

Resonant Diffraction Radiation from inclined Targets

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- *Introduction*
- *Smith-Purcell Radiation*
- *Resonant Diffraction Radiation*
- *RDR Monitor for Bunch Length Diagnostics*



Bunch Length Diagnostics

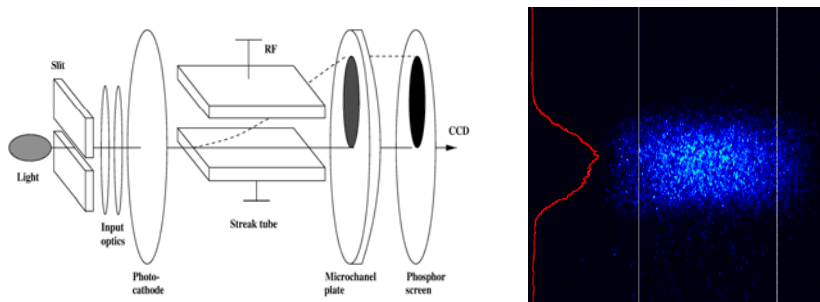
- purpose

high resolution measurement ↔

machine tuning

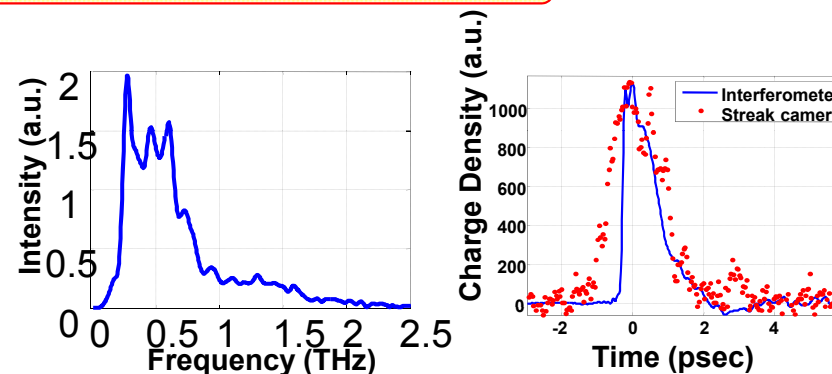
- principles

- streak camera



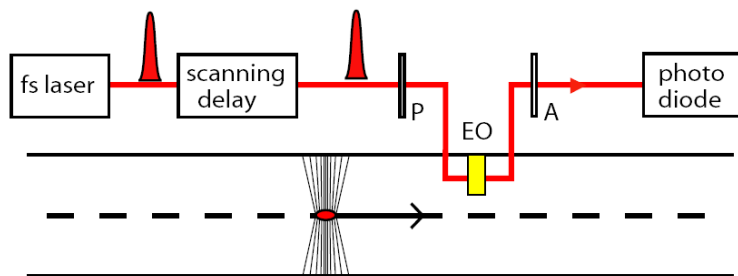
courtesy D.Lipka (DESY)

- coherent radiation diagnostics



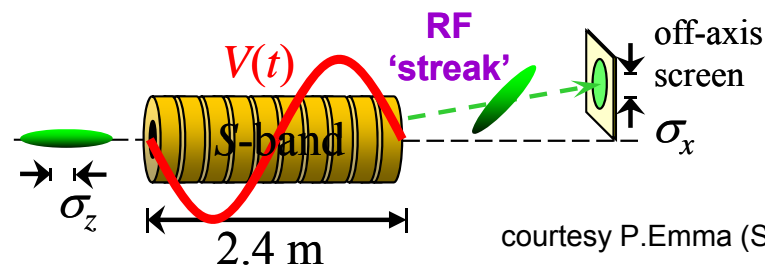
courtesy O.Grimm (DESY)

- EO techniques



courtesy B.Steffen (DESY)

- RF techniques



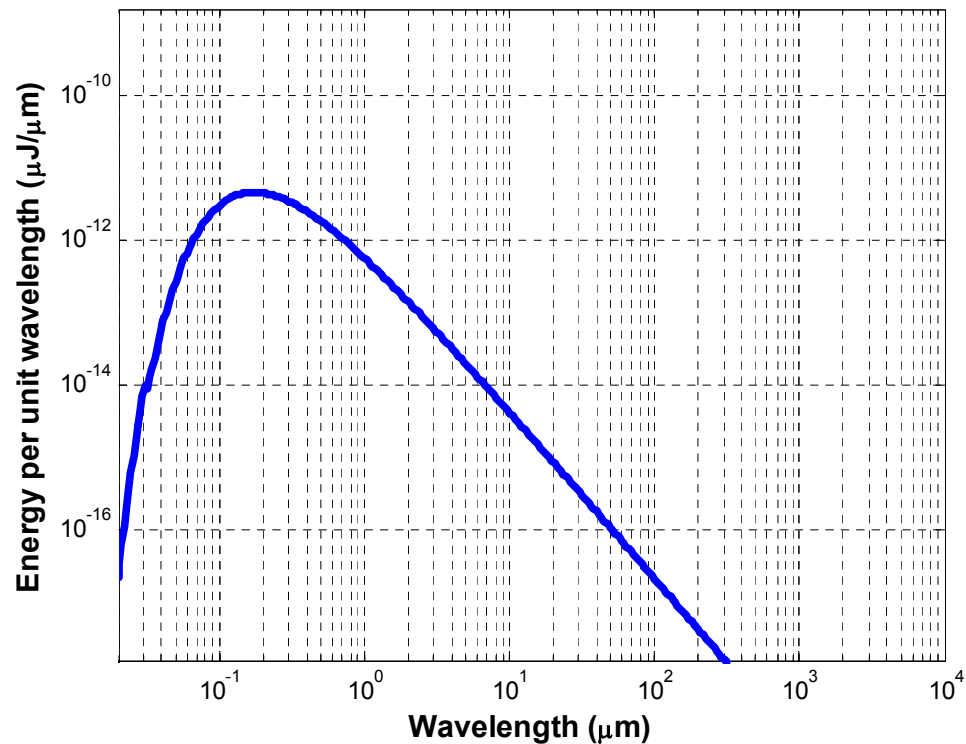
courtesy P.Emma (SLAC)

and more ...

Basic Principle of CRD

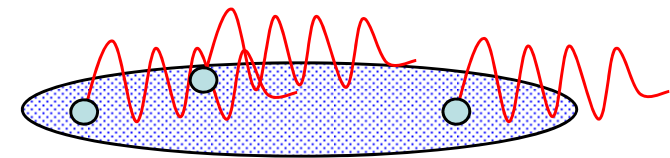
- single electron synchrotron radiation spectrum

 - ▶ circular motion, $E = 130 \text{ MeV}$, $\rho = 1.6 \text{ m}$

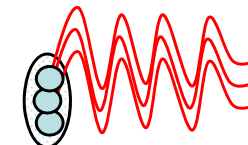


- longitudinal coherence

long bunch ($\lambda < \sigma_z$)



short bunch ($\lambda > \sigma_z$)

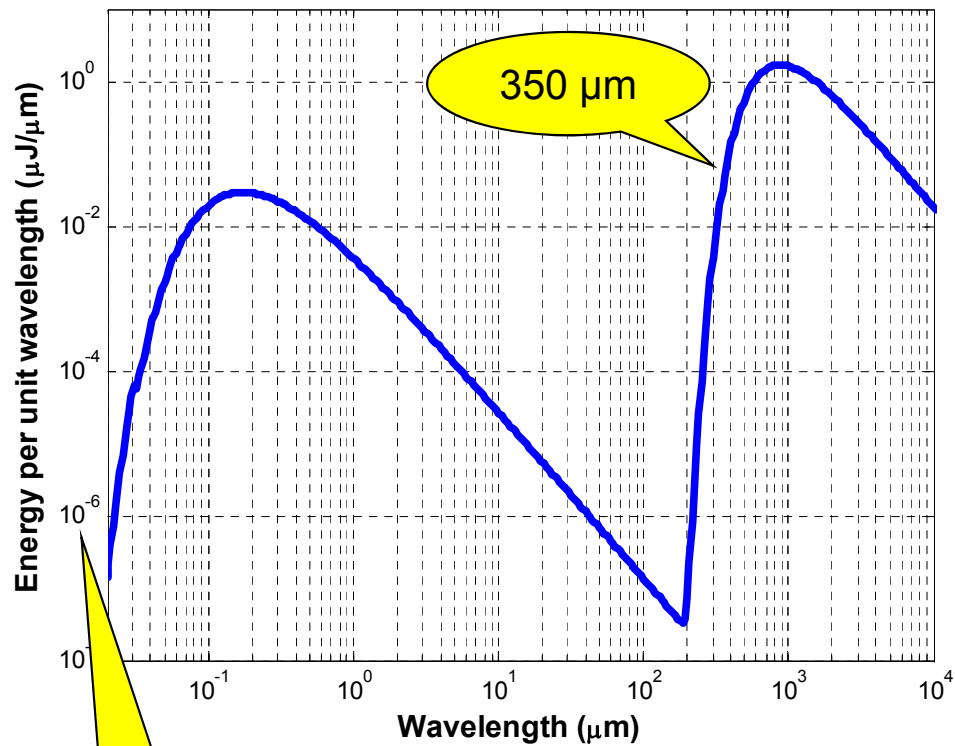


Courtesy O. Grimm (DESY)

Basic Principle of CRD

● synchrotron radiation spectrum for charge 1 nCb

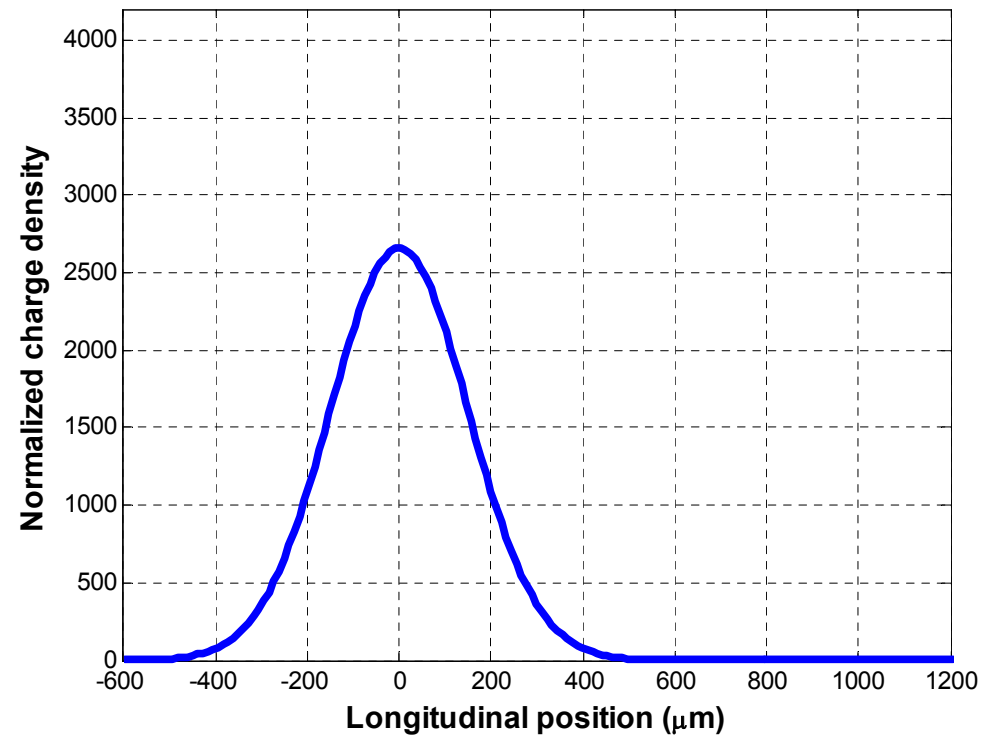
➤ circular motion, $E = 130 \text{ MeV}$, $\rho = 1.6 \text{ m}$



Scale change

Gaussian (line) bunch

FWHM=350 μm

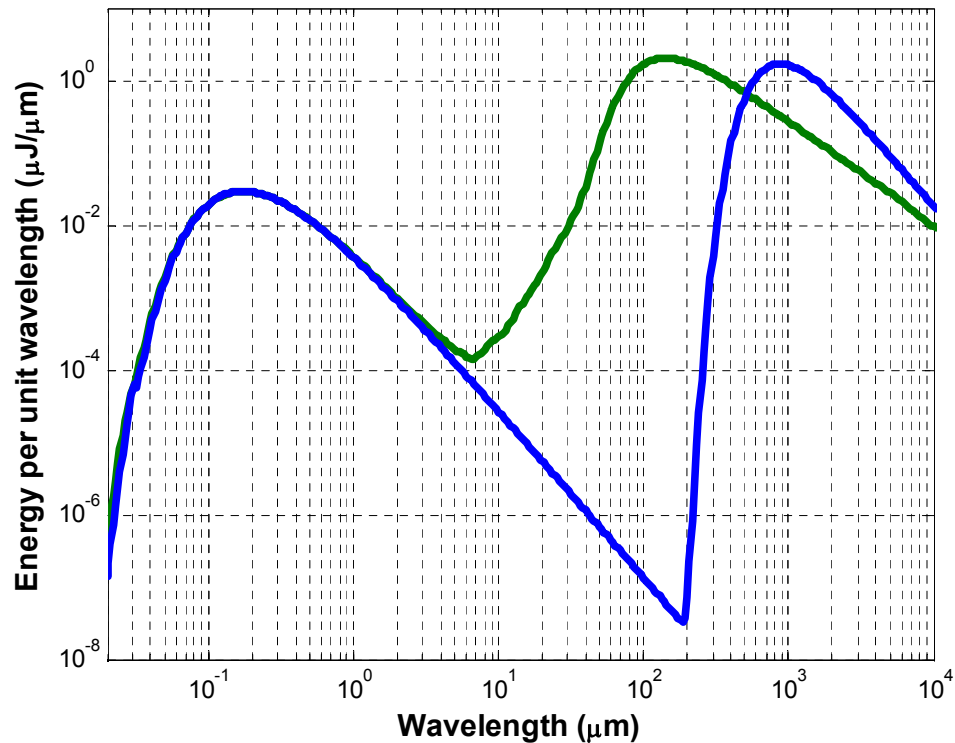


Courtesy O. Grimm (DESY)

Basic Principle of CRD

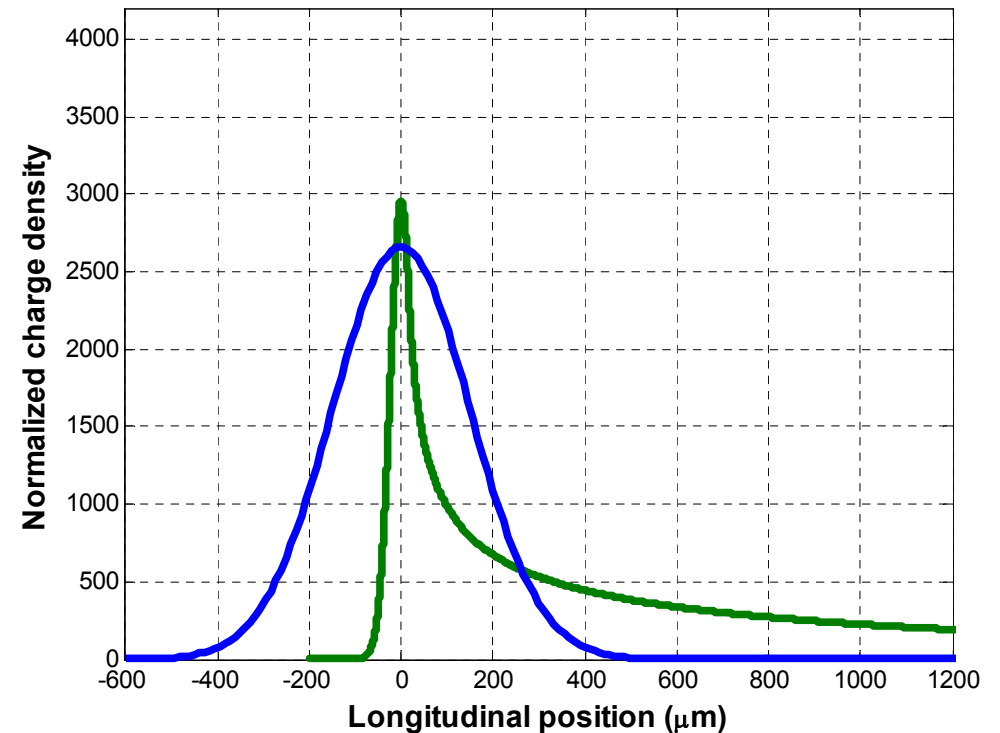
● synchrotron radiation spectrum for charge 1 nCb

➤ circular motion, $E = 130 \text{ MeV}$, $\rho = 1.6 \text{ m}$



Spiked bunch

FWHM=70 μm

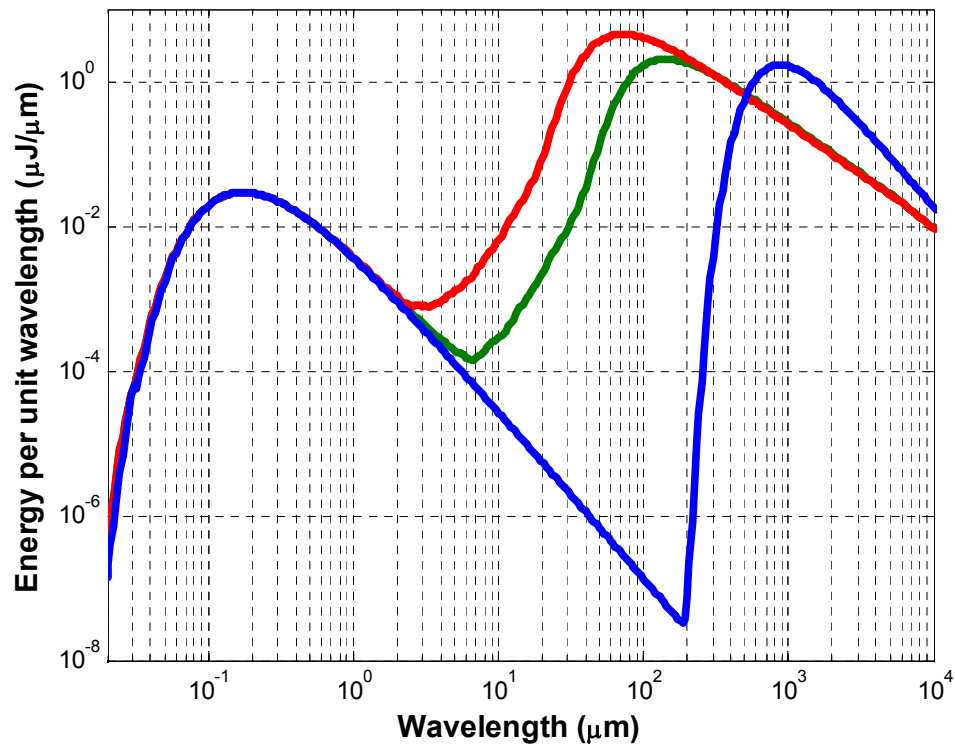


Courtesy O. Grimm (DESY)

Basic Principle of CRD

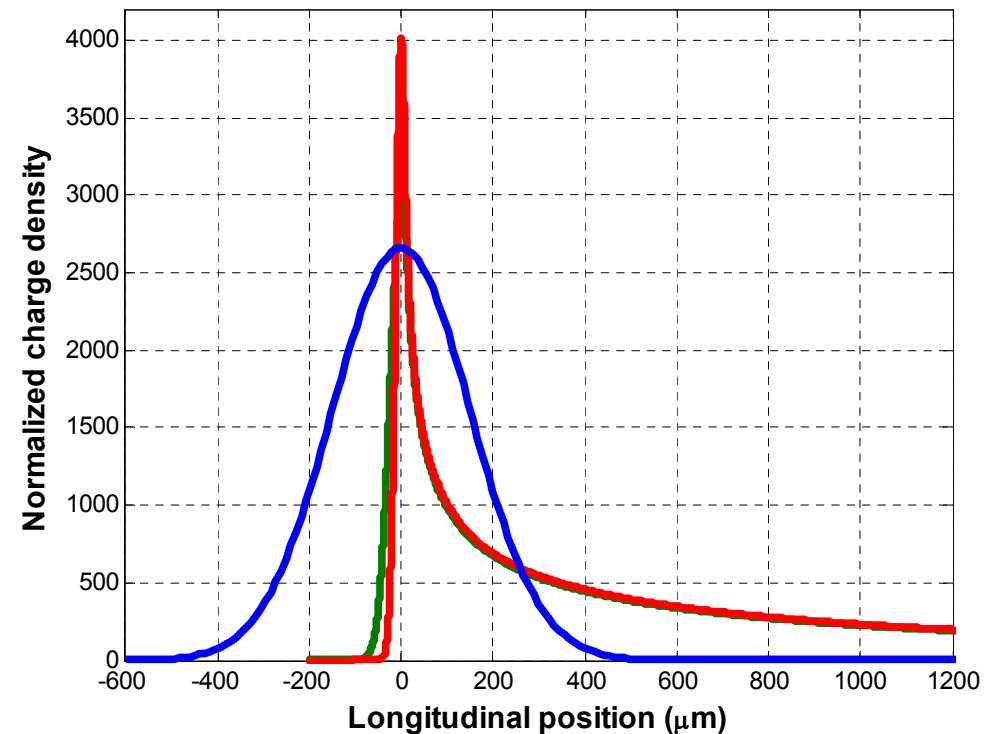
● synchrotron radiation spectrum for charge 1 nCb

➤ circular motion, $E = 130 \text{ MeV}$, $\rho = 1.6 \text{ m}$



Spiked bunch

FWHM=40 μm

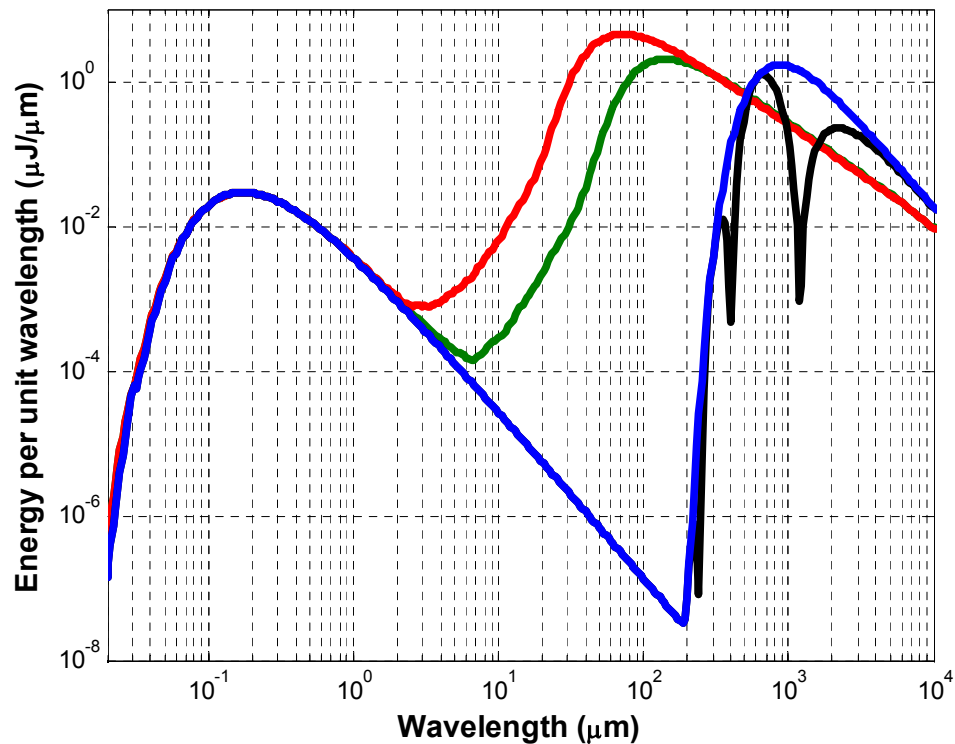


Courtesy O. Grimm (DESY)

Basic Principle of CRD

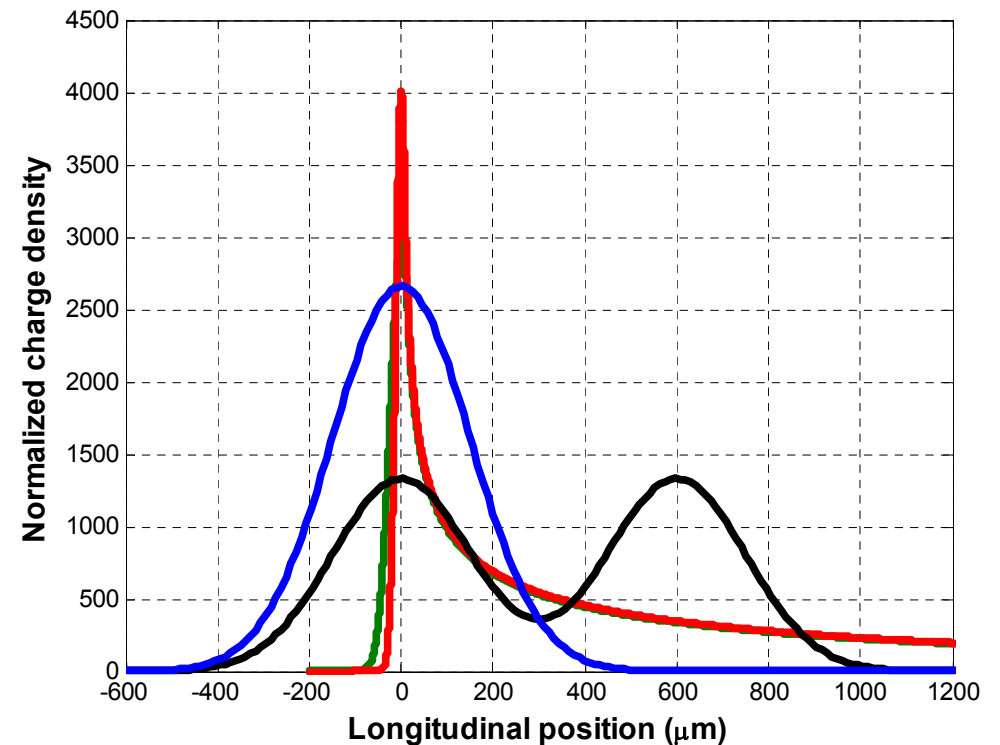
● synchrotron radiation spectrum for charge 1 nCb

➤ circular motion, $E = 130 \text{ MeV}$, $\rho = 1.6 \text{ m}$



Double Gaussian Bunch

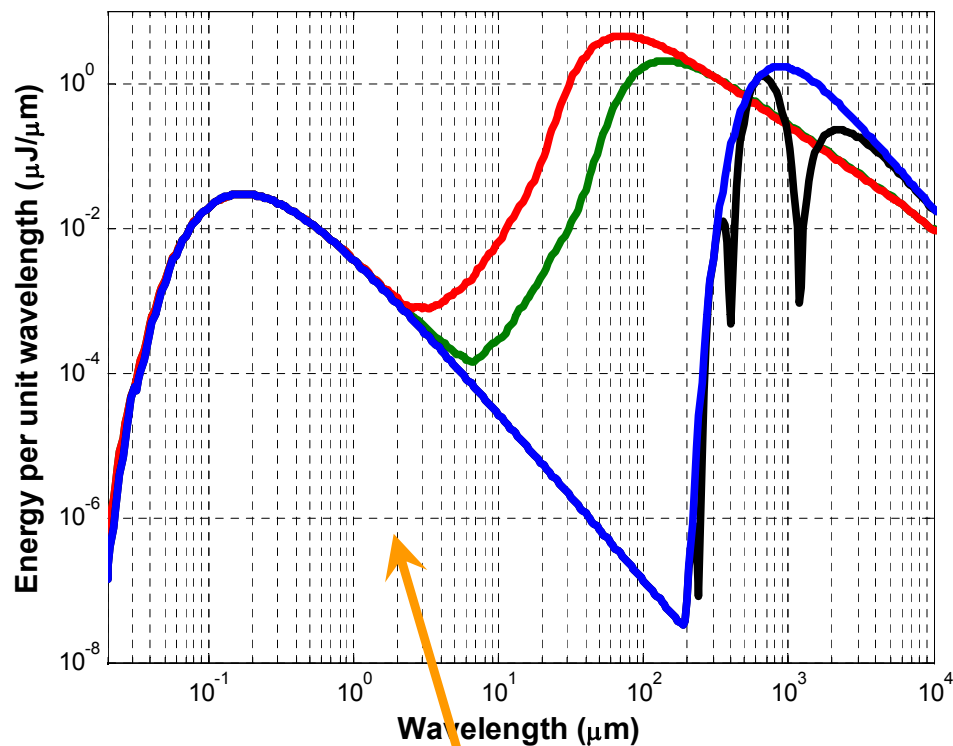
FWHM=350 μm , $\Delta=600 \mu\text{m}$



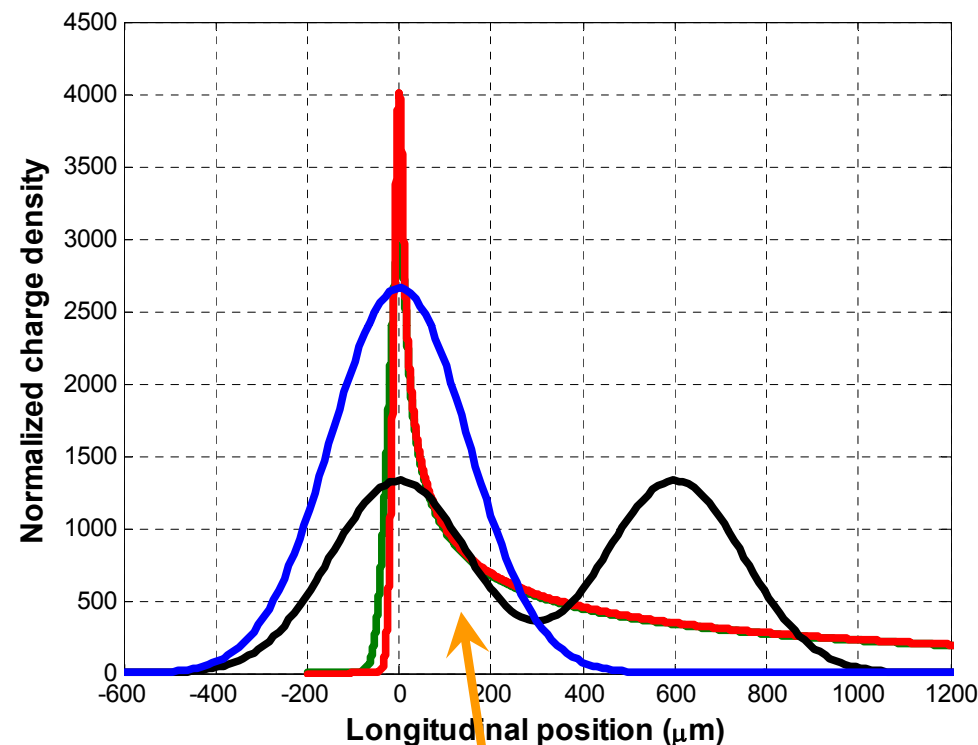
Courtesy O. Grimm (DESY)

Basic Relation of CRD

Courtesy O. Grimm (DESY)



Double Gaussian Bunch
FWHM=350 μm, Δ=600 μm

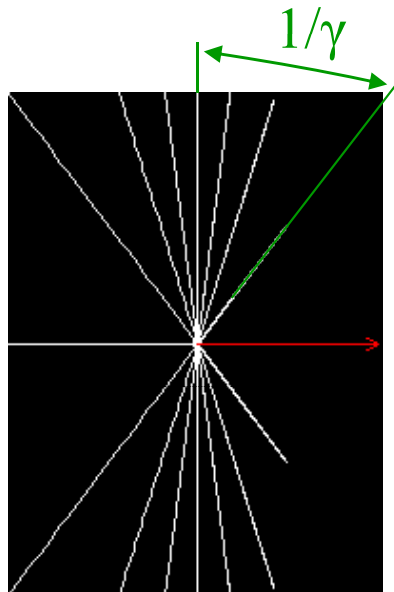


$$\frac{dU}{d\lambda} = \left(\frac{dU}{d\lambda} \right)_1 \left(N + N(N-1) |F(\lambda)|^2 \right) \quad F(\lambda) = \int S(z) e^{\frac{2\pi iz}{\lambda}} dz$$

→ Emission spectrum depends on *longitudinal* charge distribution

Radiation Generation

radiation generation via particle electromagnetic field



electric field lines
in LAB frame

Lorentz factor

$$\gamma = E / m_0 c^2$$

E : total energy

$m_0 c^2$: rest mass energy

$\gamma \rightarrow \infty$: plane wave

➤ $mc^2 = 0$ MeV :

light → „real photon“

➤ ultra relativistic energies : idealization → „virtual photon“

exploit analogy between real/virtual photons:

- light reflection/refraction at surface ↔ backward/forward transition radiation (TR)
- light diffraction at edges ↔ diffraction radiation (DR)
- light diffraction at grating ↔ Smith-Purcell radiation

Radiation Source

reminder: coherent radiation diagnostics

- principle: bunch length/shape dependent emission spectrum of coherent radiation

single particle spectrum bunch form factor

$$\frac{dU}{d\lambda} = \left(\frac{dU}{d\lambda} \right)_1 \left(N + N(N-1) |F(\lambda)|^2 \right)$$

no. of particles per bunch

with

$$F(\lambda) = \int dz S(z) e^{i \frac{2\pi z}{\lambda}}$$

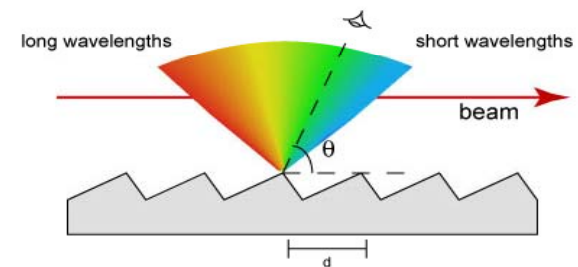
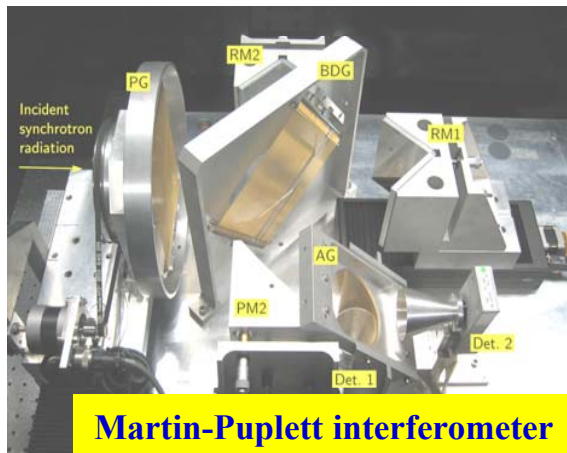
bunch profile

- spectral decomposition and Fourier transform:
 - bunch length and shape

- transition radiation (TR), diffraction radiation (DR):
 - polychromatic angular distribution
 - spectrometer for decomposition

- Smith-Purcell radiation (SPR):
 - (virtual) photon diffraction at 1D Bravais-structure
 - grating provides discrete momenta $p_n = n 2\pi\hbar / d$
 - angular distribution wavelength-dependent

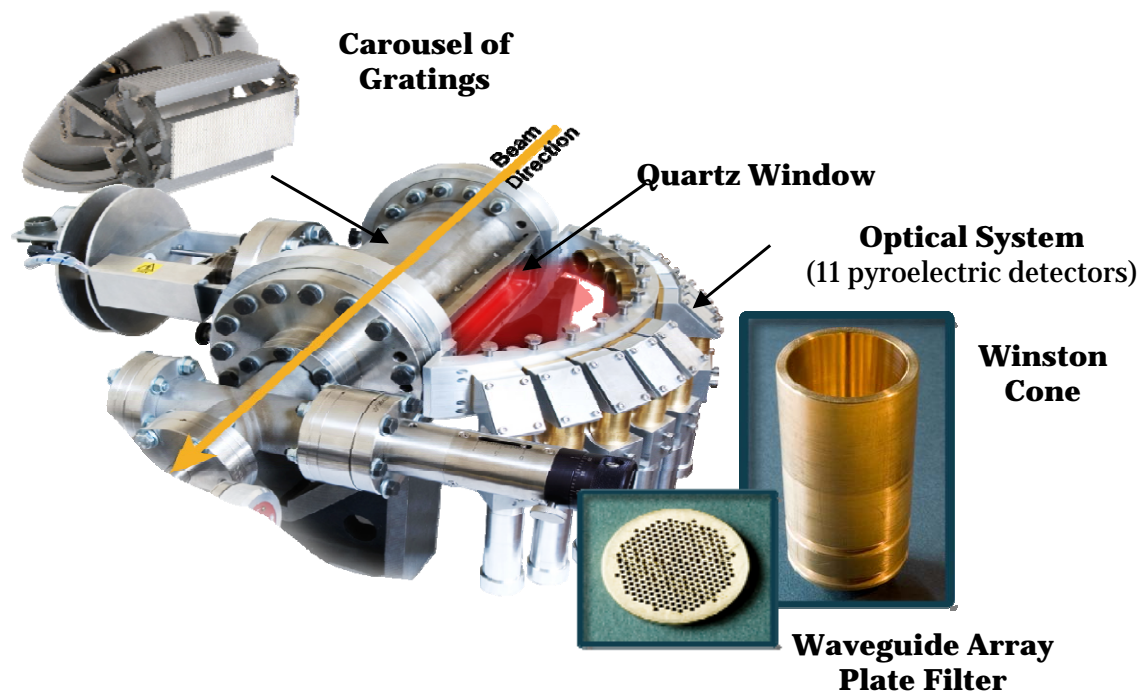
→ no additional spectrometer



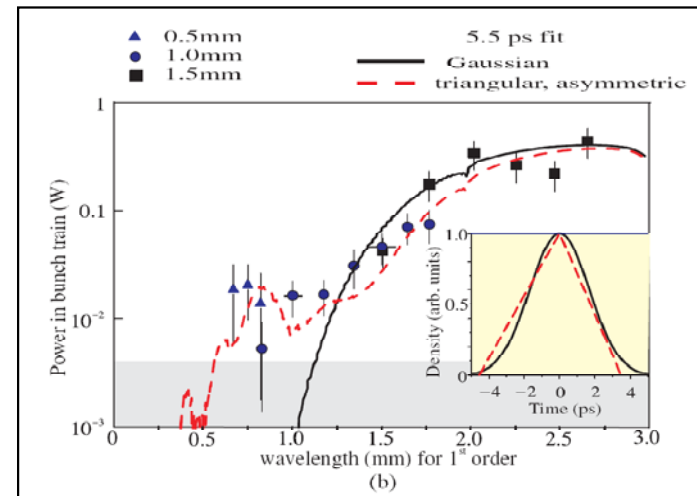
SPR Bunch Length Diagnostics

- bunch length monitor based on Smith-Purcell radiation

Measurement at 45 MeV, FELIX



Courtesy G. Doucas, V. Blackmore (Oxford)



G. Doucas et al., PRST 9 (2006) 092801

Experiment at 28.5 GeV, SLAC

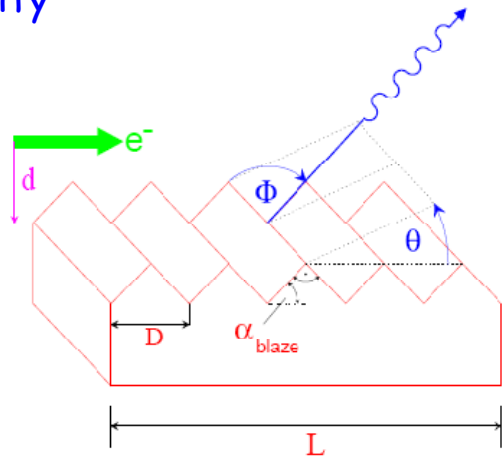
V.Blackmore et al., PRST 12 (2009) 032803

- critical items

- number of detectors limits the number of points for reconstruction
→ interferometer: about 200 points
- influence of the grating structure

Smith-Purcell Radiation

intensity



$$\frac{d\dot{N}}{d\Omega} = \alpha \cdot n \cdot \frac{I}{e} \cdot \frac{L}{D} \cdot |R_n|^2 \cdot \frac{\sin^2 \theta \cdot \sin^2 \Phi}{(1/\beta - \cos \theta \cdot \sin \Phi)^2} \cdot e^{-\kappa \cdot d}$$

- α : fine structure constant
- n : diffraction order
- I : beam current
- e : elementary charge
- D : spacing of grooves
- L : grating length
- d : distance between beam and grating surface
- R_n : radiation factor, $R_n = R_n(\gamma, \theta, \Phi, \alpha_{blaze})$
- θ, Φ : angle of observation
- κ : evanescent scale, $\kappa = h_{int}^{-1} \cdot \sqrt{1 + (\beta\gamma \cos \Phi)^2}$
- h_{int} : interaction length

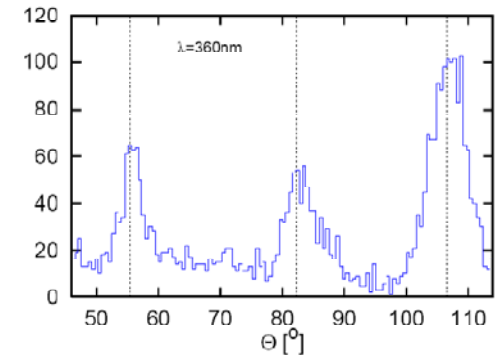
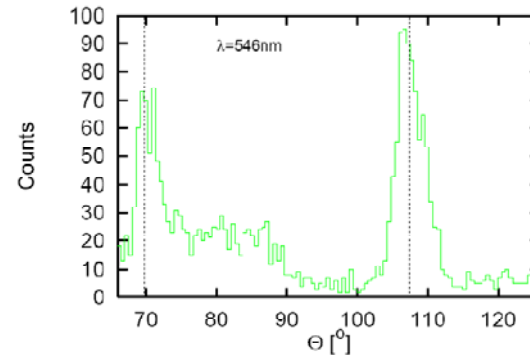
$$h_{int} = \frac{\beta\gamma}{4\pi} \cdot \lambda$$

P.M.van den Berg, J.Opt.Soc.Am. 63 (1973) 1588

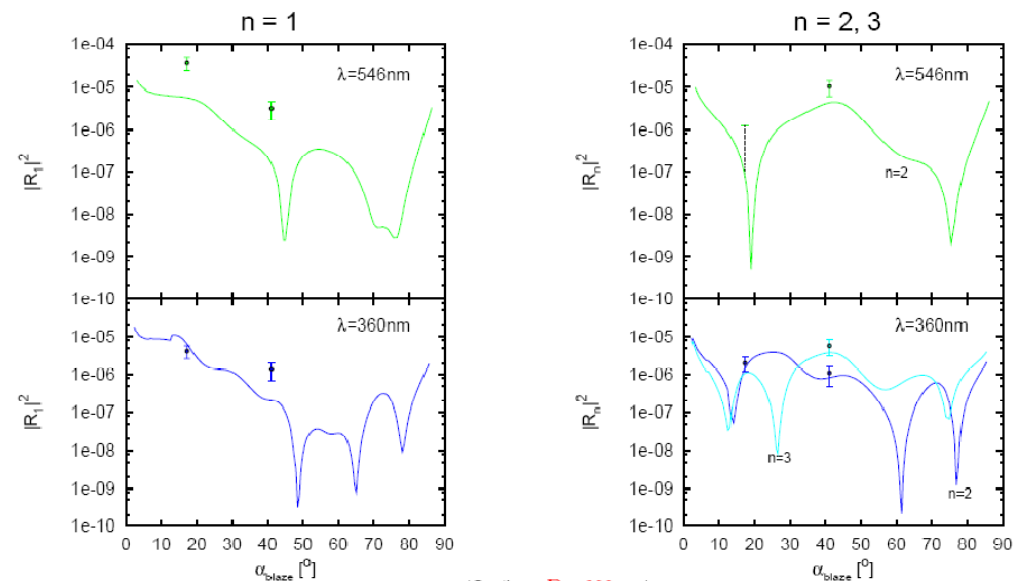
coherence condition

$$n\lambda = D(1/\beta - \cos \Theta)$$

$E = 855 \text{ MeV}$, $D = 833 \text{ nm}$, $\alpha_{blaze} = 41.12^\circ$



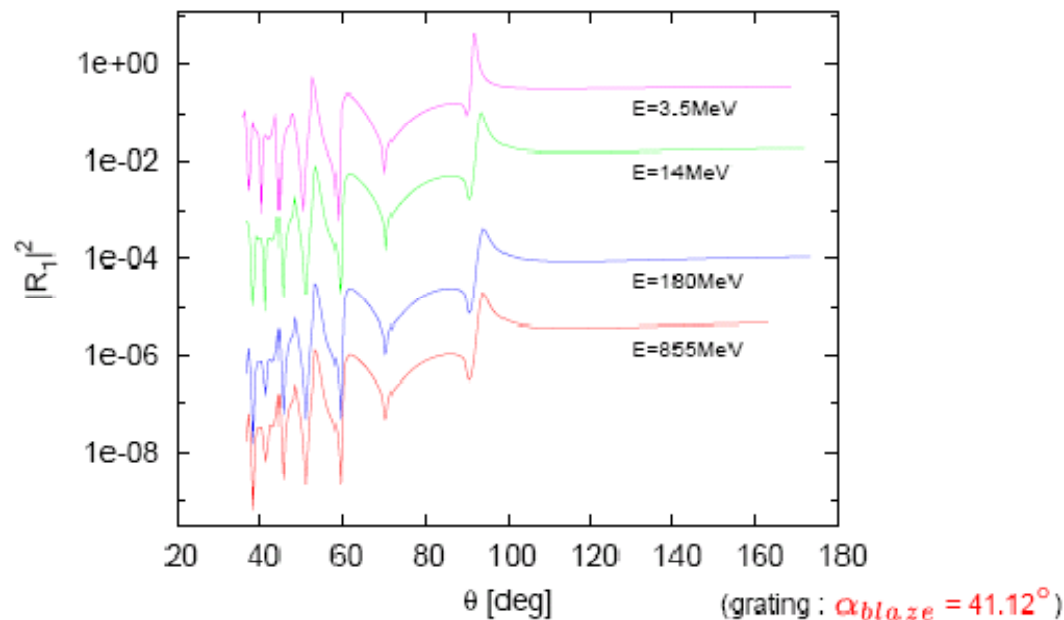
radiation factor



G.Kube et al., Phys.Rev. E 65 (2002) 056501

SP Radiation Factors

radiation factors for blazed gratings



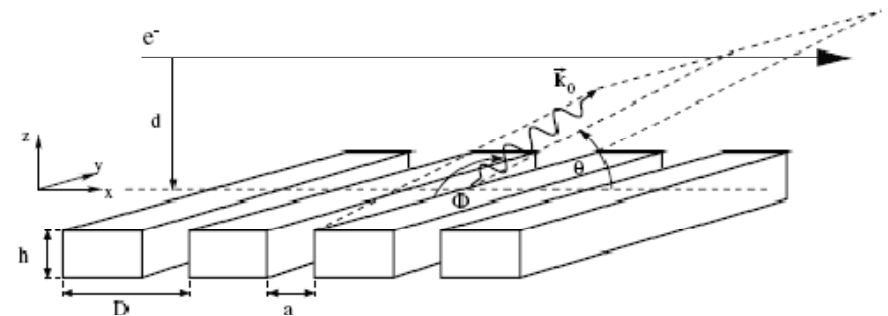
P.M.van den Berg, J.Opt.Soc.Am. 63 (1973) 1588

- pronounced resonance structures
 - Wood-Rayleigh anomalies (optical grating theories)
- strong modification of $\frac{dU}{d\lambda}$
 - decreased sensitivity on bunch length

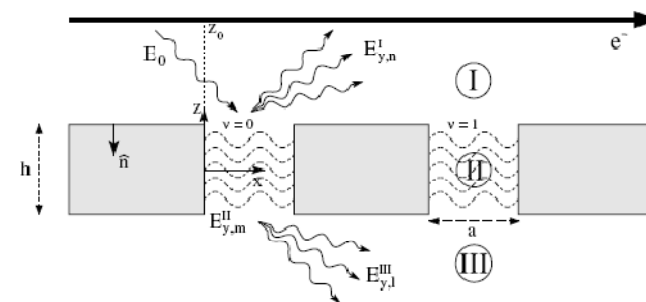
G.Kube, Proc. DIPAC '03, Mainz (Germany) 2003, p.40

volume strip grating

G.Kube, Nucl.Instrum.Meth. B 227 (2005) 180



- solution for reflected and transmitted field
 - modal expansion

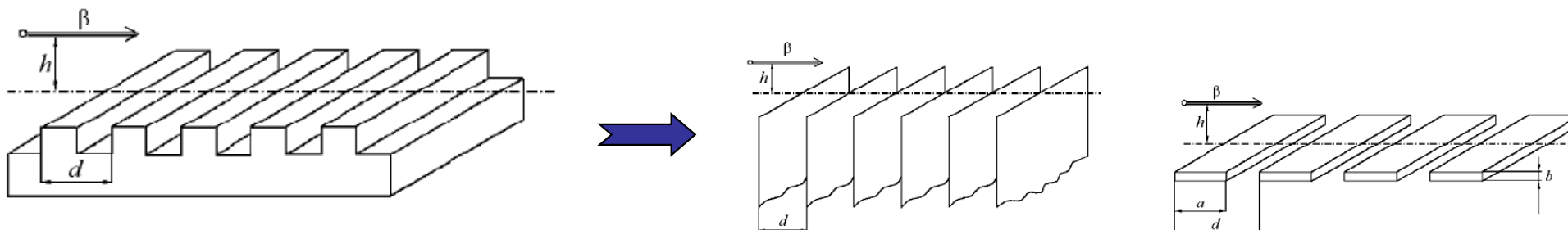


- limit $h \rightarrow 0$:
 - influence of resonances to neglect
 - better suited for bunch length diagnostics

- Smith-Purcell radiation from periodic stack of diffraction radiators

A.P.Potylitsyn, Nucl.Instrum.Meth. B 145 (1998) 60

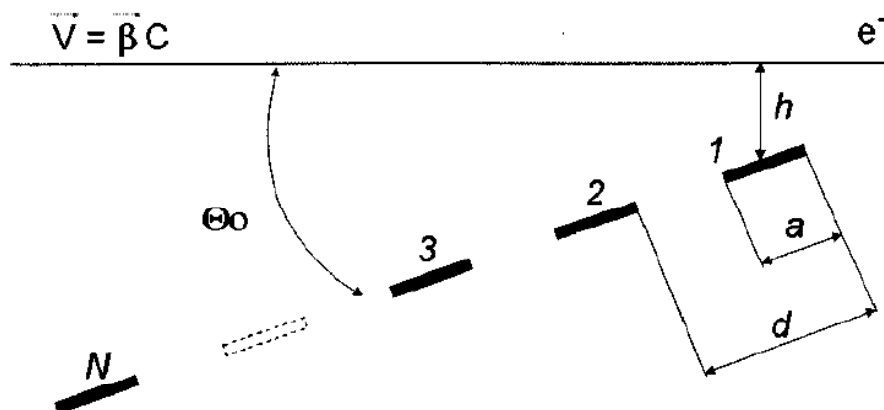
A.P.Potylitsyn and M.N.Strikhanov, Rus.Phys.J. 45 (2002) 905



Resonant Diffraction Radiation

- Resonant diffraction radiation from inclined target

A.P.Potylitsyn, P.V.Karataev and G.A.Naumenko, Phys.Rev. E 61 (2000) 7039



RDR from inclined Targets

... and application for bunch length diagnostics

A.P.Potylytsyn, D.V.Karlovetz, G.Kube, Nucl.Instrum.Meth. B 226 (2008) 3781

critical items

- ▶ number of detectors limits the number of points for reconstruction
 - use of one/two detectors at fixed positions
 - variation of grating inclination angle wrt. beam axis
 - reduced number of detectors has additional advantage:
sensitivity of each individual detector must be known with high accuracy
(reconstruction of bunch shape relies on absolute intensities)
- ▶ influence of the grating structure
 - use strip grating instead of reflection grating to avoid resonance structures
 - strip grating allows to exploit transmitted and reflected radiation at the same time

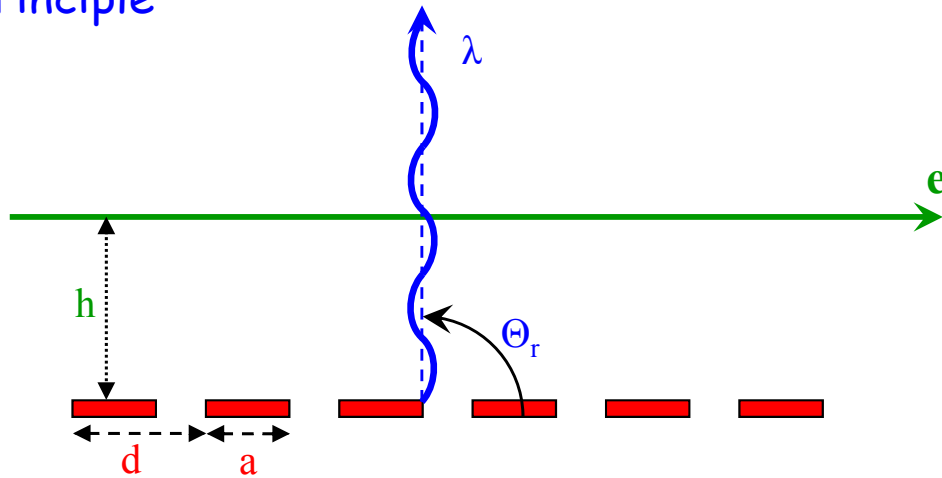
proposed DITANET project

- ▶ experiment to be carried out at 100 MeV injector linac of Swiss Light Source (PSI)
- ▶ develop monitor for beam tuning (no high resolution measurements)
- ▶ collaboration between DESY, PSI and Tomsk Polytechnic University (Russia)
- ▶ looking for Experienced Researcher

... still searching for suitable candidate

RDR for Bunch Length Diagnostics

- principle

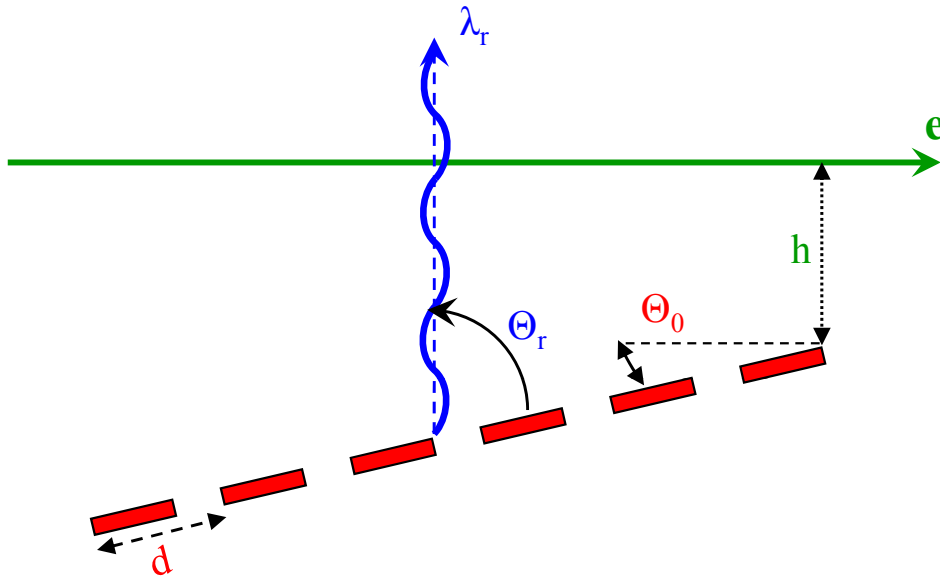


- ▶ coherence condition

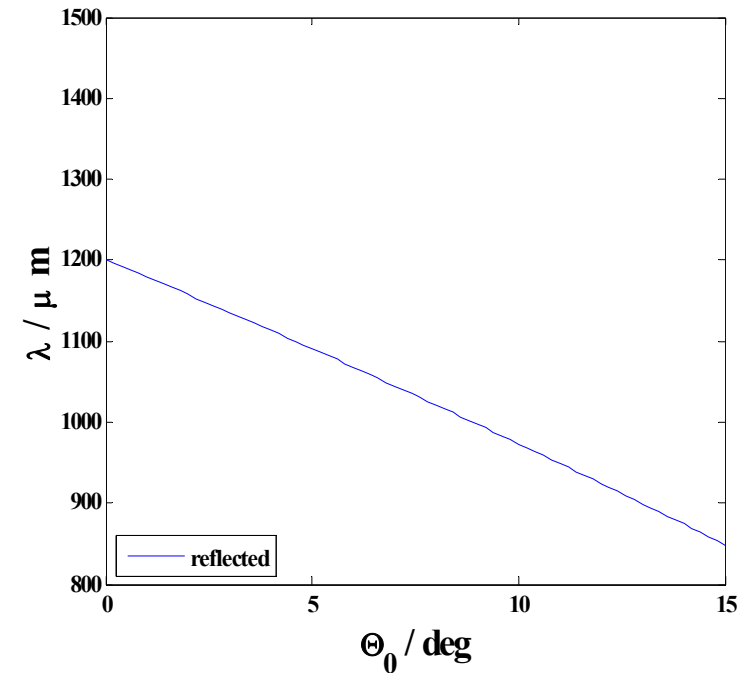
$$n\lambda = d \left(\frac{1}{\beta} - \cos \Theta \right)$$

RDR for Bunch Length Diagnostics

- principle



- ▶ spectral decomposition



$n = 1, d = 1.2 \text{ mm}, \gamma = 200$

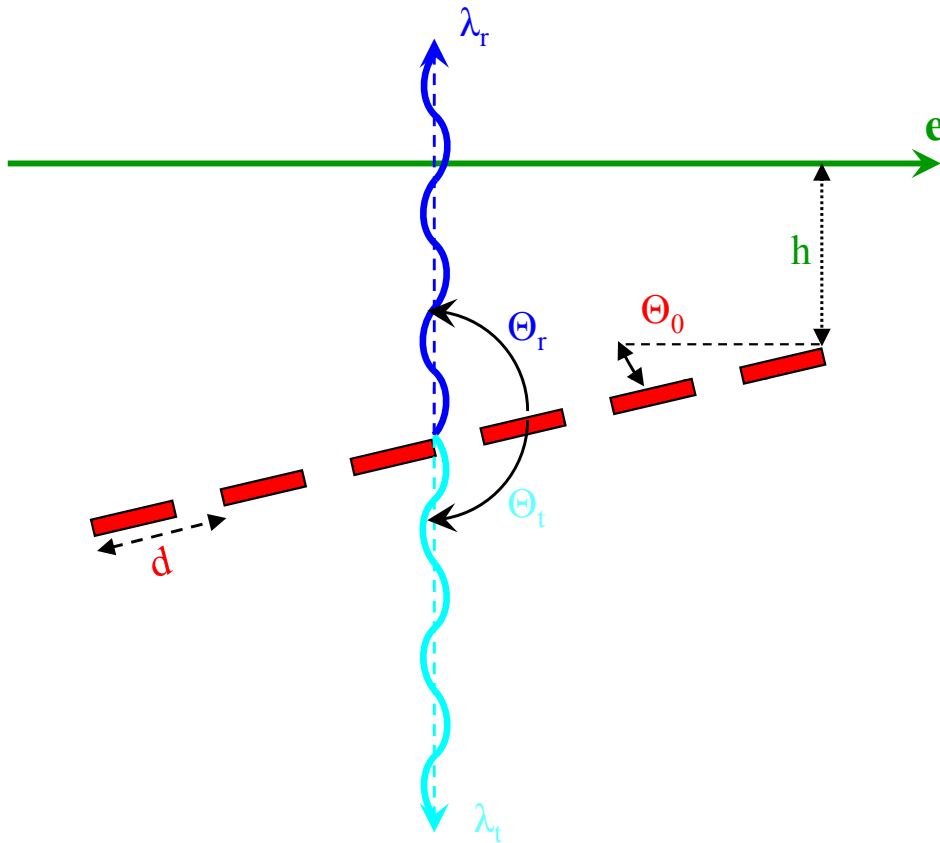
- ▶ coherence condition

$$n\lambda = d \left(\cos \Theta_0 / \beta - \cos(\Theta - \Theta_0) \right)$$

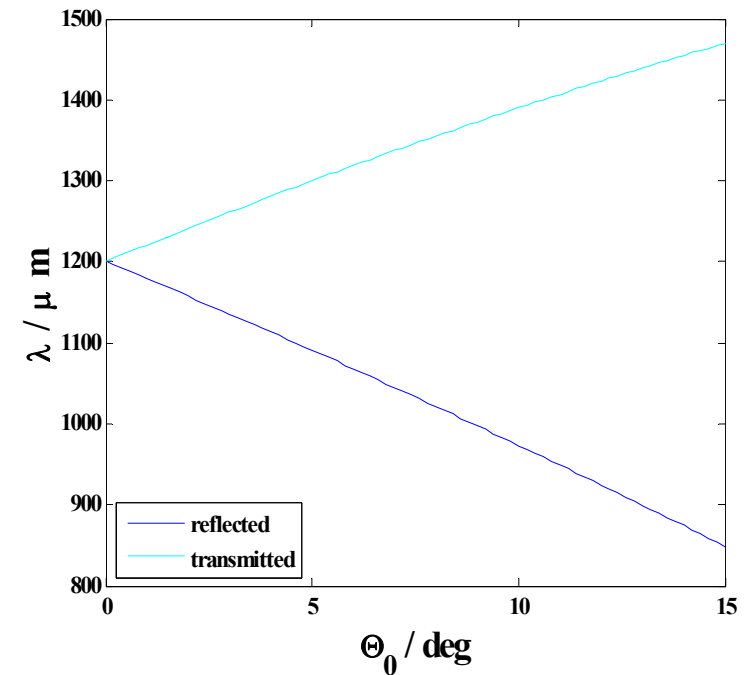
with $\Theta = \Theta_r = + 90^\circ$

RDR for Bunch Length Diagnostics

- principle



- spectral decomposition



$$n = 1, d = 1.2 \text{ mm}, \gamma = 200$$

- coherence condition

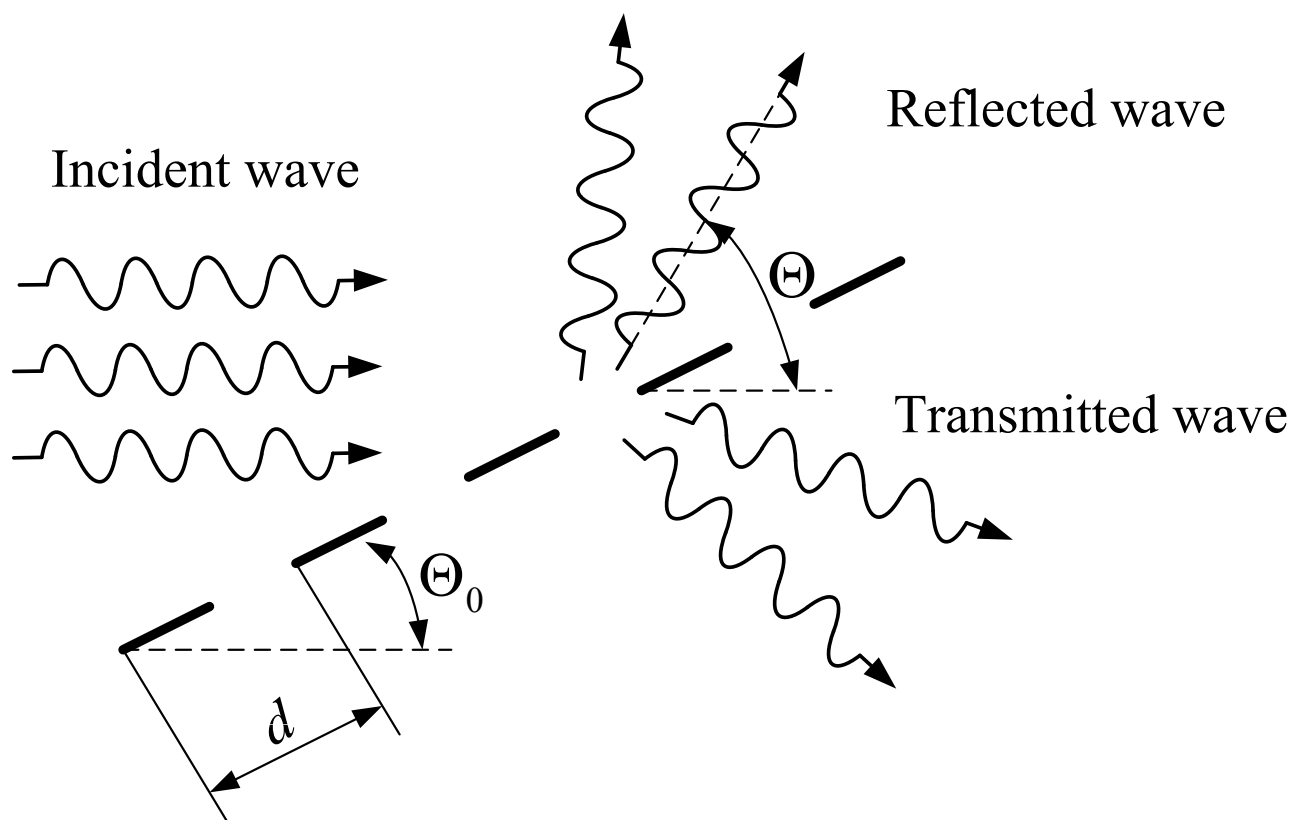
$$n\lambda = d \left(\cos \Theta_0 / \beta - \cos(\Theta - \Theta_0) \right)$$

with $\Theta = \Theta_r = +90^\circ$

$\Theta = \Theta_t = -90^\circ$

Optical Analogon

Analogy from classical optics:
semi-transparent grating

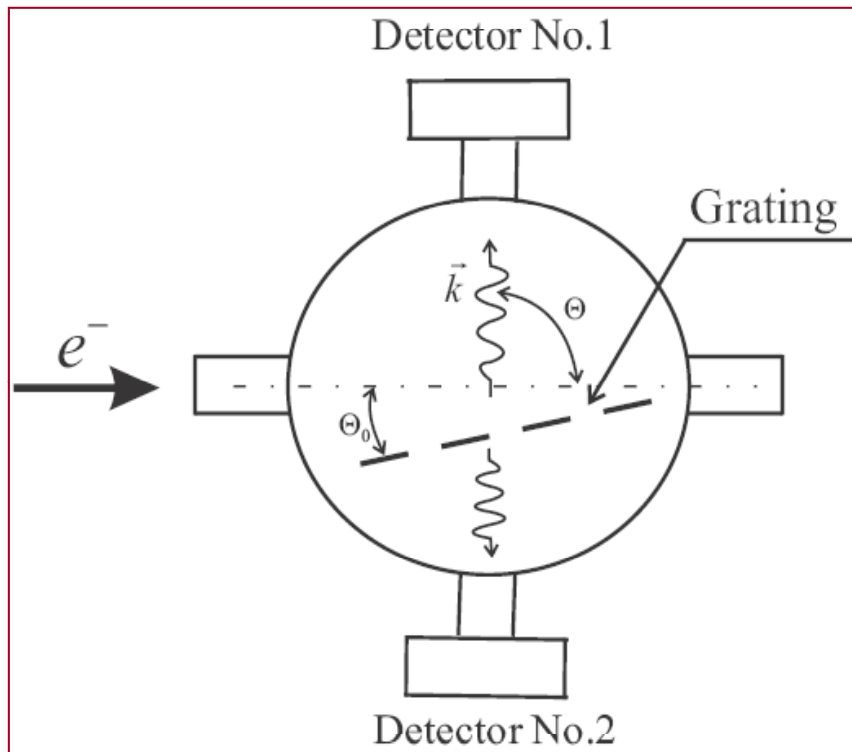


$$\lambda_n = \frac{d}{n} (\cos \Theta_0 - \cos(\Theta_0 - \Theta))$$

$$\lambda_n = \frac{d}{n} (\cos \Theta_0 - \cos(\Theta_0 + \Theta))$$

Proposed RDR Experiment

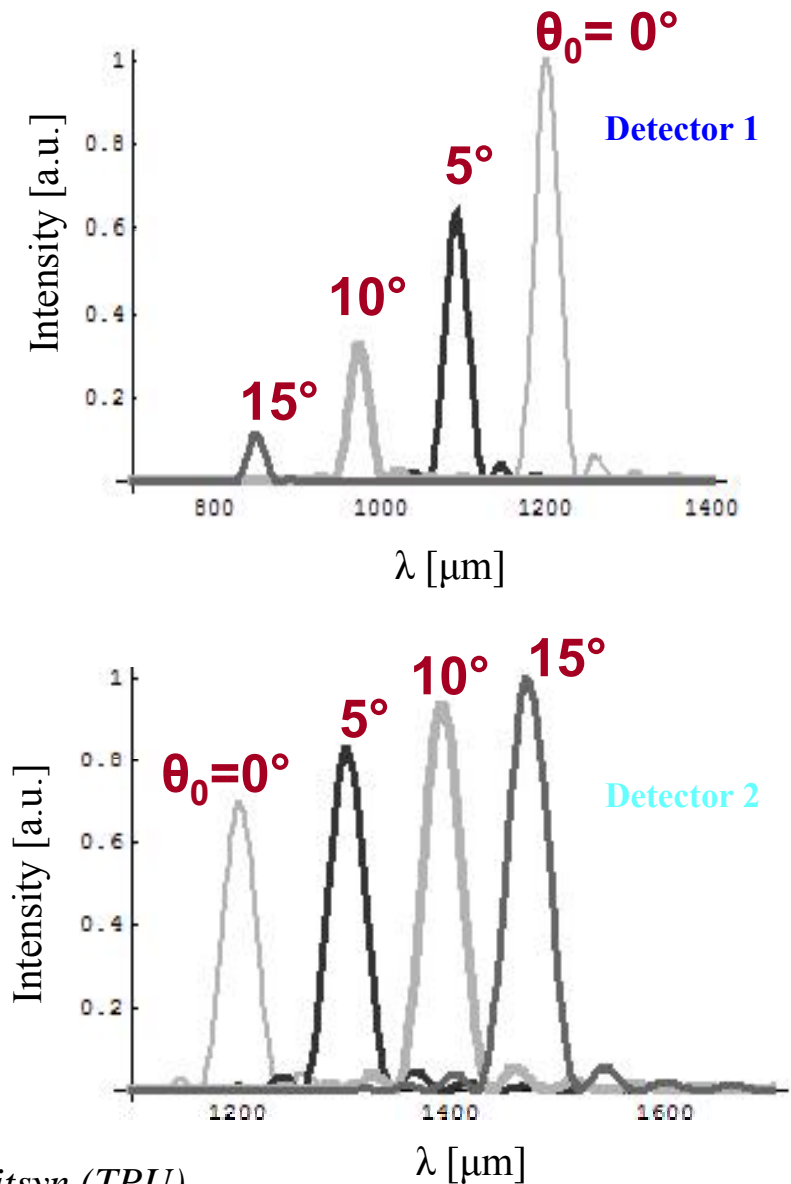
● experimental scheme



➤ parameters

grating period	$d = 1.2 \text{ mm}$
number of grating strips	$N = 30$
beam energy	$\gamma = 200$
bunch length (Gaussian)	$\sigma = 0.44 \text{ mm}$
observation angle	$\Theta = \pm 90^\circ$

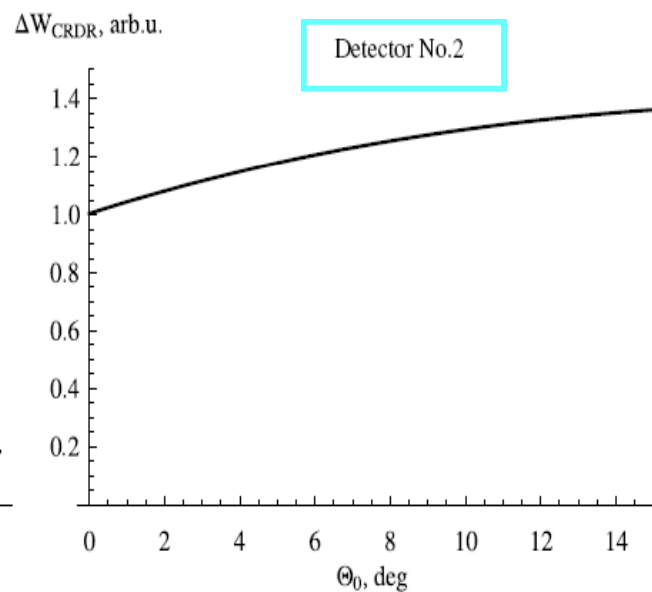
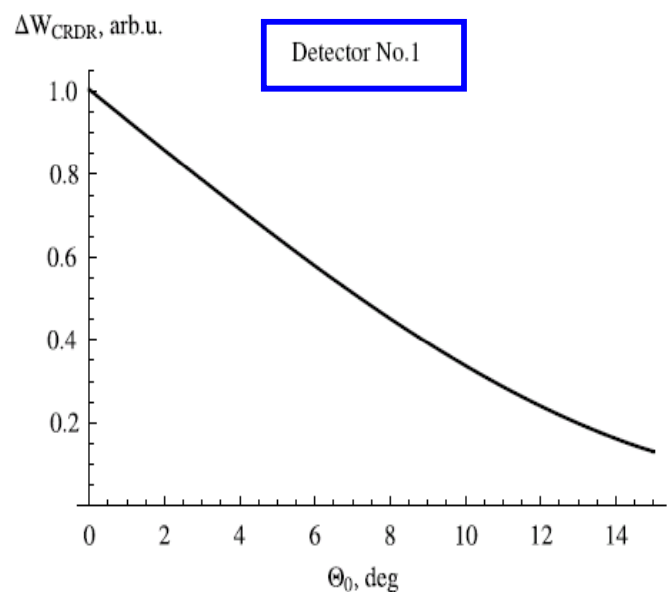
● signature



Courtesy A.P. Potylitsyn (TPU)

RDR Intensity Dependence

● intensity dependence



► parameters

grating period	$d = 1.2 \text{ mm}$
strip width	$a = d/2$
number of periods	$N = 30$
beam energy	$\gamma = 200$
bunch length (Gaussian)	$\sigma = 0.44 \text{ mm}$
observation angle	$\Theta = \pm 90^\circ$
detector aperture	$S = 1 \text{ cm}^2$
distance detector/grating	$r_0 = 1 \text{ m}$

- **detector 1:** increase of grating tilt angle Θ_0
- wavelength shift to smaller λ
 - reduced contribution of coherent emission
 - **intensity decrease**

- **detector 2:** increase of grating tilt angle Θ_0
- wavelength shift to larger λ
 - increased contribution of coherent emission
 - **intensity increase**

...parameter optimization to increase sensitivity

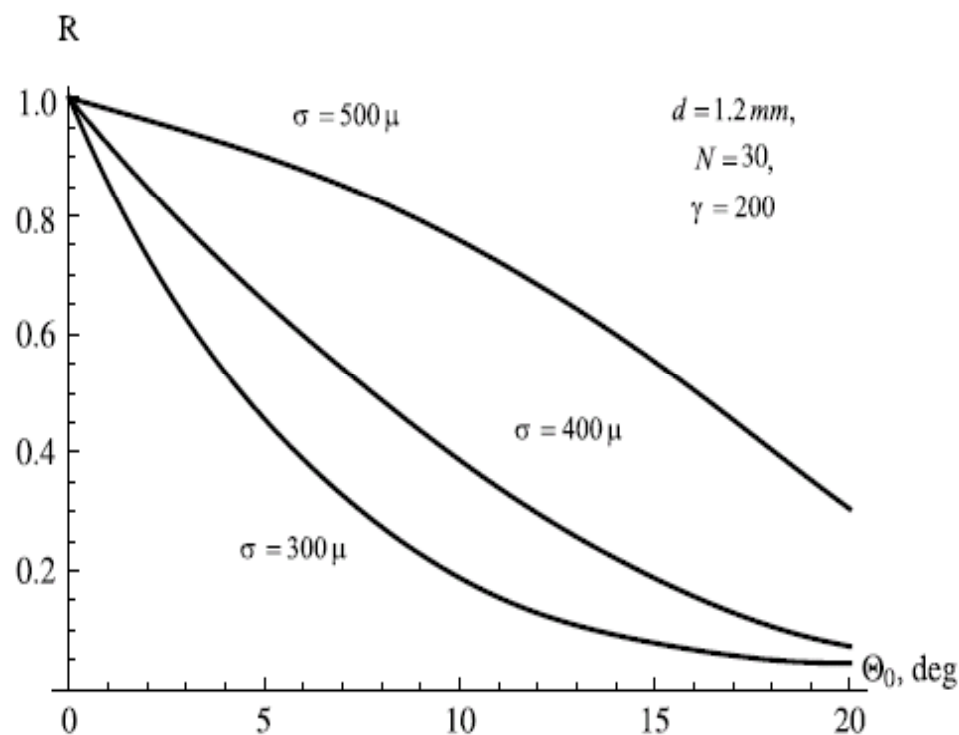
RDR Signal Ratio

● difficulty

- ▶ knowledge of absolute intensity required
- ▶ spectral response of each individual element must be known to high level of accuracy

● simplification

- ▶ intensity ratio of D1/D2



- ▶ ratio sensitive on beam size variation
- ▶ prerequisite: detectors with flat response

→ **simple monitor for beam tuning**

RDR Power Estimation

coherent RDR yield for parallel orientation

grating period	$d = 1.2 \text{ mm} \rightarrow \lambda = 1.2 \text{ mm}$
strip width	$a = d/2$
number of periods	$N = 30$
tilt angle	$\Theta_0 = 0^\circ$
beam energy	$\gamma = 200$
bunch length (Gaussian)	$\sigma = 0.44 \text{ mm}$
distance beam/grating	$h = 2 \text{ mm}$
observation angle	$\Theta = \pm 90^\circ$



$$\frac{dW_{CRDR}}{d\Omega} \approx 3 \cdot 10^{13} \frac{\text{eV}}{\text{sr bunch}}$$

measured yield

detector aperture	$S = 1 \text{ cm}^2$
distance detector/grating	$r_0 = 1 \text{ m}$



$$\Delta W_{CRDR} \approx 0.5 \frac{\text{nJ}}{\text{bunch}}$$

estimated power level

$$P_{CRDR} \approx \Delta W_{CRDR} / \tau_b$$

τ_b : bunch duration $\approx 2.36 \sigma / c \approx 3.5 \text{ psec}$





$$P_{CRDR} \approx 140 \text{ W}$$

→ **high power level even allows use of broadband room-temperature detectors**

G. Naumenko, A. Potylitsyn, G. Kube, O. Grimm, V. Cha, Yu. Popov, Nucl.Instrum.Meth. A 603 (2009) 35

Summary & Conclusion

- coherent radiation as tool for bunch length diagnostics
- Smith-Purcell radiation suitable radiation source
 - dispersive emission process → no additional spectrometer required 
 - influence of grating structure → modification of intensity distribution 
- Smith-Purcell radiation from flat strip grating
- radiation from inclined target
 - resonant diffraction radiation
- monitor concept for bunch length monitoring based on RDR
 - experimental proof of principle still pending

⇒ END

