



# COMPARISON BETWEEN MECHANICAL MEASUREMENTS AND FEA RESULTS OF THE D2 SHORT MODEL MBRDS1c

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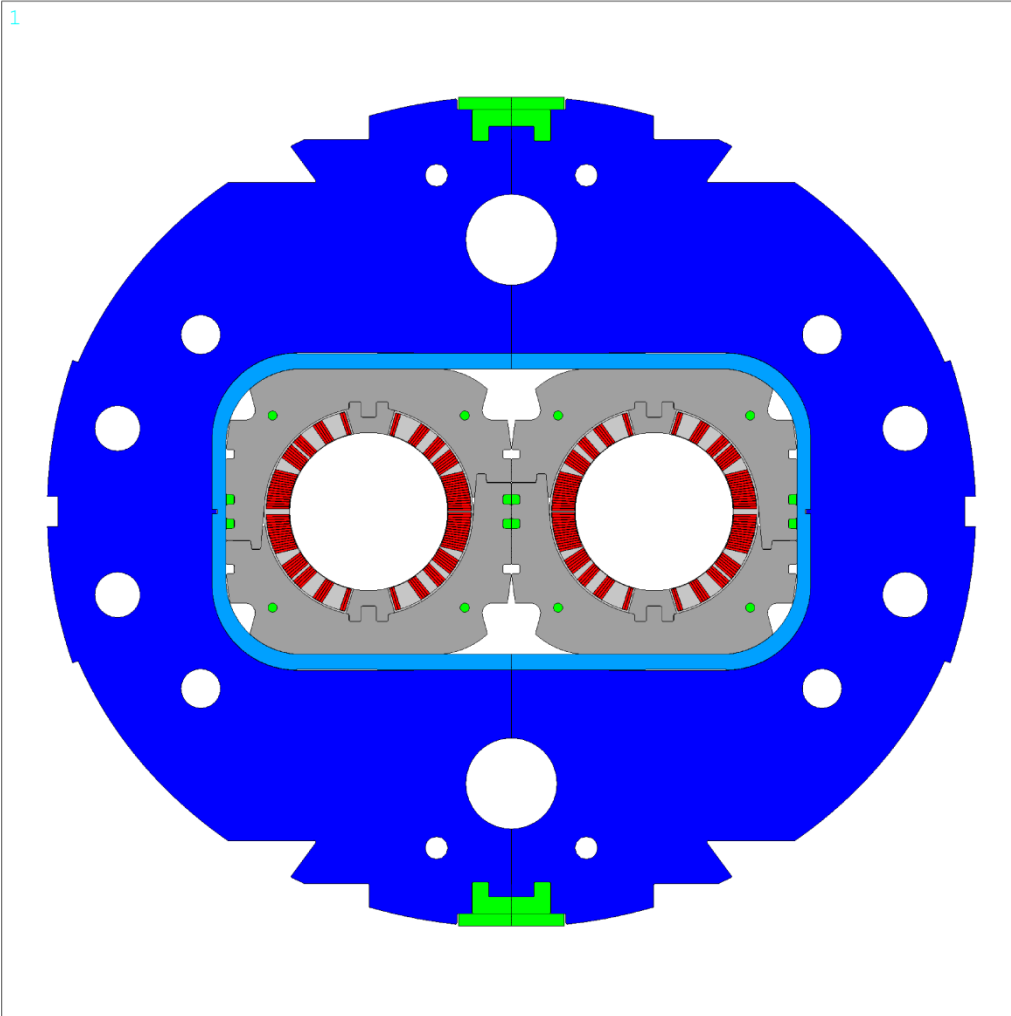
Sept. 2<sup>nd</sup> 2020

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A horizontal bar at the top of the slide, divided into a red section on the left and a teal section on the right.

# FEA 2D MODEL

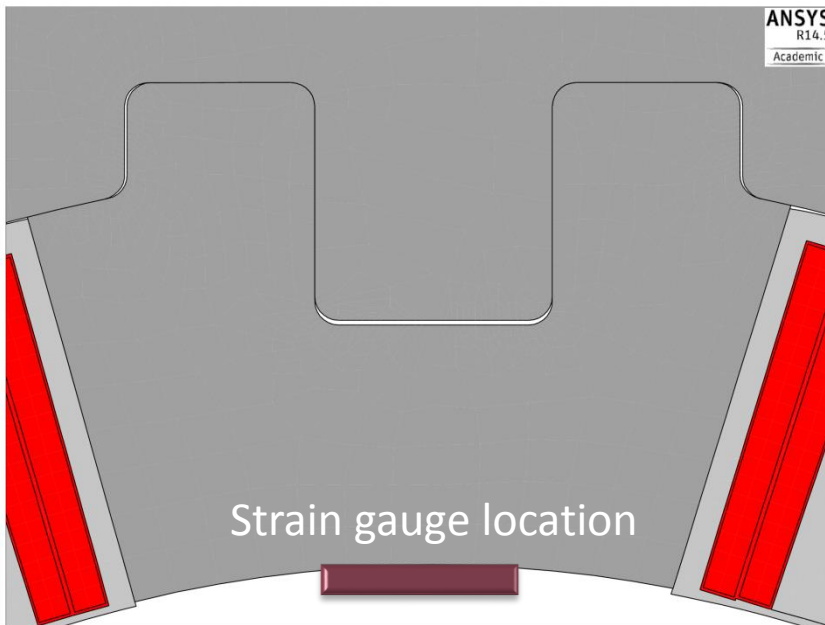
# FEA 2D model



- The 2D model is built piling up turns from the pole towards the midplane, simulating real winding
- The dimensions of the turns are determined previously simulating the stack tests
- Following operations are: collaring, insertion of the Al sleeves, yoking, welding of the outer shell, cool-down, energization up to ultimate current

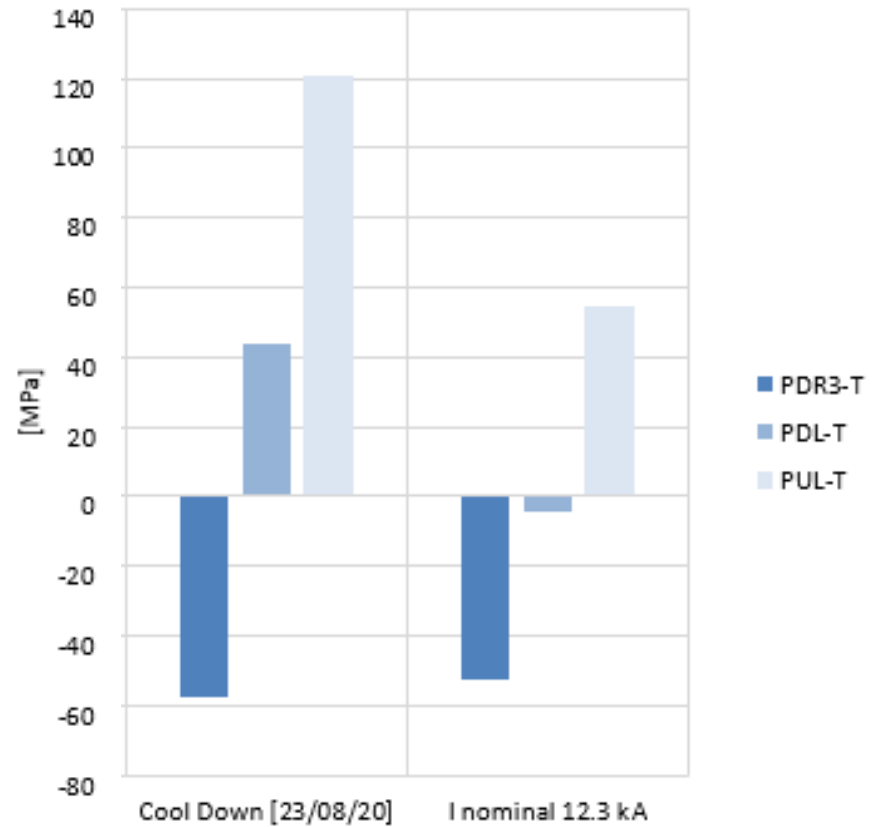
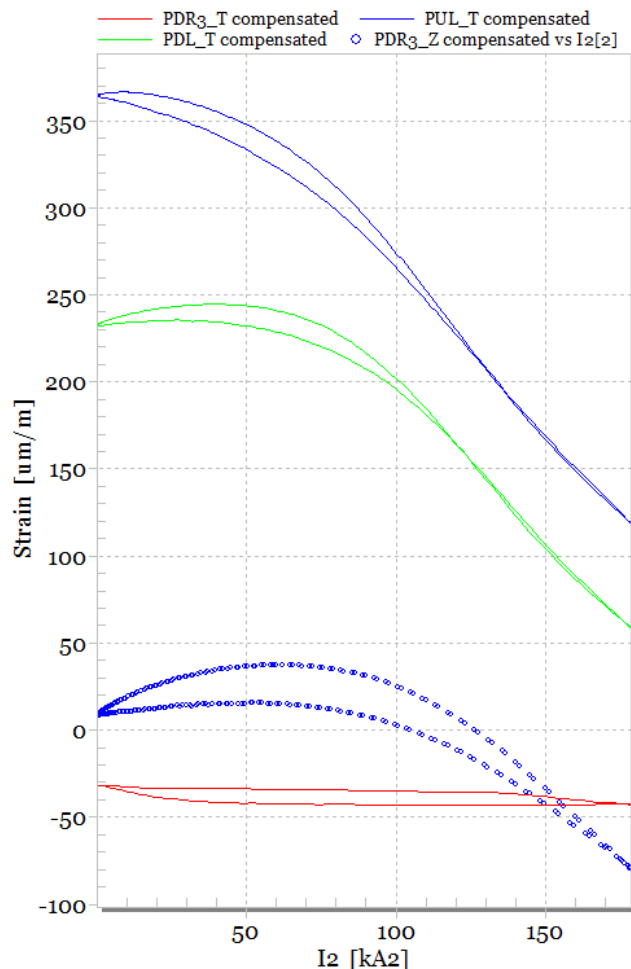
# Pole unloading

- Unfortunately, only few strain-gauges survived
- However, it emerged quite clearly that the pole unloading was of the order of 40 MPa



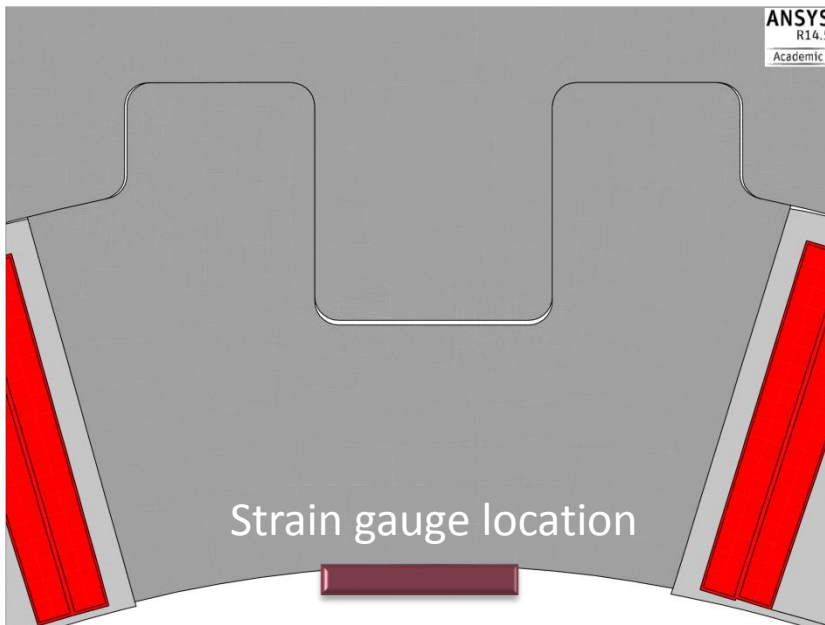
# Pole unloading measurements

Quench\_2020\_07\_31\_12\_07\_33 - Compensated data



# Pole unloading

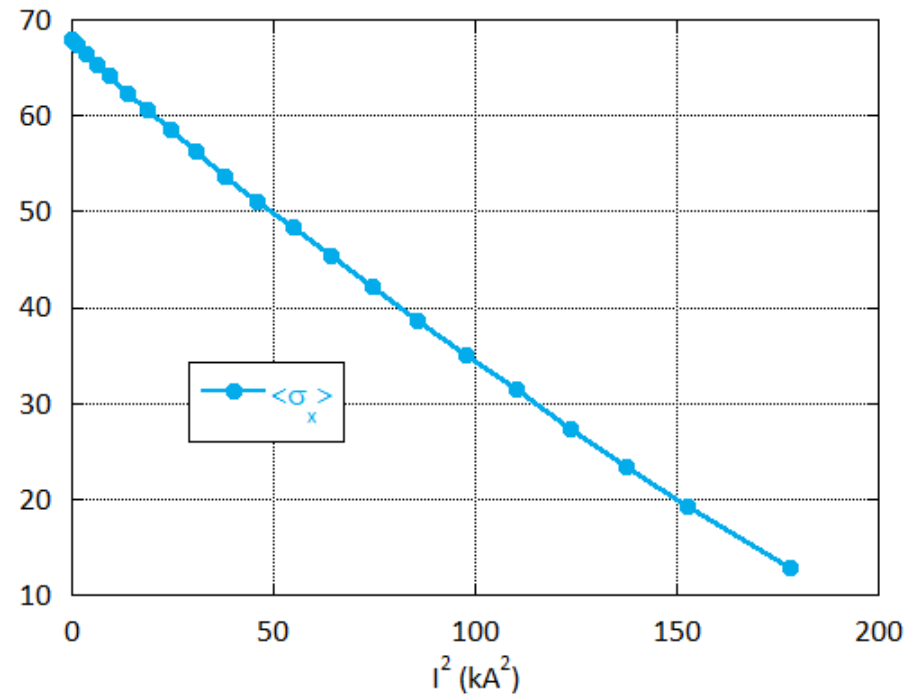
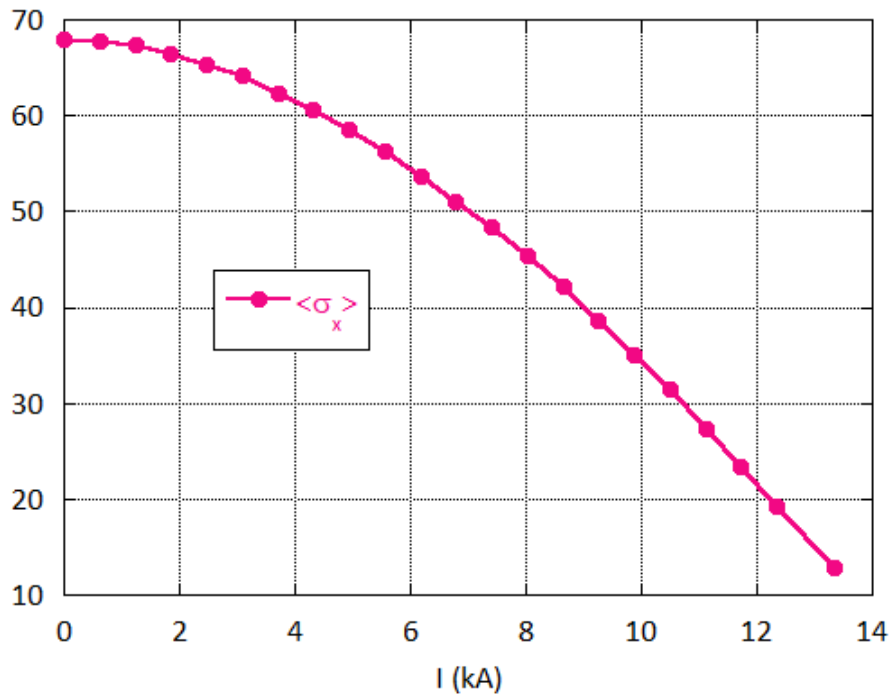
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- To evaluate this unloading, we compute the average stress in the x direction in the elements belonging to the pole and adjacent to the strain gauge position

# Pole unloading comparison

- The calculated unloading between cool-down and nominal current is 48.6 MPa

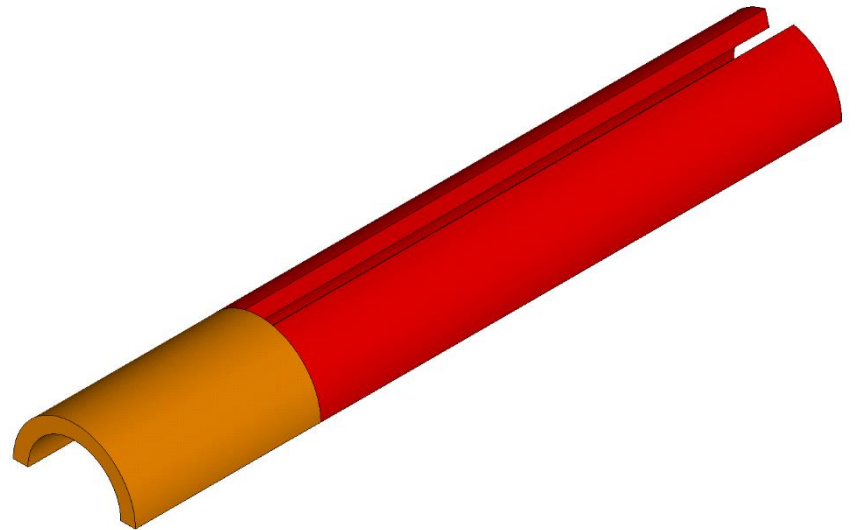
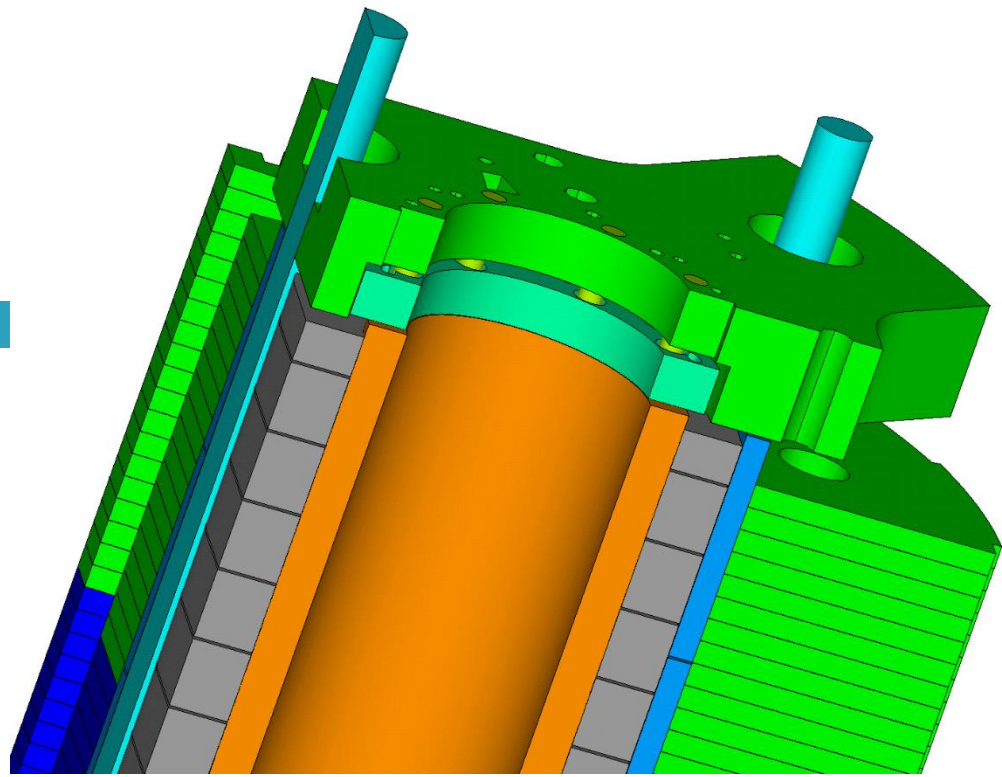
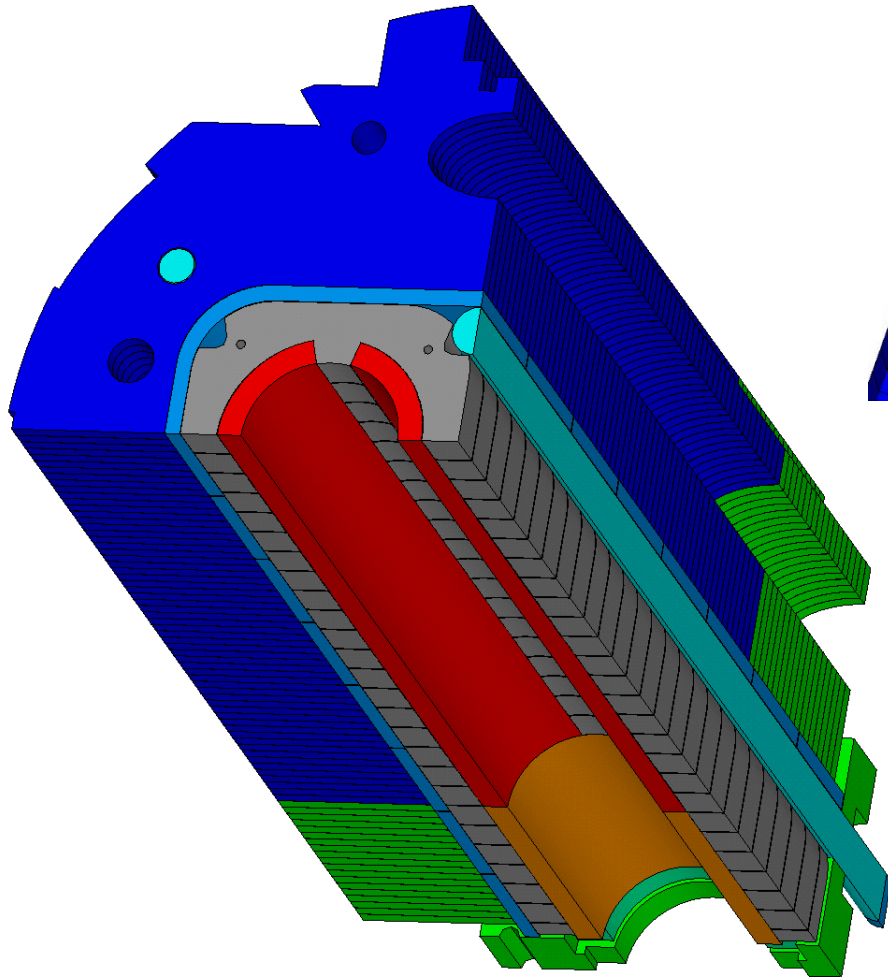


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# FEA 3D MODEL



# FEA 3D model



# Longitudinal pre-loading system

- The 6 tie rods (2 M33 and 4 M24) are loaded up to 125 kN, corresponding to 50% of the Lorentz force
- In the last measurement campaign too many strain gauges were lost, so no comparison with FEA is possible
- However, we can compare the results coming from the tests performed last year and already published (*The HL-LHC Short model recombination D2 dipole: Cold test results and analysis*, IEEE Trans. Supercond. 30, 4 , June 2020, DOI: 10.1109/TASC.2020.2976963)

*The HL-LHC Short model recombination D2 dipole: Cold test results and analysis, IEEE Trans. Supercond. 30, 4 , June 2020*

#### IV. COOLING DOWN PHASE

The cool down was performed in a vertical cryostat limiting the thermal gradient to 50 K. The initial total axial preload at room temperature of 125 kN +/- 5 in the six tie rods was increased by 15 kN during the cool down.

#### V. POWER ELECTRICAL TEST

The axial rods were loaded under powering test to a maximum of 20 MPa, i.e 17 % above estimated values, with a linear load increase rate of 118 N/kA<sup>2</sup> on the central largest diameter tie rods compared to 48 N/kA<sup>2</sup> on smaller ones.

# Reaction forces on tie rods

FEA results	M33 (kN)	M24 (kN)	Total (kN)
Assembly	30.4	16.1	125.2
Cool-down	29.2	15.8	121.6
Powering	49.8	23.1	192.0

- During cool-down, the initial longitudinal preload was increased by 15 kN
- FEA instead shows a small decrease of 3.6 kN

# Reaction forces on tie rods

FEA results	M33 (kN)	M24 (kN)	Total (kN)
Assembly	30.4	16.1	125.2
Cool-down	29.2	15.8	121.6
Powering	49.8	23.1	192.0

- During powering, the M33 rod showed a load increase rate of  $118 \text{ N/kA}^2$ , corresponding to 18.0 kN at nominal current, the M24 rod showed a load increase rate of  $48 \text{ N/kA}^2$ , corresponding to 7.3 kN at nominal current.
- At nominal current, FEA shows a load increase between cooldown and powering of 20.6 kN for the M33 rod and 7.3 kN for the M24 rod, in very good agreement with the tests.

# Force balance (kN) in magnet components

	coil	collars	sleeves	iron yoke	tie rods	total
assembly	-241.3	+116.3	0	0	+125.0	0
cool-down	-102.3	-50.1	+30.7	+0.1	+121.6	0
powering	-12.2	+31.6	+44.5	+0.2	+191.9	+256.0

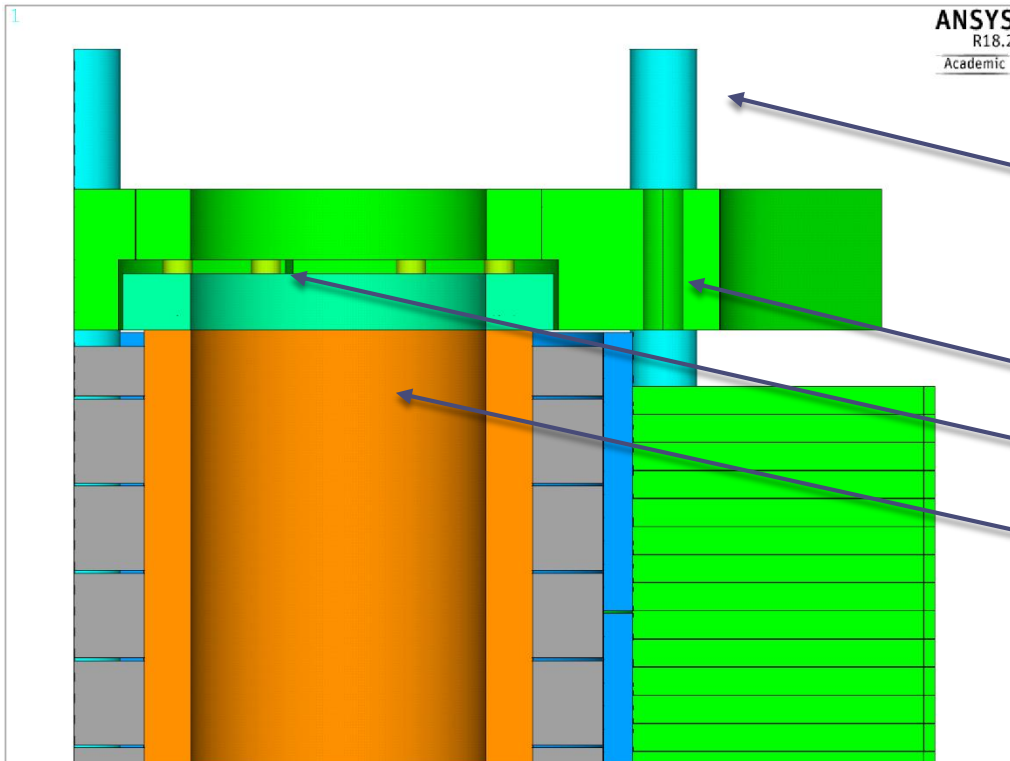
preload

Lorentz force

- It is worth noting that powering generates a completely different equilibrium between the different reactions with respect to cool-down, so that the tie rods are loaded only by  $191.9 - 121.6 = 70.3$  kN instead of the full 256 kN of the Lorentz force
- In average, we do expect that each bullet, from cool-down to I nominal, is additionally strained by:  

$$70.3 \text{ kN} / 16 / 200 \text{ GPa} / \pi / (5.3235 \text{ mm})^2 = 250 \text{ } \mu\text{m/m}$$

# Longitudinal preloading system



- Preload is applied to tie rods by screwing the superbolts
- Tie rods transfer the load to the flange
- then to the bullet
- and finally to the winding

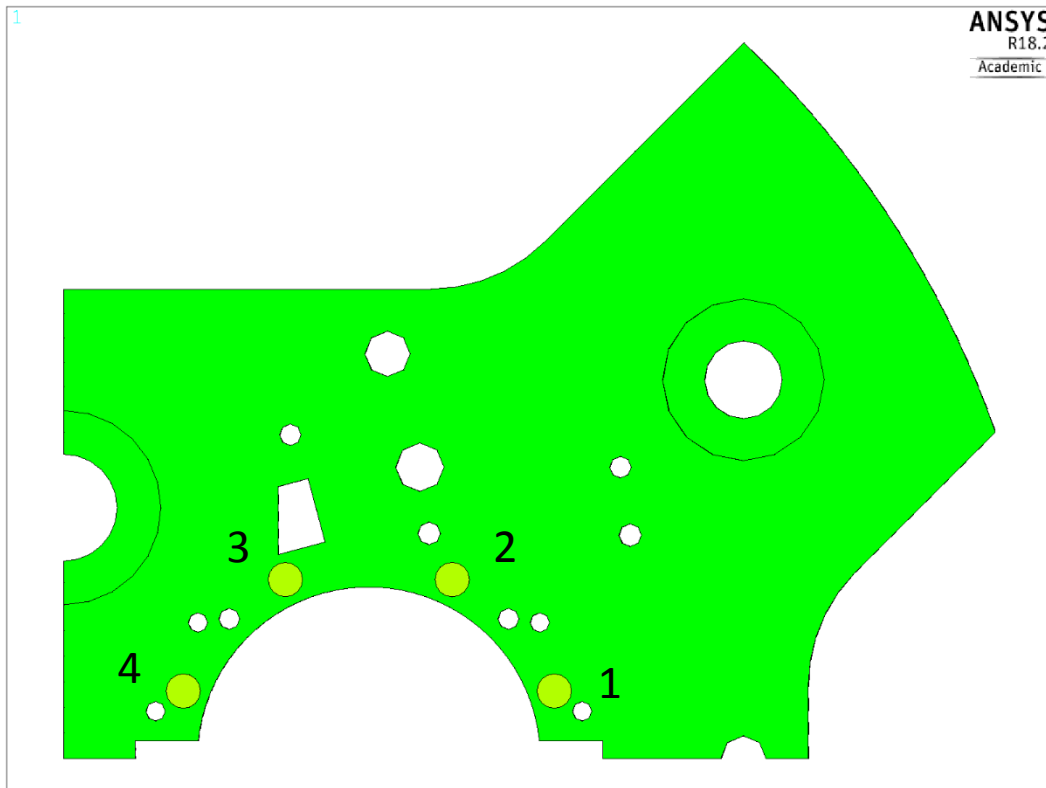
# Bullet gauge measurements

			Test 2020 @ CERN							
			Arrival at CERN	SM18 Insert Room Temp.	I nominal 12.3 kA		Warm Up [12/08/20]	Cool Down [23/08/20]	I nominal 12.3 kA	
	Label	Unit	293K	293K	1.9 K	Loading	293K	1.9 K	1.9 K	Loading
Bullet gauges [kN]	BDL1	μm/m	754	674	825	215	651	572	785	213
	BDL2	μm/m	-620	-510	-703	-188	-483	-478	-660	-181
	BDL3	μm/m	OFVL	OFVL						
	BDL4	μm/m	633	540	836	132	510	693	807	114
	BDR1	μm/m	916	881	827	304	808	483	799	316
	BDR2	μm/m	1053	OFVL						
	BDR3	μm/m	Short-circuit	Short-circuit						
	BDR4	μm/m	OFVL	OFVL						
	BUL1	μm/m	Short-circuit	Short-circuit						
	BUL2	μm/m	-1027	-925	-779	-106	-916	-638	-746	-109
	BUL3	μm/m	-352	-243	-139	-82	-205	-9	-101	-92
	BUL4	μm/m	-966	-846	-827	-214	-798	-567	-794	-227
	BUR1	μm/m	-62	-35	-48	-241	47	224	-11	-236
	BUR2	μm/m	-655	-608	-480	-198	-541	-248	-449	-201
	BUR3	μm/m	-592	-527	-373	-81	-470	-259	-348	-88
	BUR4	μm/m	624	-560	516	184	505	300	493	193



# Bullet gauge FEA results

- Measurements: loading between  $-80$  and  $-240 \mu\text{m}/\text{mm}$



	1.9 K $\mu\text{m}/\text{mm}$	I nominal $\mu\text{m}/\text{mm}$	Loading $\mu\text{m}/\text{mm}$
1	-510.8	-880.0	-369.3
2	-565.0	-796.5	-231.5
3	-404.5	-568.0	-163.5
4	-285.5	-540.5	-255.0

Average loading strain:  $255 \mu\text{m}/\text{m}$

THANKS FOR THE ATTENTION

Sept. 2<sup>nd</sup> 2020

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