



# New Spiral Load RF Design

09.09.2020

Hikmet Bursali, Alexej Grudiev

# Outline

- Motivation
- Straight Load Model
- Design Process
  - Straight to Spiral Model
  - Spiral Model with WR90 Transition
  - Spiral Model with Vacuum Holes
  - Spiral Model with Pumping Port
- Reflection Optimisation
- Final RF Model
- Conclusion & Future Work

# Reminder

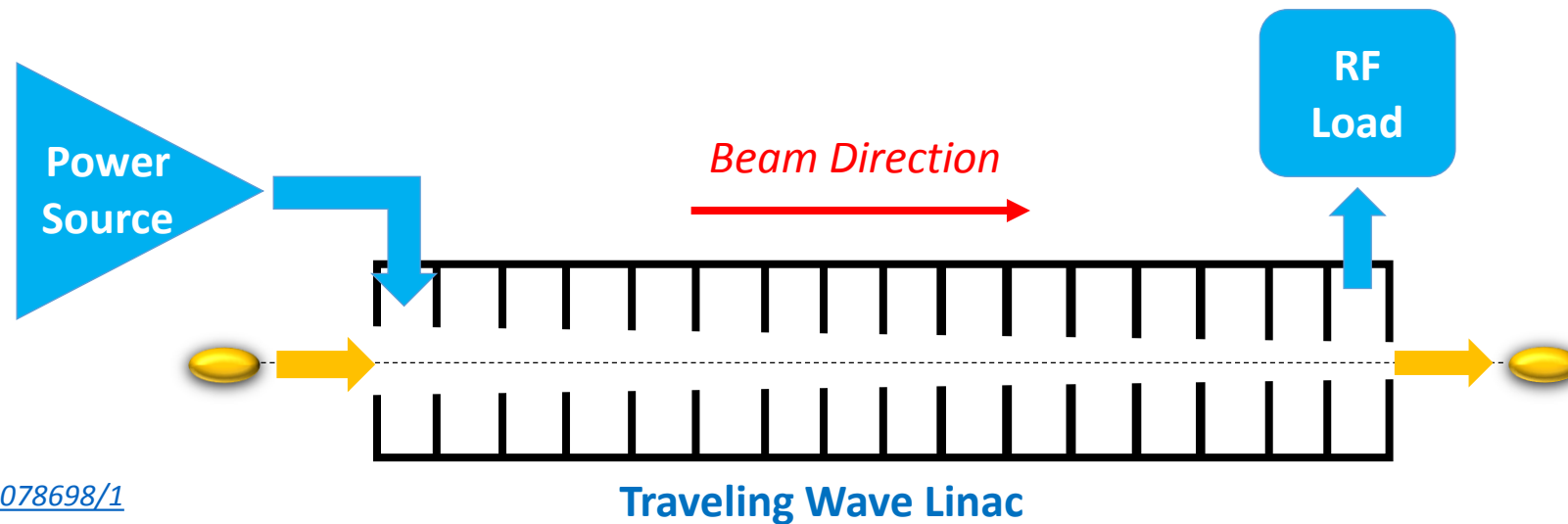
- Why do we use RF loads?

In order to absorb remaining RF power passing through the RF system. (Not used for beam acceleration or dissipated on resistive walls.)

(Ex: TD26CC  $P_{in} = 43.3\text{MW}$  – unloaded for 100MV/m)\*

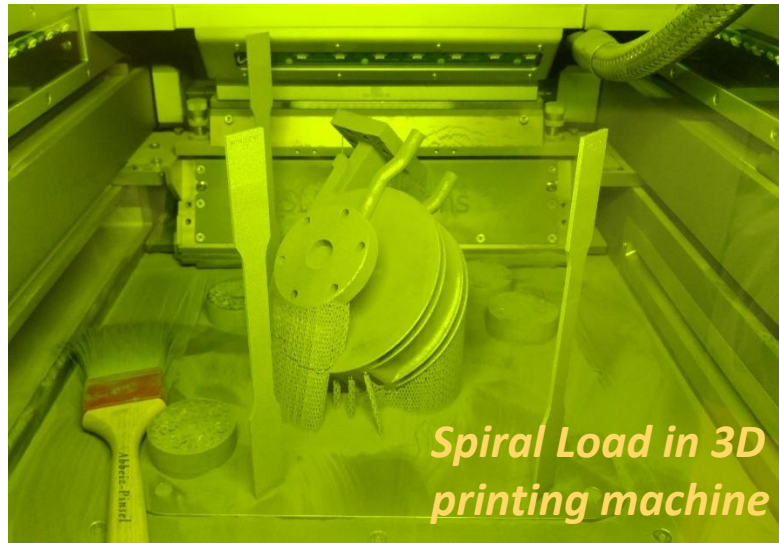
- Where do we use RF loads?

At the RF output of traveling wave type structures.



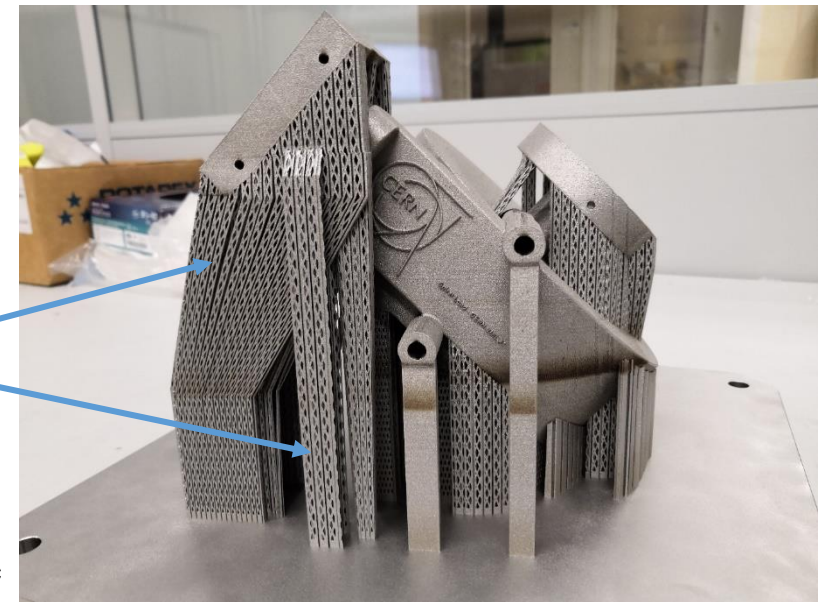
\*<https://edms.cern.ch/document/1078698/1>

# X-Band RF Loads (produced by Additive Manufacturing)



\*

- We have several RF spiral loads which were designed (CLIACOMP0071 , CLIACOMP0094), fabricated (at CERN or Vendor companies) and tested successfully. (Materials; Stainless-Steel "316L", Titanium alloy "Ti6A14V")
- For more info, please see the document; <https://edms.cern.ch/document/2323664/1>
- The current designs allow to produce only one load during an additive manufacturing cycle because of 45° oblique placing and 3D printing machine dimensions.



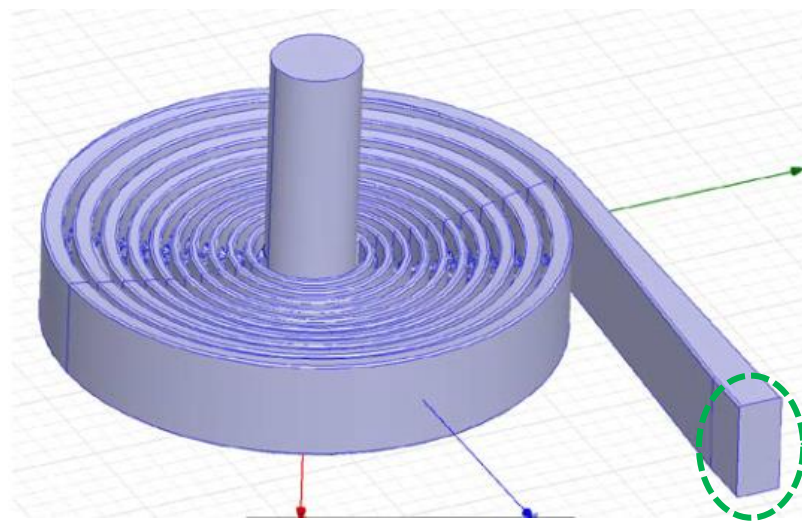
\*



\*Photos from Romain Gerard

# Motivation

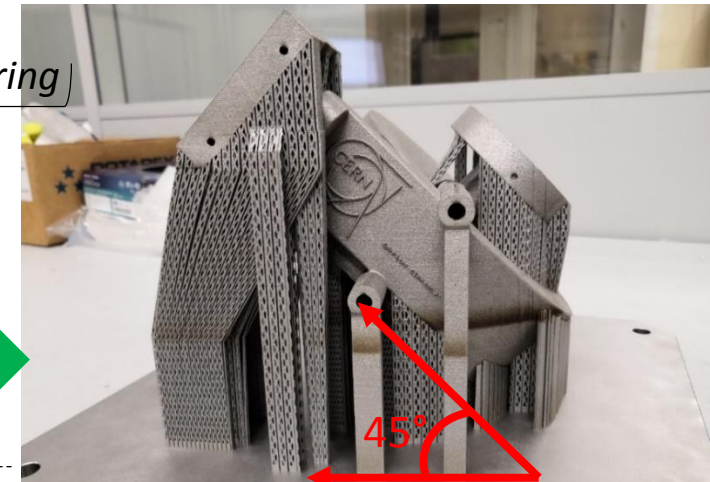
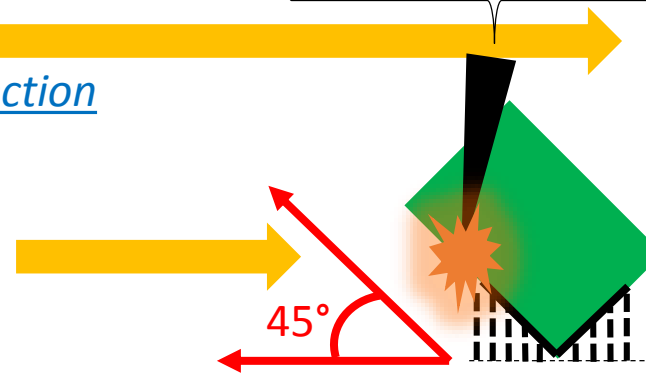
- The aim of this study is to optimise the internal cross-section of RF loads in order to create a stackable design to increase number of products per additive manufacturing cycle and so decreasing the unit price.



*Previous RF Design with rectangular internal cross section*

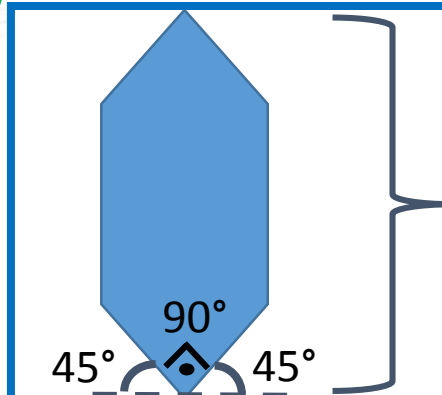
with 45° oblique placing to allow additive manufacturing

Current cross-section



New cross-section

- Placing directly (without 45°)
- Less space allowing stackable design (allows producing more than one load during one manufacturing cycle)
- Material saving with reducing material for support parts (cost reducing)

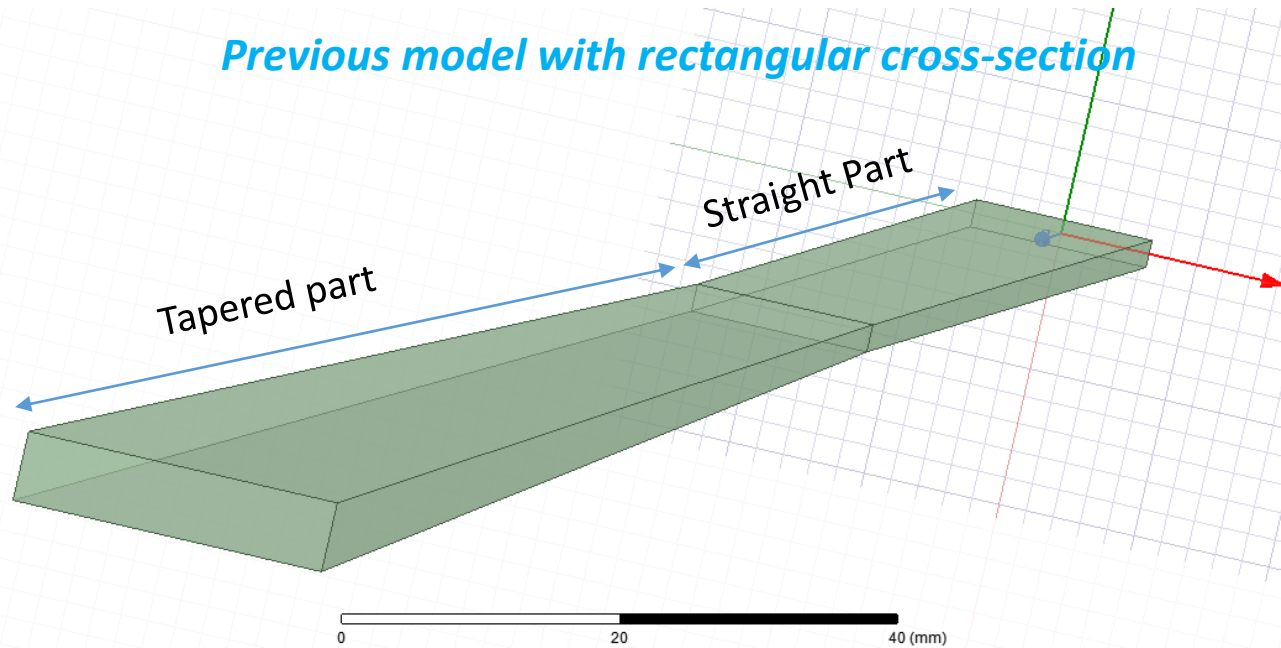


\*Development of X Band High Power RF Load for CLIC Applications Using Additive Manufacturing Techniques; D'Alessandro, Gian Luigi (<https://cds.cern.ch/record/2139981?ln=en>)

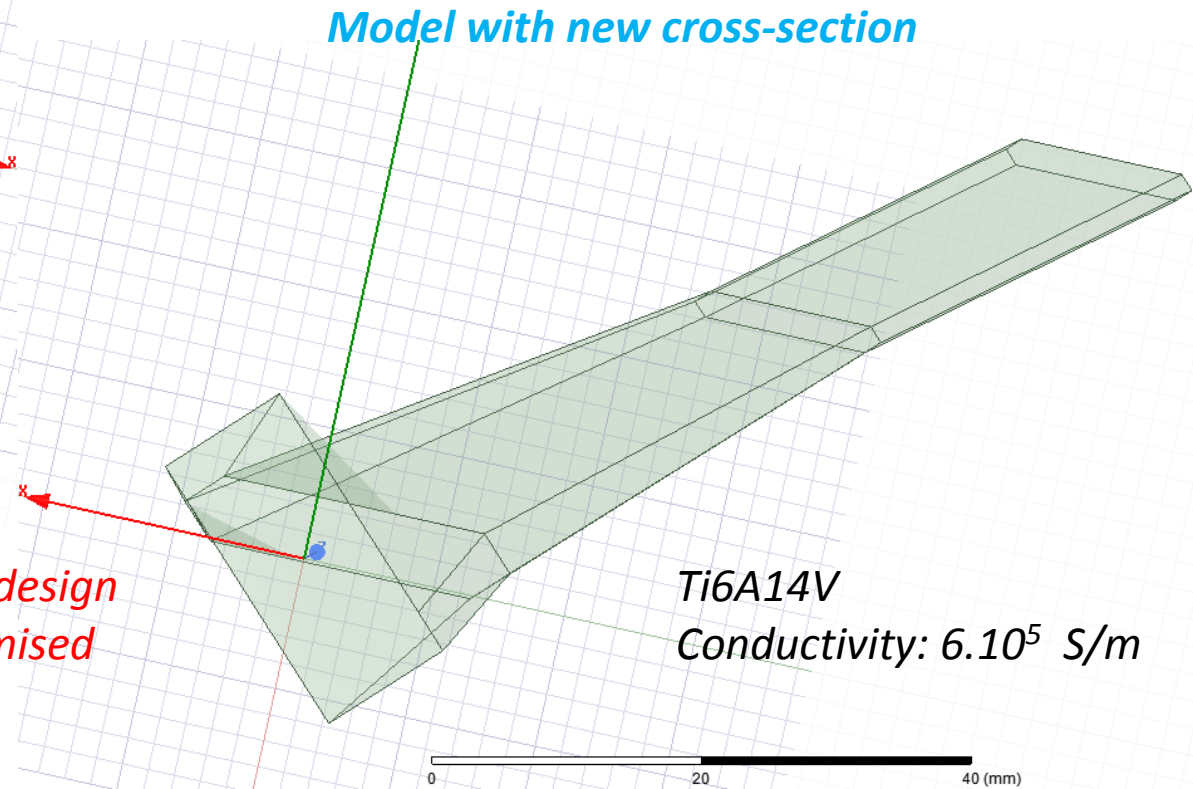
# Straight Model Reference Design

*Parametric Design*

*Previous model with rectangular cross-section*



*Model with new cross-section*



*The dimensions of previous design were used directly and optimised with the new cross-section.*

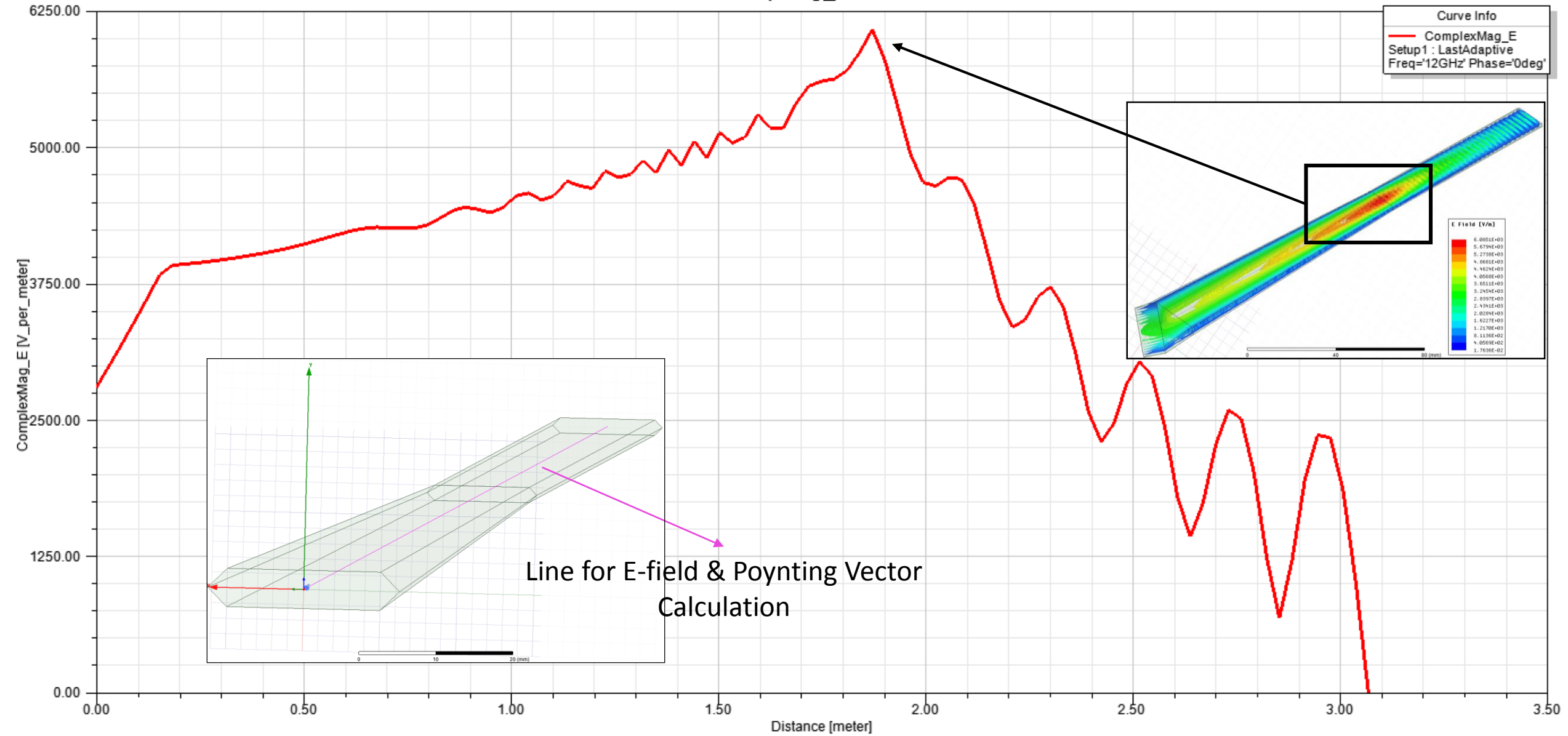
Ti6A14V  
Conductivity:  $6 \cdot 10^5$  S/m

\*Development of X Band High Power RF Load for CLIC Applications Using Additive Manufacturing Techniques;  
D'Alessandro, Gian Luigi (<https://cds.cern.ch/record/2139981?ln=en>)

# Electric Field (Complex Magnitude)

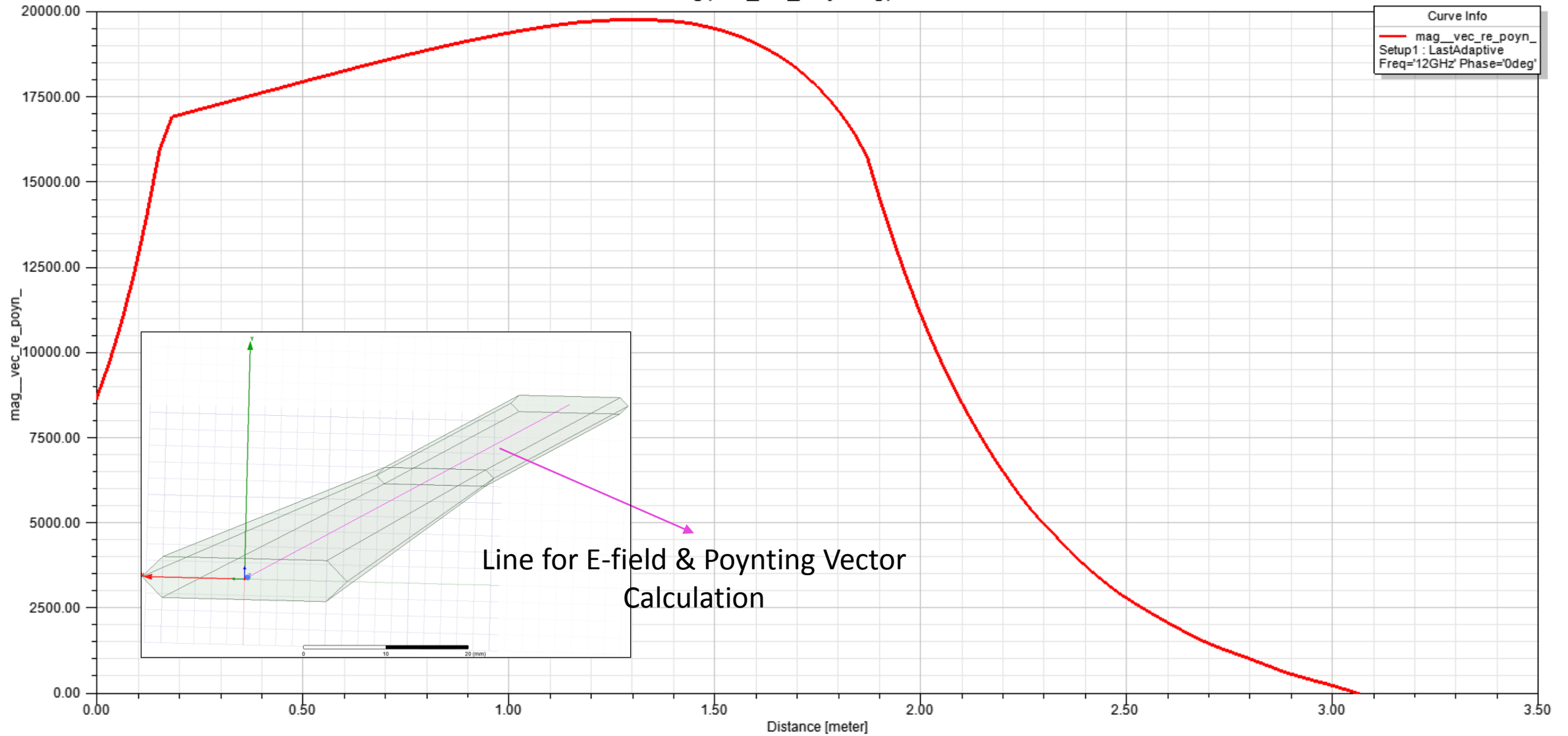
CompMag\_E

Curve Info  
— ComplexMag\_E  
Setup1 : LastAdaptive  
Freq='12GHz' Phase='0deg'



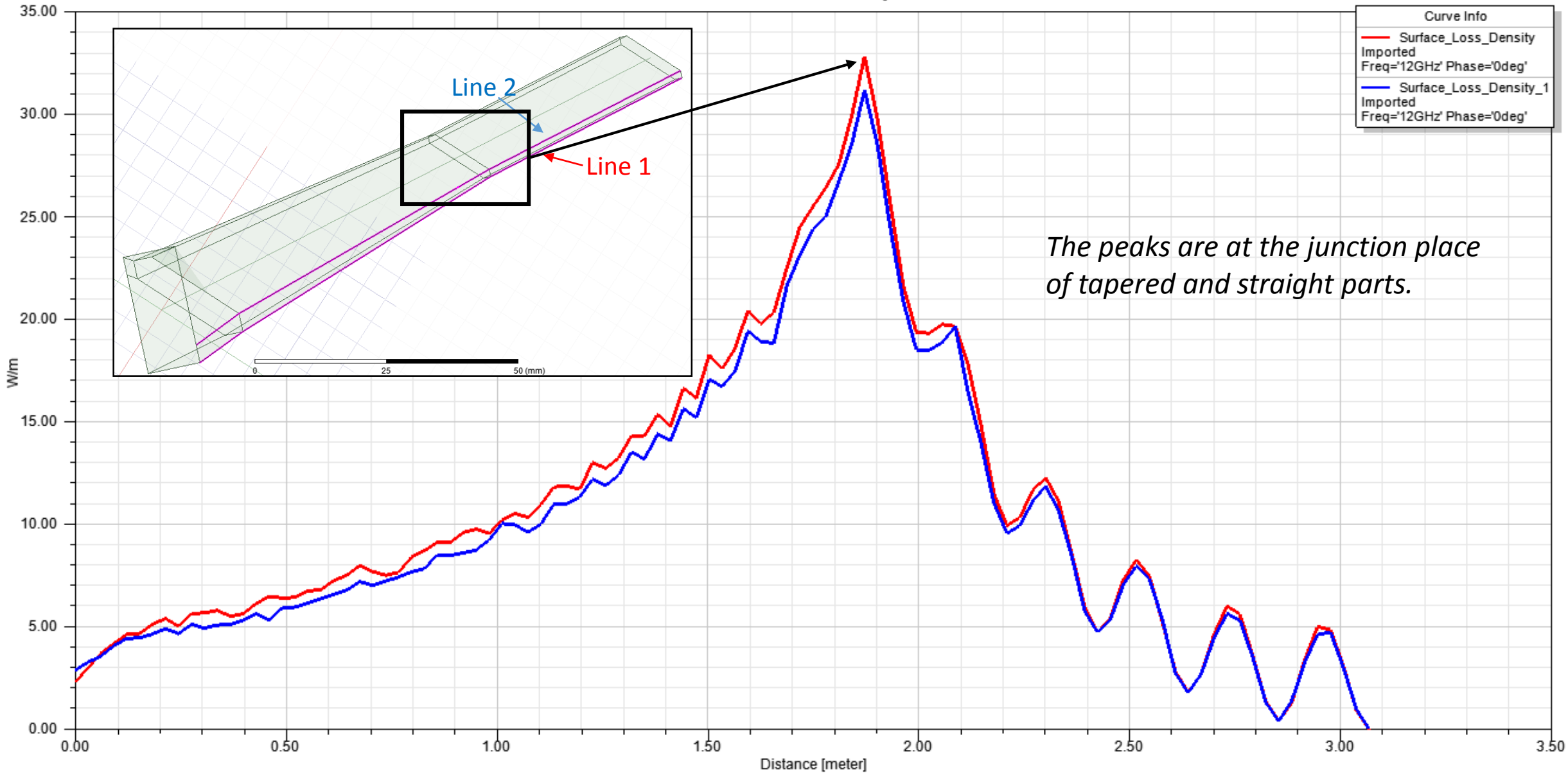
# Poynting Vector

Mag(vec\_Re\_Poynting)



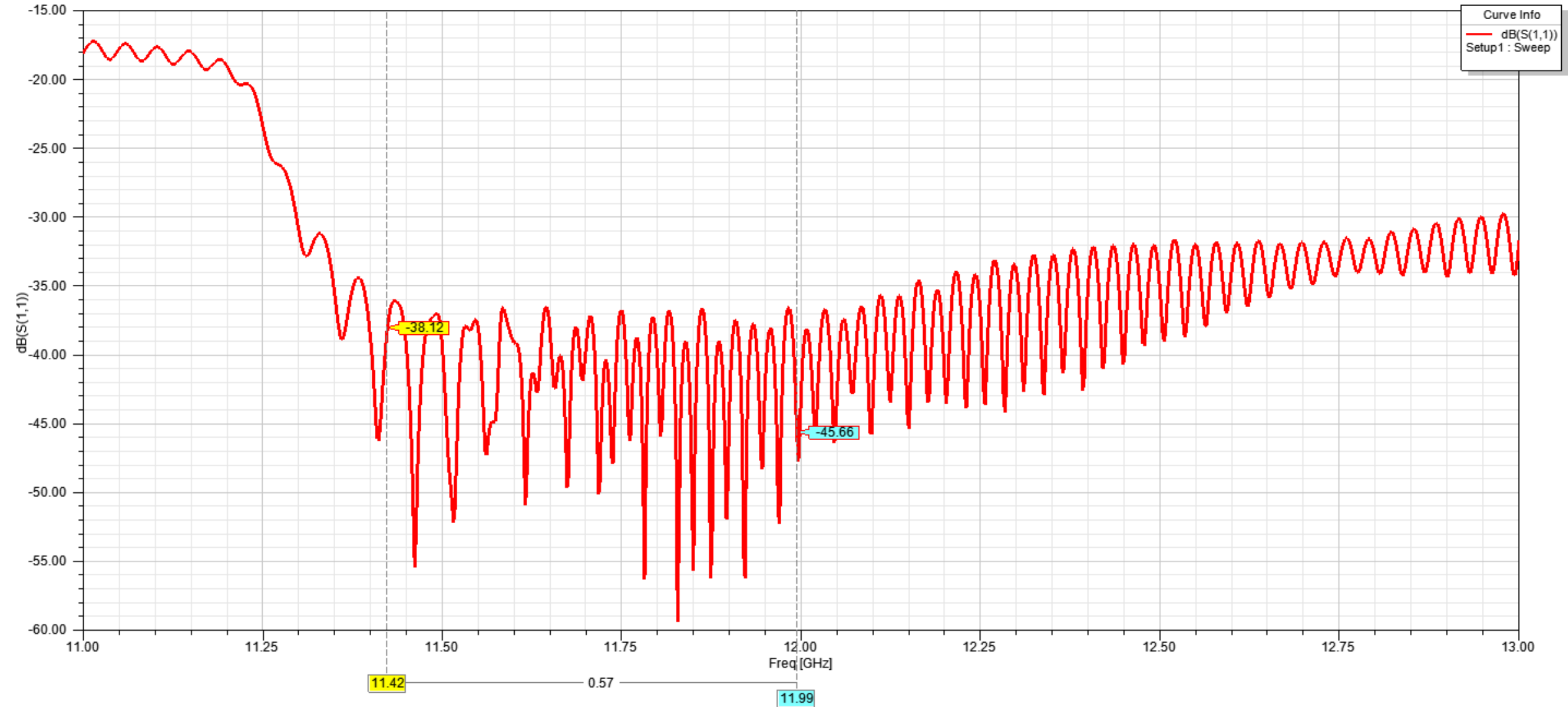


# Surface Loss Density

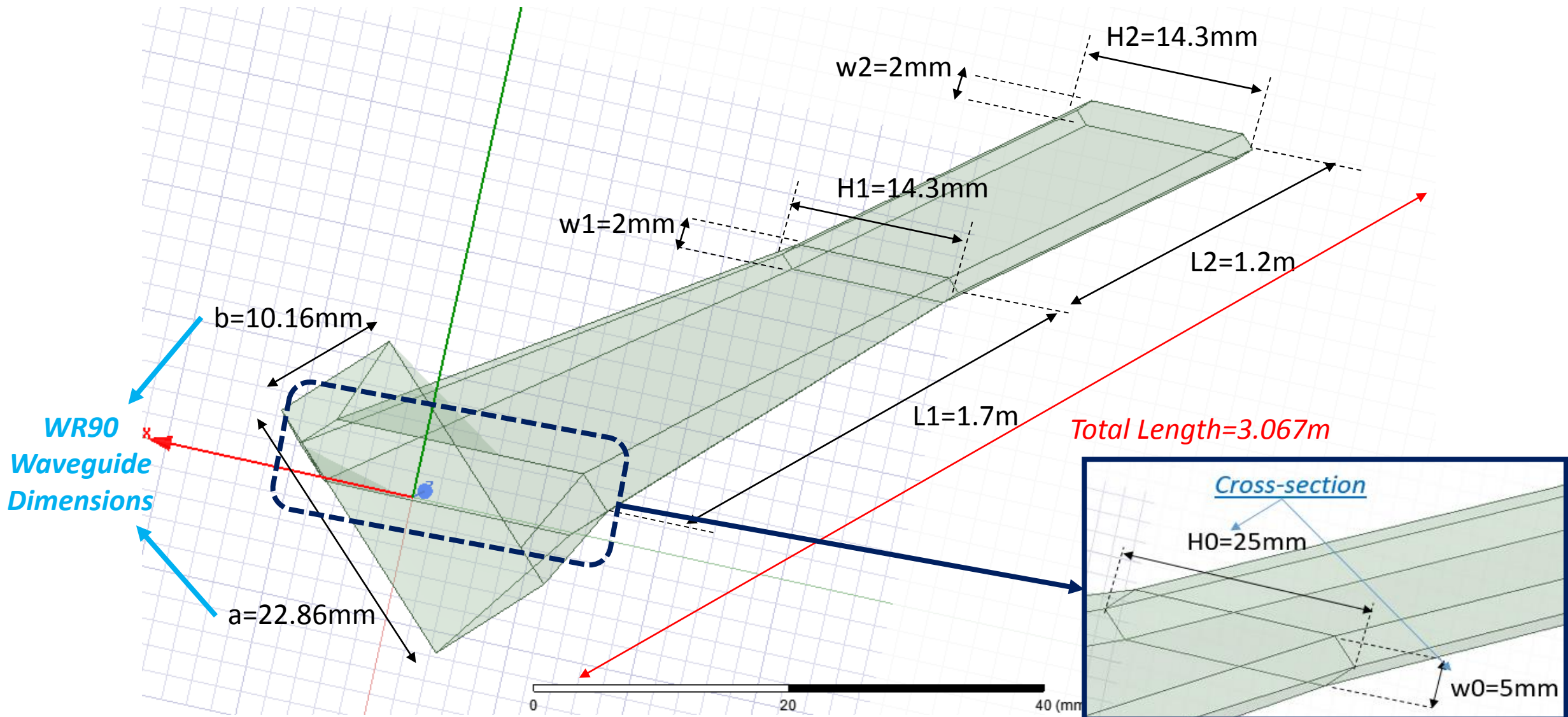


# Reflection

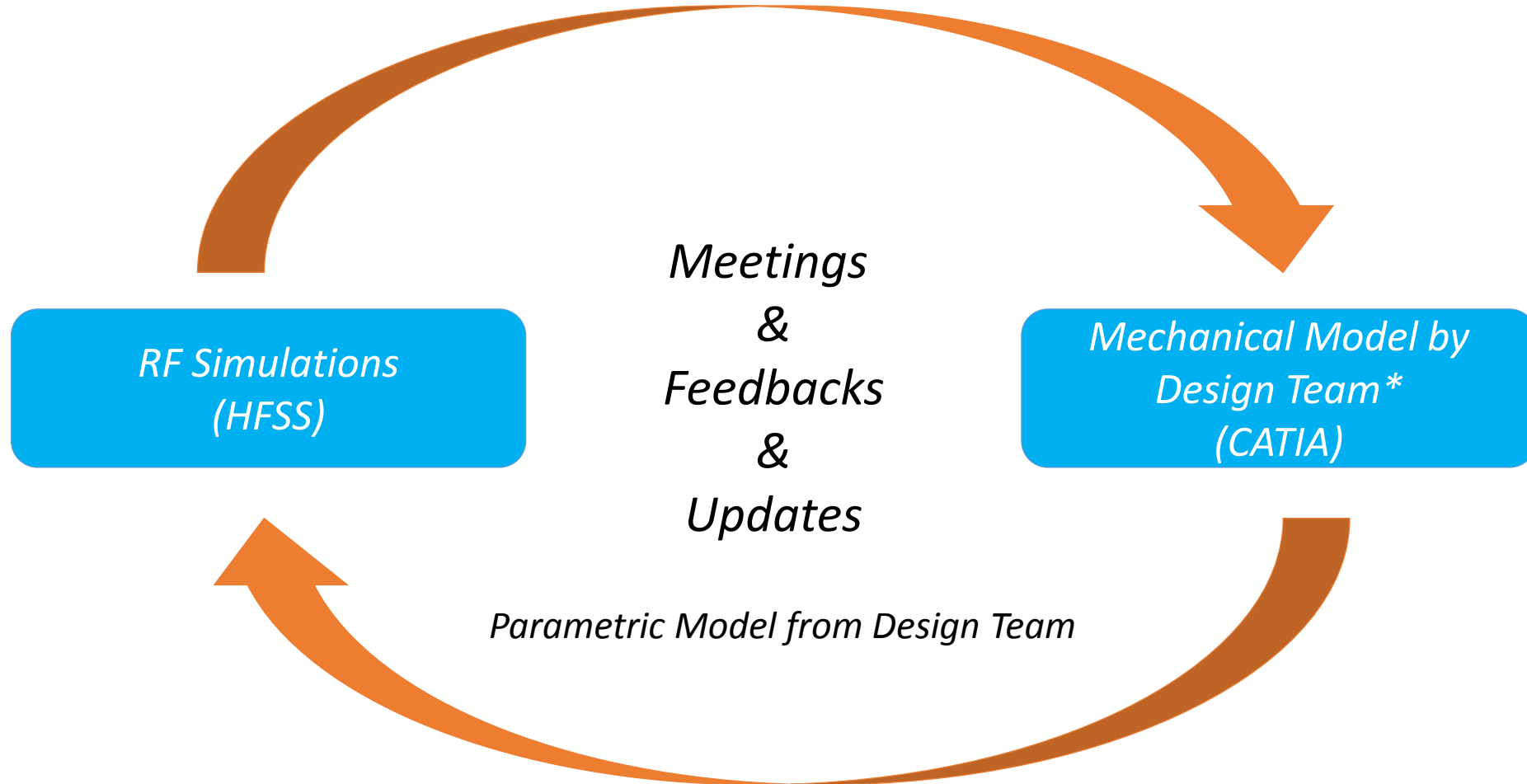
S11



# Straight Model on HFSS-Parameters



# Design Process



*\*Oleg Gumenyuk, Benoit Riffaud, Romain Gerard*

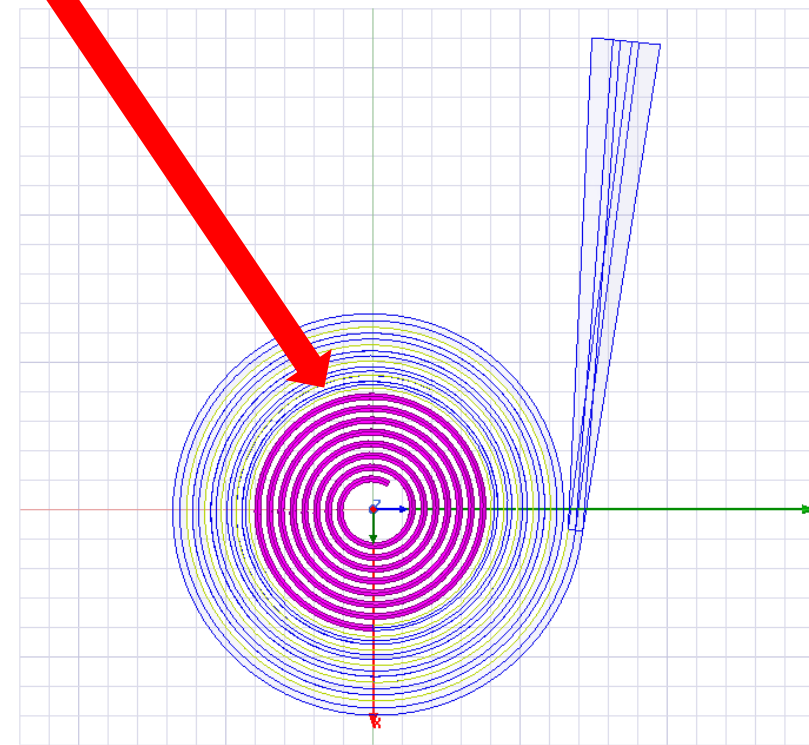
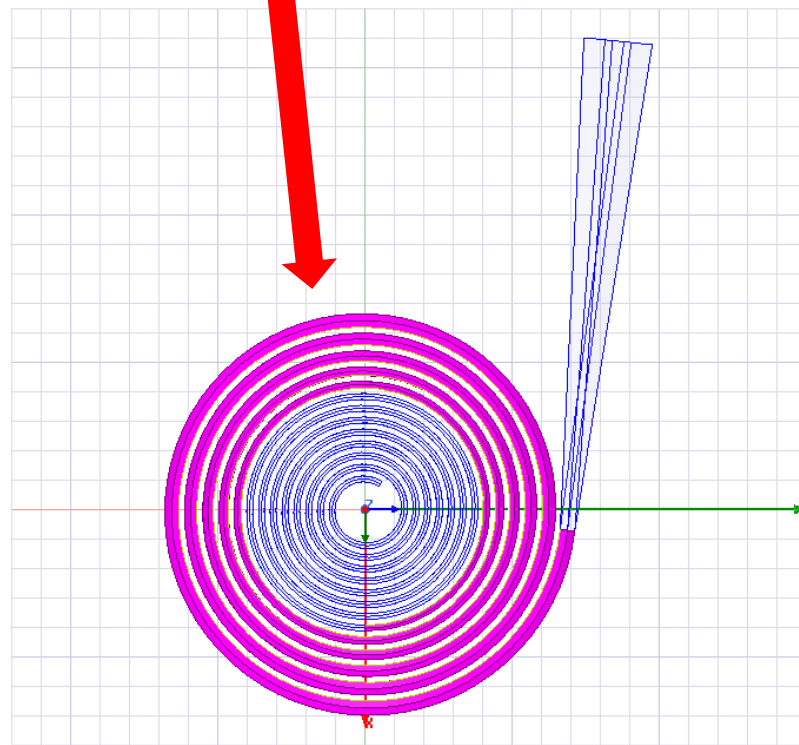
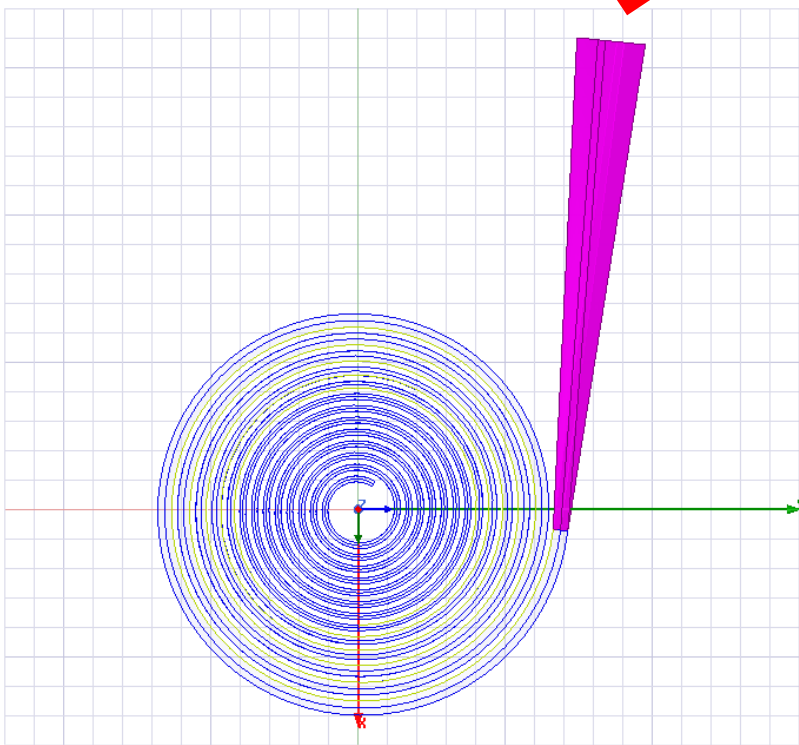
# Straight to Spiral Model

Starting section to make spiral

Transition part

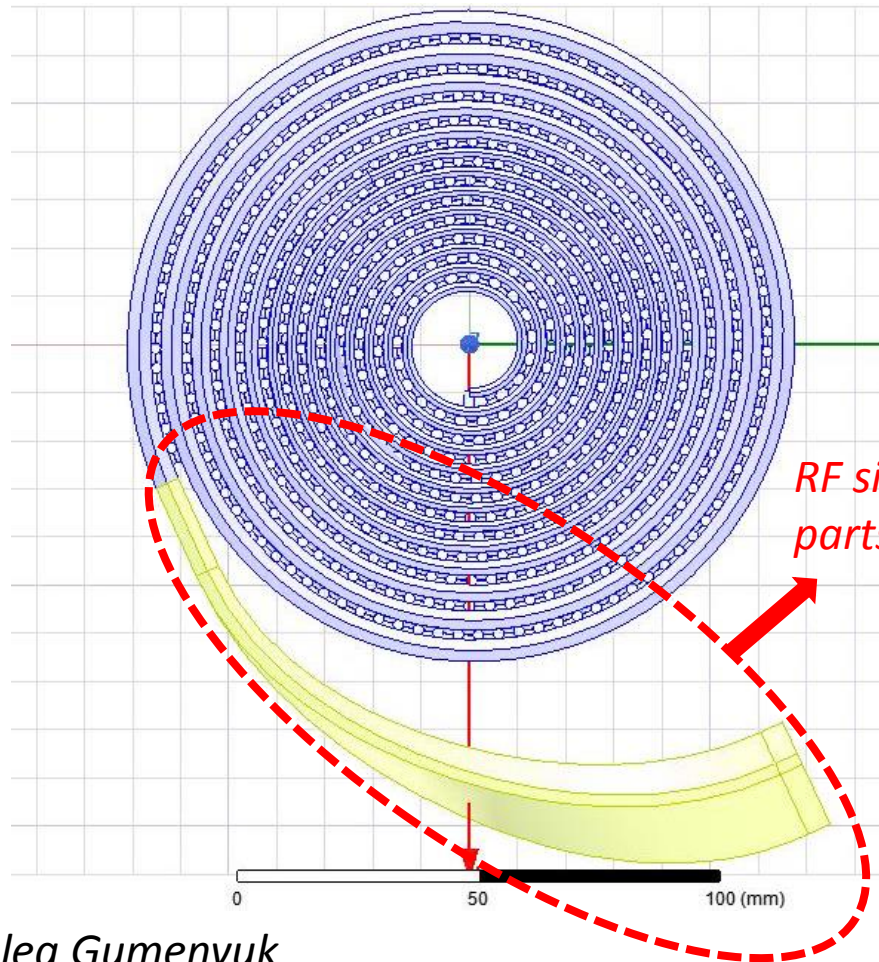
Tapered part

Straight part

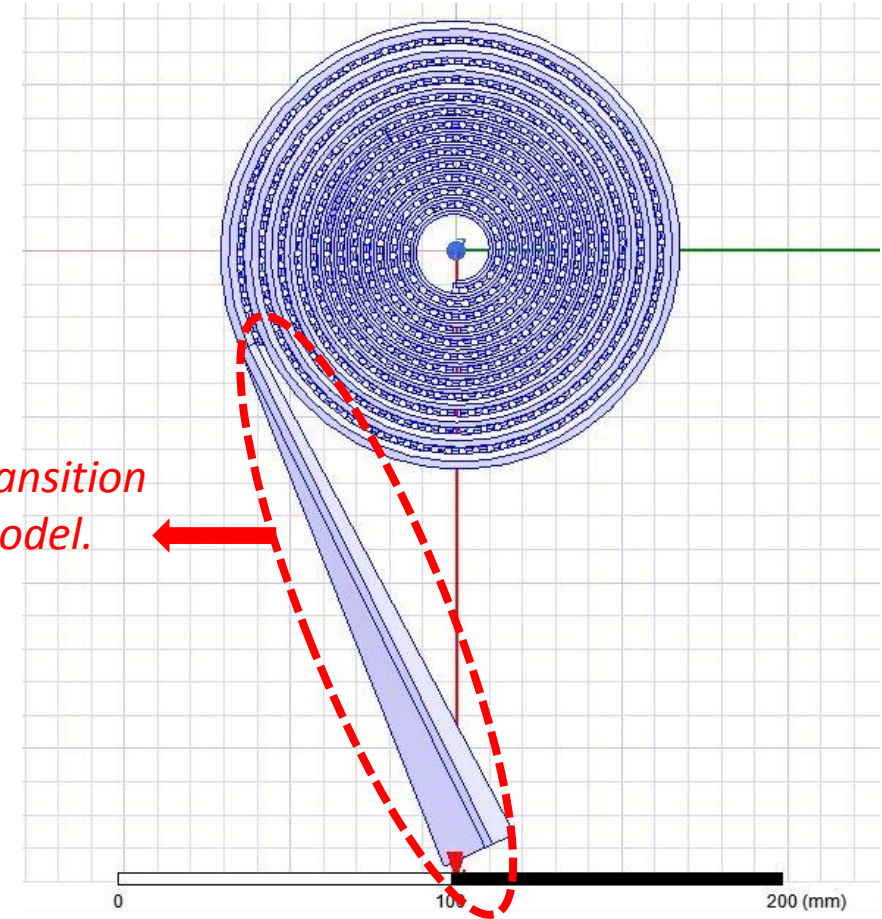


# Straight Model with WR90 Transition

Model with Bent Transition



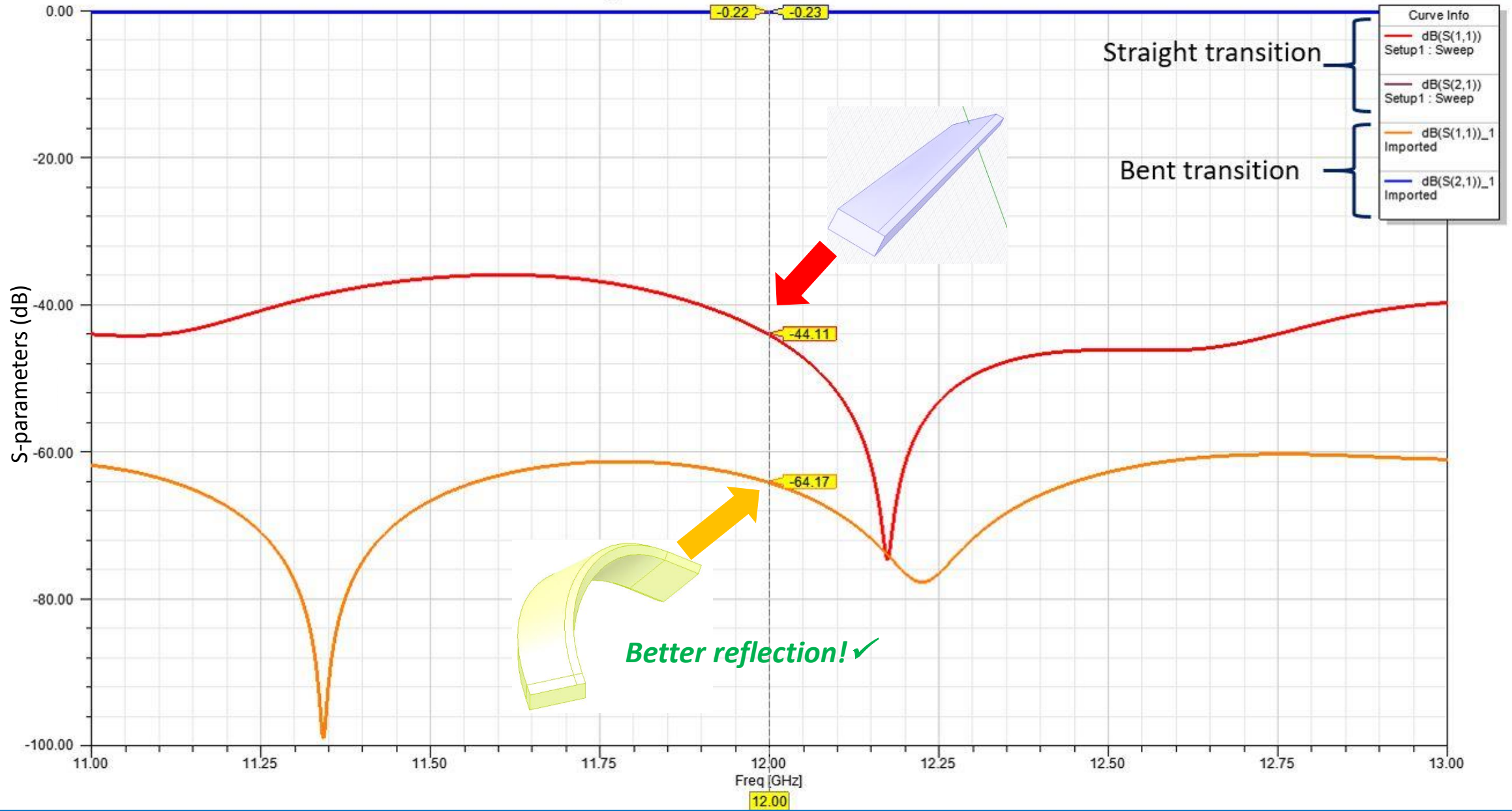
Model with Straight Transition



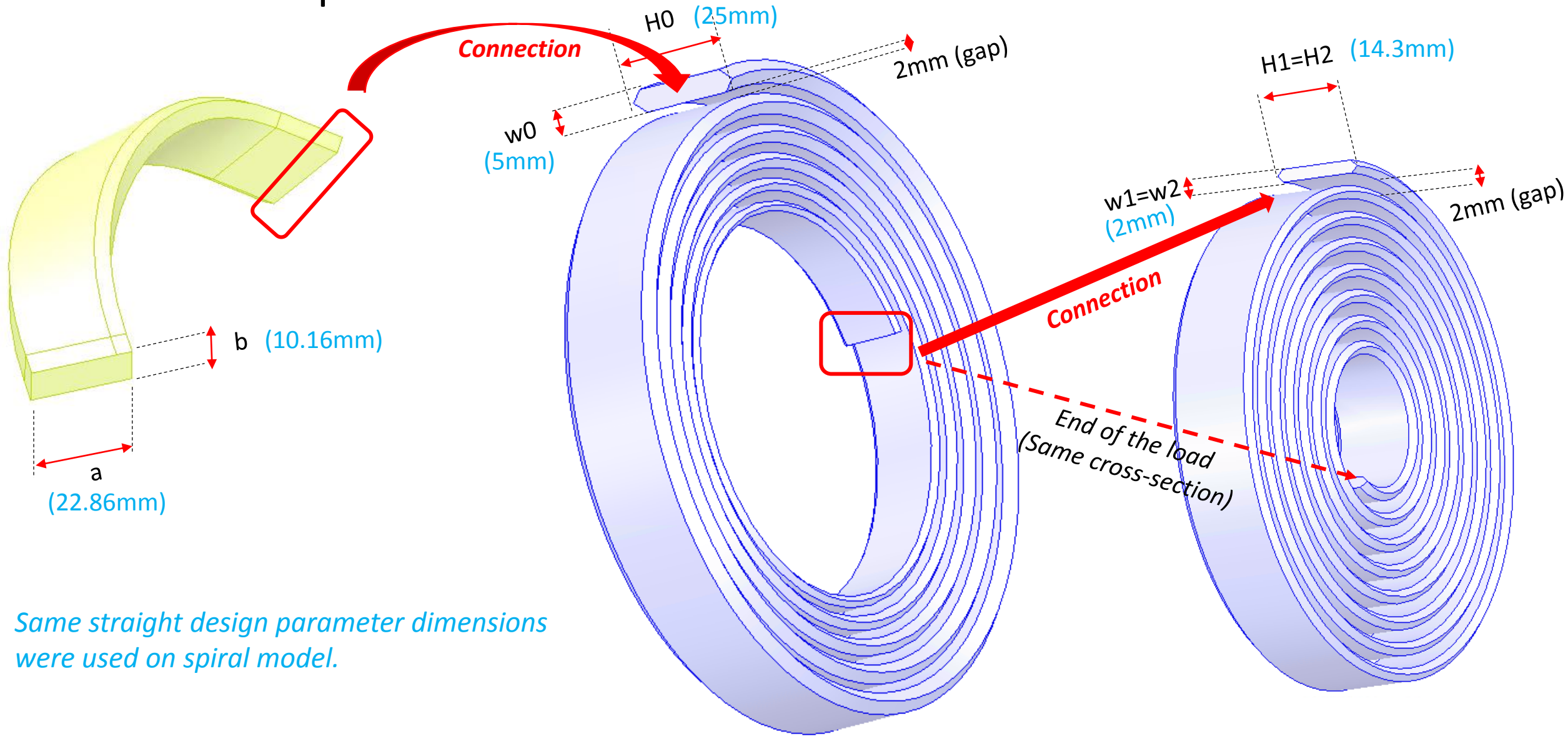
*RF simulations for transition parts to select the model.*

Oleg Gumenyuk

# Straight vs Bent Transition S11 and S21



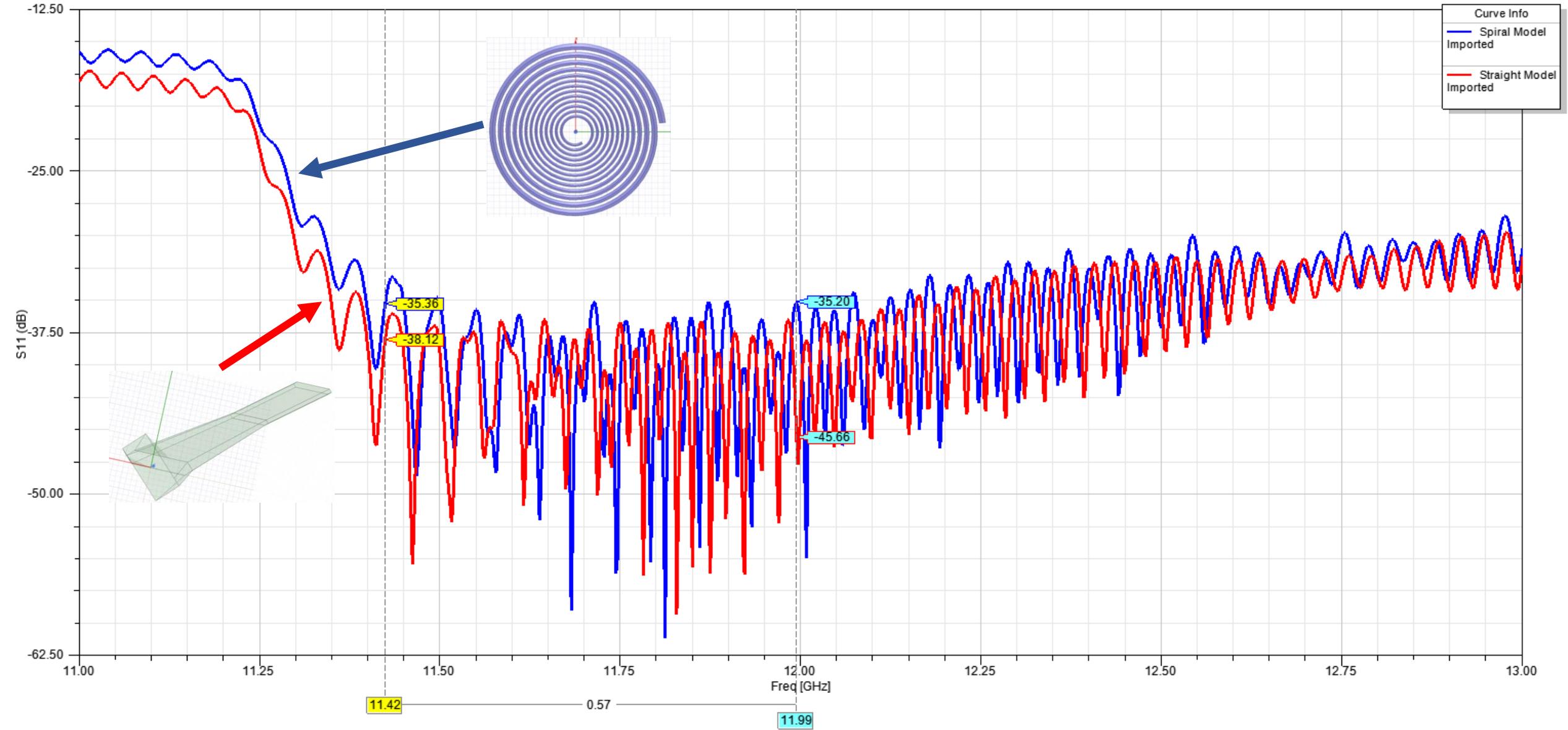
# Spiral Model Dimension Parameters



Same straight design parameter dimensions were used on spiral model.

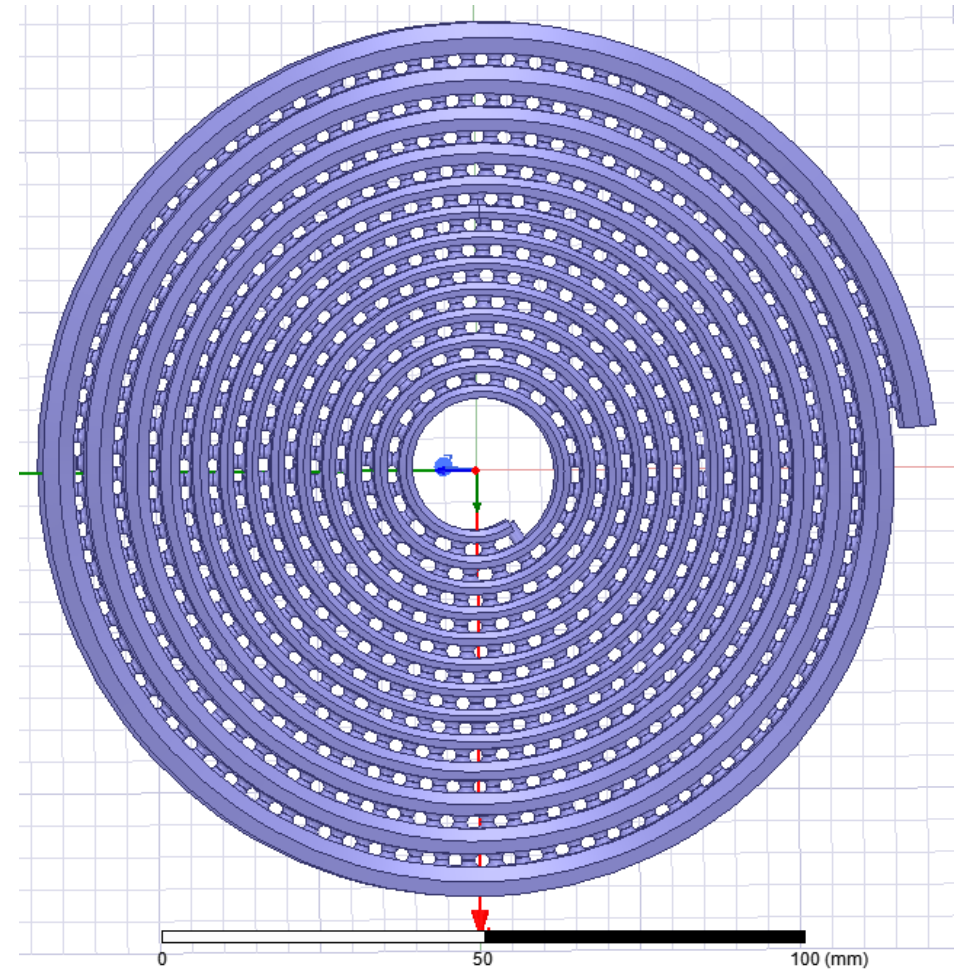
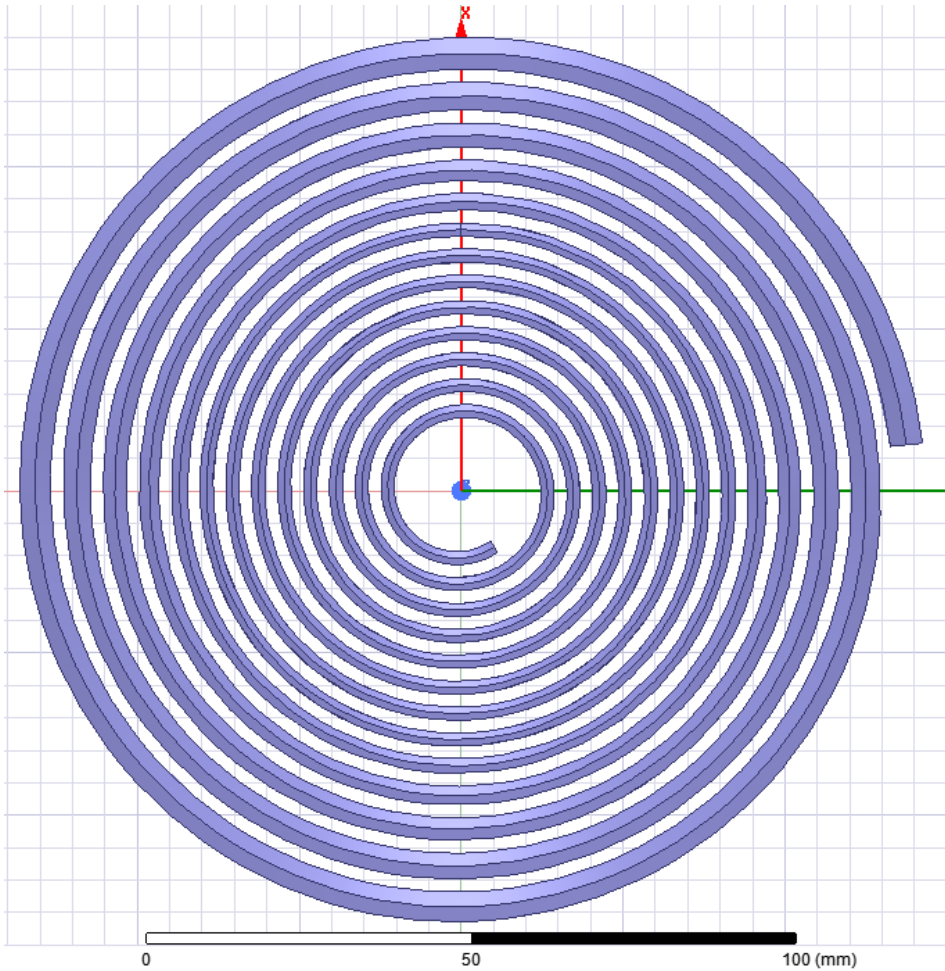


### Spiral vs Straight Model (S11)



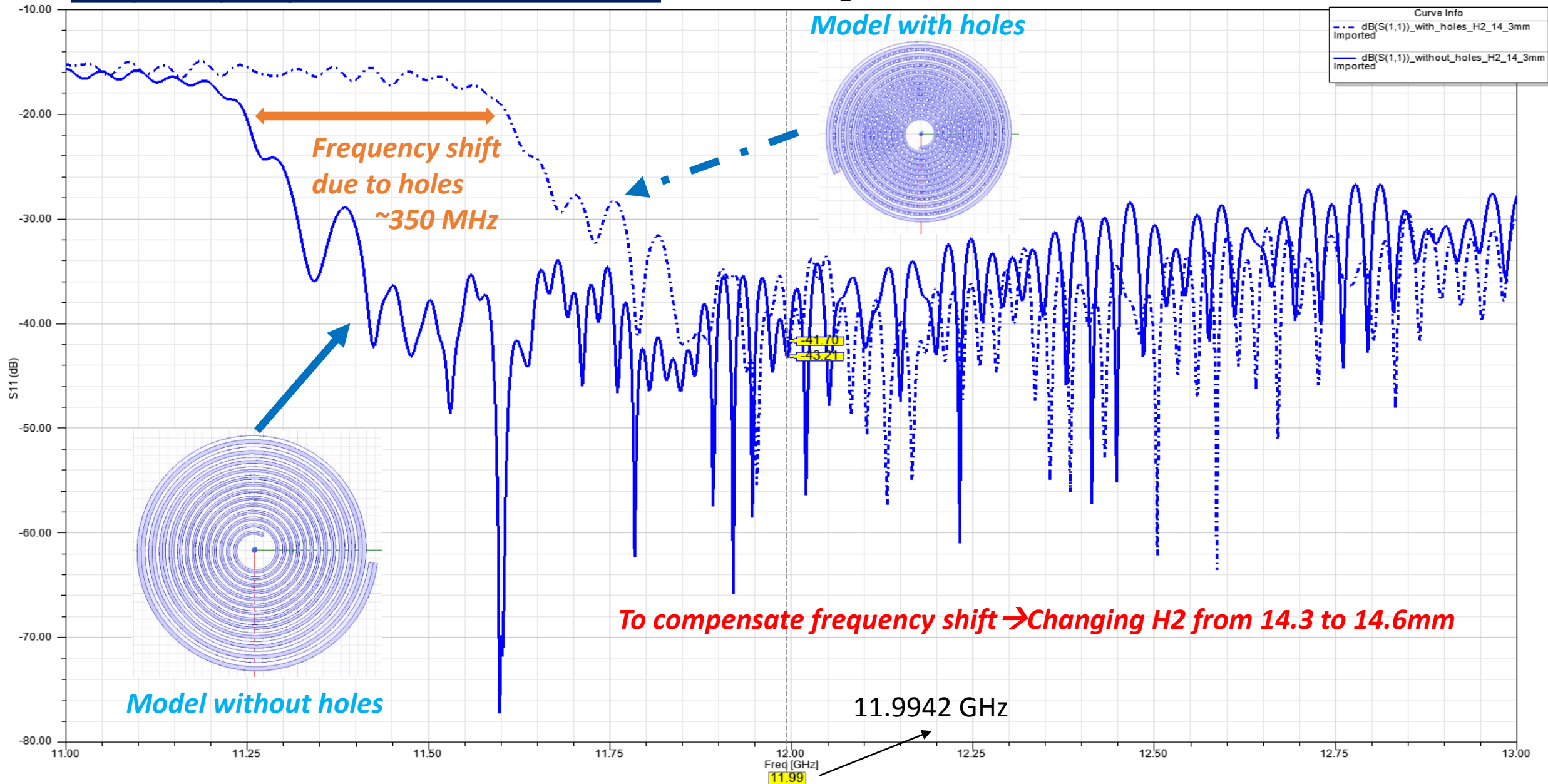
# Spiral Model with Vacuum Holes

vacuum holes with 2mm diameter

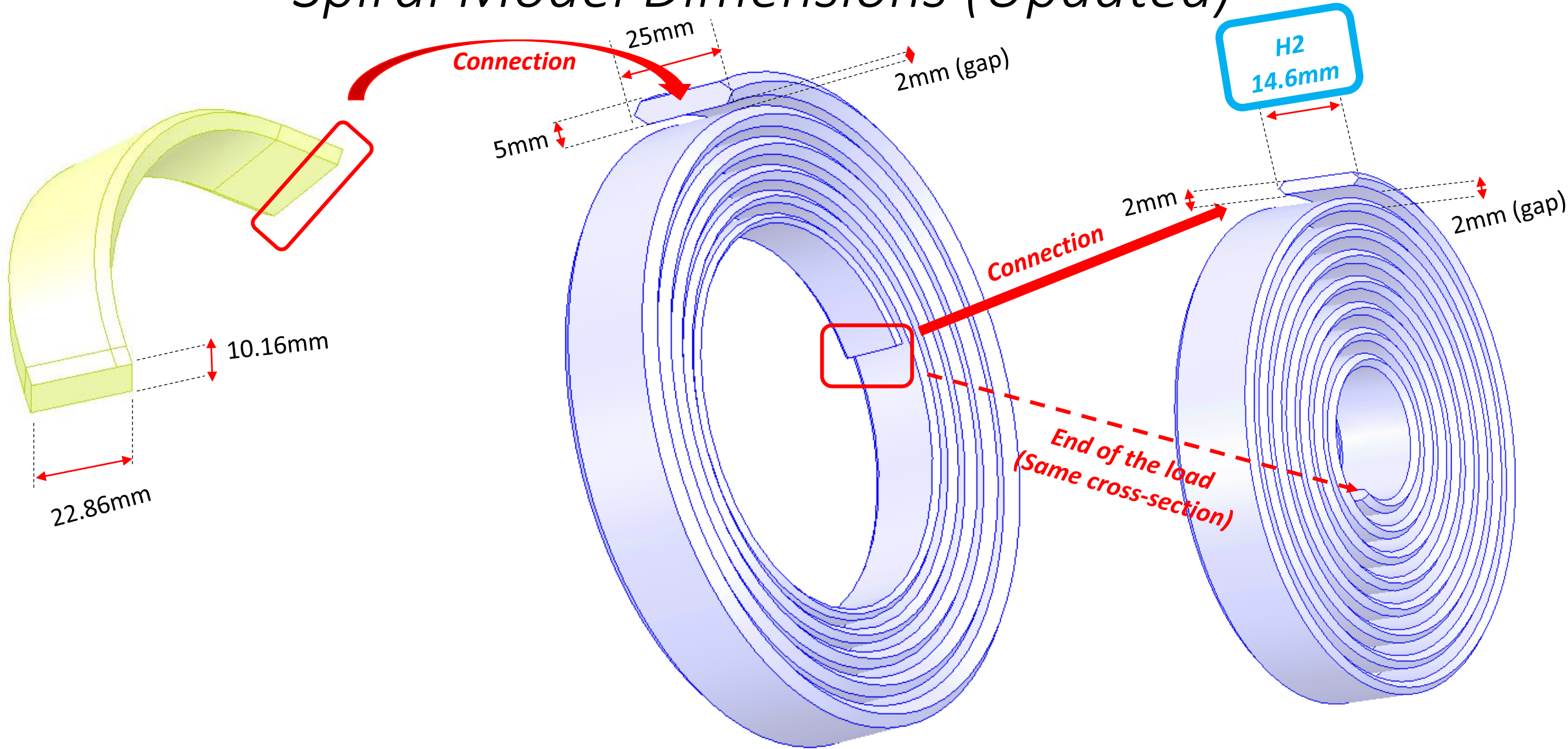


# Frequency shift due to vacuum holes

S Parameter Plot\_1



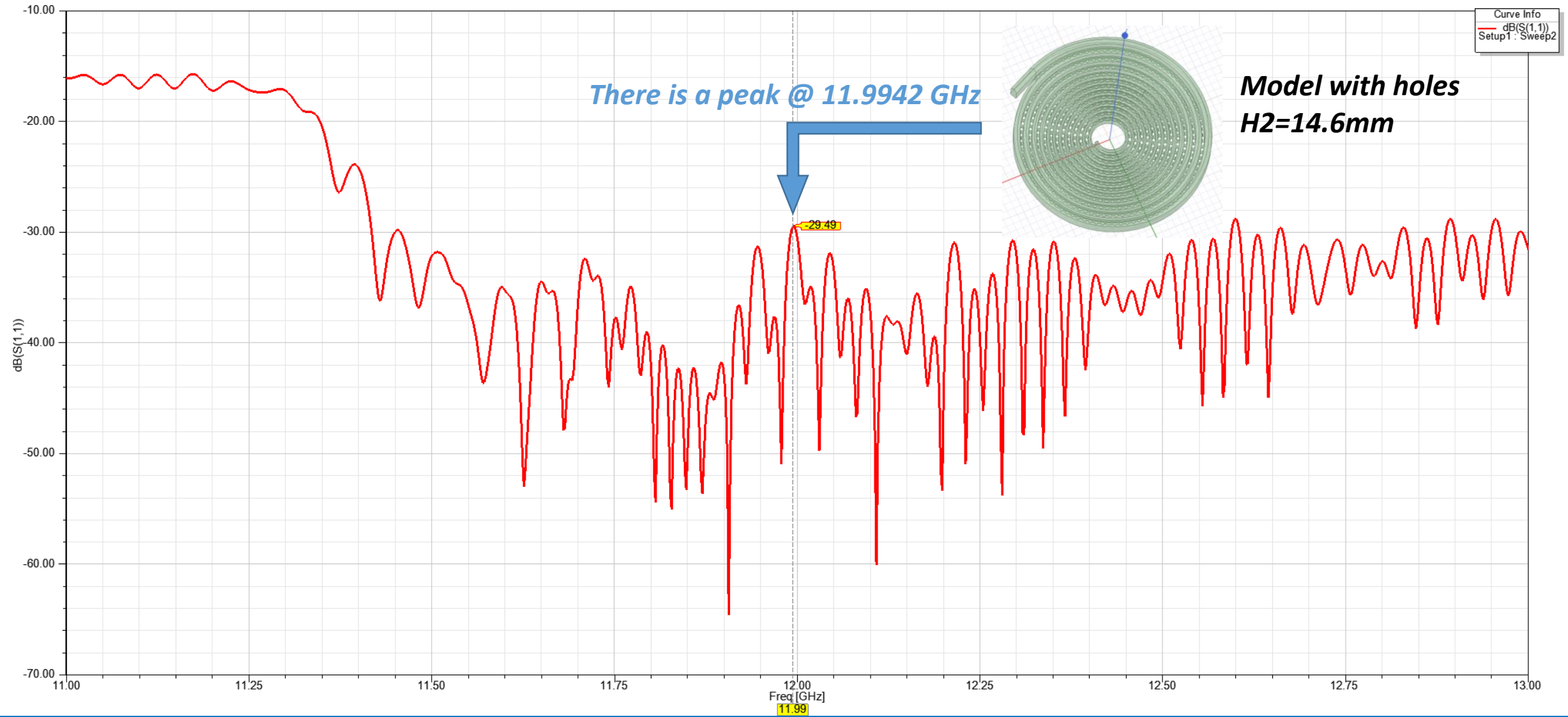
# Spiral Model Dimensions (Updated)



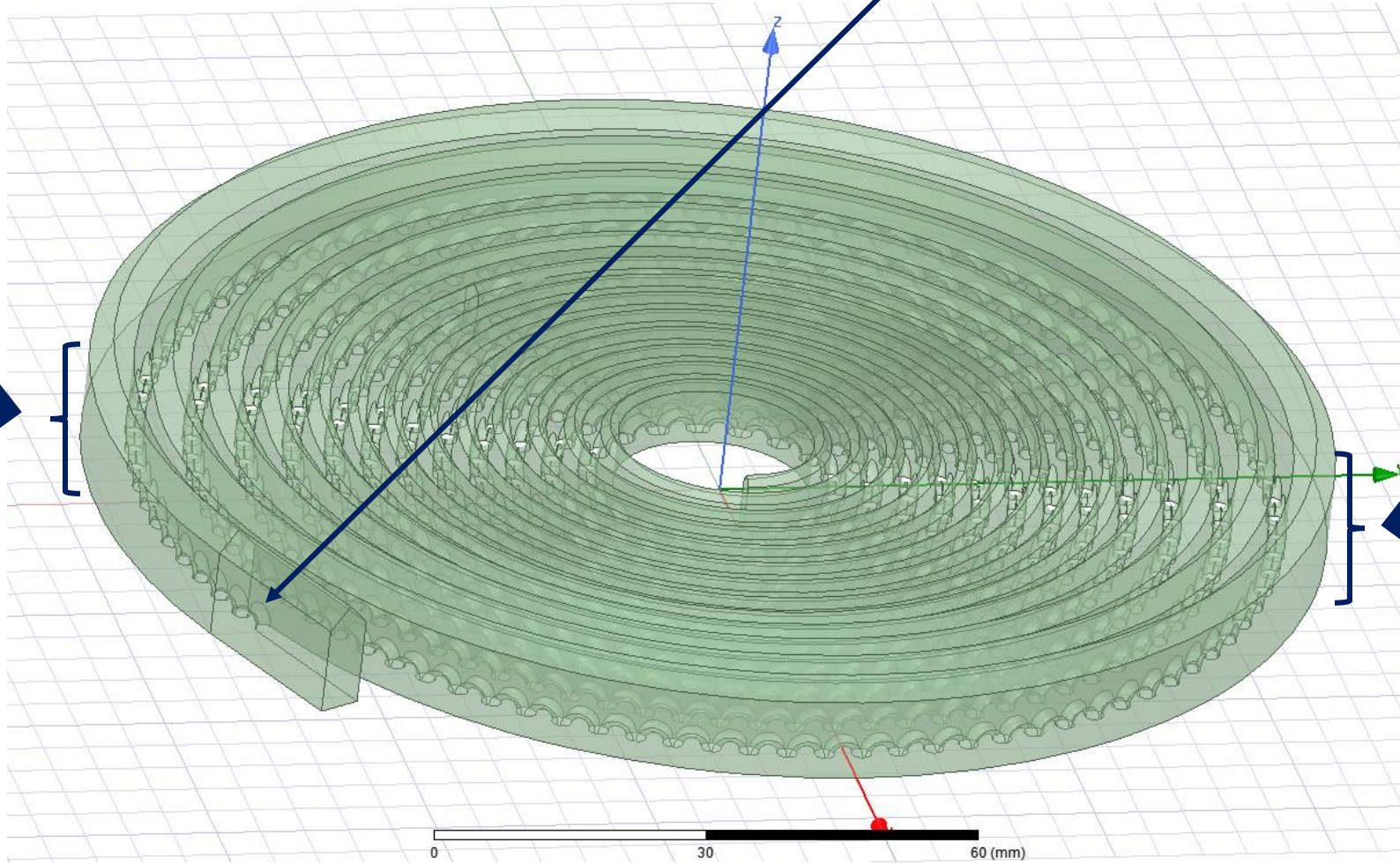


# Reflection Improvement on HFSS

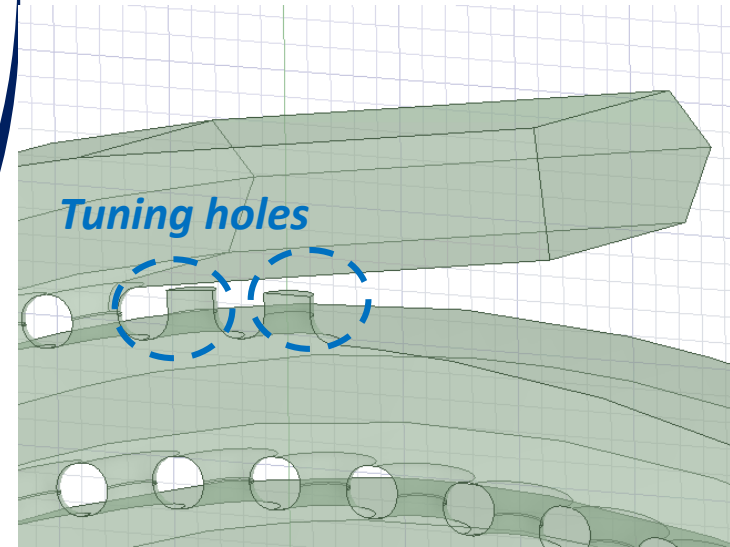
S Parameter Plot 1



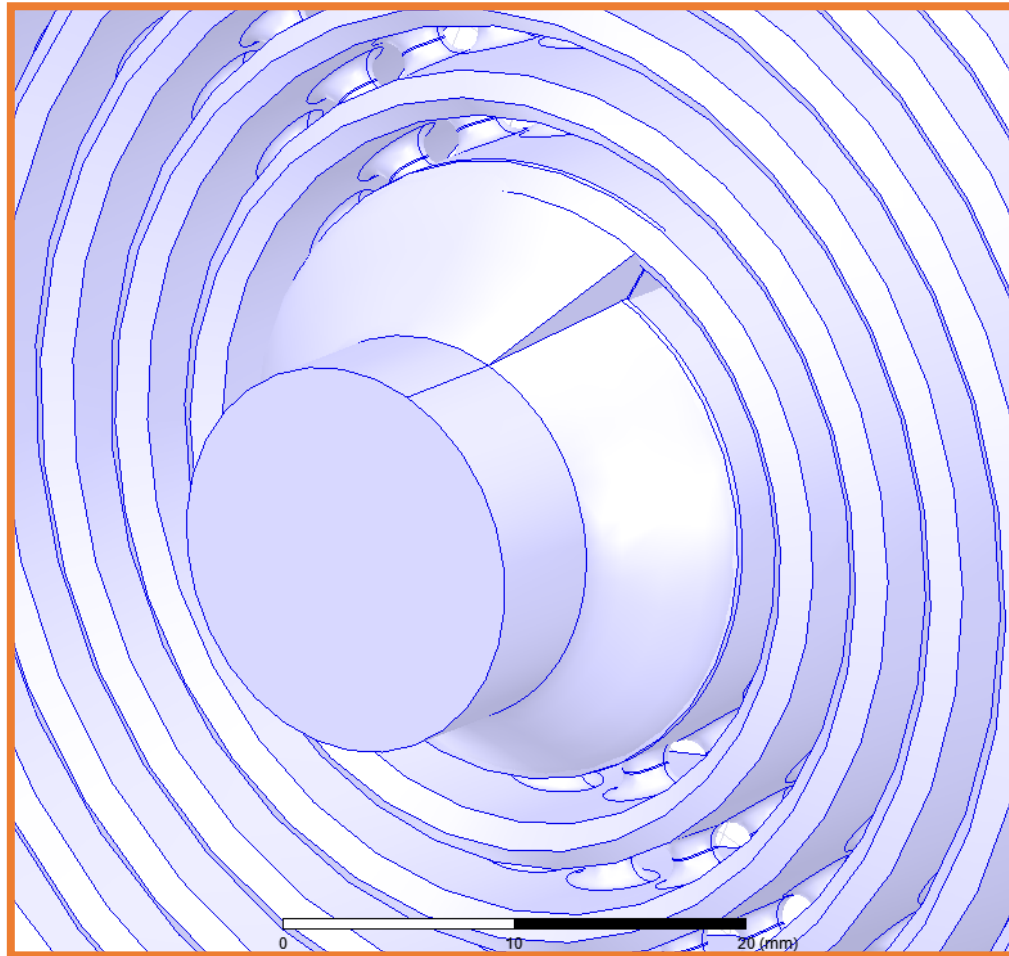
***Inner waveguide of model has vacuum holes both sides.  
Outer face of model has vacuum holes only one side, this causes  
reflection cumulation at the last hole (under transition part).***



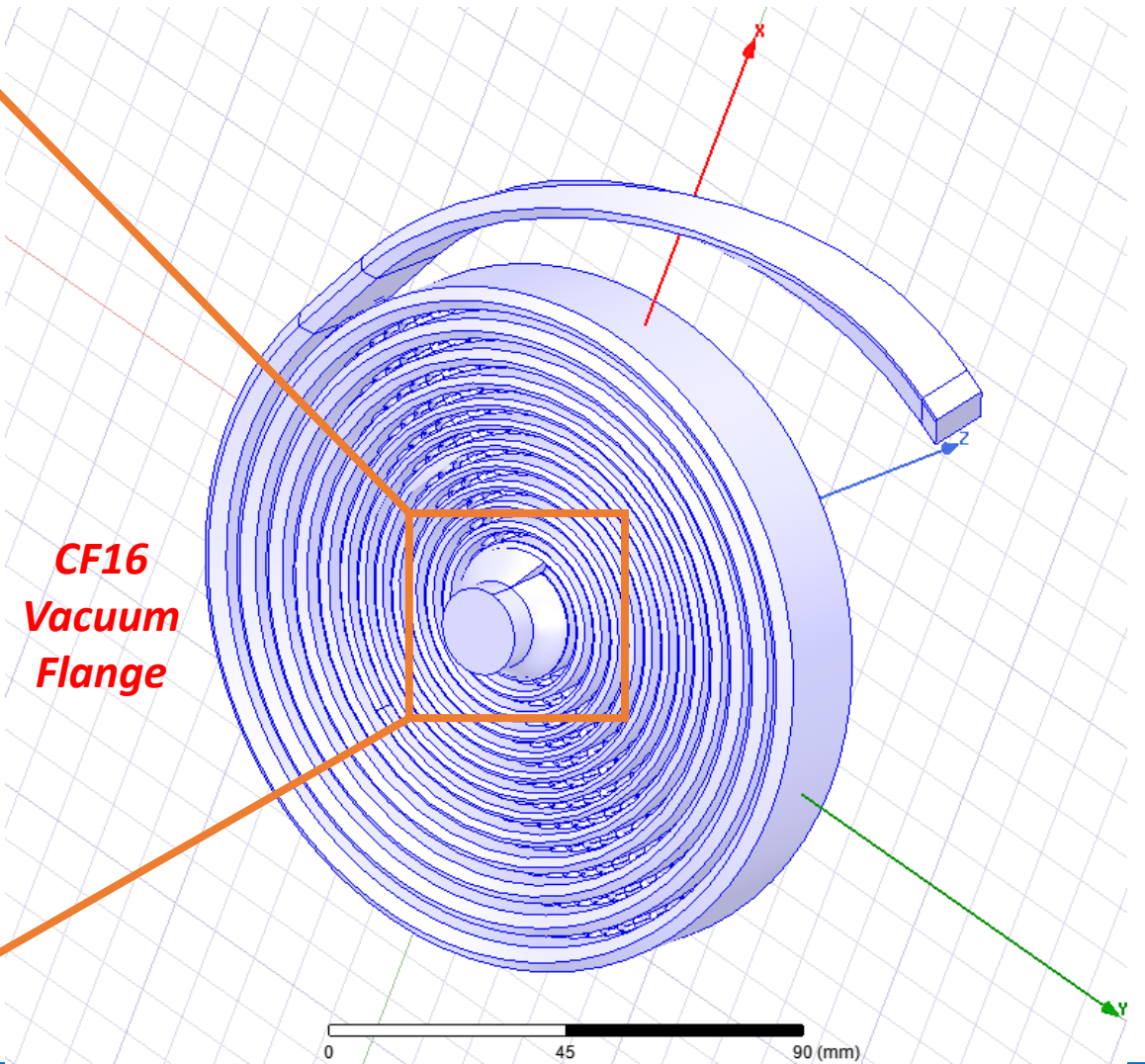
To overcome this; we have added different number of tuning holes to see how reflection changes.



# Spiral Model with Pumping Port



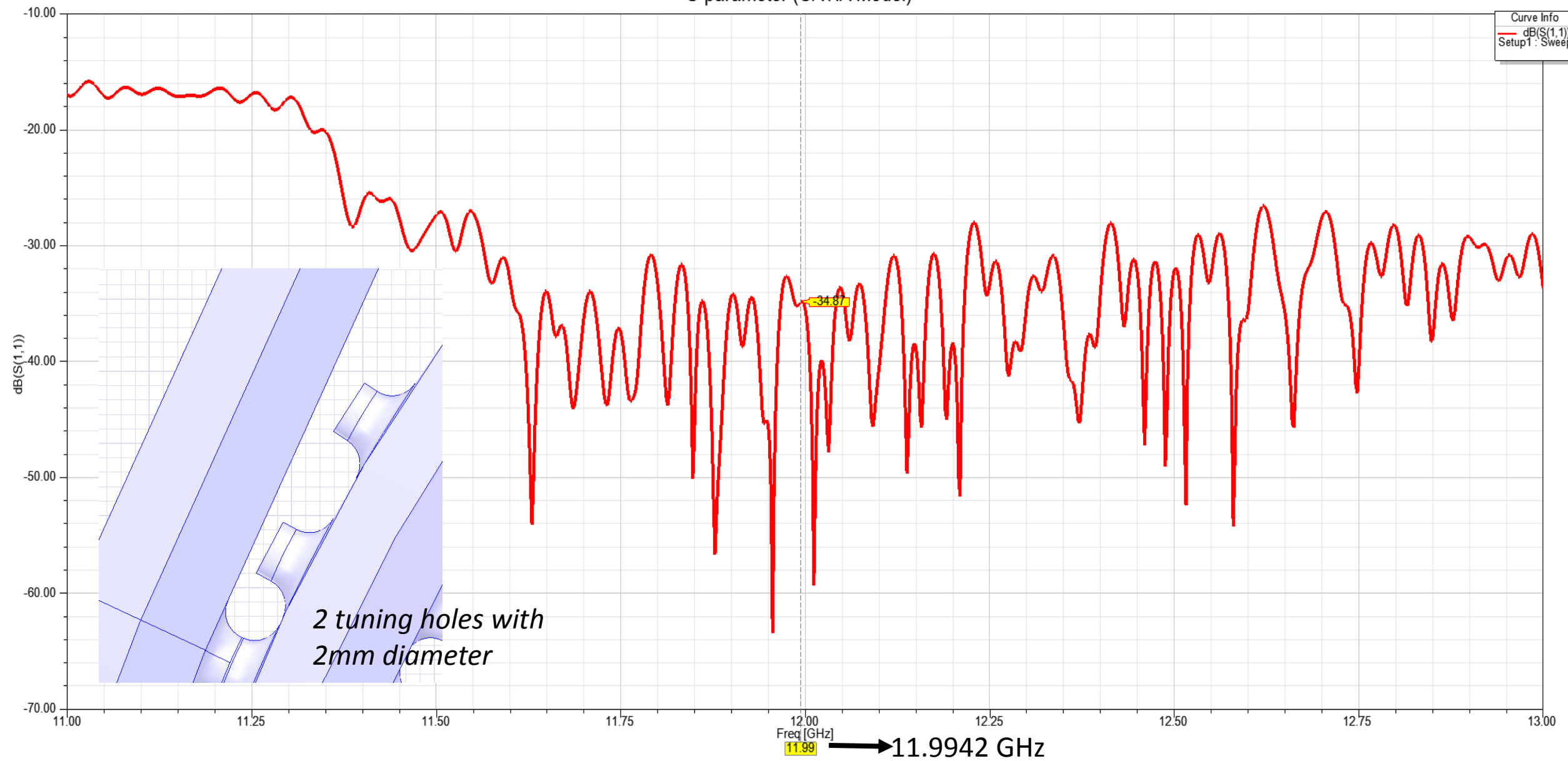
Oleg Gumenyuk





# Reflection (model with vacuum port)

S-parameter (CATIA Model)



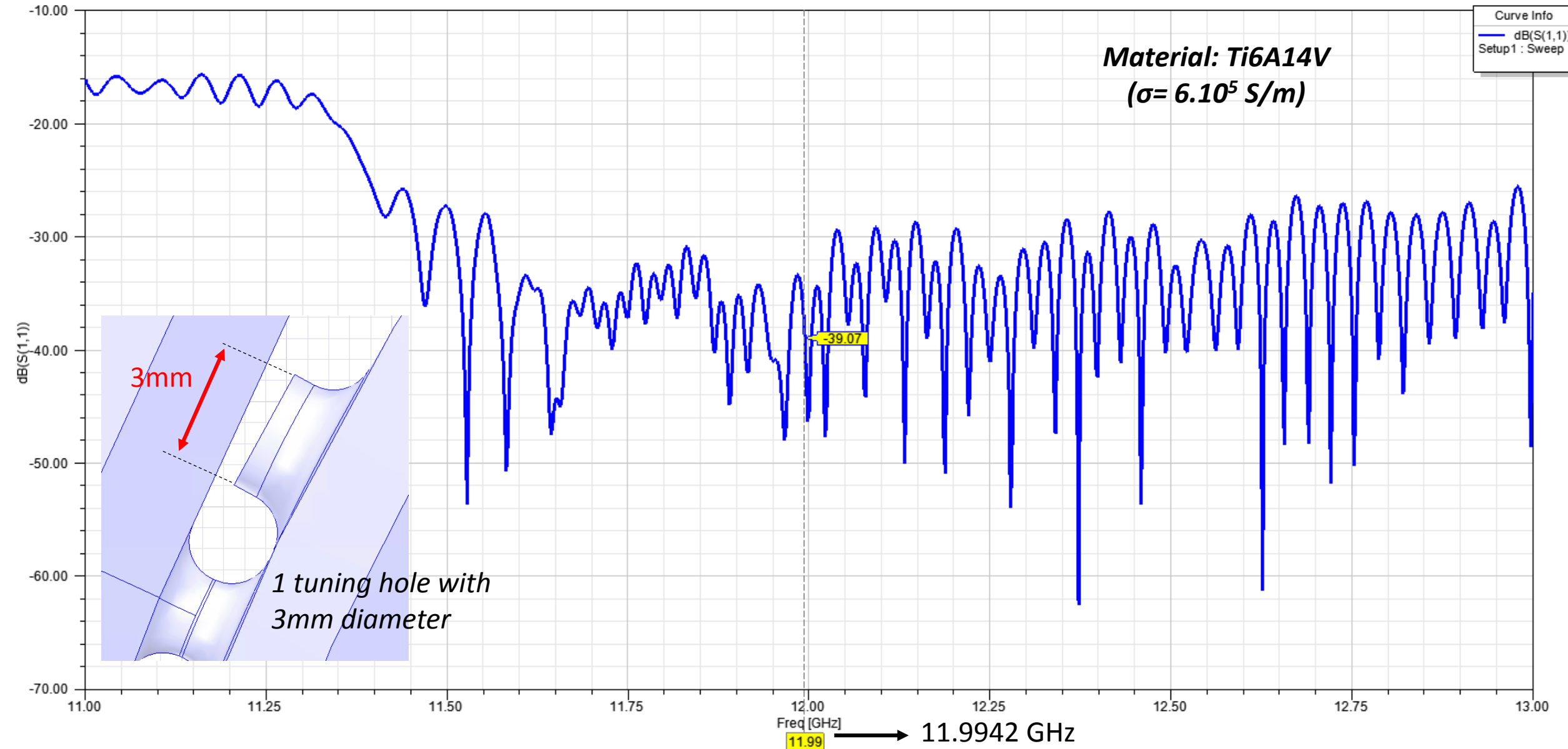
# Reflection Optimisation

S Parameter Plot 1

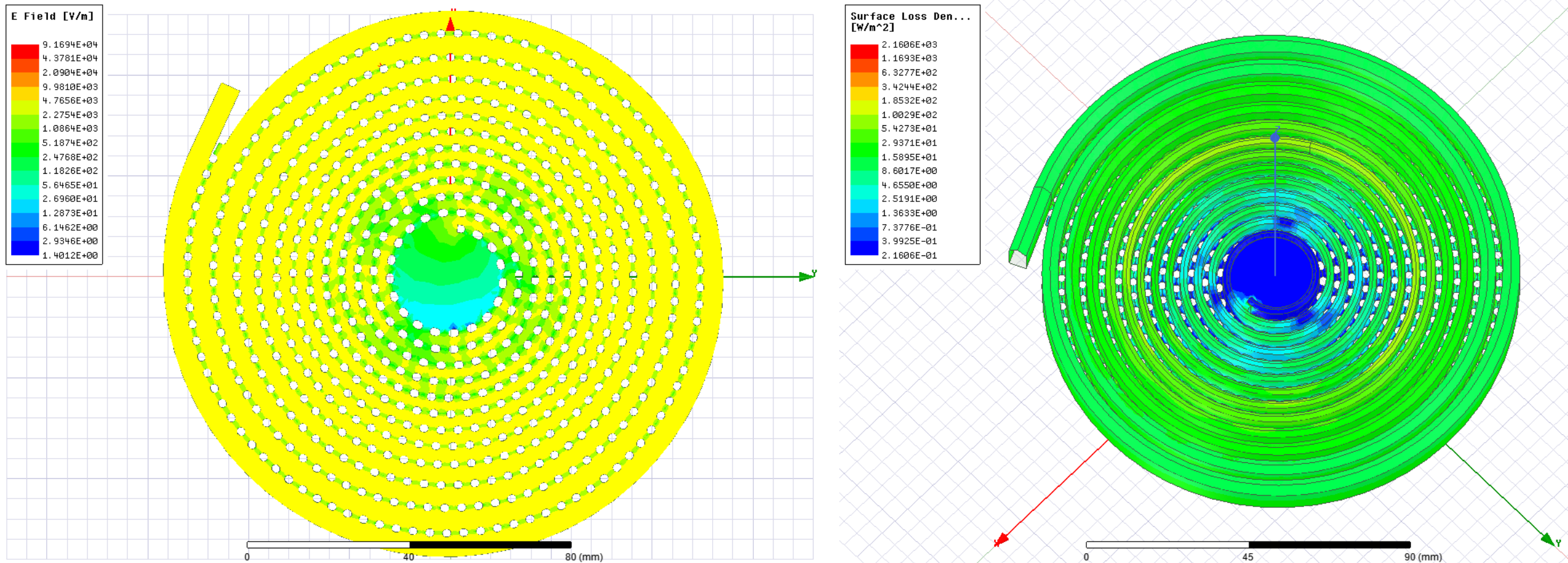
HFSSDesign3\_backup

**Material: Ti6A14V**  
**( $\sigma = 6.10^5$  S/m)**

Curve Info  
— dB(S(1,1))  
Setup1 : Sweep

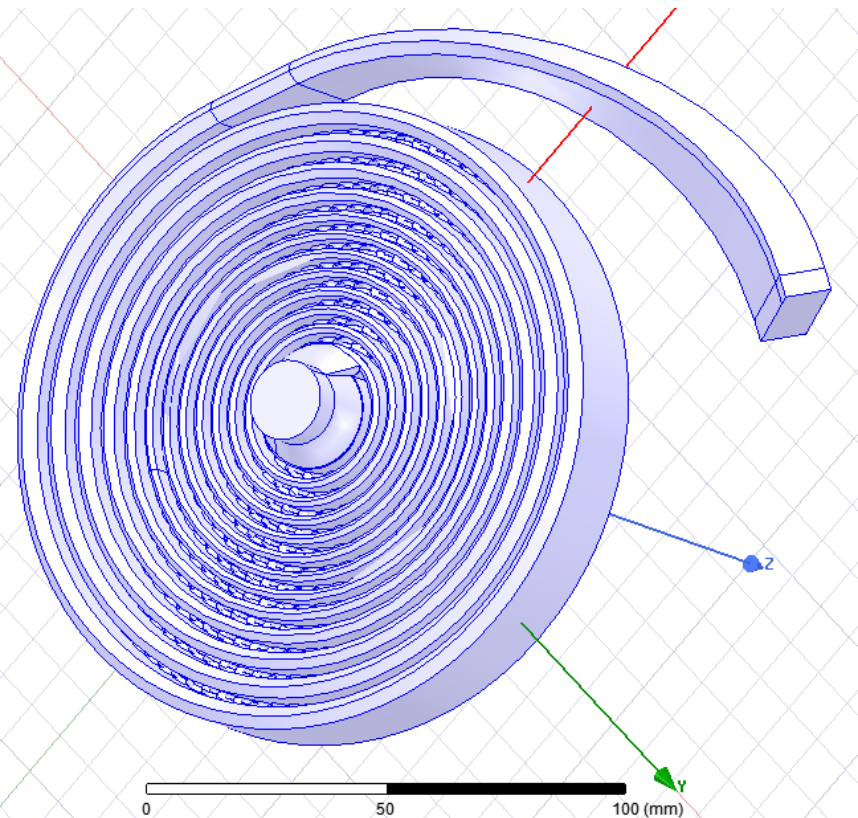


# Electric Field & Surface Loss Density @12GHz

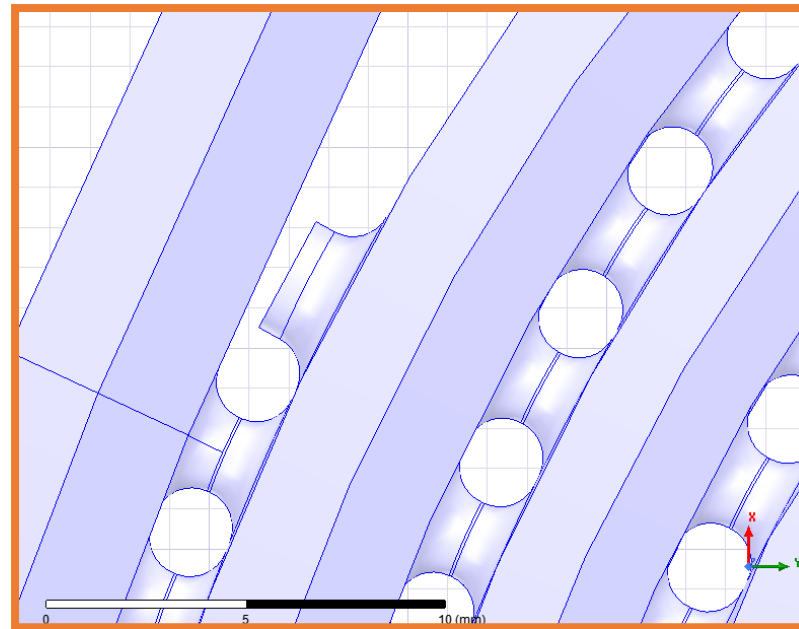


# Final Model (in HFSS)

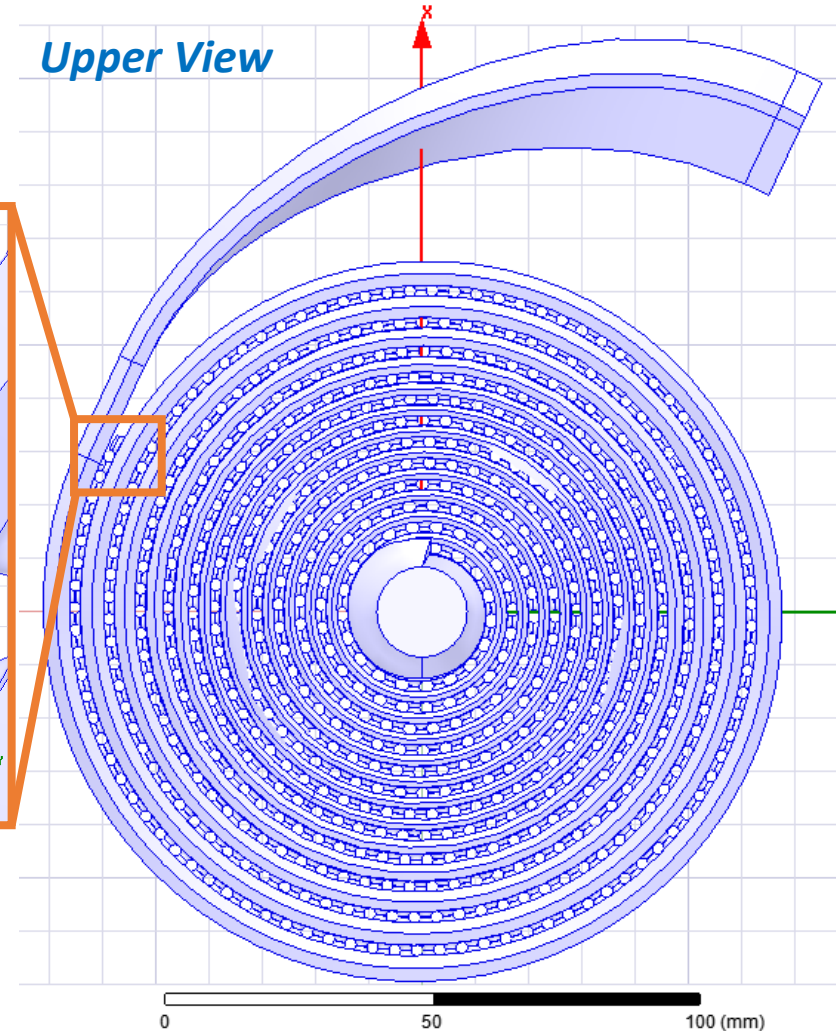
Side View



Tuning hole



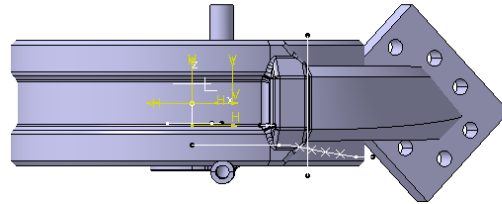
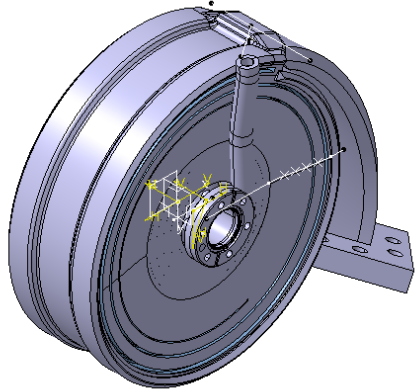
Upper View



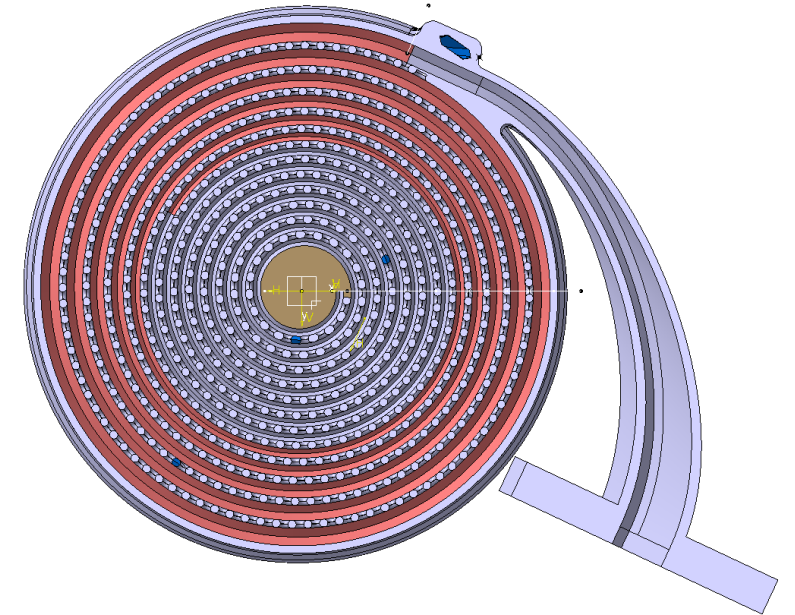
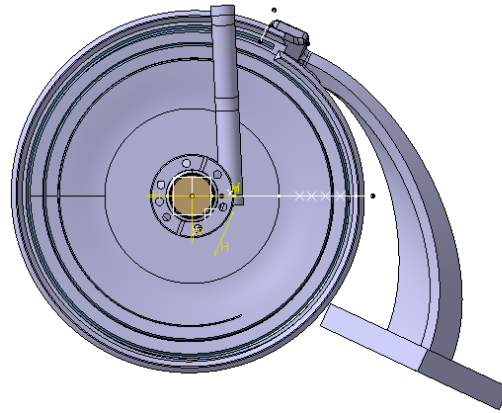
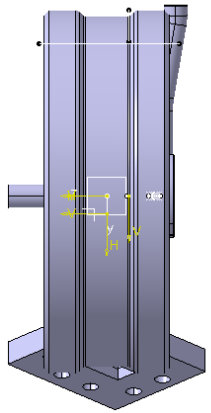
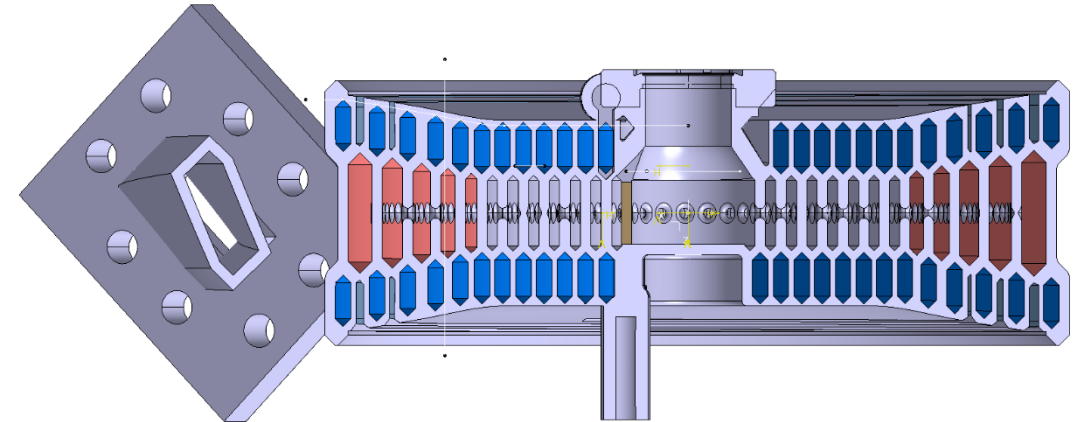
Mechanical Design by Oleg Gumenyuk

# Final Model (in CATIA)

*Side Views*



*Internal Views*



# Conclusion & Future Work

- RF Design of spiral load with new cross-section is ready!  
*(<https://edms.cern.ch/document/2404437/1>)*
- Cooling Circuit Integration
- Mechanical Design (Ongoing by Pedro Morales Sanchez)
- Thermal Simulations
- Production by Additive Manufacturing
- RF Test



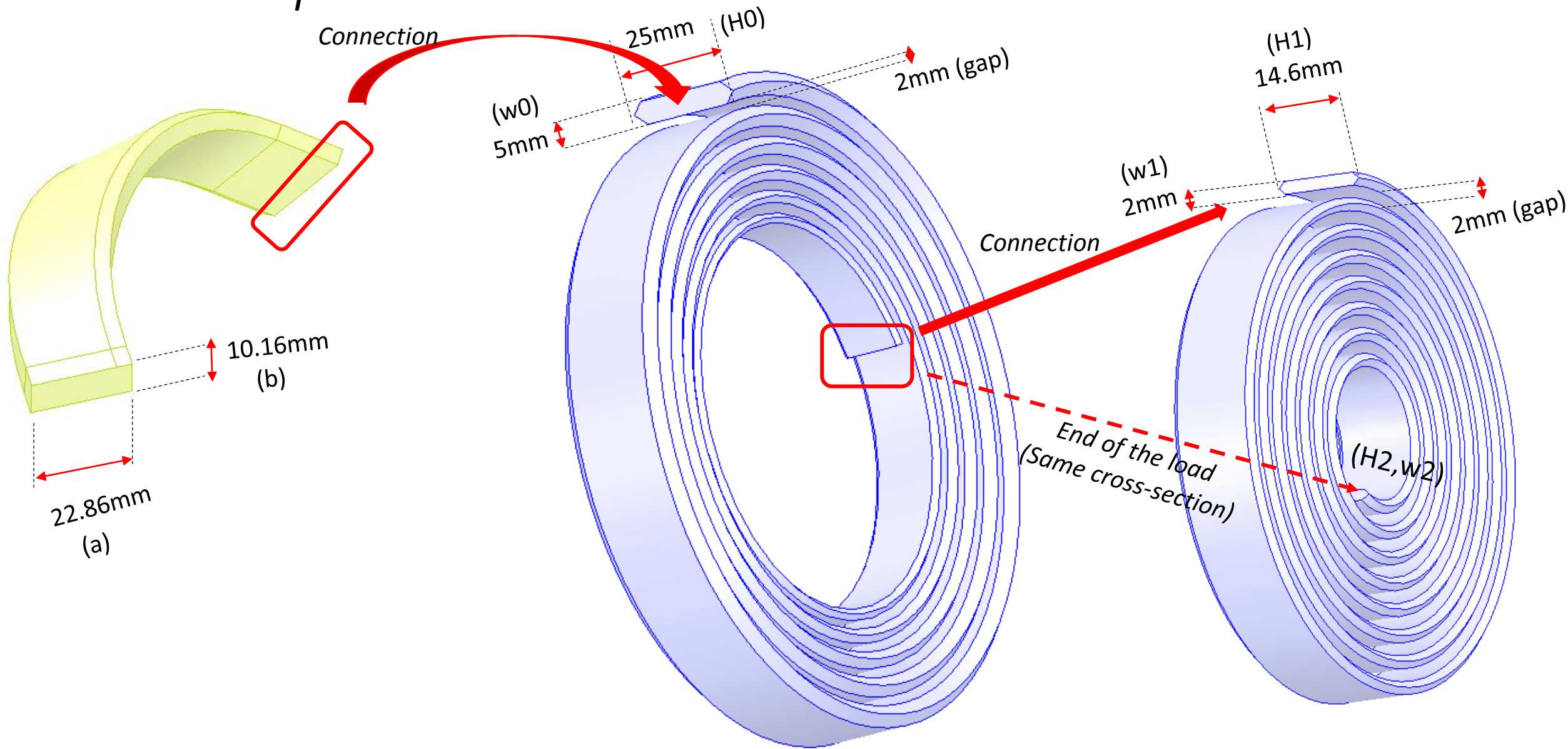
Thank you for your attention!

*Special thanks to;  
Nuria Catalan Lasheras, Benoit Riffaud, Oleg Gumenyuk,  
Romain Gerard, Joel Sauza Bedolla, Pedro Morales Sanchez*

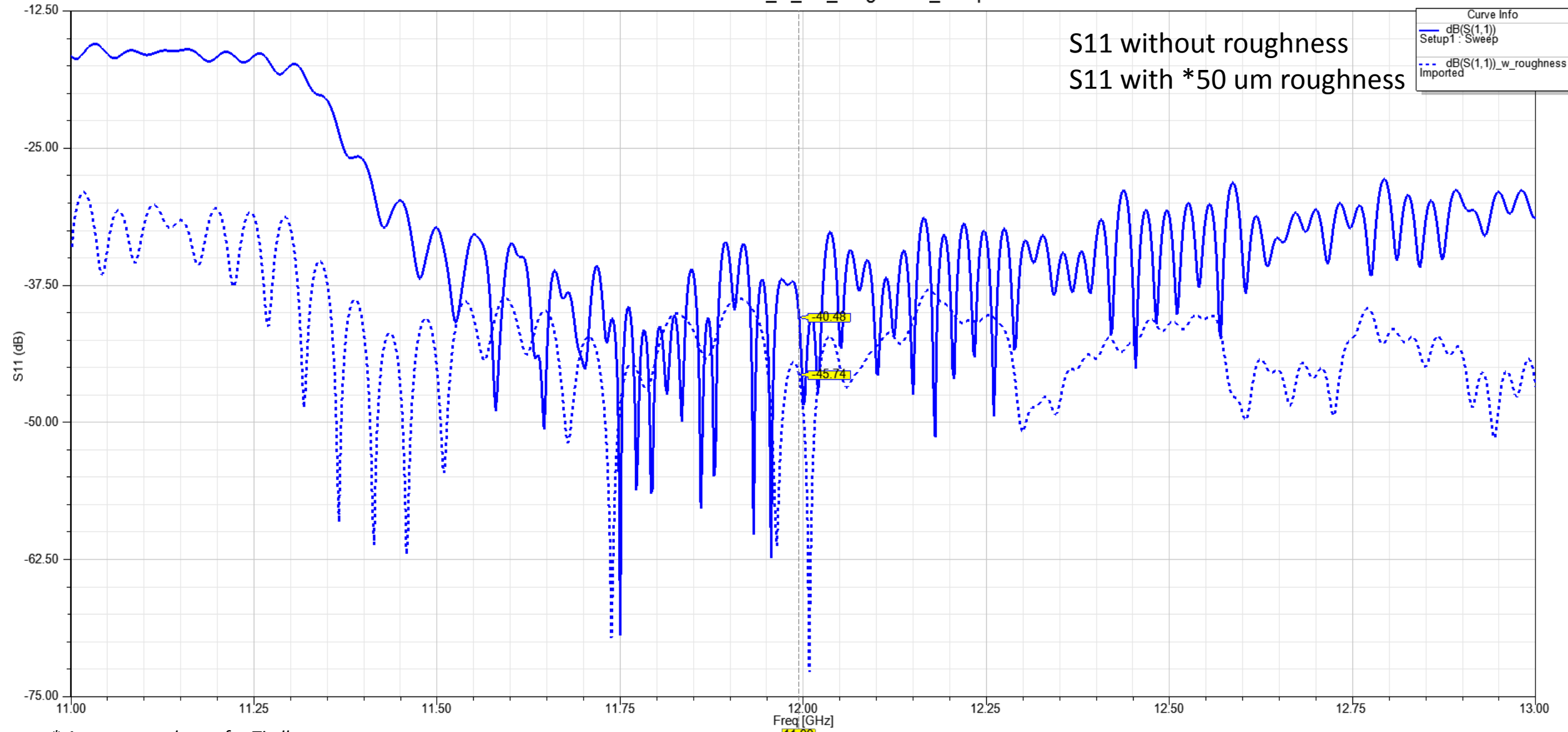
# Backup Slides



# Spiral Model Dimensions-Final Version



S Parameter Plot 1\_w\_wo\_roughness\_comp



S11 without roughness  
S11 with \*50 um roughness

Curve Info	
—	dB(S(1,1)) Setup1: Sweep
- - -	dB(S(1,1))_w_roughness Imported

\* Average roughness for Ti alloy

M.Heretis, P.Spanoudakis, N.Tsourveloudis, "Surface Roughness characteristics of Ti6Al4V alloy in conventional lathe and mill machining", Technical University of Crete, p.5 2009

11.9942 GHz

Spiral Model without vacuum port