

MSC Seminar

Electron spin resonance magnetic field sensors for the B-Train systems

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→ Introduction

→ Design

→ Results and experimental validation

→ Conclusions and future perspectives

→ Real-time magnetic field measurements:

Purpose:

- Measure the field of the main bending magnets of the Synchrotron accelerators
- ⇒ For the RF accelerating cavities
- ⇒ For beam intensity calculation
- ⇒ For the power converter of the main bending magnets

Why measurement instead of simulation?

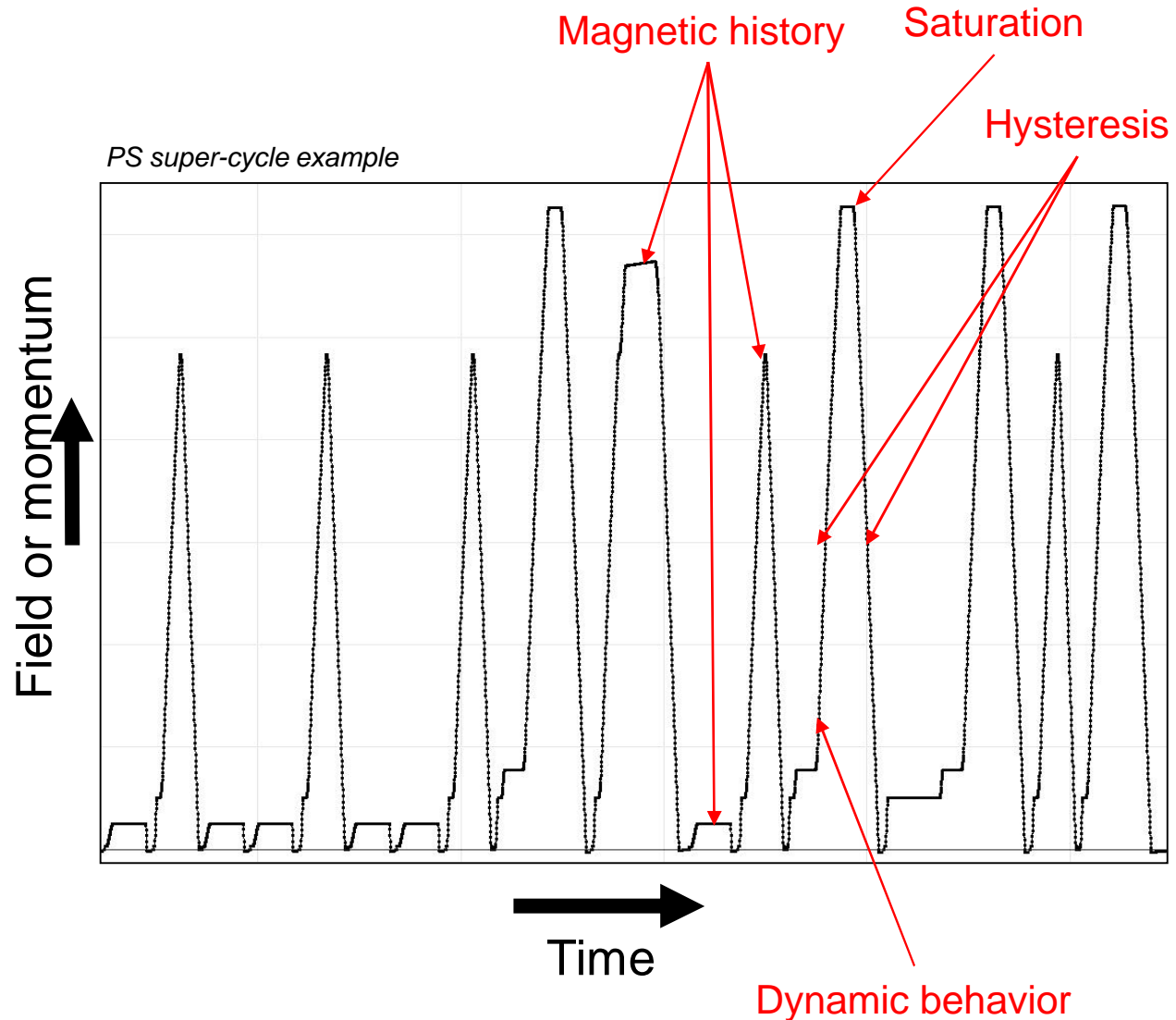
Problem to predict the **combined effects**

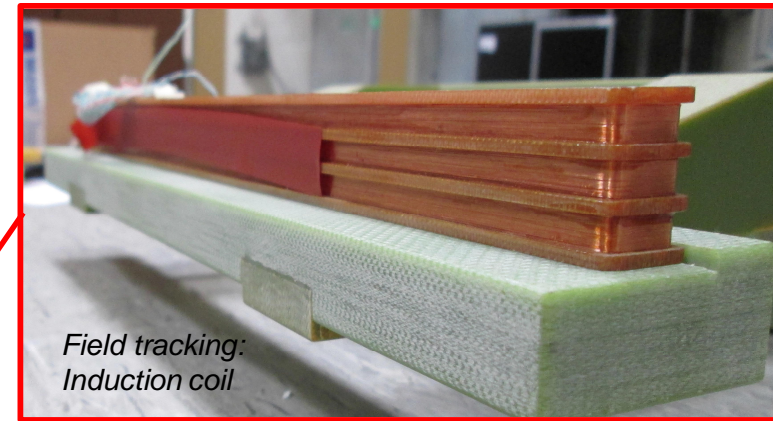
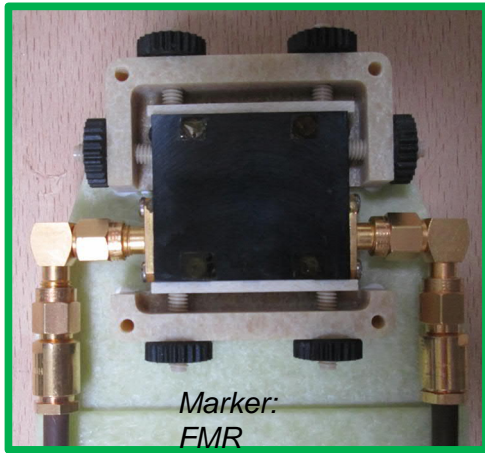
Improvement on the accelerator operation:

- Increase the field reproducibility
- Reduce the cycle time

What is needed:

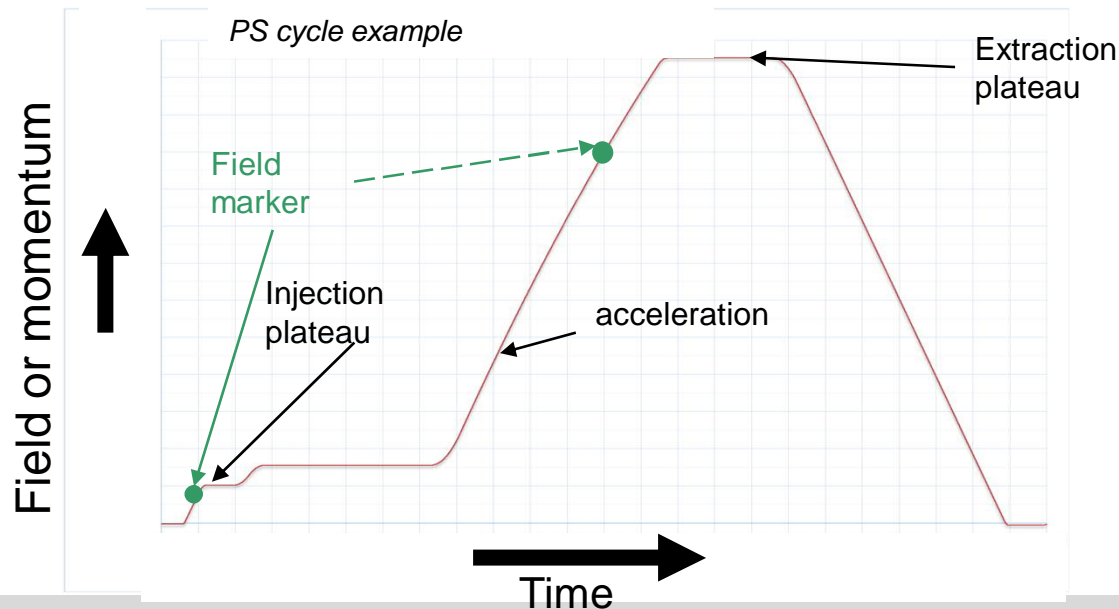
- Absolute local/integral field at 250 kHz
- Wide dynamic range from about 0 to 2 T
- A reference magnet (when available)





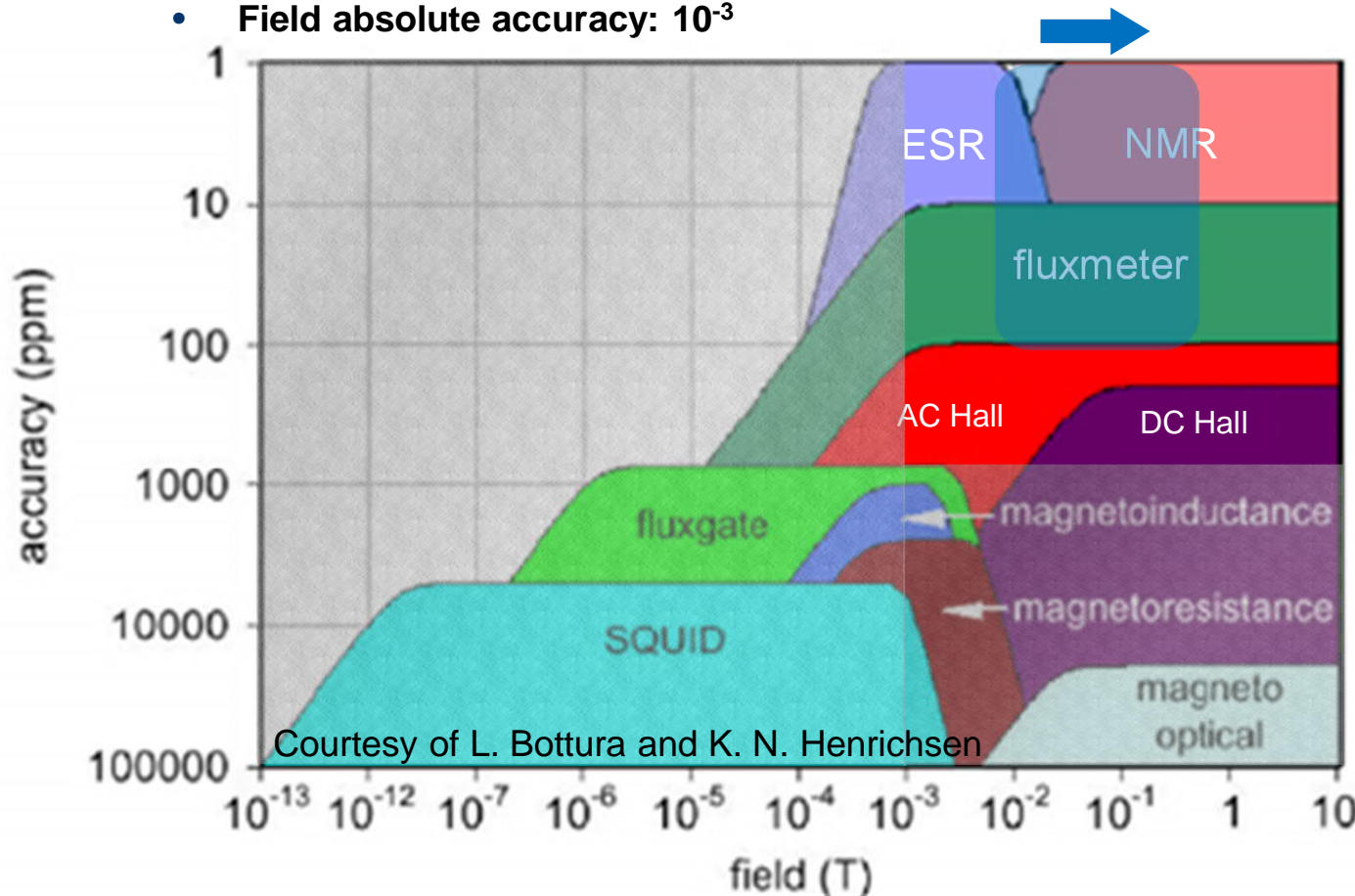
$$B(t) = \underbrace{B_{marker}(t_0)}_{\text{The reference field}} + \underbrace{\frac{1}{A_{coil}} \int_{t_0}^t V_{coil} dt}_{\text{The field variation}}$$

- The magnetic field B in (T)
- The reference field B_{marker} in (T)
- The starting time t_0 in (s)
- The coil surface A_{coil} in (m²)
- The induced coil voltage V_{coil} in (V)



→ Minimum requirements:

- Field range: up to 0.7 T
- Field ramp rate: up to 5 T/s
- Field gradient: up to 1.2 T/m, equivalent to an inhomogeneity G/B_{marker} of 10 m^{-1}
- Field reproducibility : better than 10^{-4} at beam injection
- Reliability: only few hours of downtime per year allowed
- Required lifetime: > 20 years
- Field absolute accuracy: 10^{-3}



Hall probes [1]:

- Wide dynamic range
- Low stability
- Regular calibration needed

Fluxmeter (rotating or translating):

- Not real time

NMR (Nuclear Magnetic Resonance) [2]:

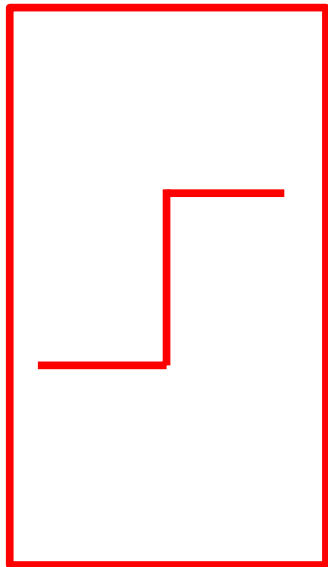
- Metrological reference
- Field inhomogeneity $< 0.06 \text{ m}^{-1}$
- Low field ramp rate $< 0.1 \text{ T/s}$

ESR (Electron Spin Resonance) [3,4]:

- High inhomogeneity field $> 5 \text{ m}^{-1}$
- High field ramp rate $> 2.3 \text{ T/s}$
- Calibration and operation
- Low field measurement $< 10 \text{ mT}$

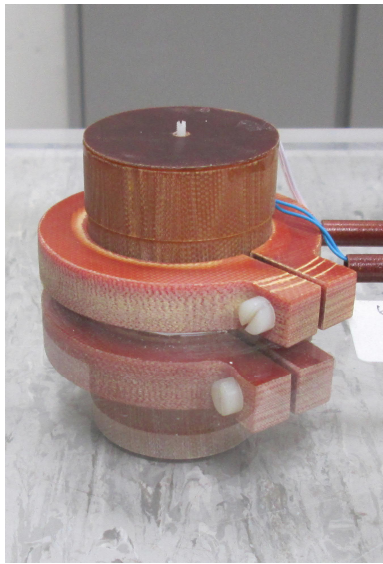
→ Markers used in the CERN accelerators

Software Marker



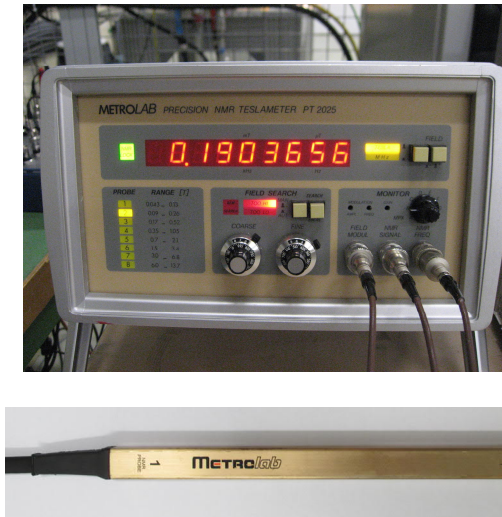
Preset value

Peaking Strip



5 mT

NMR

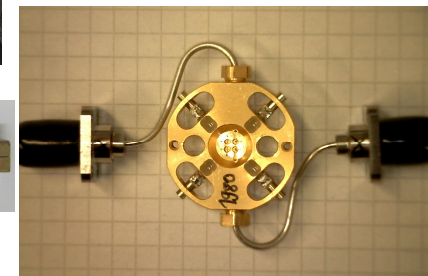


~43-2000 mT

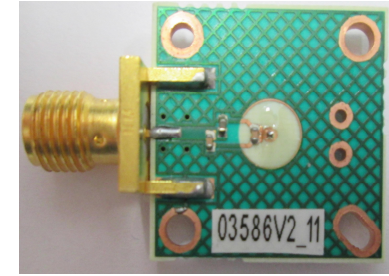
ESR

Ferrimagnetic resonance (FMR)

Electron paramagnetic resonance (EPR)

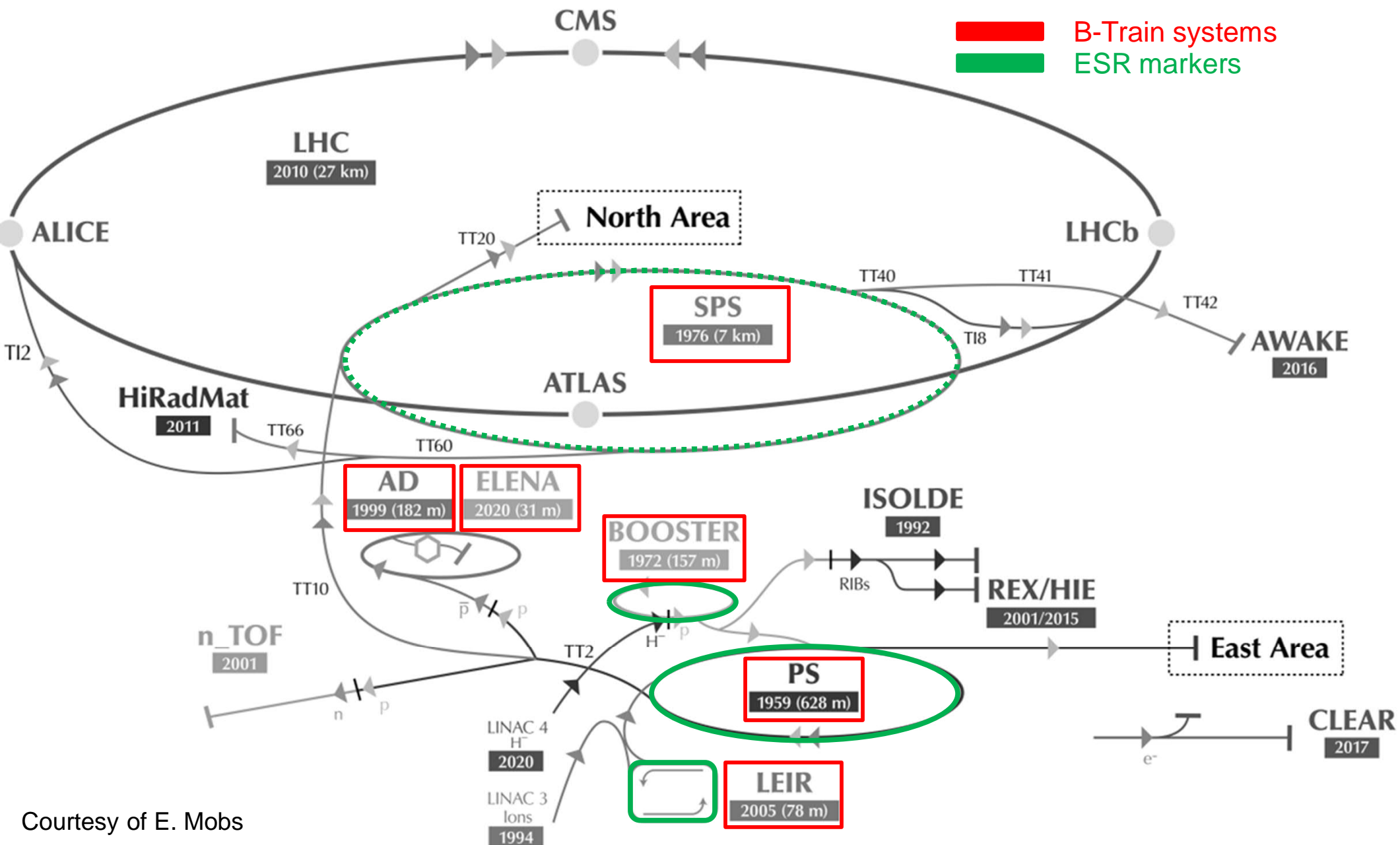


~36-50 mT



~36-760 mT

Introduction: ESR sensors at CERN



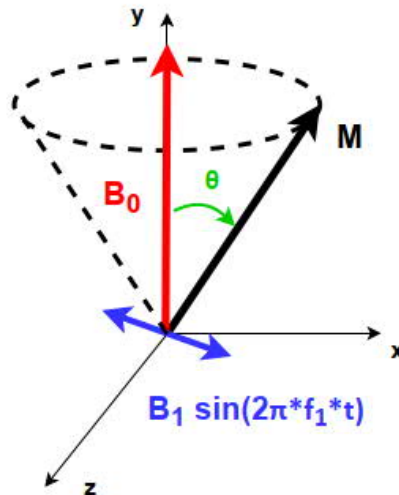
Courtesy of E. Mobs

→ Magnetic resonance:

- In presence of a background magnetic field B_0

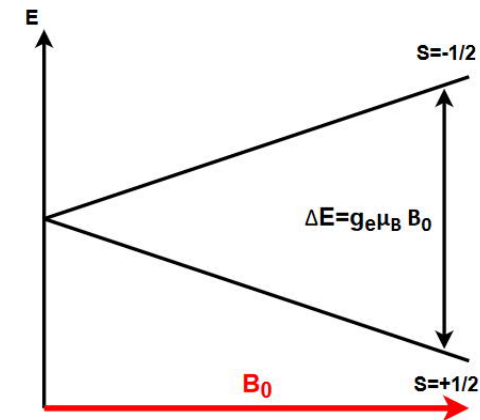
Classical view

$$\frac{1}{\gamma_e} \frac{d\mathbf{M}}{dt} = \mathbf{M} \times \mathbf{B}_0$$



Quantum view

$$\Delta E = hf_0$$



- When sample is irradiated with an external microwave $B_1 \perp B_0$

- The resonance occurs when $f_1 = f_0$:

The Larmor frequency is given by

$$f_0 = \left(\frac{\gamma}{2\pi} \right) B_0$$

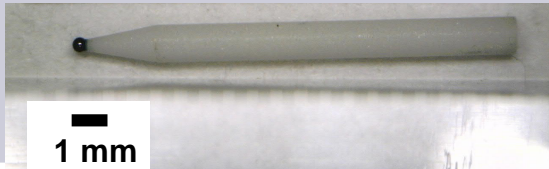
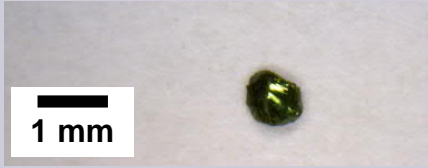
$$\frac{\gamma_{n(1H)}}{2\pi} = 42.6 \text{ MHz/T (for proton)}$$

$$\frac{\gamma_e}{2\pi} = 28025 \text{ MHz/T (for an isolated electron)}$$



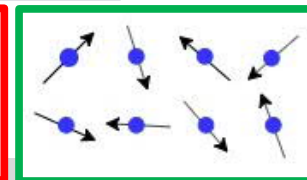
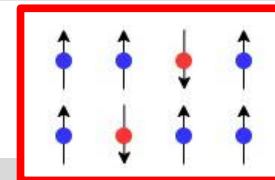
Factor ~670 !

These two gyromagnetic ratios are known within 10^{-7} accuracy or better [5]

	FMR	EPR
Magnetic property	Ferrimagnetic ¹	Paramagnetic ²
Material	Gallium doped Yttrium iron garnet (GaYIG)	Organic free radical α,γ -bisdiphenylene- β -phenylallyl (BDPA)
Chemical composition	$\text{GaY}_3\text{Fe}_5\text{O}_{12}$	C_{39}H_5
Usage	Microwave applications	Standard for EPR spectrometers
Spectrum	Single narrow linewidth	
Minimum operating field	30 mT (with Gallium doping)	$< 1 \mu\text{T}$
Anisotropy	high	very low
Signal amplitude (same detection electronic)	1500 mV	15 mV
Commercial presentation		

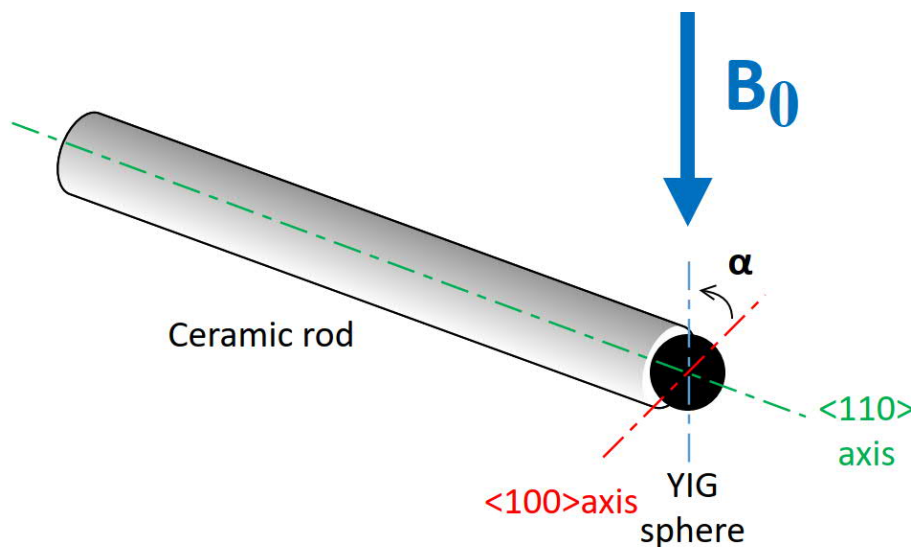
¹: Two unequal populations of atoms with anti-parallel magnetic moments and magnetization $\neq 0$

²: $B=0$ T magnetic moment $\neq 0$ but spin randomly oriented (magnetization=0)

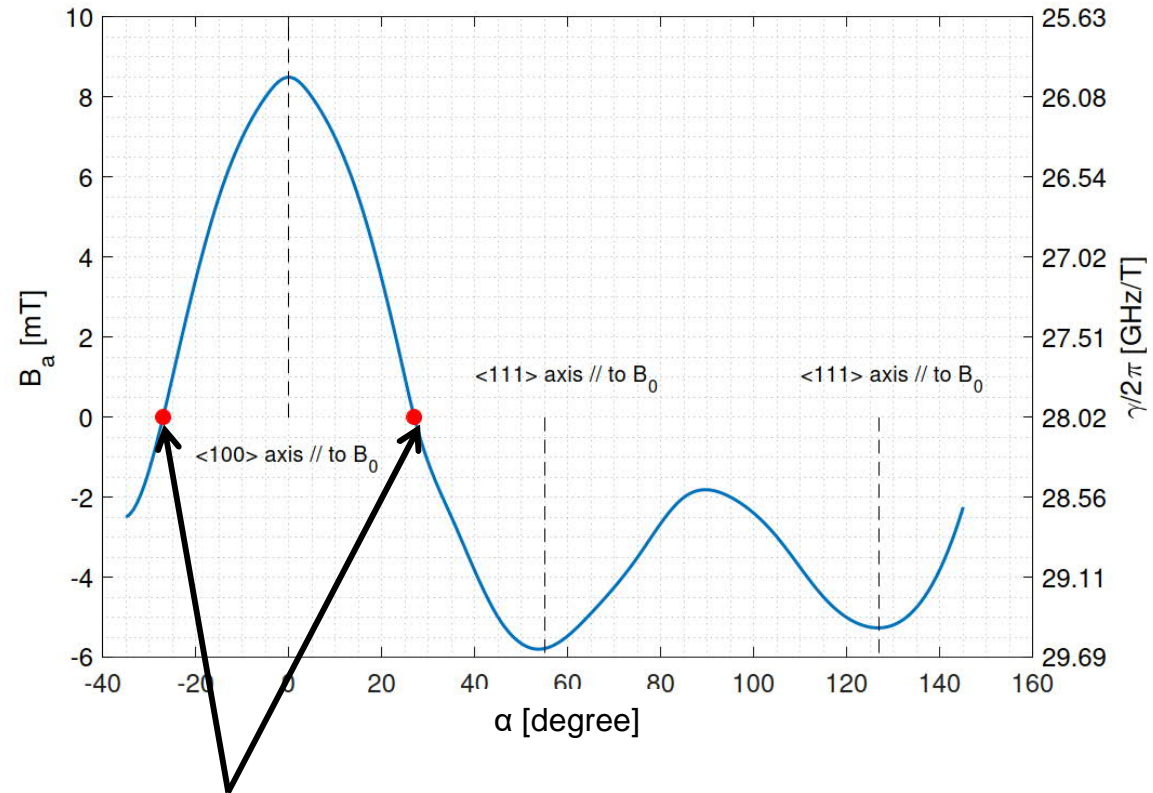


$$f_0 = \frac{\gamma_e}{2\pi} (B_0 + B_a)$$

→ B_a depends on crystal axis alignment with respect to B_0 and on the temperature



$$B_a = B'_a(\alpha) B''_a(T)$$



$B_a=0$ T therefore $\gamma = \gamma_e$, in addition
no more temperature dependency

⇒ Temperature stable axis at about $\alpha = \pm 30^\circ$

Microwave structures

Broadband devices

- Transmission line
- Coupling: typically YIG filter
 - The magnetic resonance changes the coupling coefficient

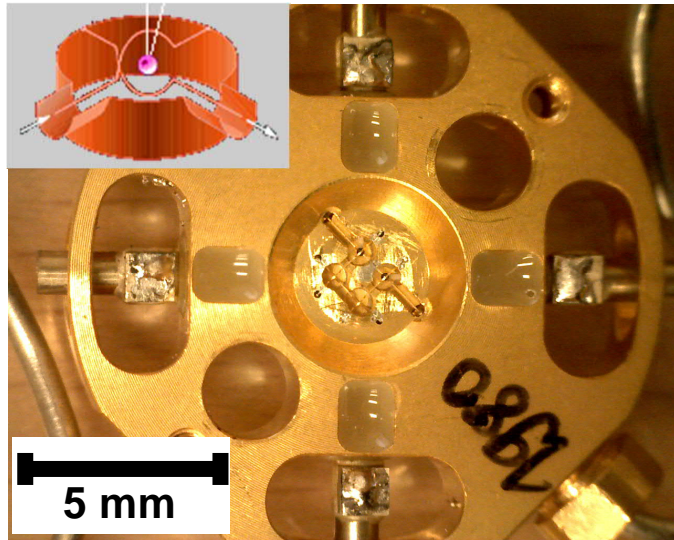
Narrowband devices (Optimized for the marker field level)

- Resonator :
 - RF source provided by external generator
- Oscillator:
 - RF source provided by internal generator (cross-coupled transistor)

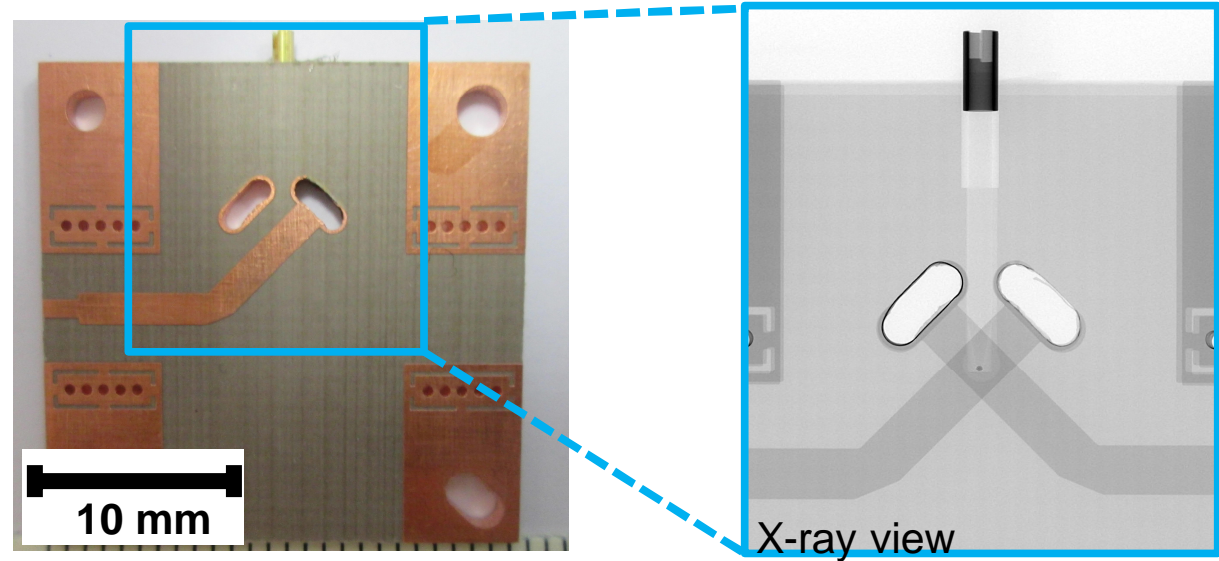
Magnetic resonance signal detection

- Amplitude
- Frequency
- Phase

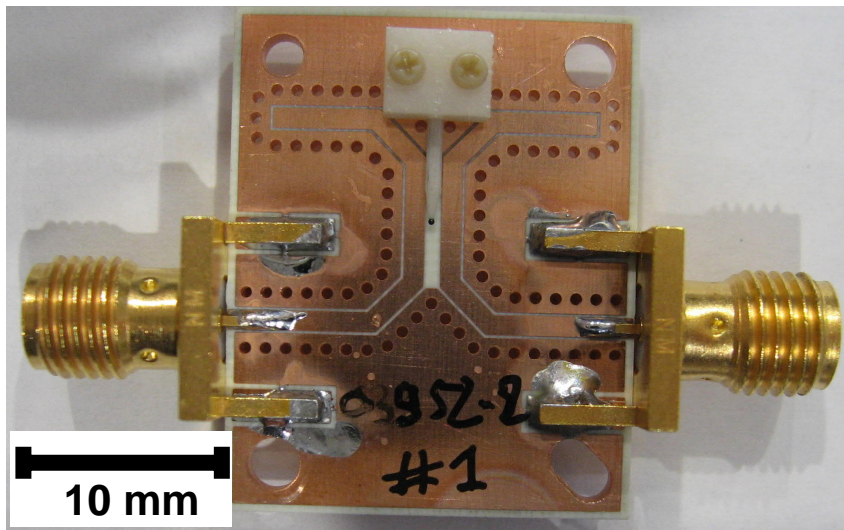
Commercial YIG filter



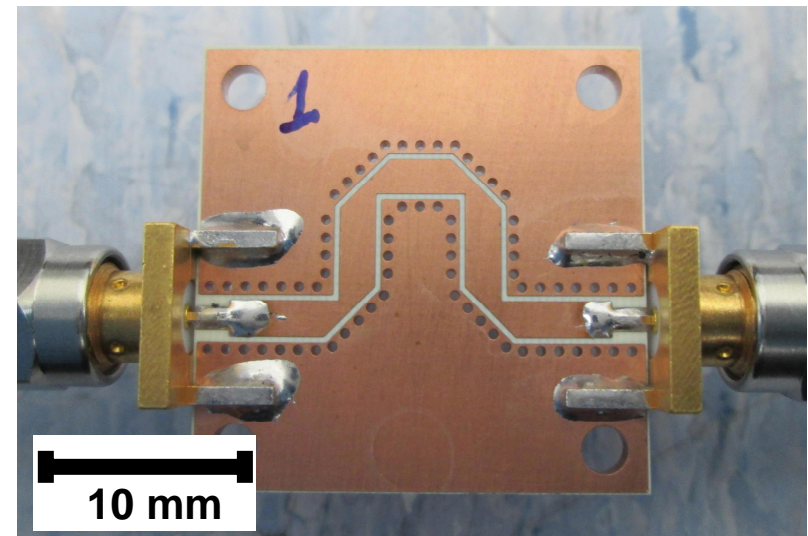
Stripline YIG filter



Coupling structure



Transmission line

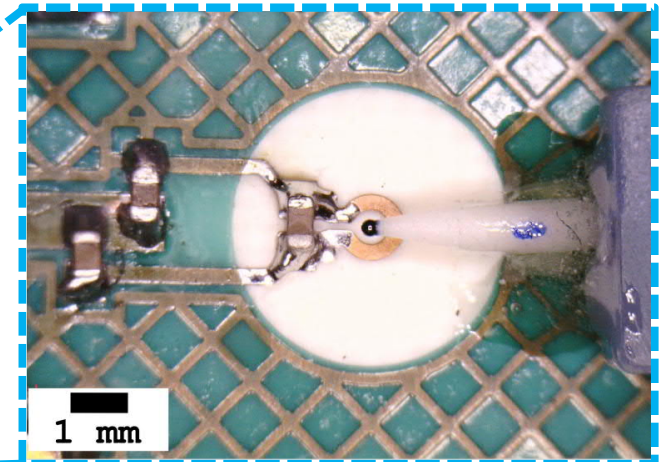


$f_0=1$ GHz $B_0=36$ mT

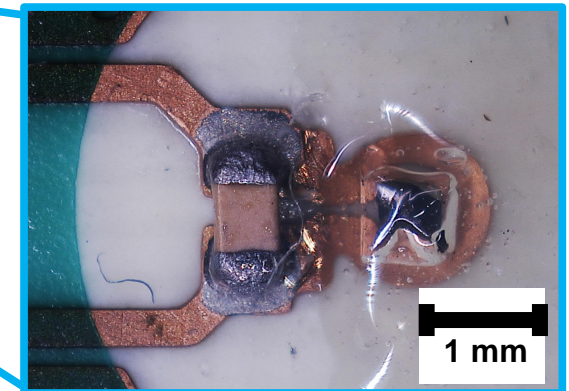
→ **Main application: PS low field marker**

- Suitable for $RF \leq 1$ GHz
- Non-ferromagnetic elements
- Tunable if varicaps are used
- Small size

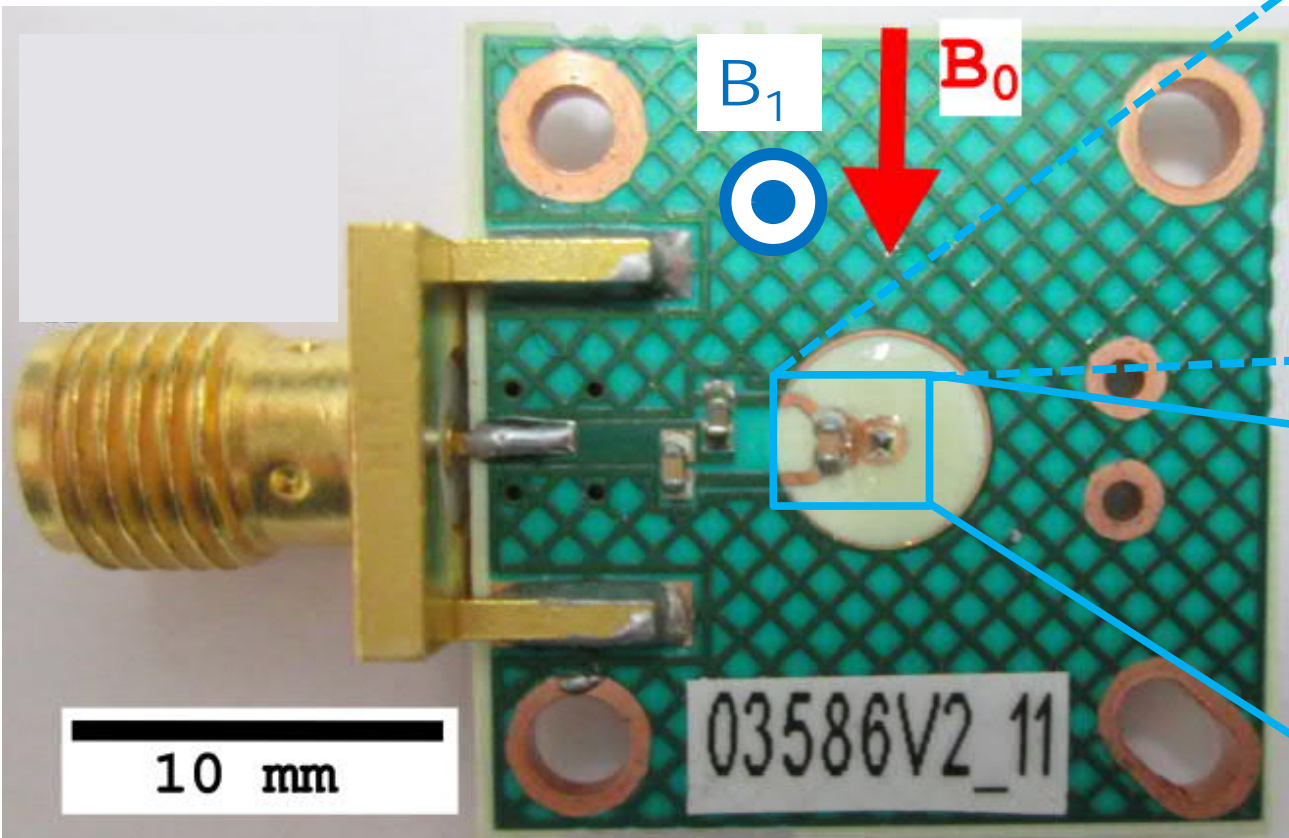
Sample types

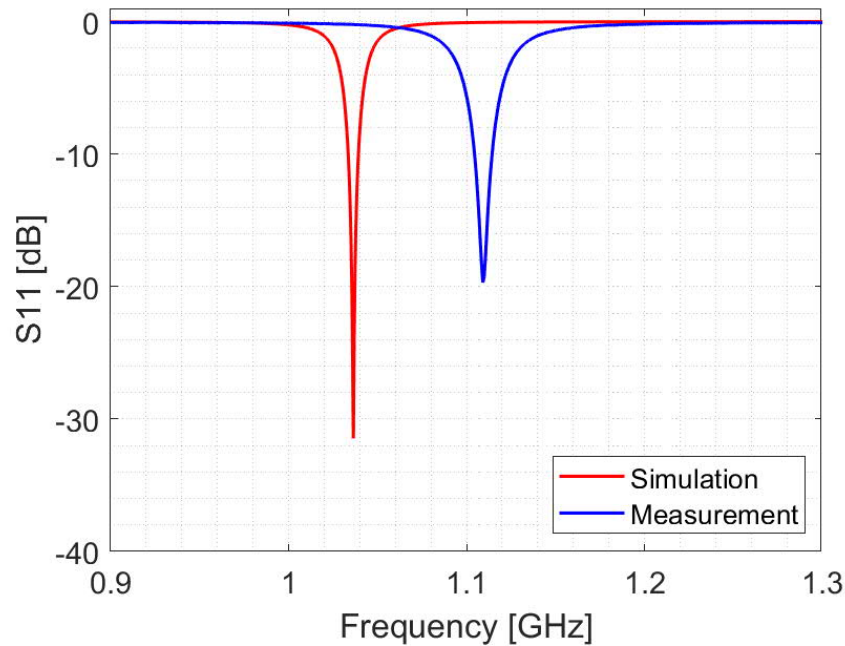
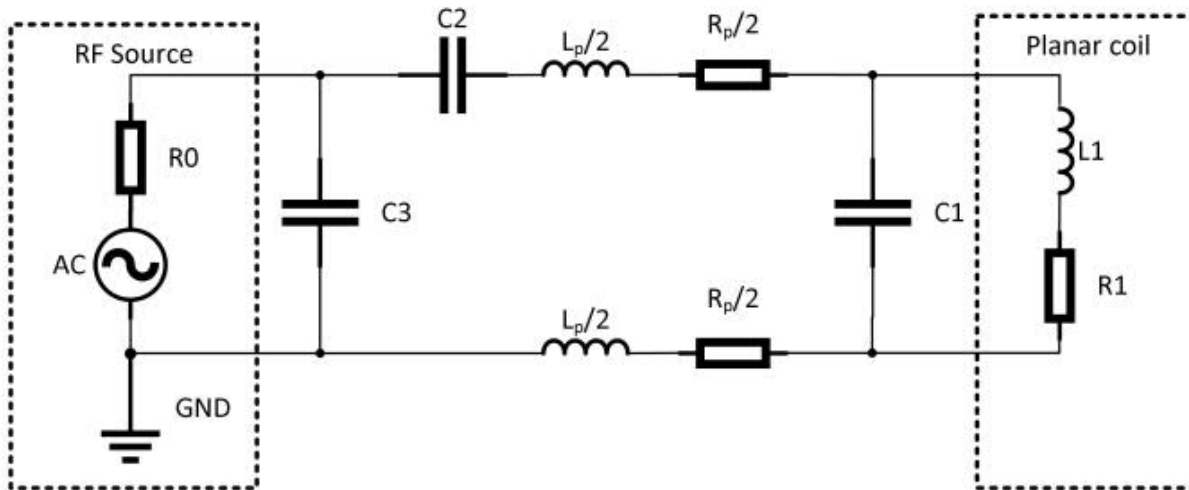


Ferrimagnetic



Paramagnetic



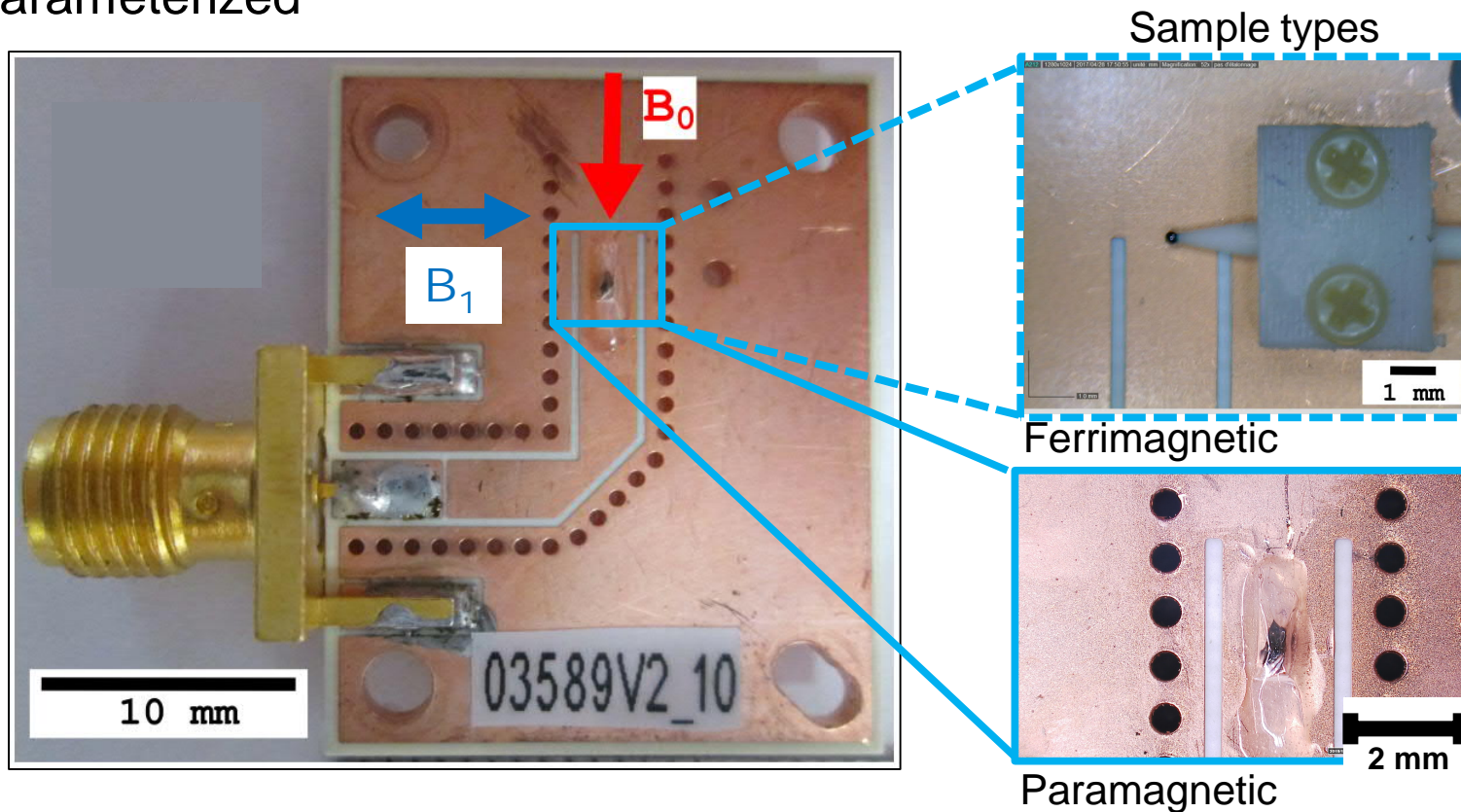


Elements	value
Substrate type	Rogers RO4350 B
Substrate size	20x20x1.5 mm ³
Tuning circuit C1	4.7 pF
Matching circuit C2	4.7 pF
Matching circuit C3	15 pF
L1	1.2 nH
R1 at 1 GHz	38 mΩ
L _p	4.13 nH
R _p	1.35 Ω
f _{res}	1.109 GHz
S ₁₁	-19 dB
Q-factor at -3 dB	36

Grounded CoPlanar Waveguide $f_0=3$ GHz $B_0=106$ mT

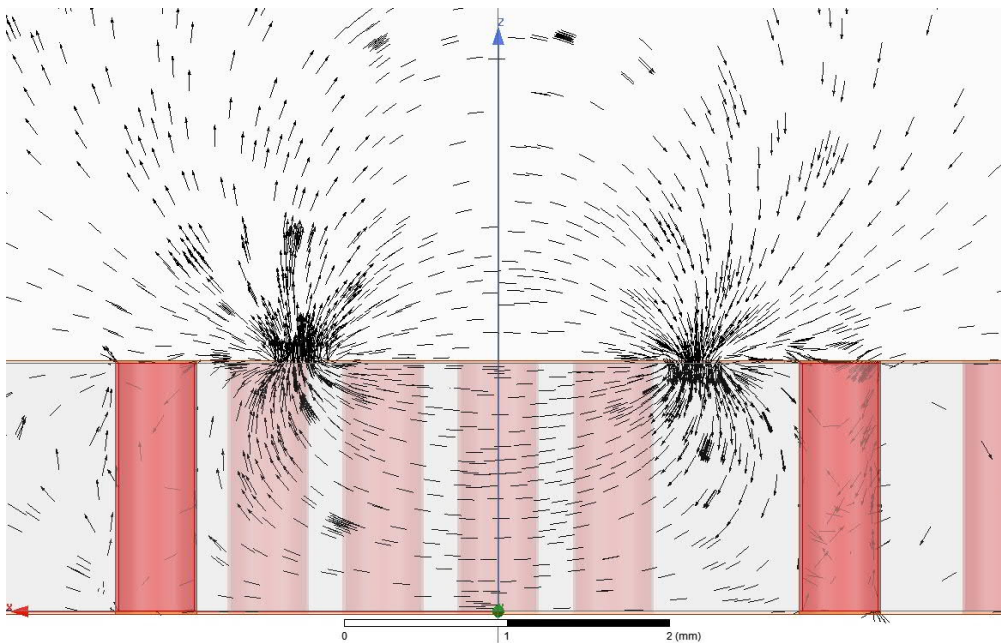
→ Main application: LEIR&PSB low field marker

- Suitable for RF > 1 GHz
- Small size when using $\lambda/4$
- Better control of the resonance frequency
- Fully parameterized

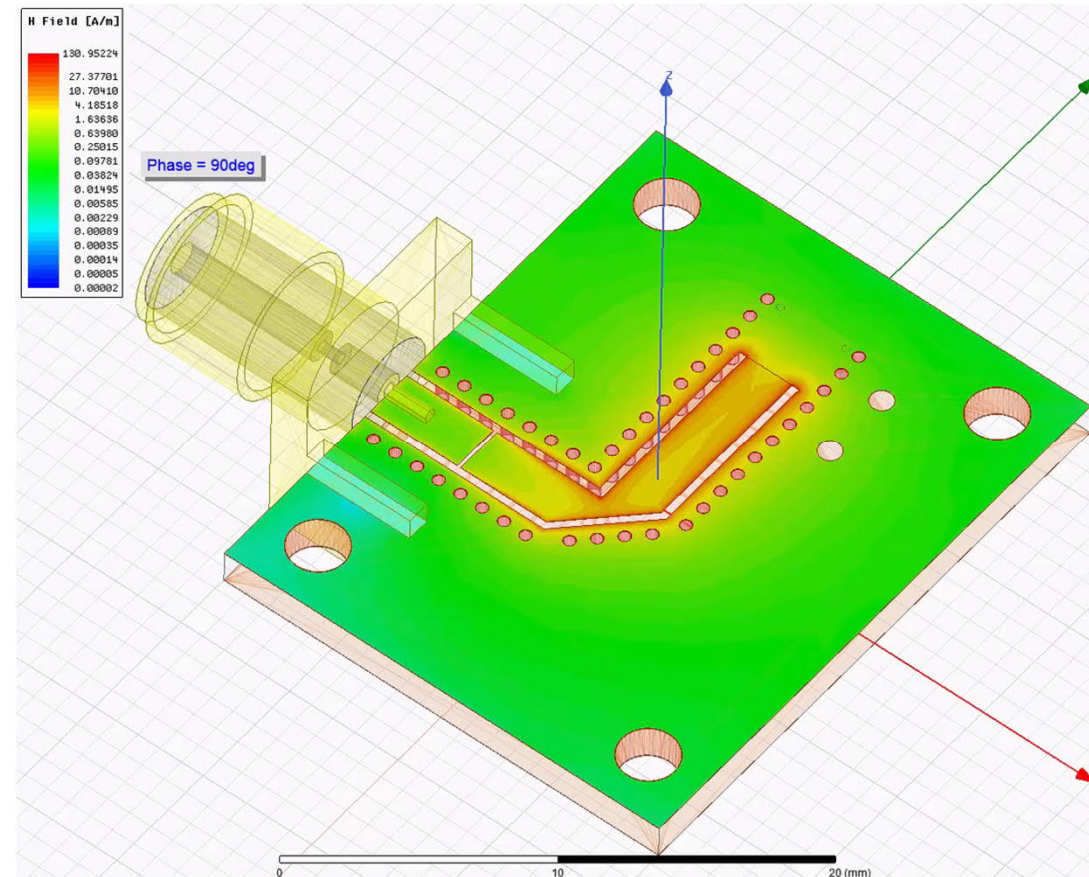


→ HFSS (Ansys Electronics Desktop) 3D simulation

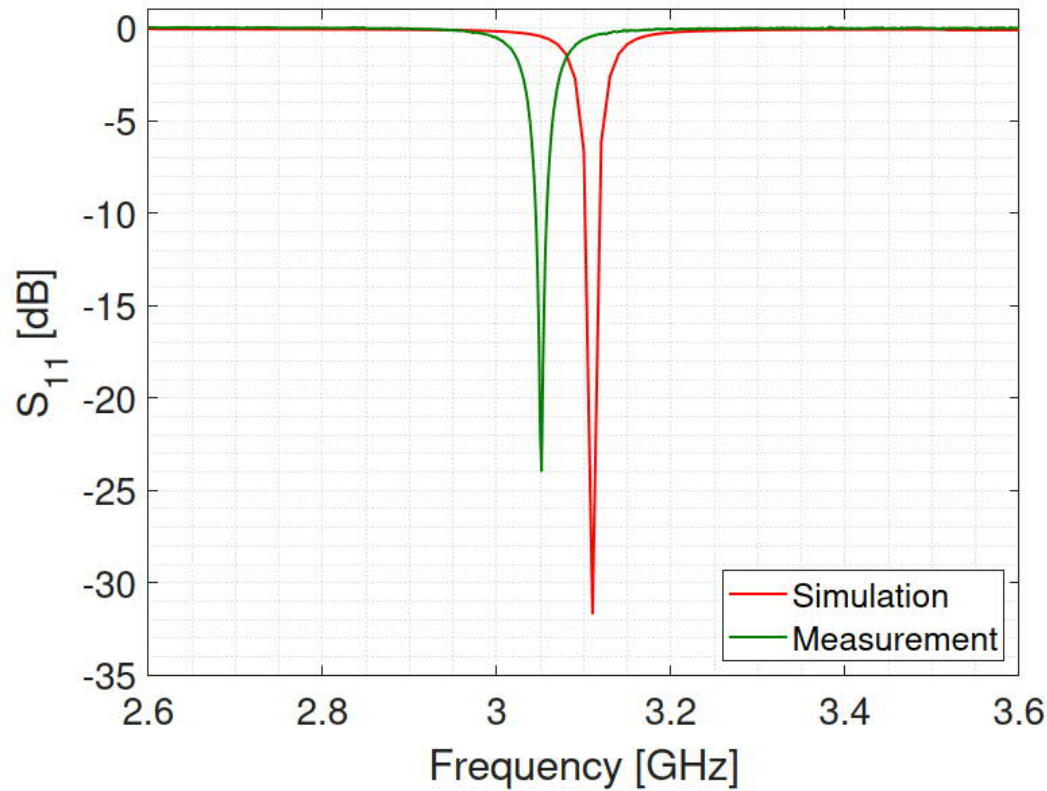
Magnetic field lines distr.



Magnetic field strength



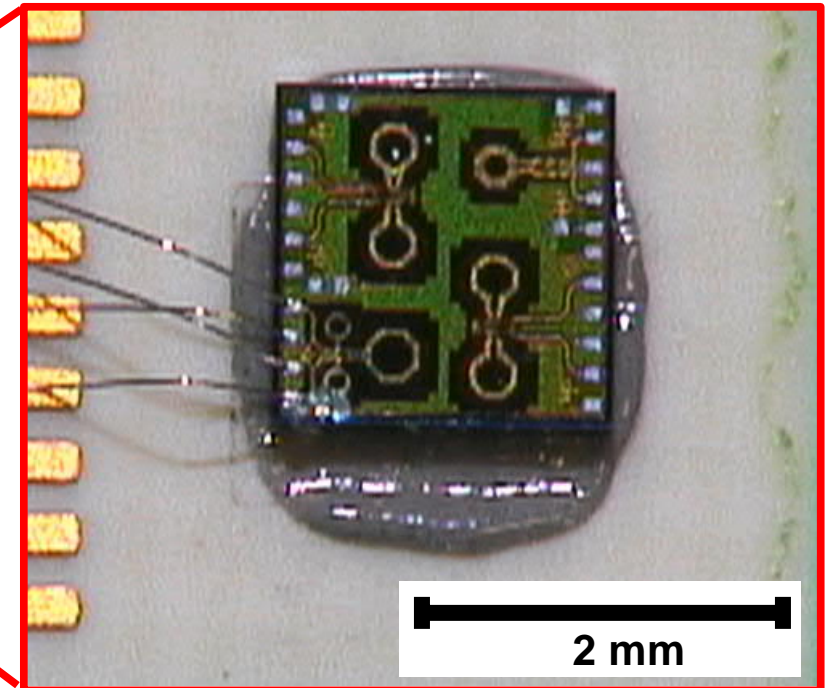
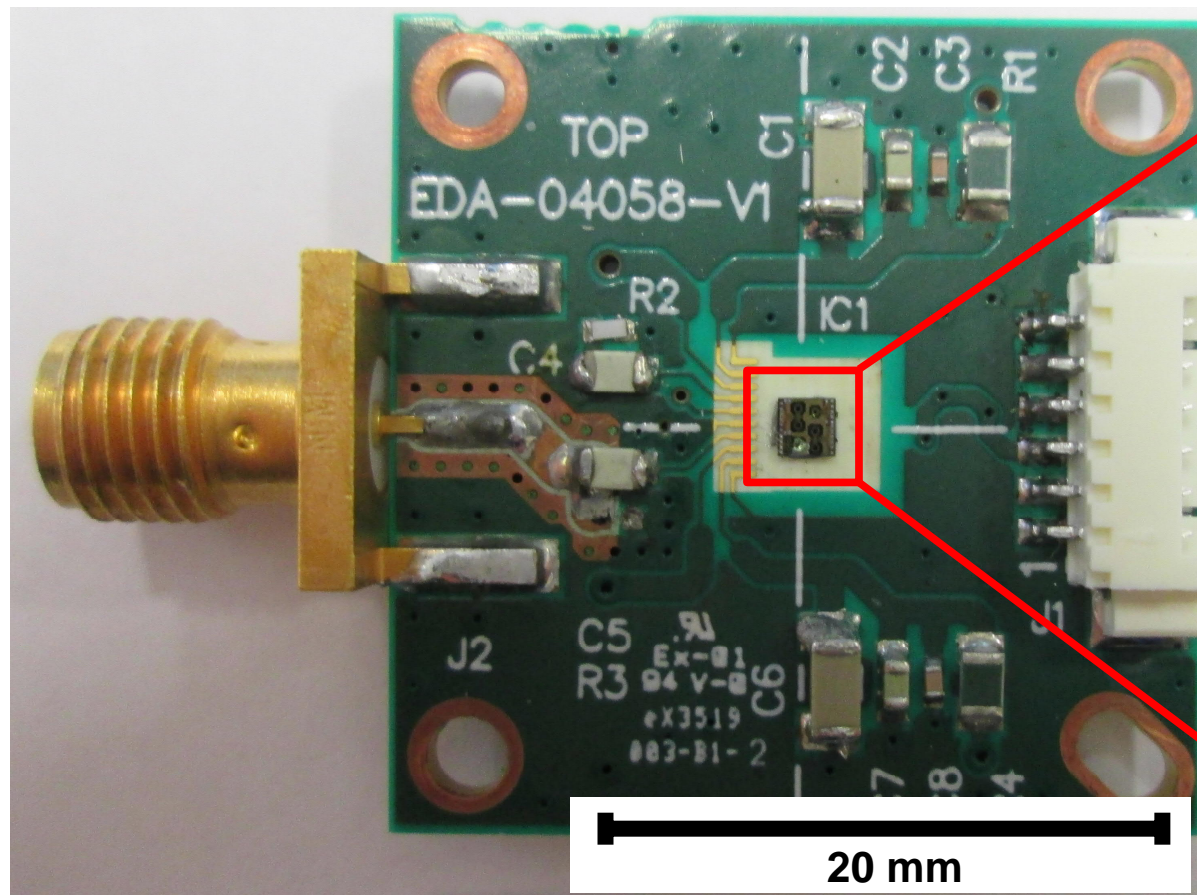
Return loss



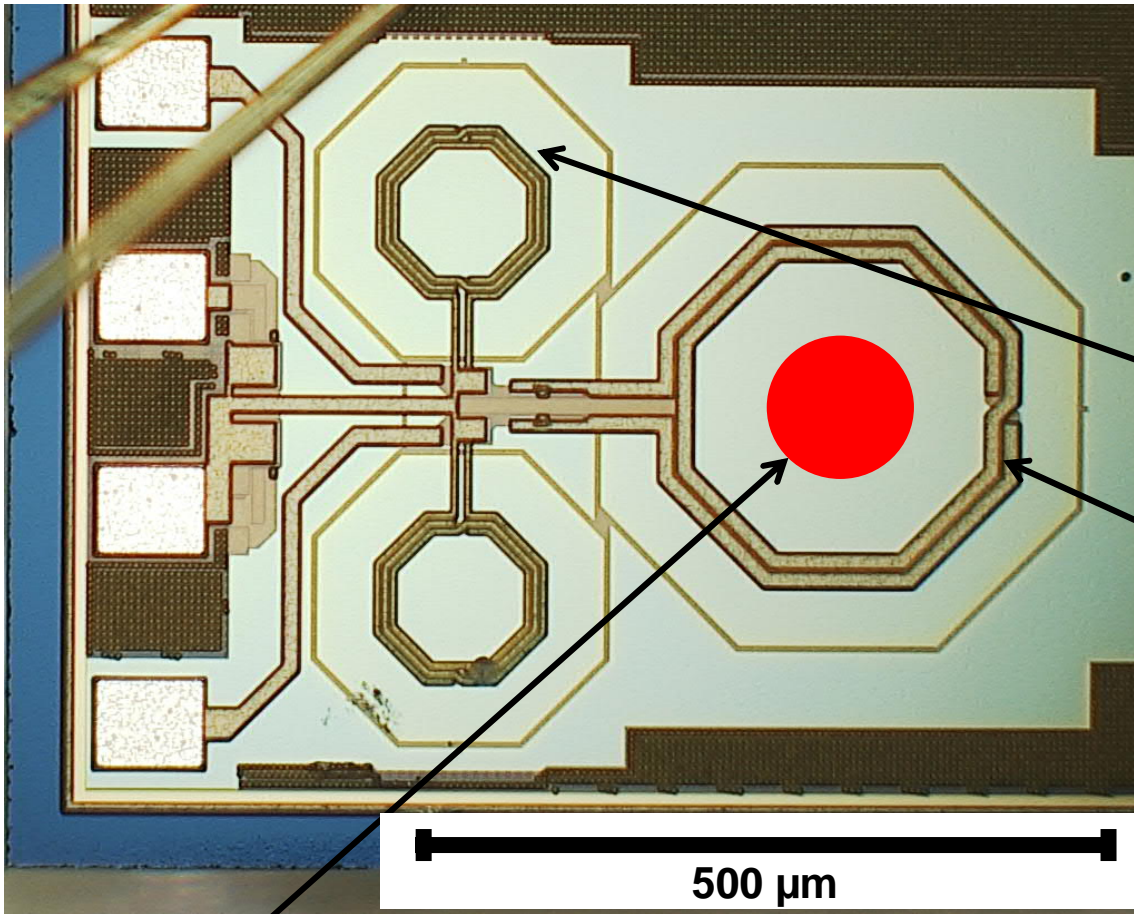
Elements	value
Substrate type	Rogers RO4350 B
Substrate size	25x20x1.5 mm ³
Strip width	2.1 mm
Strip length	15.25 mm
f_{res}	3050 GHz
S_{11}	-24 dB
Q-factor at -3 dB	70

Integrated oscillators chip

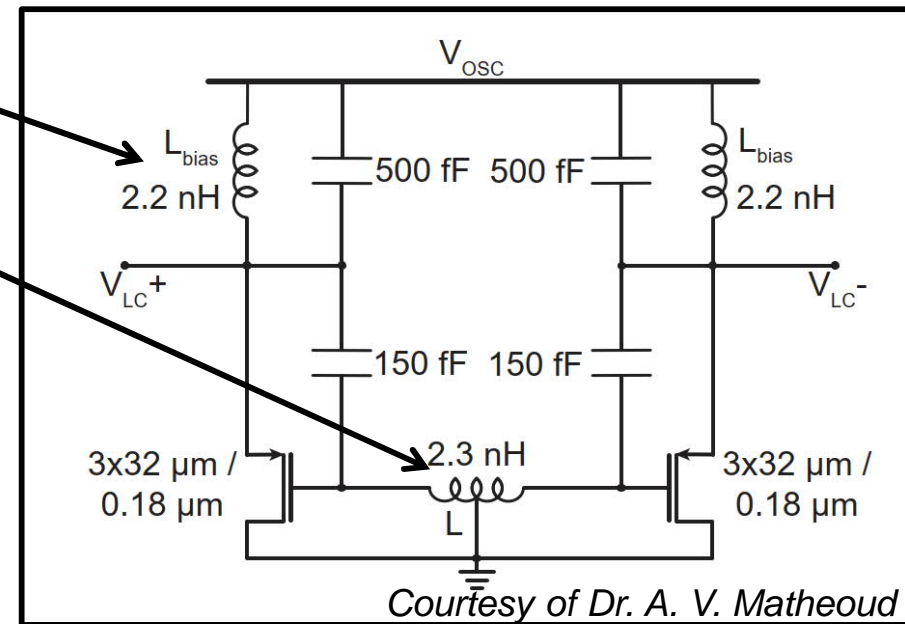
Designed at EPFL by Dr. G. Boero and Dr. A. V. Matheoud



Used of Integrated oscillator $f_0=10$ GHz $B_0=360$ mT [6]

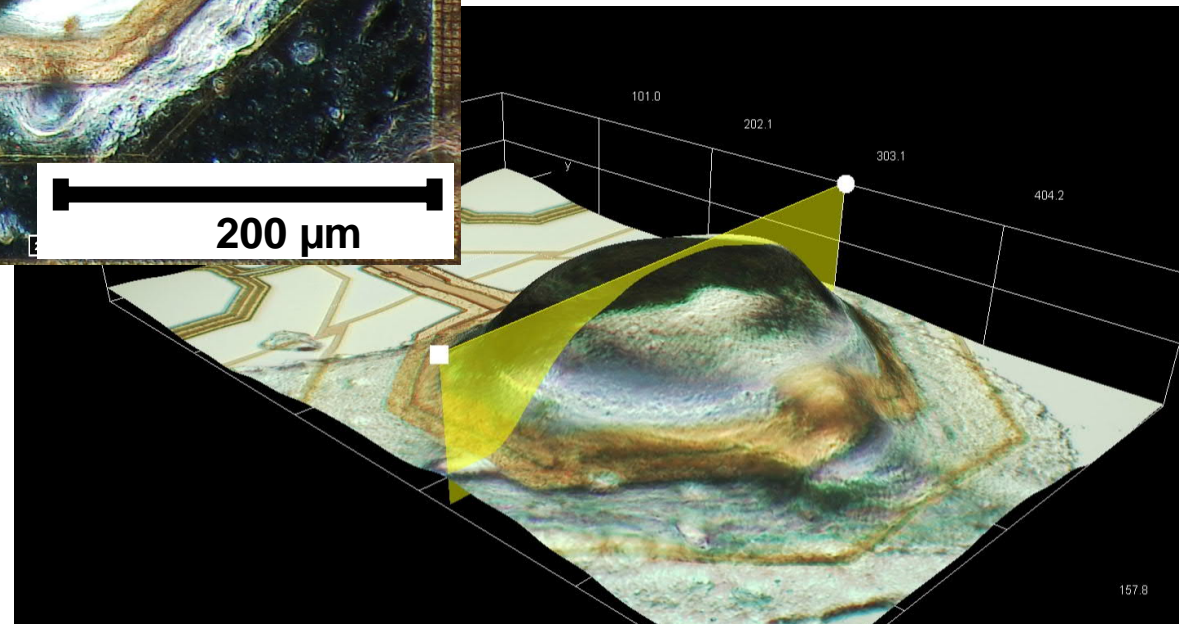
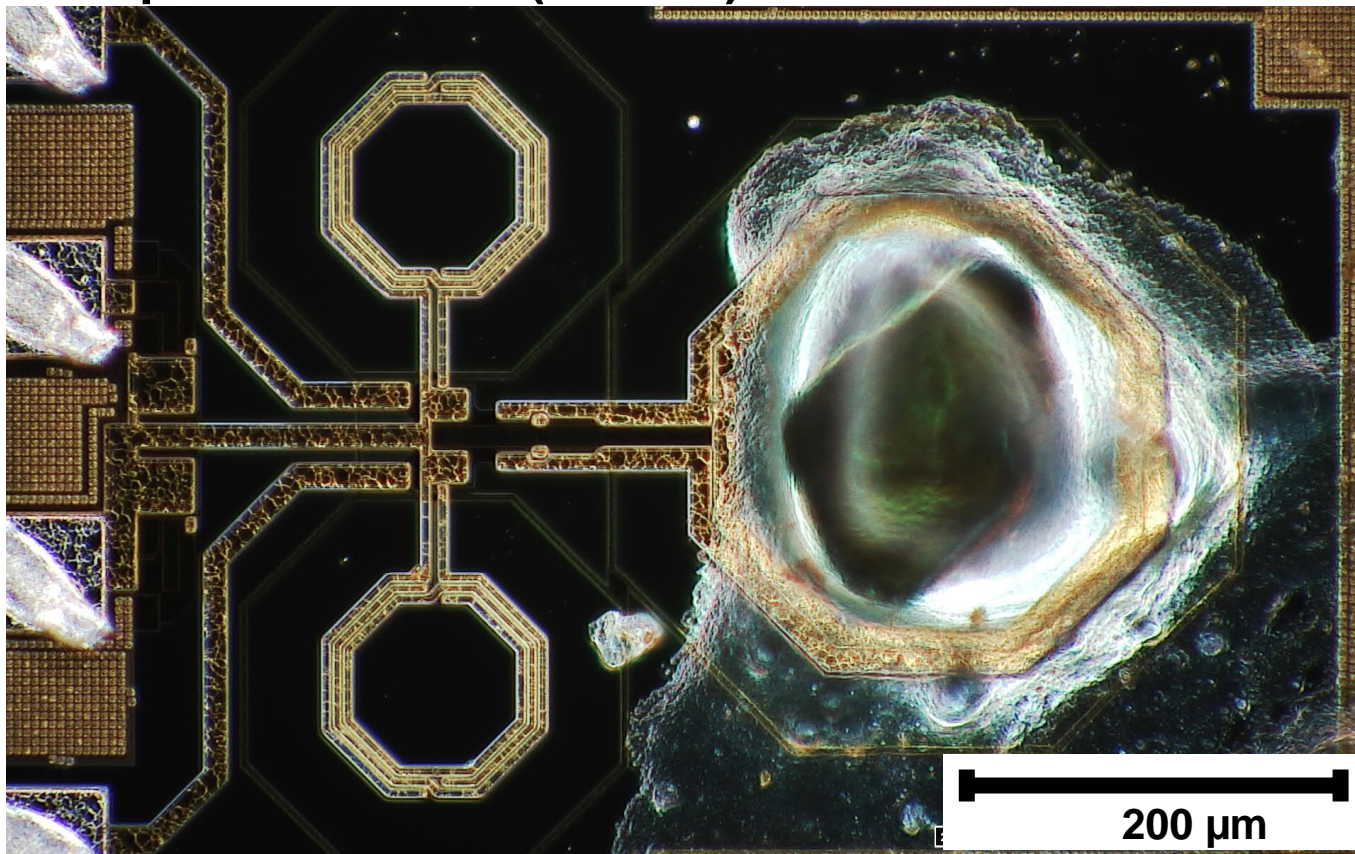


- Cross-coupled LC oscillator
- Manufactured in CMOS integrated circuit technology
- Fixed frequency

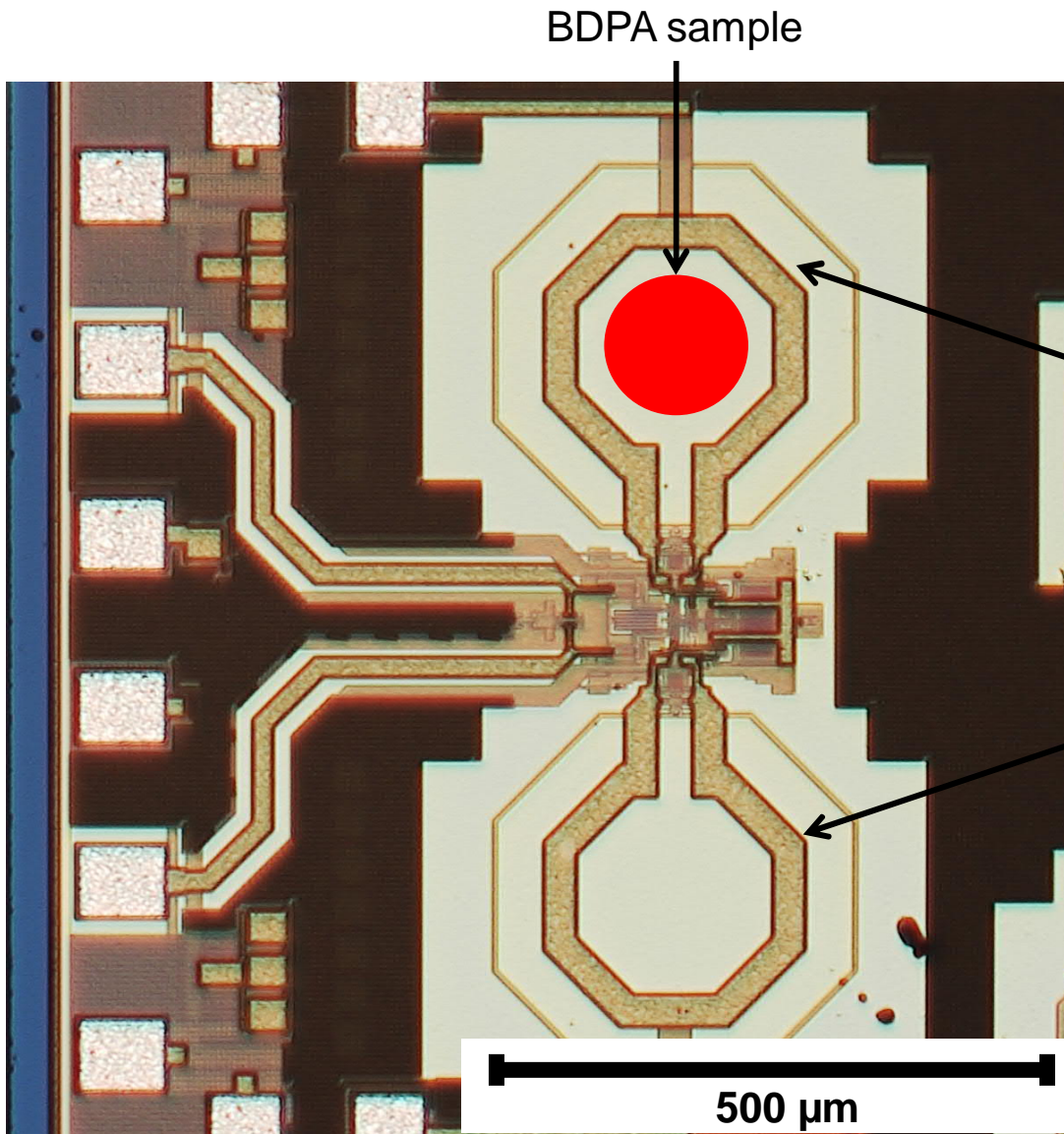


BDPA sample

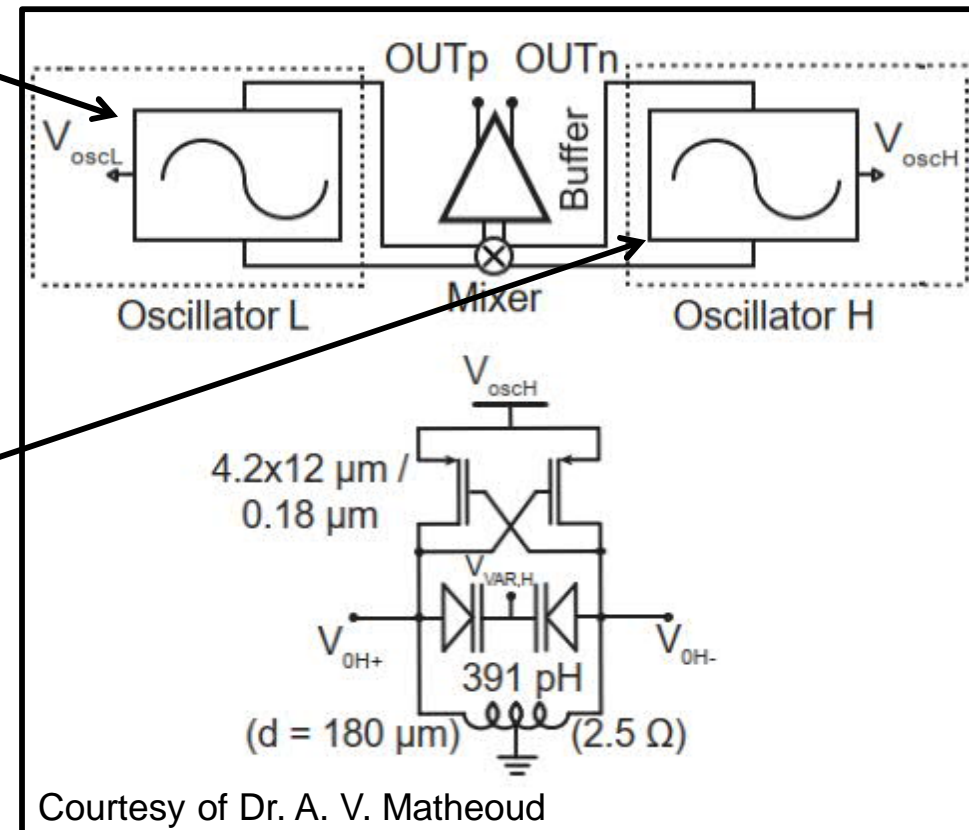
Sample installation (10 GHz)



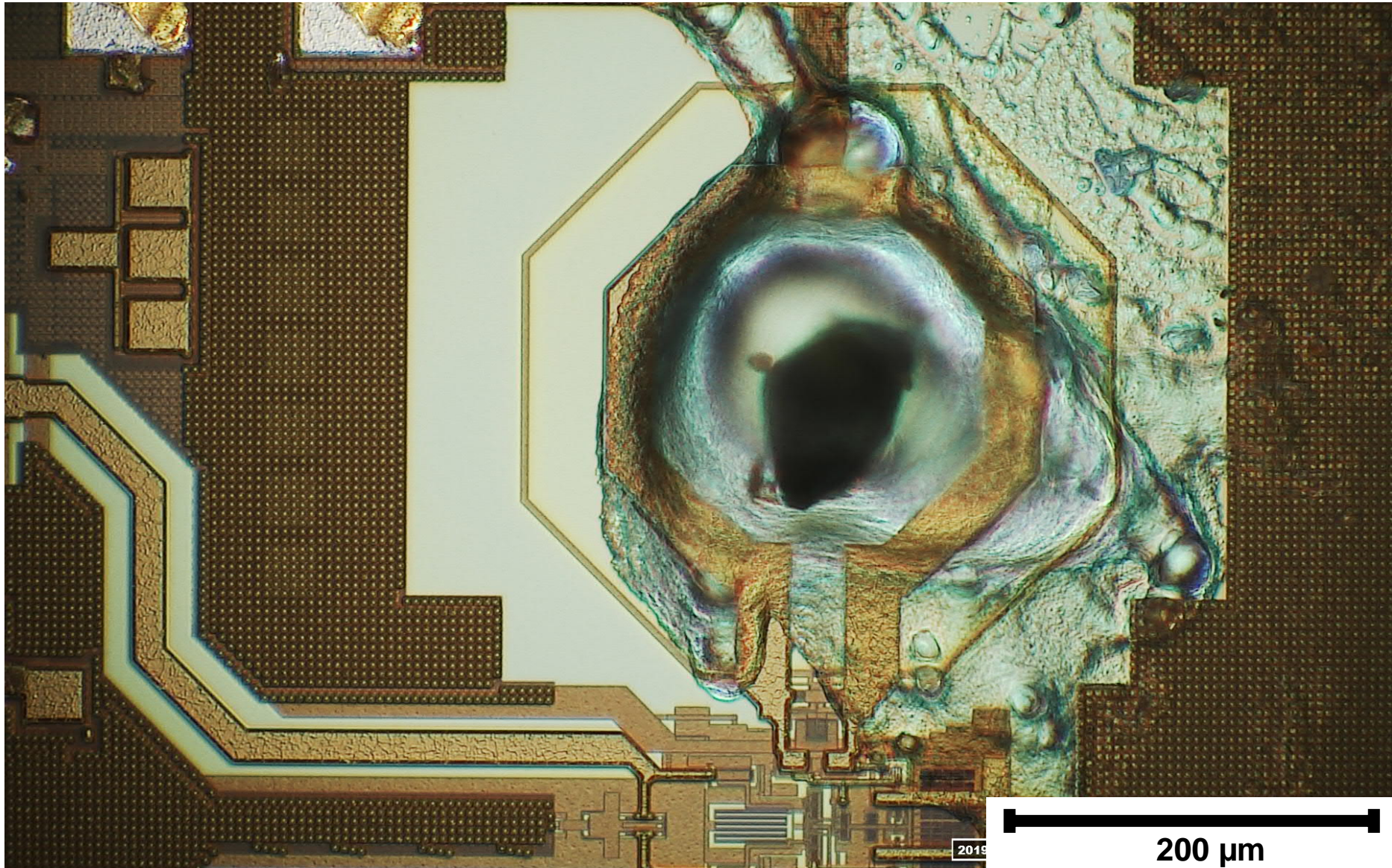
Used of Integrated oscillator $f_0=20$ GHz $B_0=710$ mT [7]



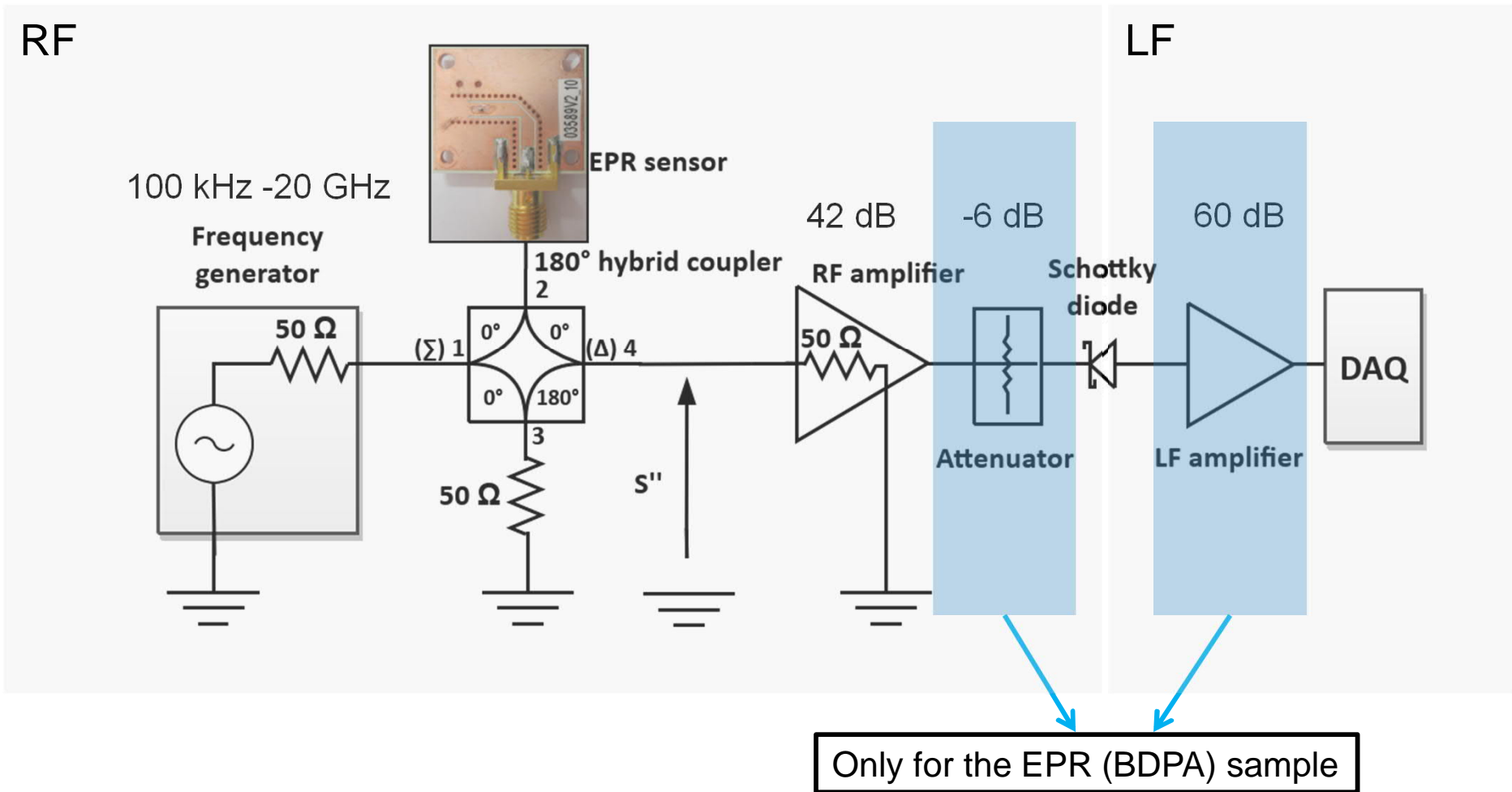
- Cross-coupled LC oscillator structure
- Variable frequency with varicap
- Output freq. 18.5-20.2 GHz



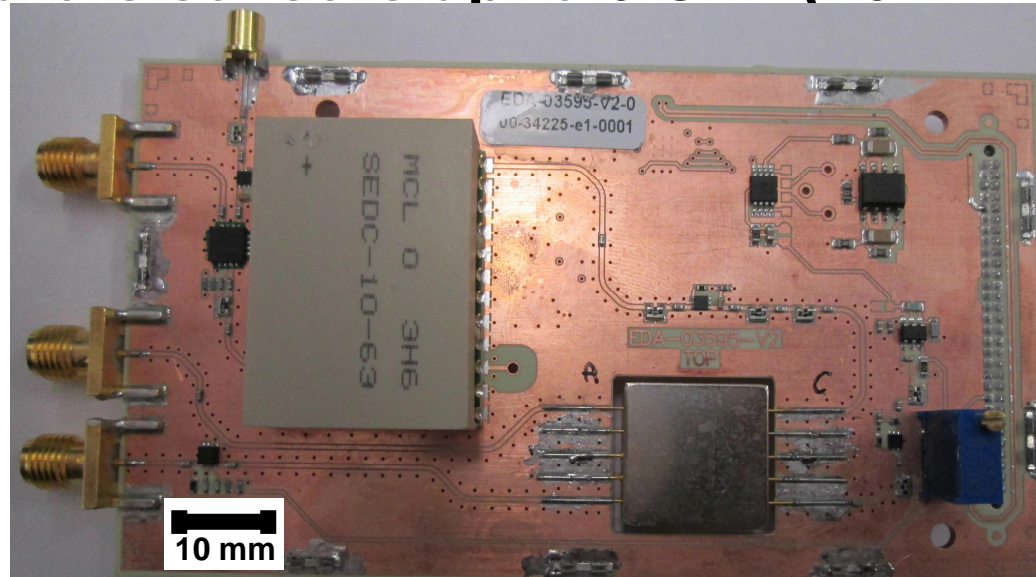
Sample installation (20 GHz)



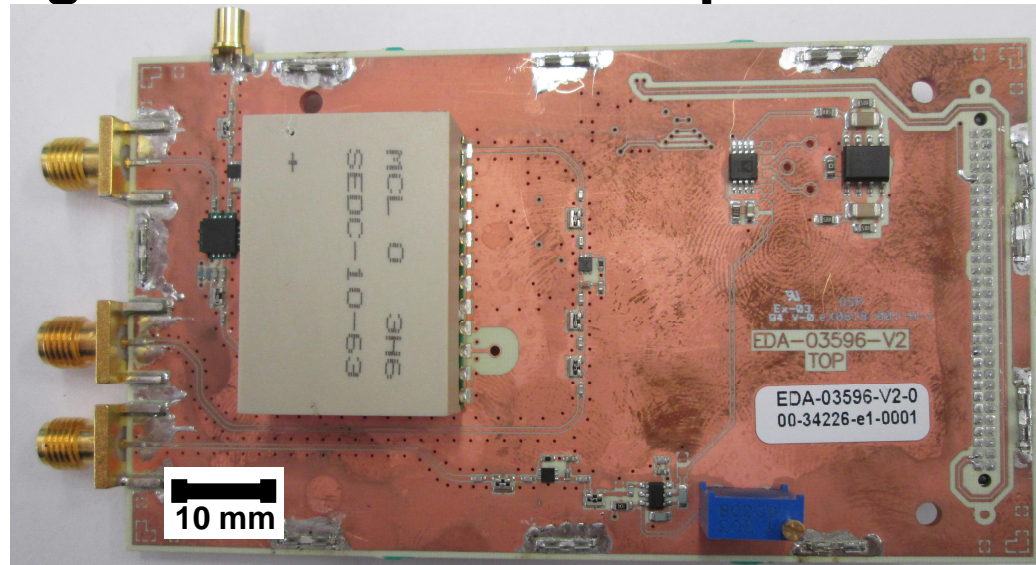
→ Resonators



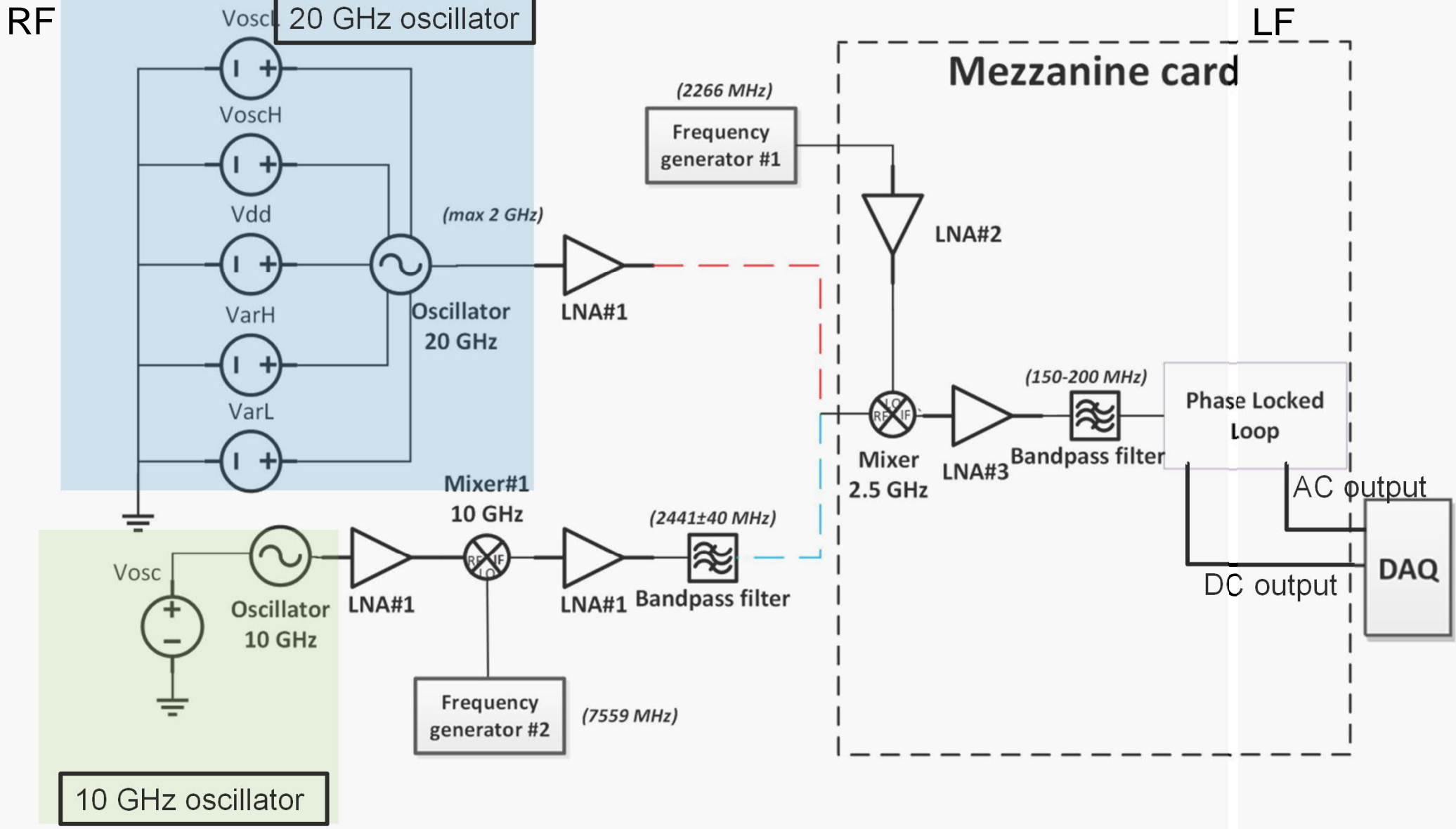
→ For resonators sensors up to 6 GHz (~ 0.22 T)



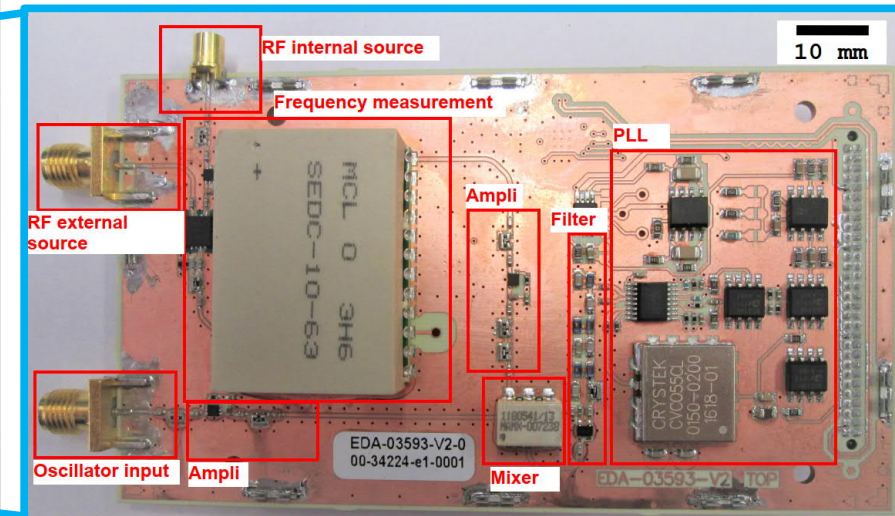
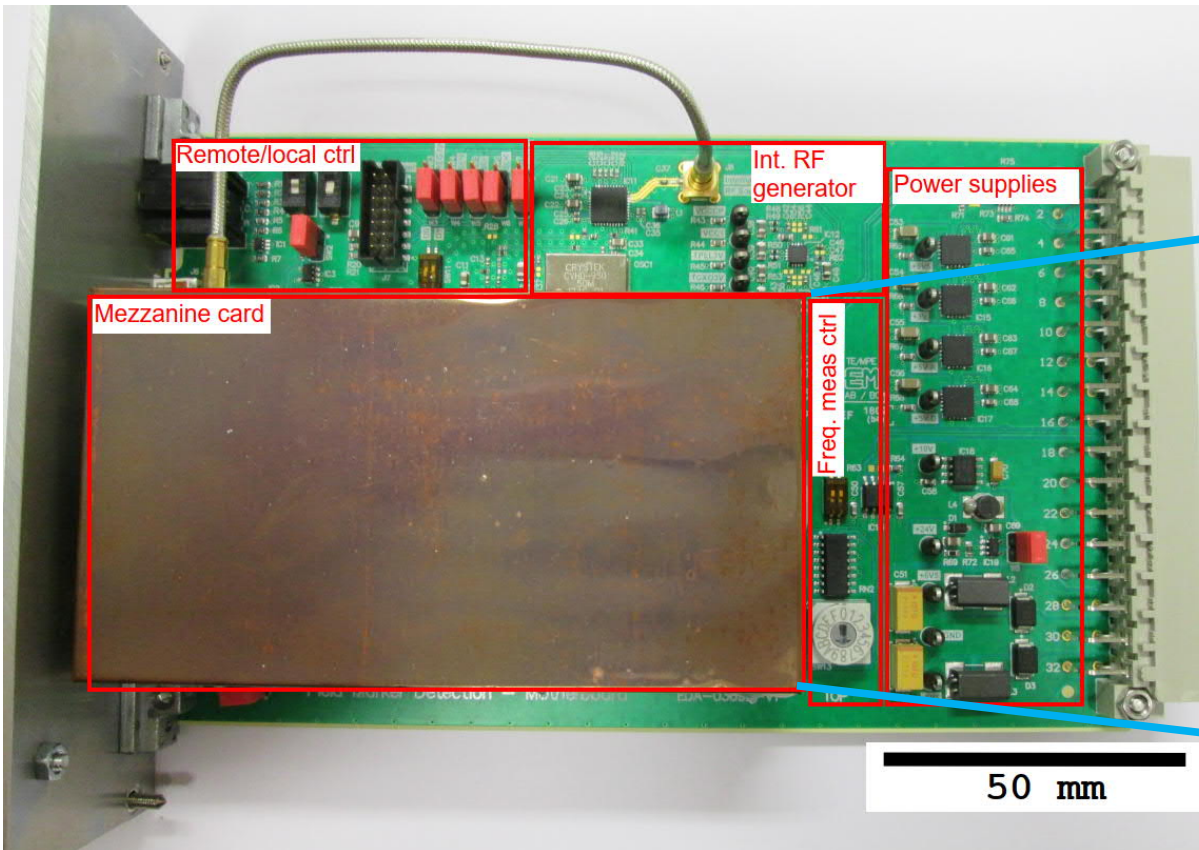
→ For coupling structure sensors up to 6 GHz (~ 0.22 T)



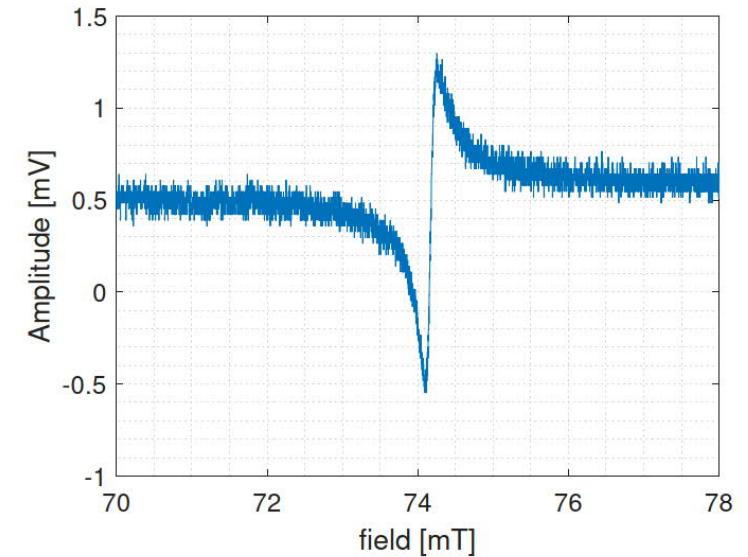
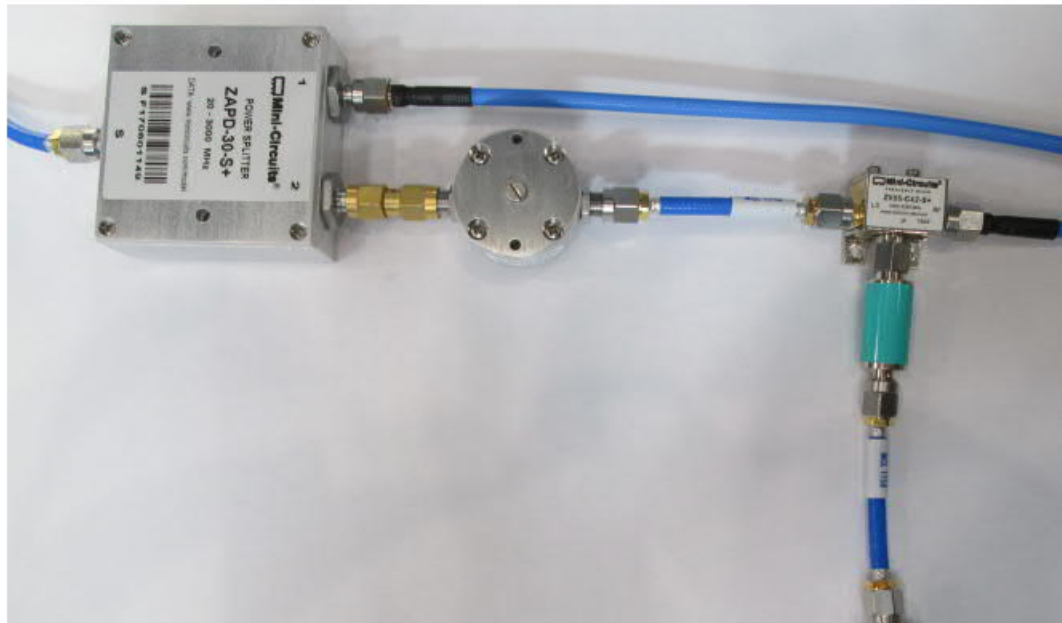
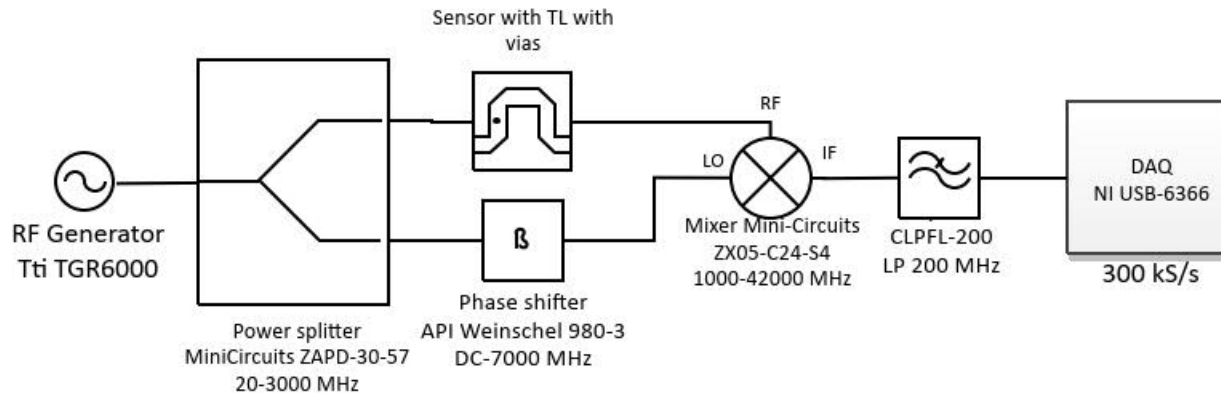
→ Oscillators



→ Electronic board with PLL mezzanine card

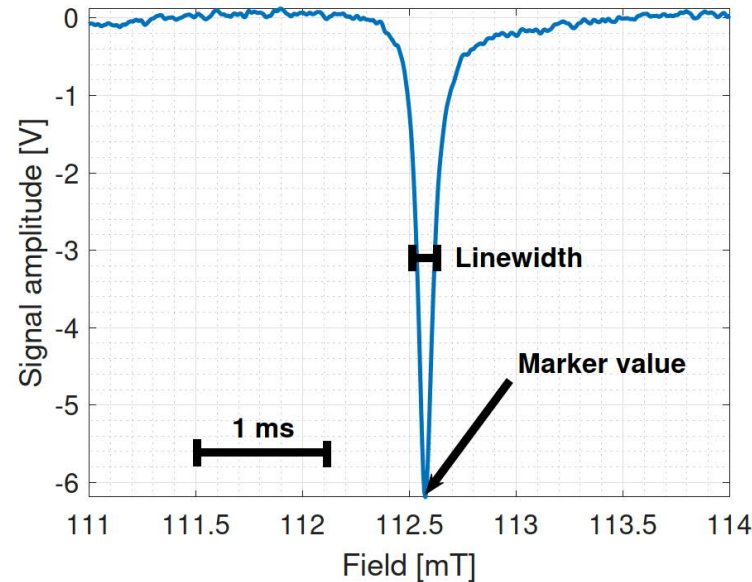


→ Phase detection used with transmission line



→ Typical ESR signal in marker mode (sweep B_0 , fixed f_1)

Amplitude detection



Frequency detection

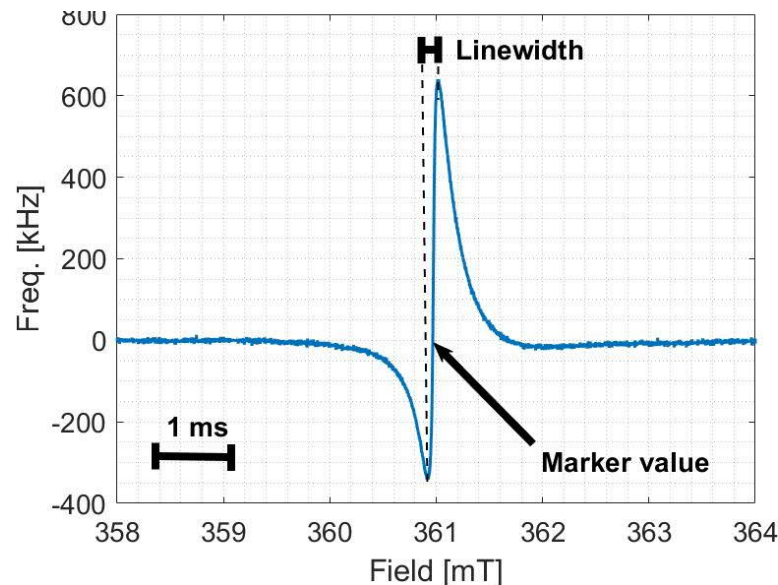


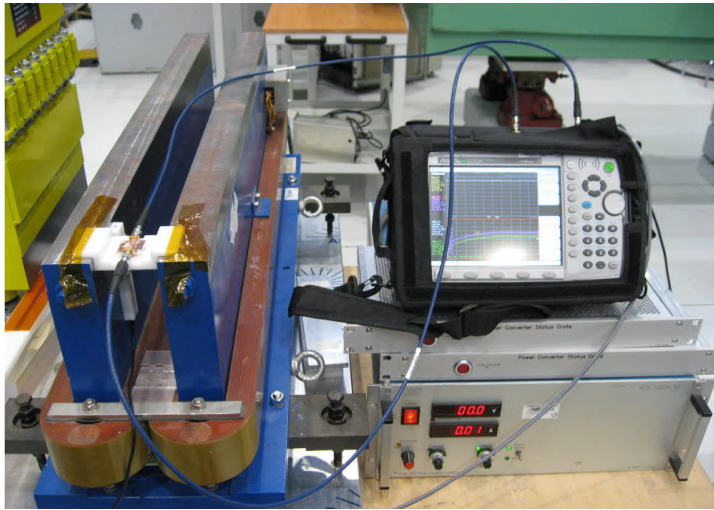
Figure-of-merit:

1. The signal-to-noise ratio
2. The shape distortion
3. The marker value
4. The linewidth
5. The resolution

Signal affected by

- Gyromagnetic ratio (absolute calibration)
- Temperature
- Ramp rate
- Field direction
- Gradient

→ Characterization steps



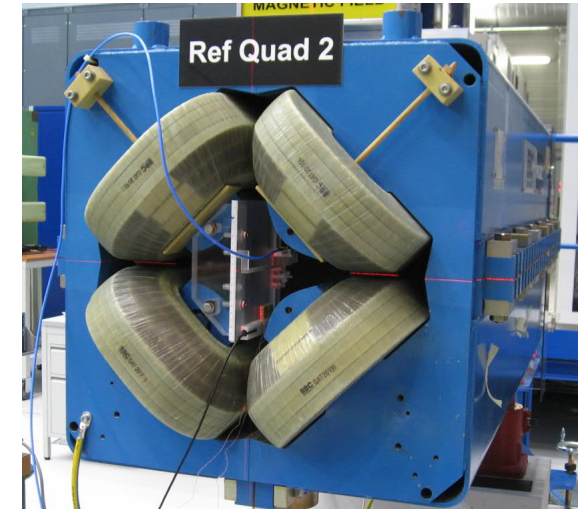
- The temperature stable axis

Static B_0 field



- Effective gyromagnetic ratio
- The resolution
- Temperature dependency
- Ramp rate dependency
- Field direction dependency

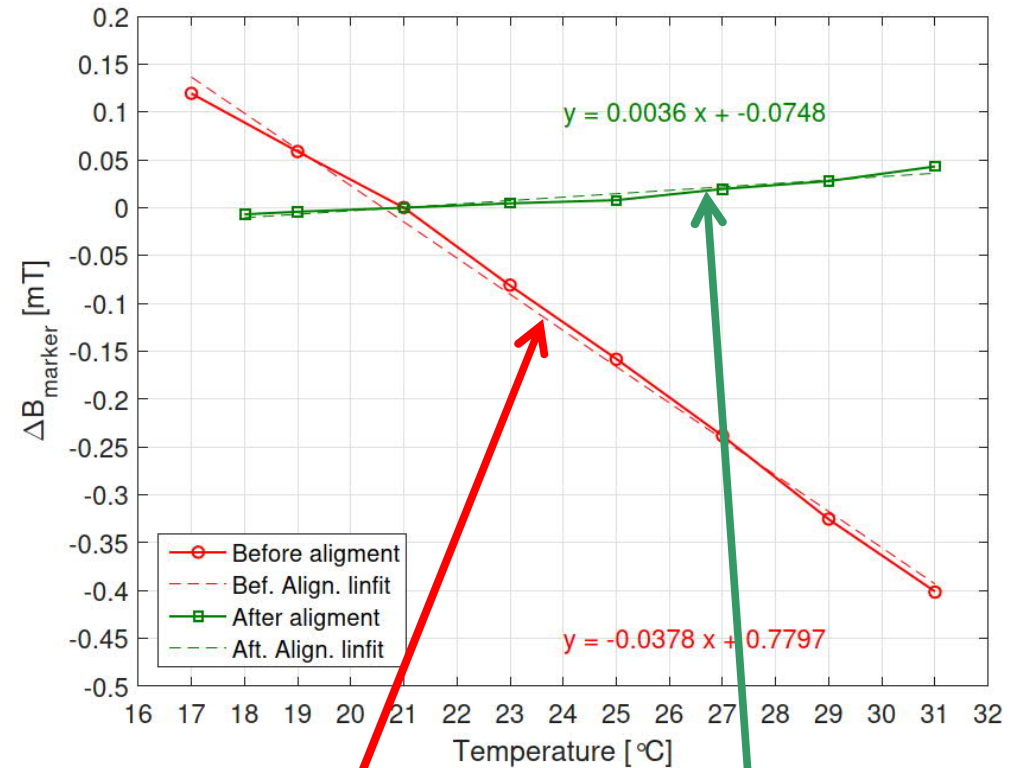
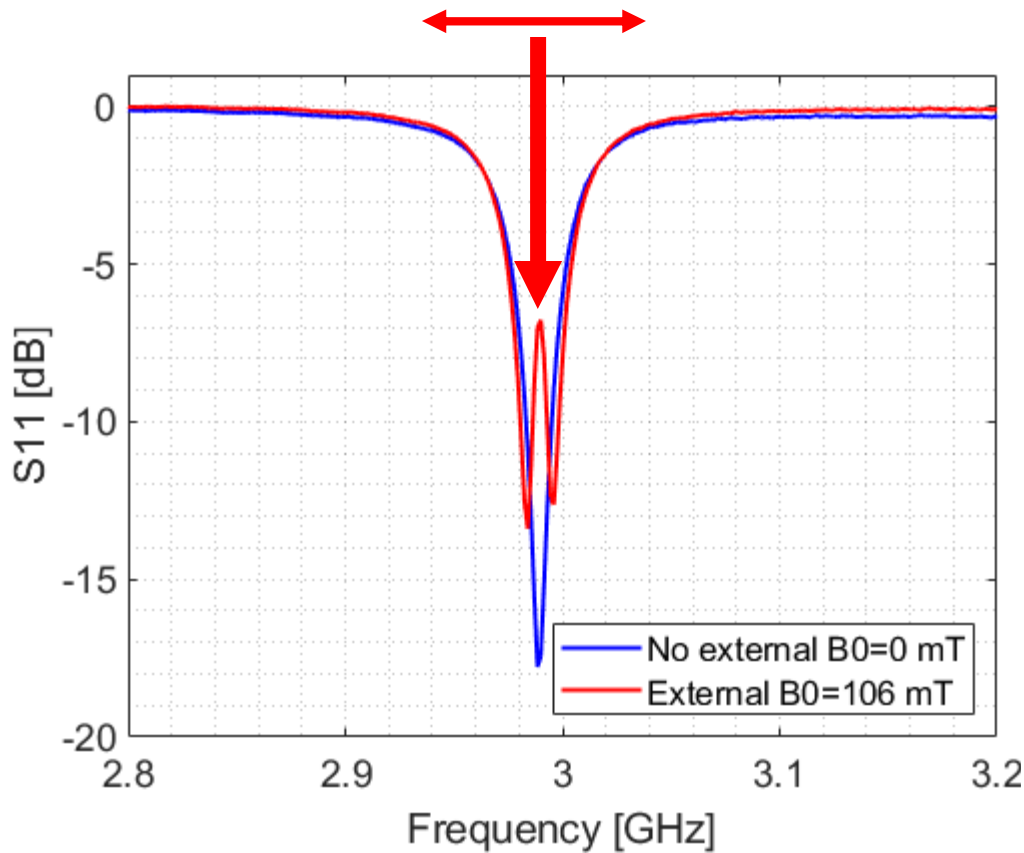
Time-transient B_0 field



- Gradient sensitivity

→ Temperature stable axis alignment (fixed B_0 , sweep f_1)

Resonance peak position changes with temperature when sphere is not aligned

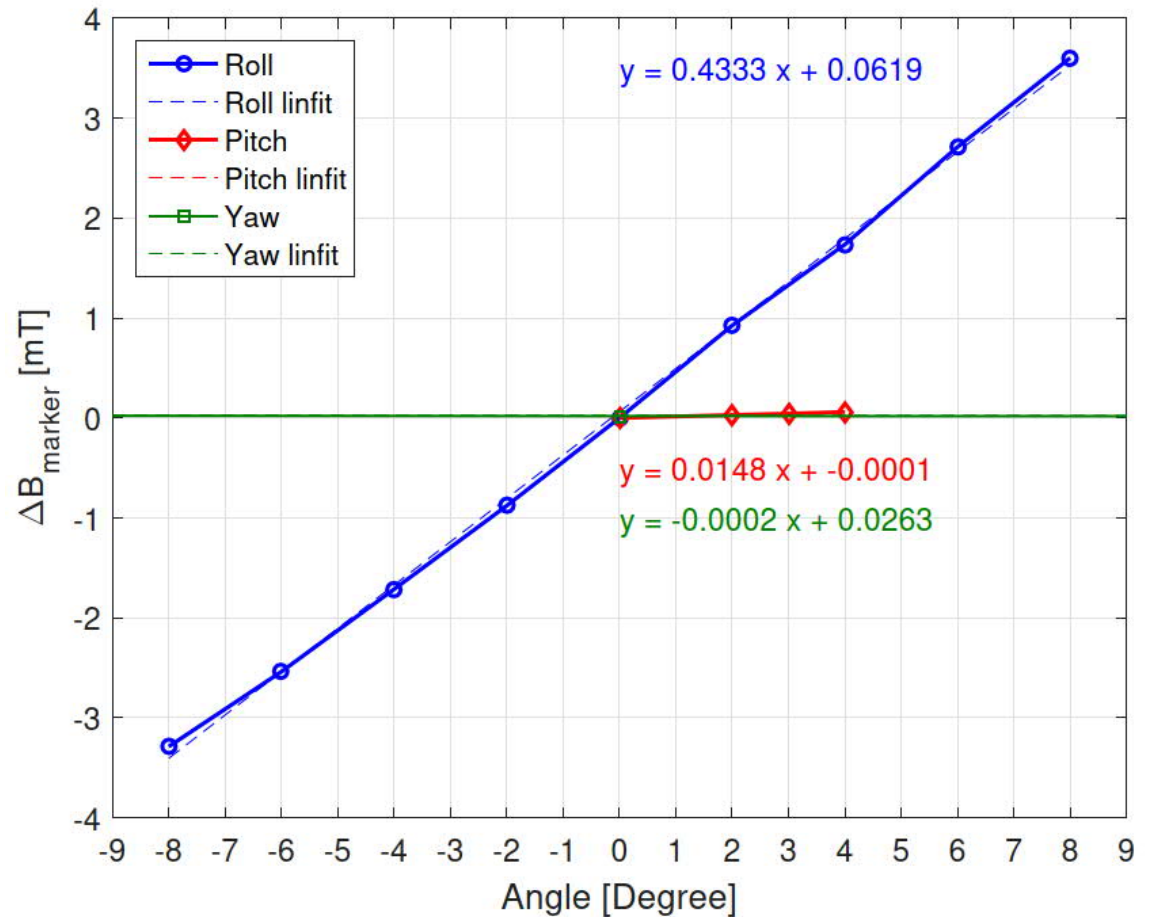
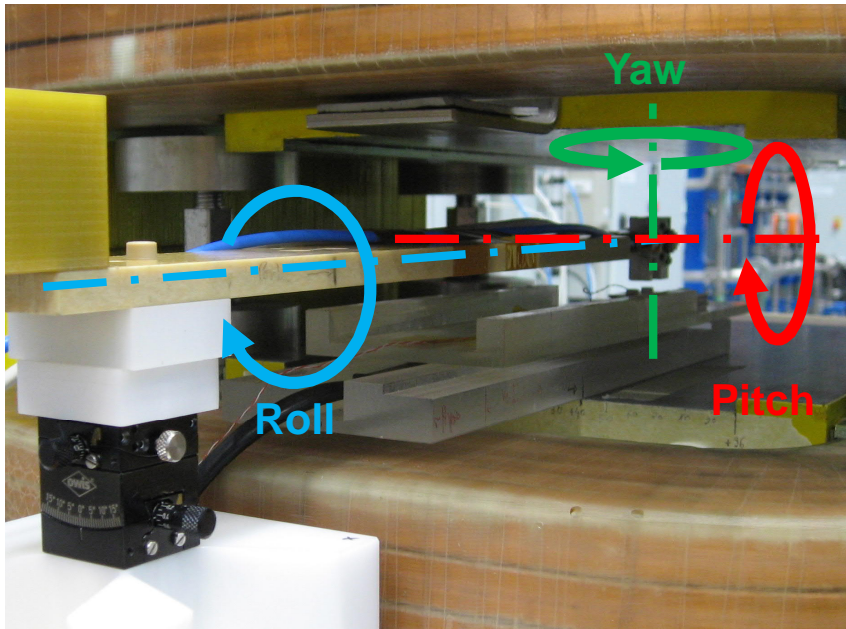


Before alignment
 $40 \mu\text{T}/\text{degC}$

After alignment
 $4 \mu\text{T}/\text{degC}$

=> Temperature sensitivity is improved by an order of magnitude

→ Field direction effect

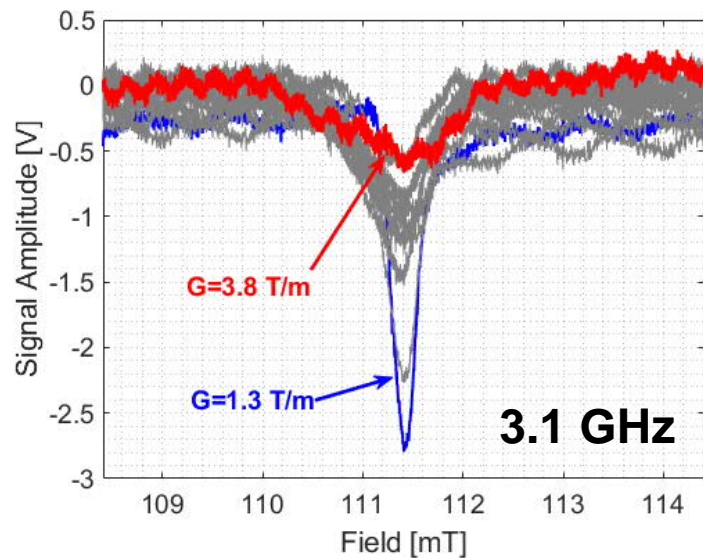
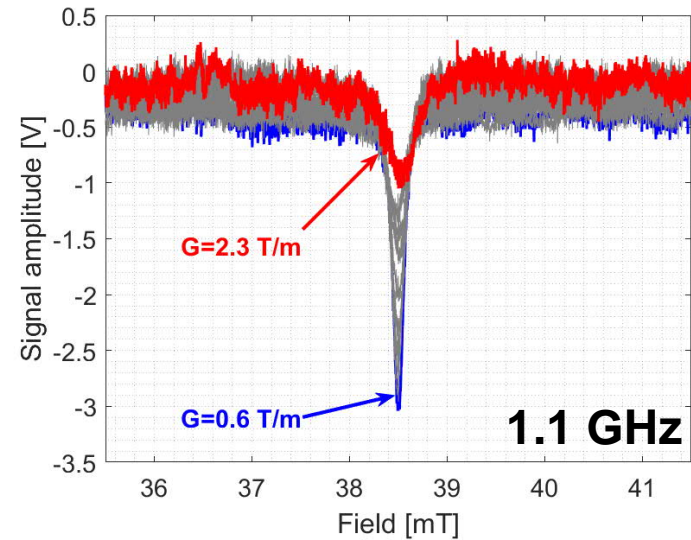


⇒ Relevant influence on the roll angle by 430 $\mu\text{T}/\text{deg}$

FMR sensors are insensitive to field ramp rates up to 5 T/s and gradients up to 12 T/m

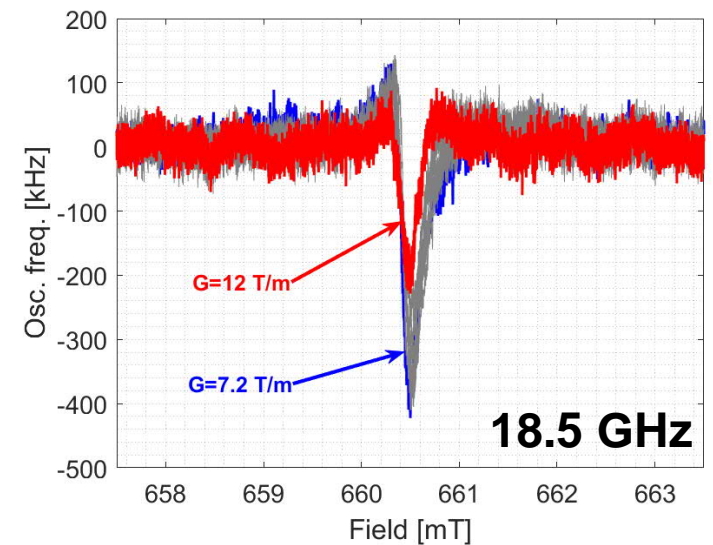
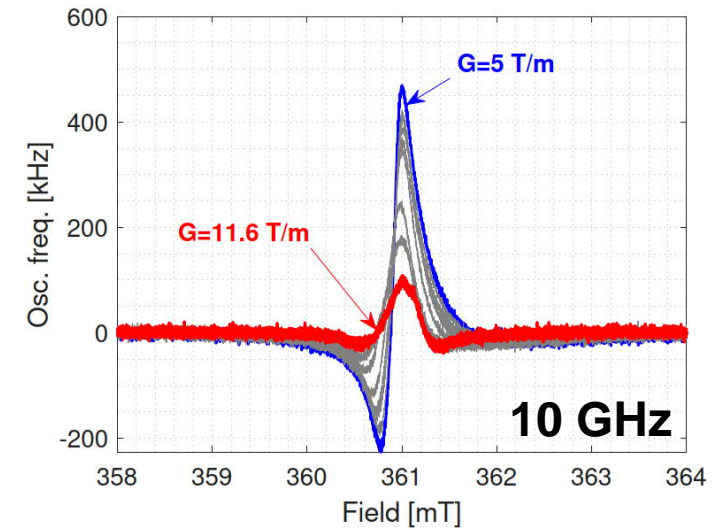
→ Gradient effect

Resonators



⇒ Able to measure gradient up to 2 T/m

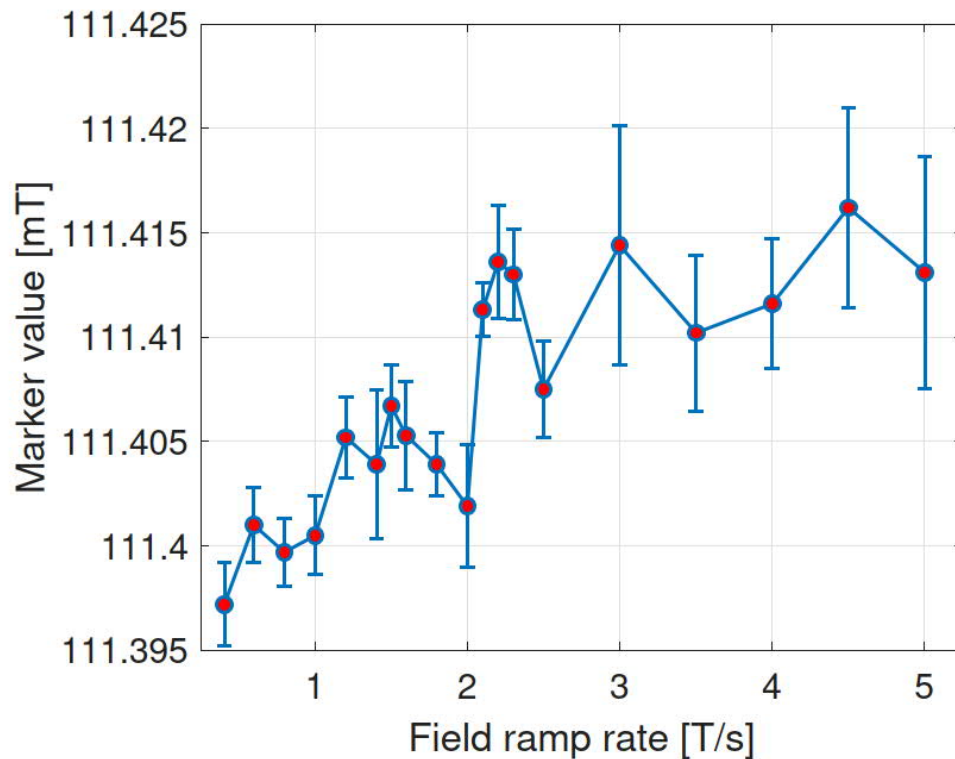
Oscillators



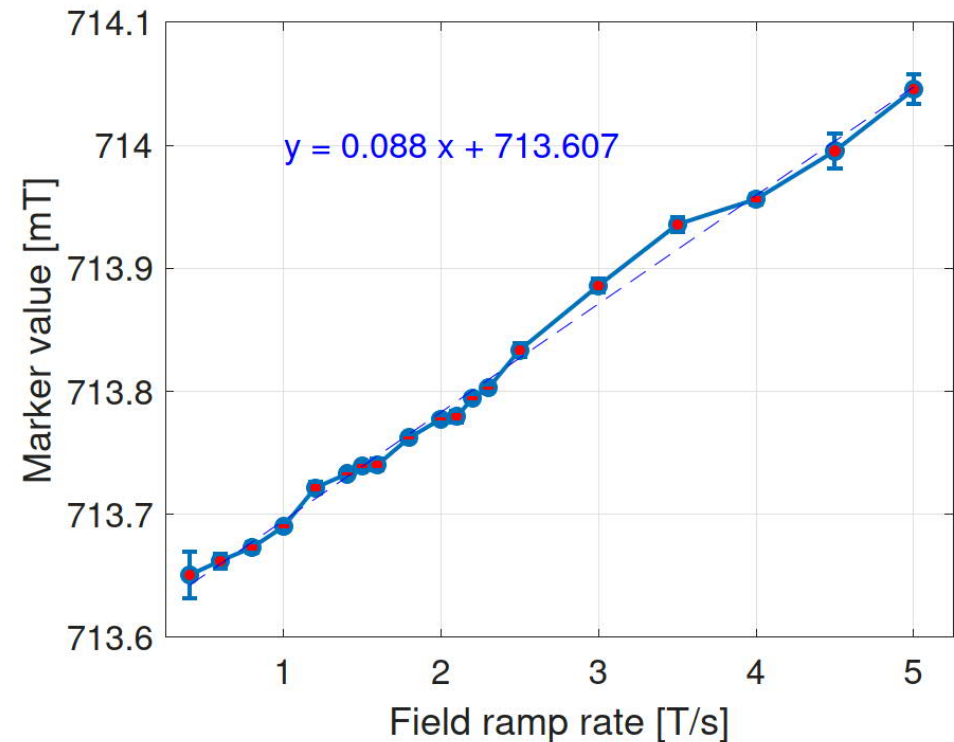
⇒ Able to measure gradient up to 12 T/m

→ Ramp rate effect (\dot{B})

Resonators



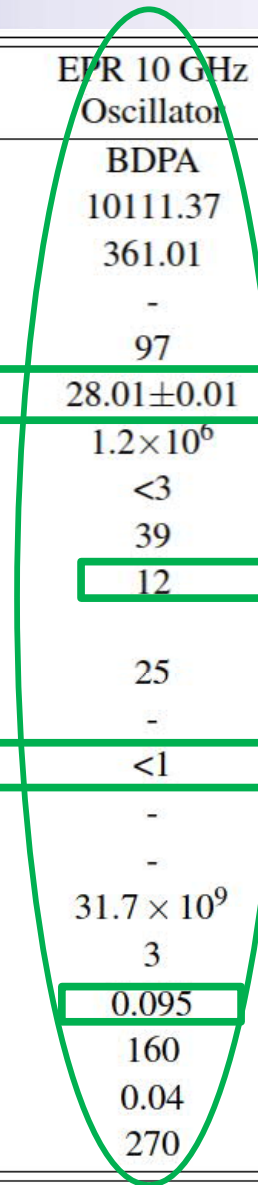
Oscillators



**Relevant marker value variation function of by field ramp rate with the 20 GHz oscillator
=> Electromotive forces on the varicaps and power supplies voltage**

Results: performance summary

Parameters	FMR 1 GHz Resonator	FMR 3 GHz Resonator	EPR 1 GHz Resonator	EPR 3 GHz Resonator	EPR 10 GHz Oscillator	EPR 20 GHz Oscillator
Sample material	GaYIG	GaYIG	BDPA	BDPA	BDPA	BDPA
Operating frequency (MHz)	1109	3050	1078.9	3123	10111.37	20000 ^a
B_m (mT)	35.9	106.3	38.52	111.41	361.01	713.65
B_m tuning range (mT)	-	-	-	-	-	660-720
Linewidth (μ T)	320	370	94	85	97	121
Effective γ (GHz/T)	28.29	28.69	28.01 \pm 0.01	28.03 \pm 0.01	28.01 \pm 0.01	28.02 ^a
Sample volume (μ m ³)	14.1 \times 10 ³	14.3 \times 10 ³	63 \times 10 ⁶	160 \times 10 ⁶	1.2 \times 10 ⁶	0.07 \times 10 ⁶
\dot{B} sensitivity (μ T/(T/s))	<3	<3	4	4	<3	90
Gradient sensitivity (μ T/(T/m))	-56	-	160	480	39	<10
Maximum gradient (T/m)	1.2	1.5	1.2	1.5	12	12
Maximum field inhomogeneity (m ⁻¹)	31	13	31	13	25	17
Temperature sensitivity (μ T/ $^{\circ}$ C)	3.6	2.2	4.8	7	-	-
Field direction sensitivity ψ (μ T/ $^{\circ}$)	433	368	<1	<1	<1	<1
Resonator sensor sensitivity (V/T)	4256	2286	47450	90800	-	-
Resonator noise floor (V/Hz ^{1/2})	3.2 \times 10 ⁻⁶	3 \times 10 ⁻⁶	0.26 \times 10 ⁻³	0.2 \times 10 ⁻³	-	-
Oscillator sensor sensitivity (Hz/T)	-	-	-	-	31.7 \times 10 ⁹	17.2 \times 10 ⁹
Oscillator noise floor (Hz/Hz ^{1/2})	-	-	-	-	3	35
Resolution (nT/Hz ^{1/2})	0.7	1.3	5.5	2.2	0.095	2
Bandwidth (kHz)	150	150	100	100	160	160
Integrated resolution (μ T _{RMS})	0.3	0.5	1.7	0.70	0.04	0.8
SNR (-)	1620	750	40	100	270	30



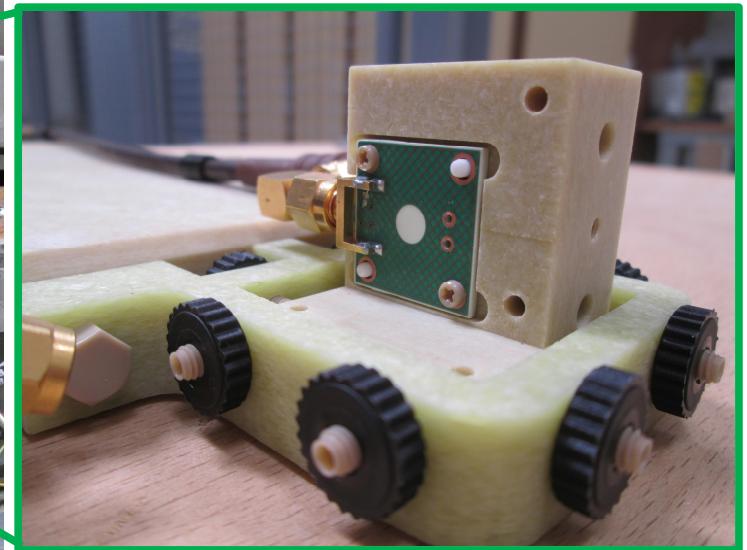
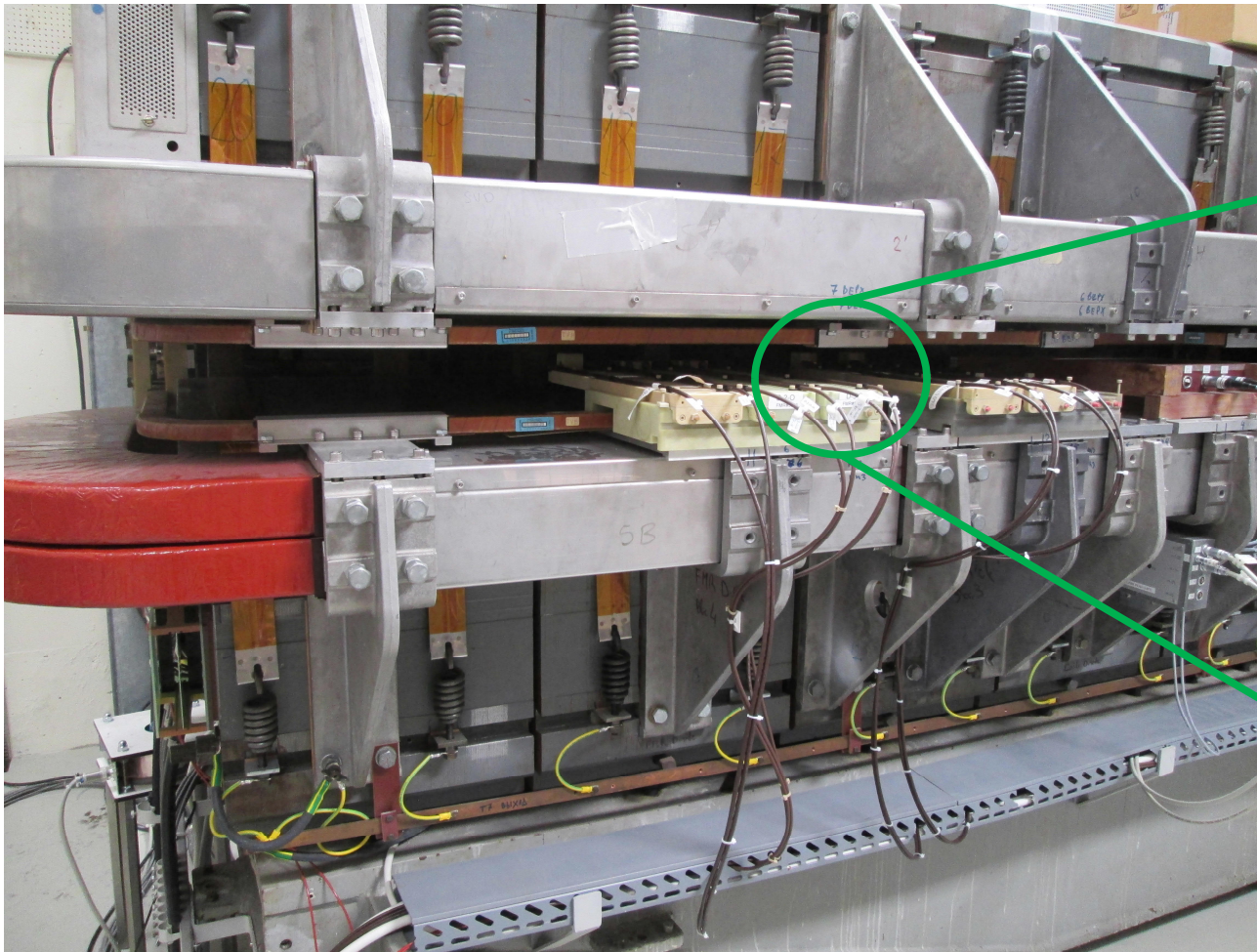
Low performance

Medium performance

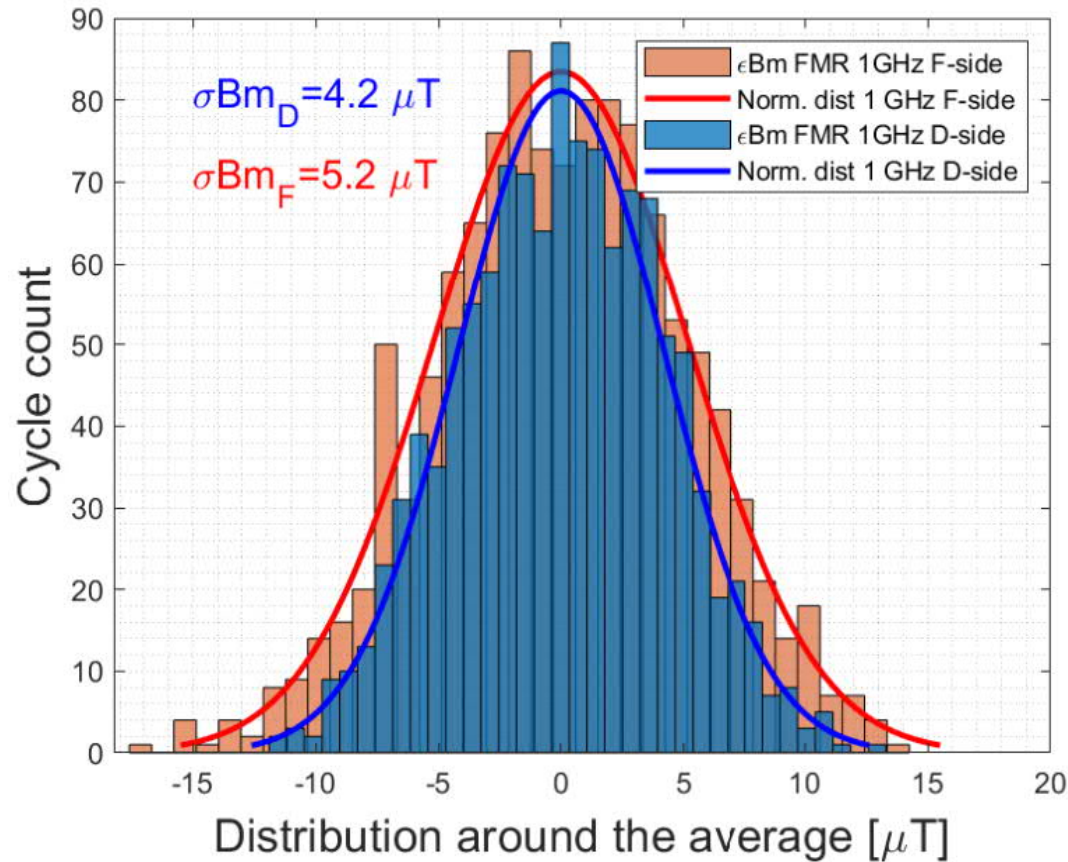
high performance

^a The 20 GHz oscillator has no direct frequency output. As a consequence, the oscillation frequency and the effective γ cannot be measured. The reported oscillation frequency is computed measuring the magnetic field with an NMR magnetometer and an induction coil and assuming an effective $\gamma = \gamma_{BDPA} = 28.02$ GHz/T.

FMR sensor at 36 mT (1 GHz) is installed in the focusing and defocusing sides of the PS reference magnet MU101

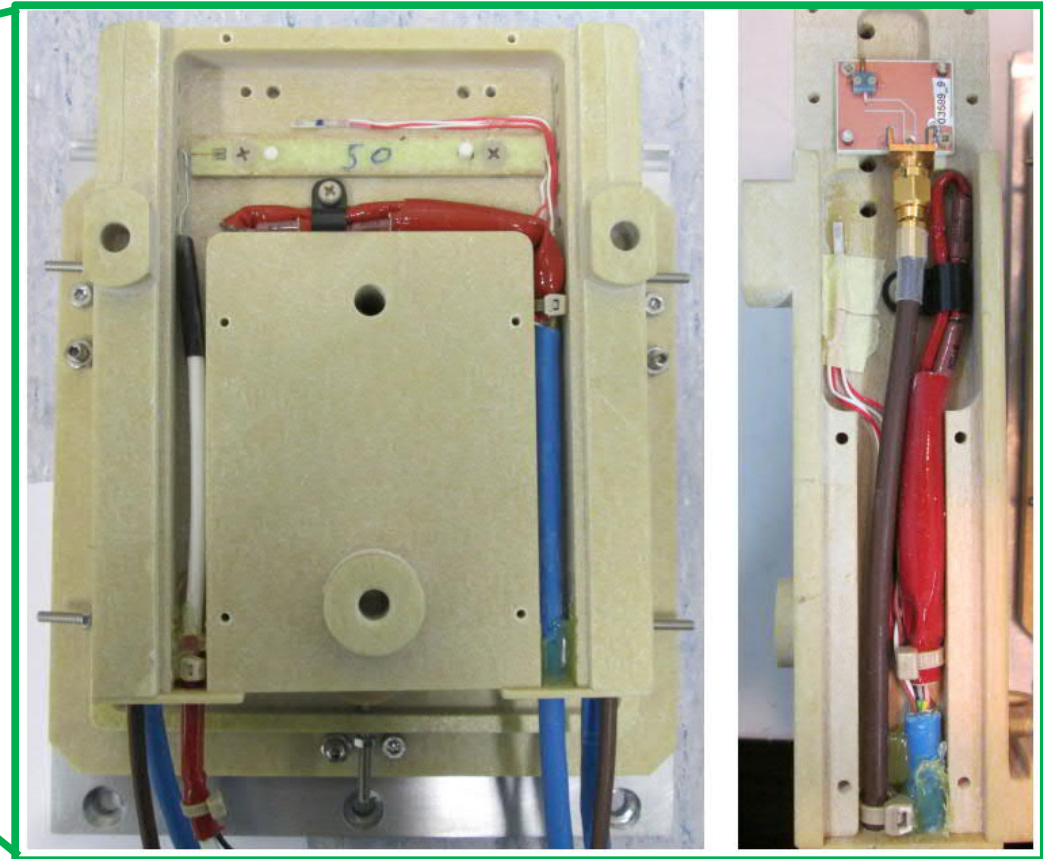
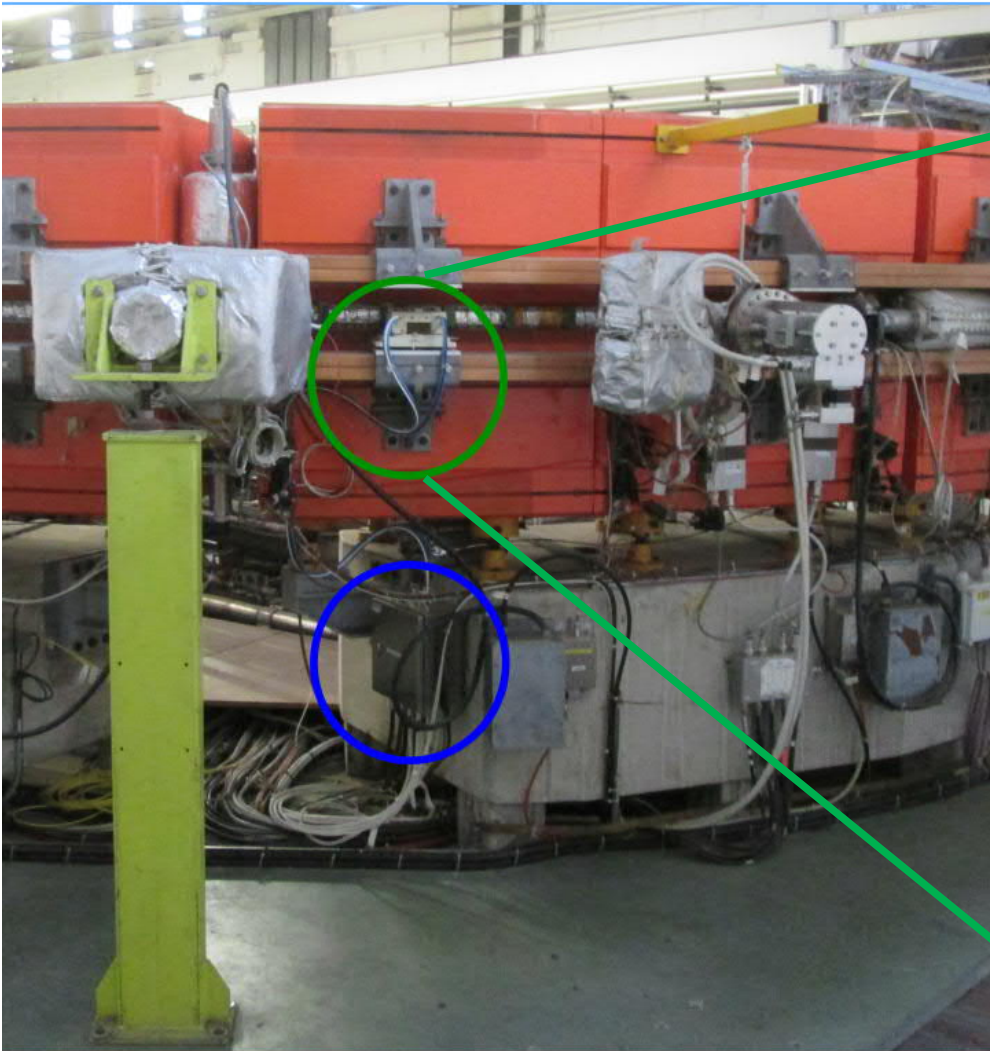


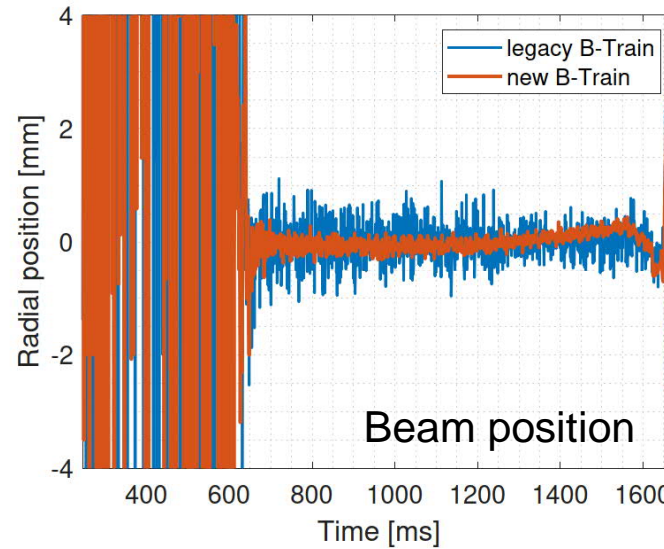
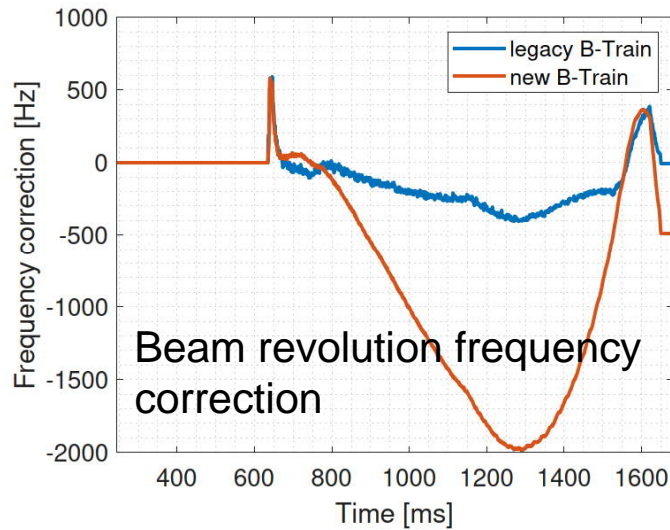
FMR sensor at 36 mT (1 GHz)



=> Reproducibility by about 5 μT corresponding to 5×10^{-5} at injection, that is, within the PS operation requirement

The FMR sensor at 106 mT (3 GHz) is used in the fringe field of the main bending magnet



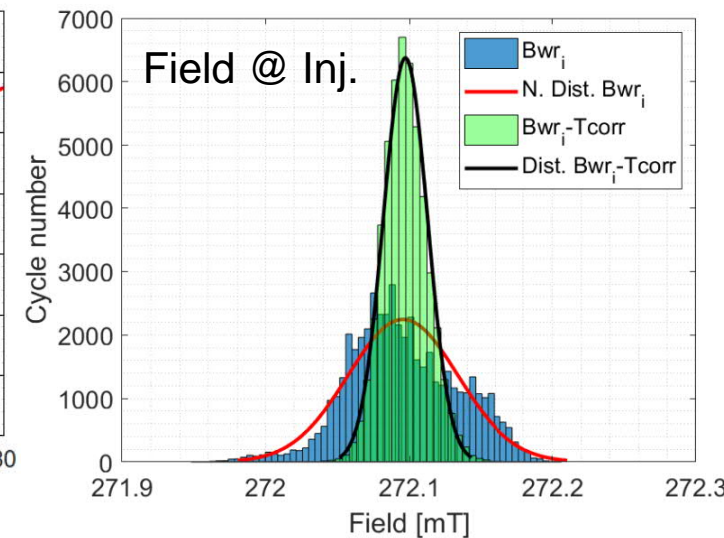
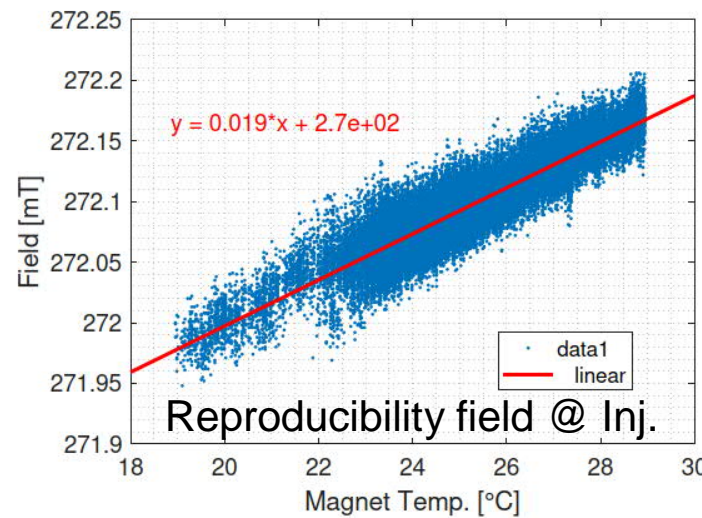
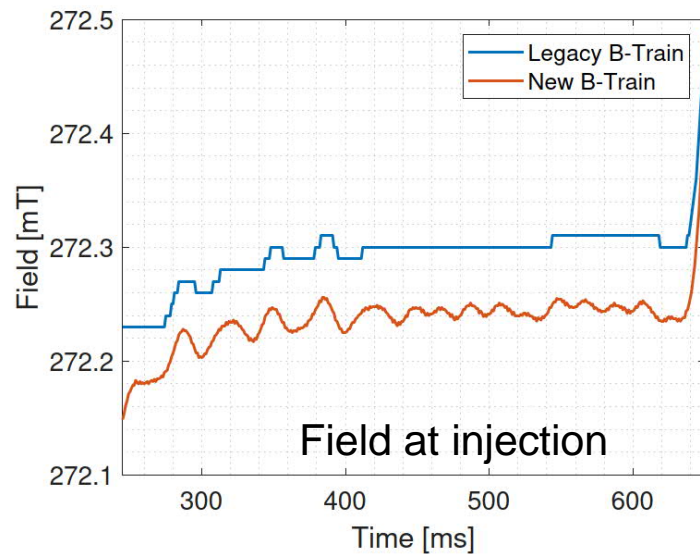


New B-train measurement:

- ⇒ Resolution from 10 to 0.2 μT
- ⇒ Radial position stability from 0.6 to 0.1 mm RMS
- ⇒ Max field error 1.5 mT (0.2%)

Impact of new marker:

- ⇒ Cycle-to-cycle reproducibility from several 100 μT down to 38 μT (1.4×10^{-4})



- **The proposed ESR sensors have a reproducibility better than 1.4×10^{-4} . They operate in a field range up to 0.7 T, in a field gradient up to 12 T/m and with ramp rate up to 5 T/s.**
- **FMR sensors were implemented and validated on two B-Train systems.**
- **The parametric model of the waveguide resonator allows easy adaptation to different field marker levels.**
- **Extended versions of the EPFL's oscillator architecture could be used to measure fields above 1 T.**
- **The implementation of a modulation coil on the marker sensor with an adapted detection electronics, would allow operation in static background field.**

Thank you for your attention

Questions?

- The B-Train team M. Amodeo, M. Colciago, V. Di Capua, C. Grech, D. Oberson, A. Parrella, M. Roda, J. Vella Wallbank
- The B-Train users
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- The wire bounding and QART Labs
 - G. Corradini (EPFL)
 - A. La Rosa, F. Manolescu, I. Mcgill (EP/DT)

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