F4E

PF coils manufacturing hall

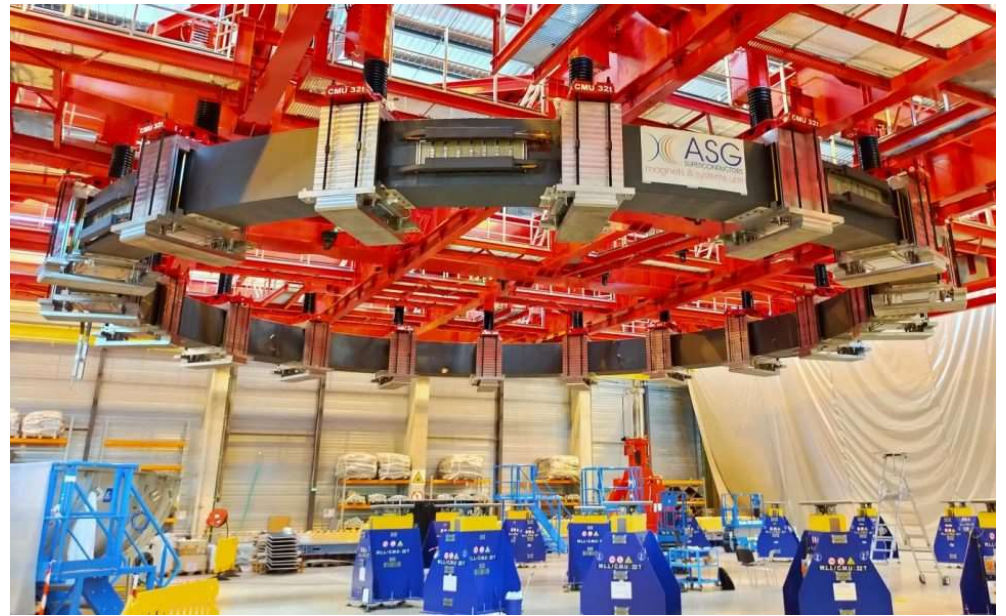
Manufacturing status

PF coils



Courtesy F4E

PF2 resin impregnation preparation



Courtesy F4E

PF5 resin impregnated

Manufacturing status

PF coils



PF1 ground insulated

Courtesy Efremov



PF6 cold testing preparation

Courtesy F4E

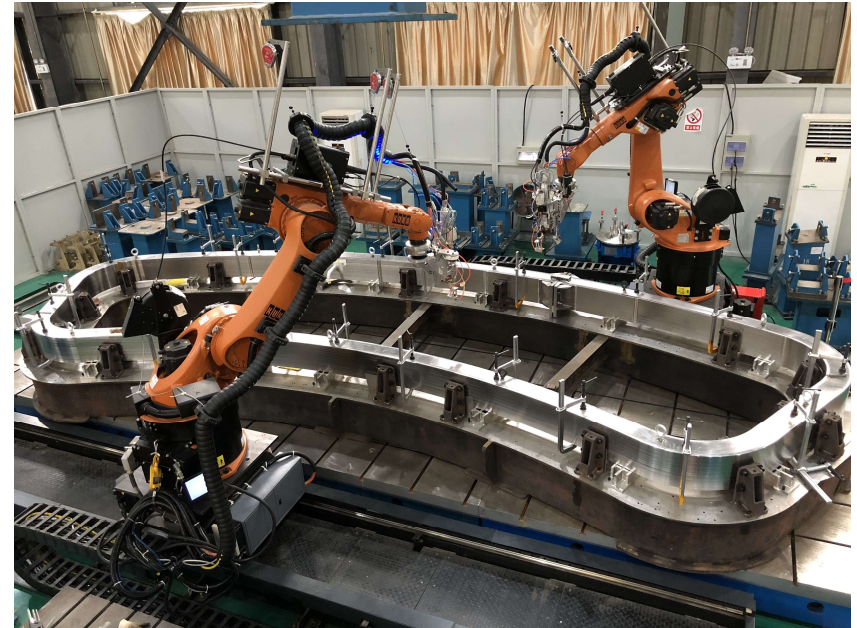
Manufacturing status

Correction coils



Courtesy ASIPP

BCC1 winding-pack



Courtesy ASIPP

Prototype BCC case closure welding

Manufacturing status

Summary

ITER Magnet System component	Status
Nb ₃ Sn conductor lengths	Delivered to coil manufacturers
NbTi conductor lengths	Delivered to coil manufacturers
TF coils	3 TF coils delivered to IO
PF coils	PF6 prepared for cold testing PF5 resin impregnated PF4 under winding PF1 ground insulated
CS coils	Module 1 cold tested Module 2 prepared for cold testing Module 3 resin impregnated Module 4 ground insulated Module 5 under turn insulation application Module 6 stacked, preparing for heat treatment
Correction Coils	6 BCC coils manufactured, ready for delivery to IO