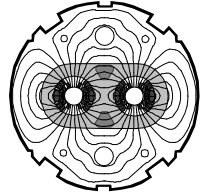




MSD beam dump septum magnets: overview and fault scenarios



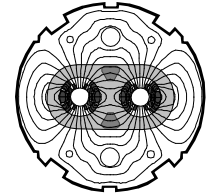
M. Sassowsky (SL/MS)

CERN: M. Gyr, E. Weisse, R. Guinand, W. Weterings, S. Bidon, D. Gerard, M. Sassowsky
IHEP: E. Ludmirsky, N. Tyurin, A. Kleshchov, P. Korobchuk, A. Ivanenko, N. Yarygin,
V. Noskov, E. Gudkova, V. Komarova

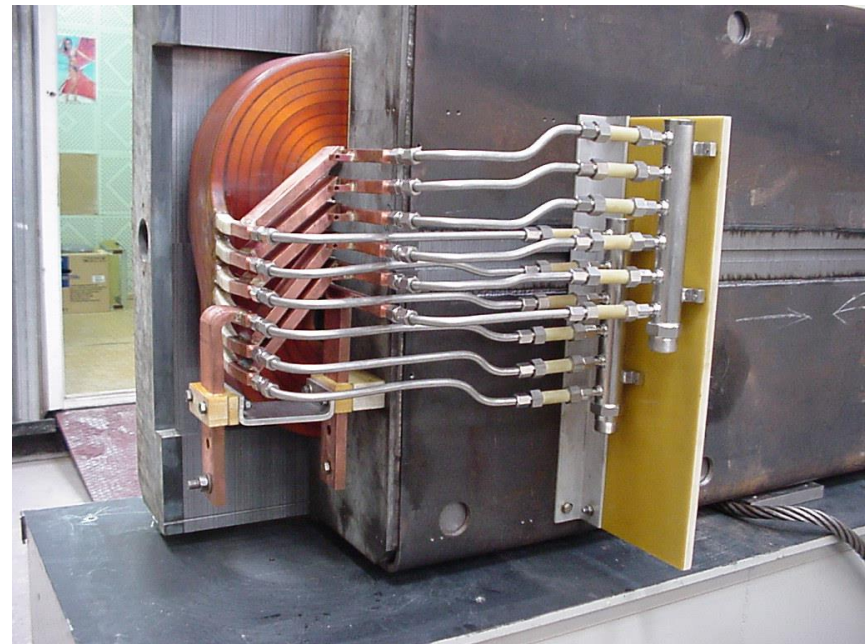
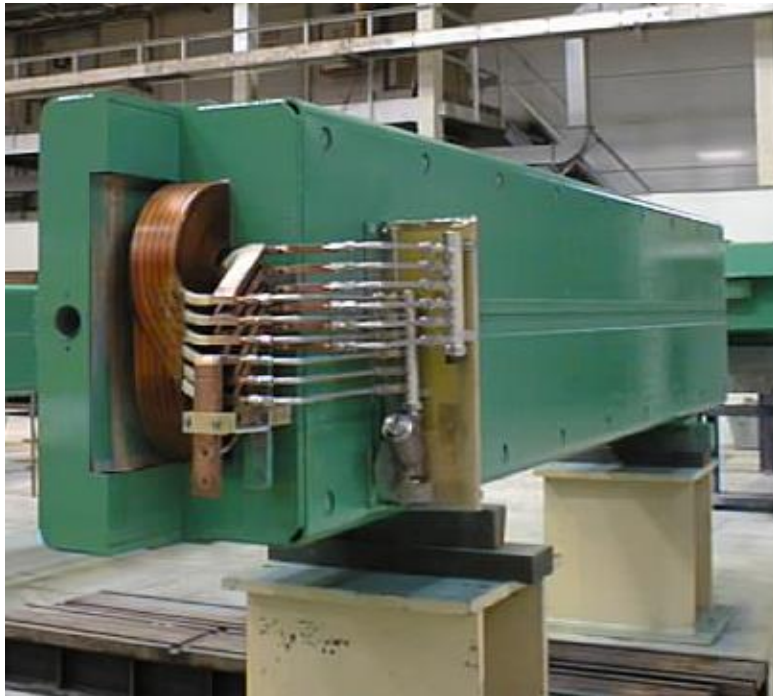
- ◆ **Status**
- ◆ **Calibration curve**
- ◆ **Cooling and thermal protection**
- ◆ **Coil design**
- ◆ **Interturn short-circuits**



Status

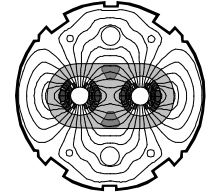


- ◆ 1 MSDC prototype built by IHEP
- ◆ Mechanical, electrical and magnetic measurements OK
- ◆ Shipment of prototype foreseen end of May 2001

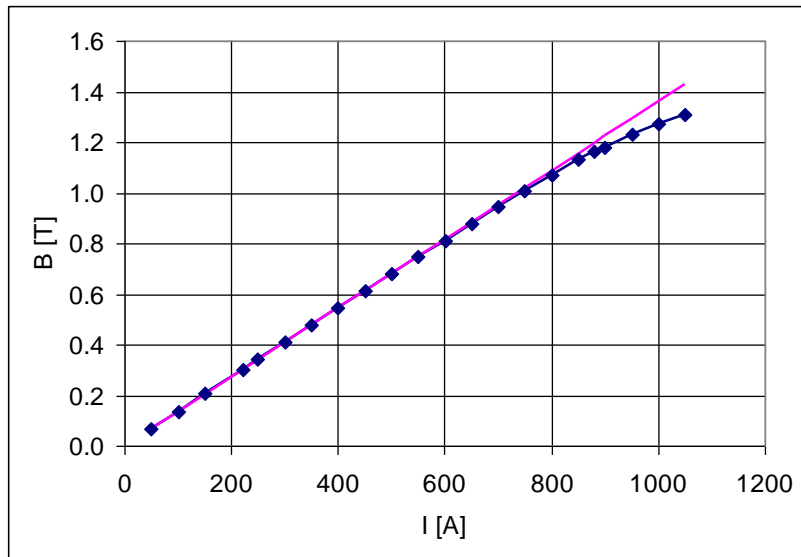




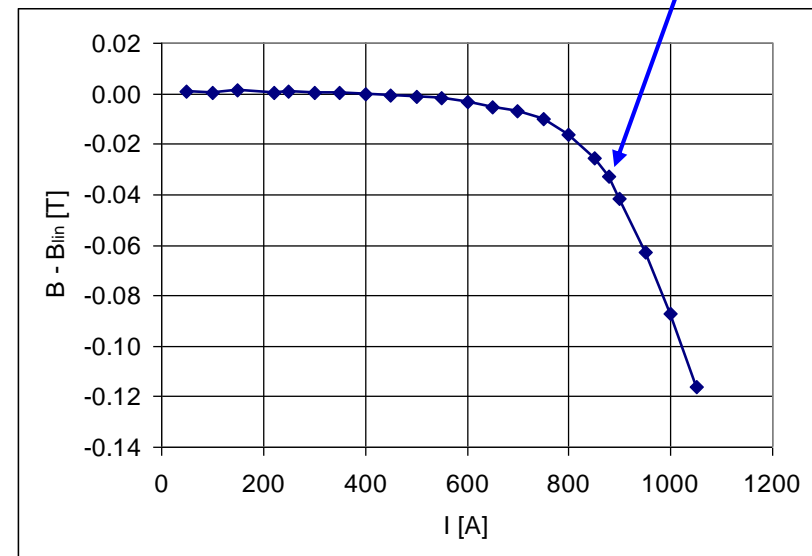
Calibration curve (1)



◆ B vs. I using NMR probe

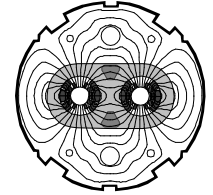


At nominal current (880 A)
for top energy:
Non-linearity ~2.8 percent

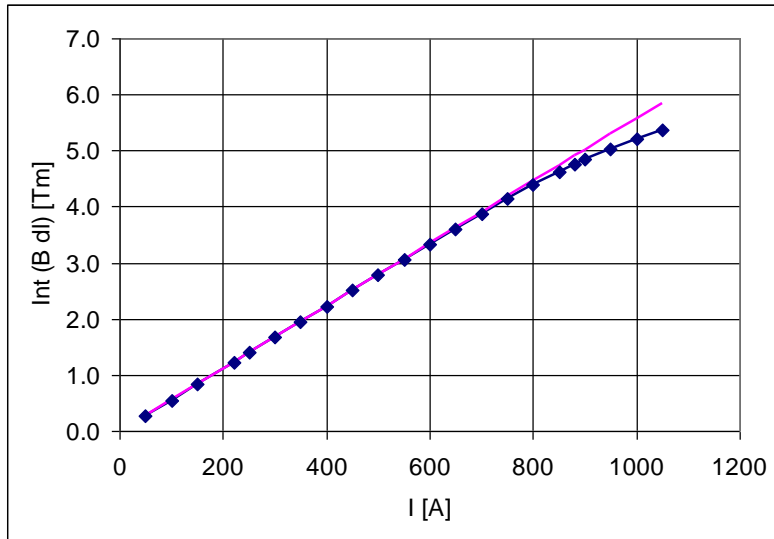




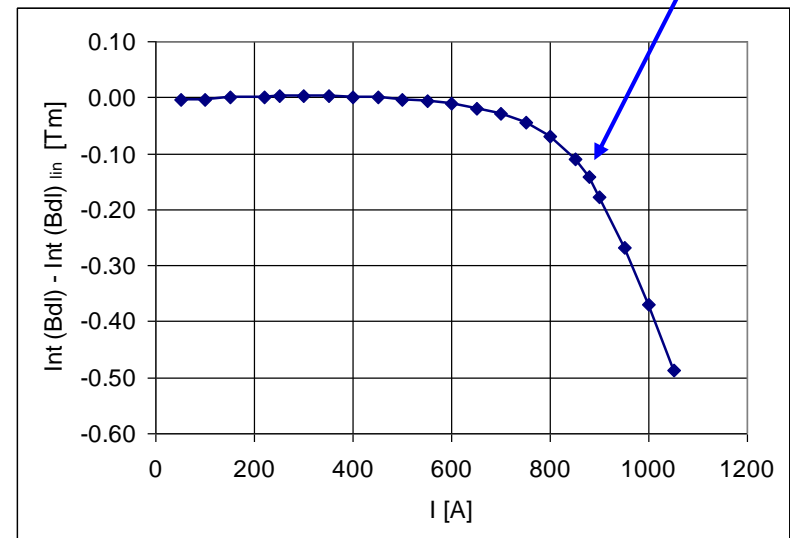
Calibration curve (2)



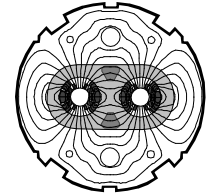
◆ $\int B dl$ vs. I using stretched wire technique



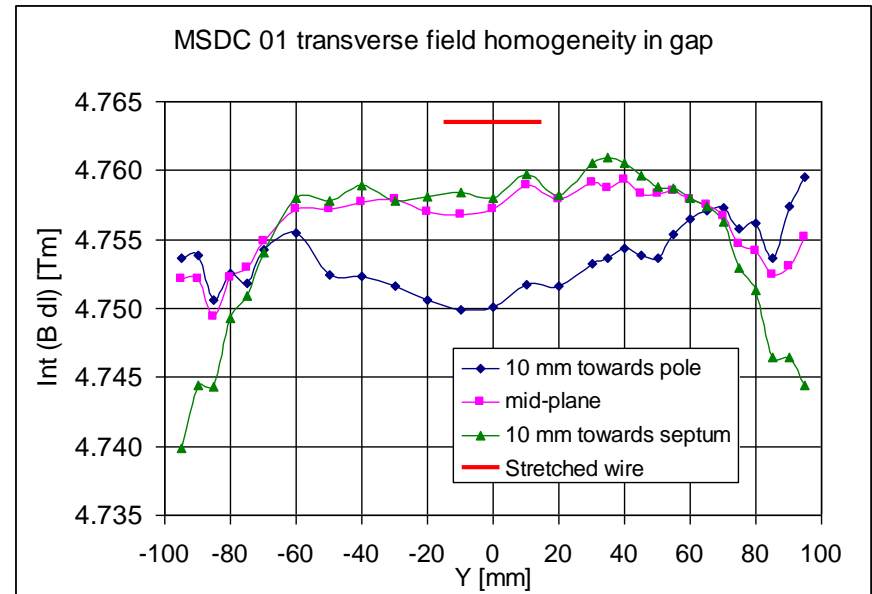
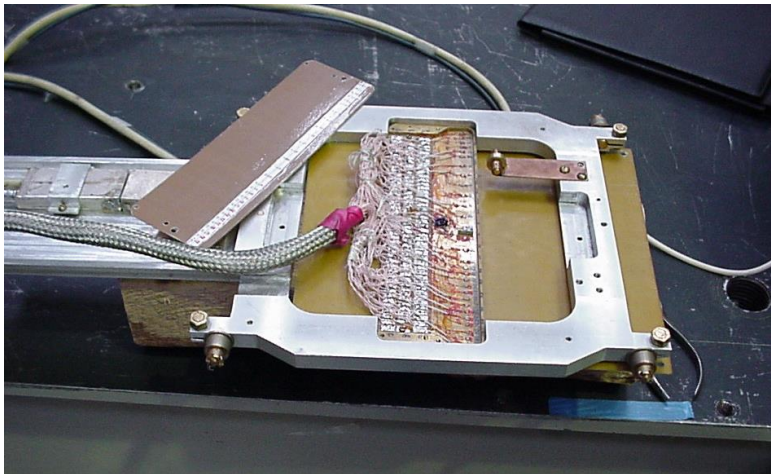
At nominal current (880 A)
for top energy:
Non-linearity ~3.0 percent



Calibration curve (3)

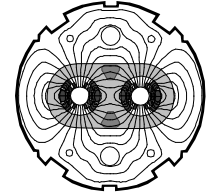


- ◆ **Cross-check: $\int B dl$ at $I = 880$ from field map with Hall probe array**





Cooling



◆ **Basic formulae:**

$$RI^2 = cQ(T_{out} - T_{in})$$

$$\frac{\Delta p}{l} = k \frac{Q^{1.75}}{d^{4.75}}$$

◆ **Temperature dependence of Resistance:**

$$R(T) = R(T_0) \cdot (1 + \alpha(T - T_0))$$

$$\alpha = 3.8 \cdot 10^{-3} / K \quad (\text{for Copper})$$

◆ **Average coil temperature:**

$$T \approx \frac{1}{2}(T_{out} + T_{in})$$

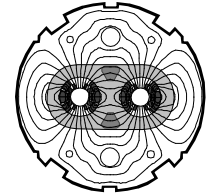
◆ **Actual average coil temperature depends on T_{in} and I_{RMS}**

◆ **For continued operation at 880 A: $(T_{out} - T_{in}) \approx 20^\circ C$**

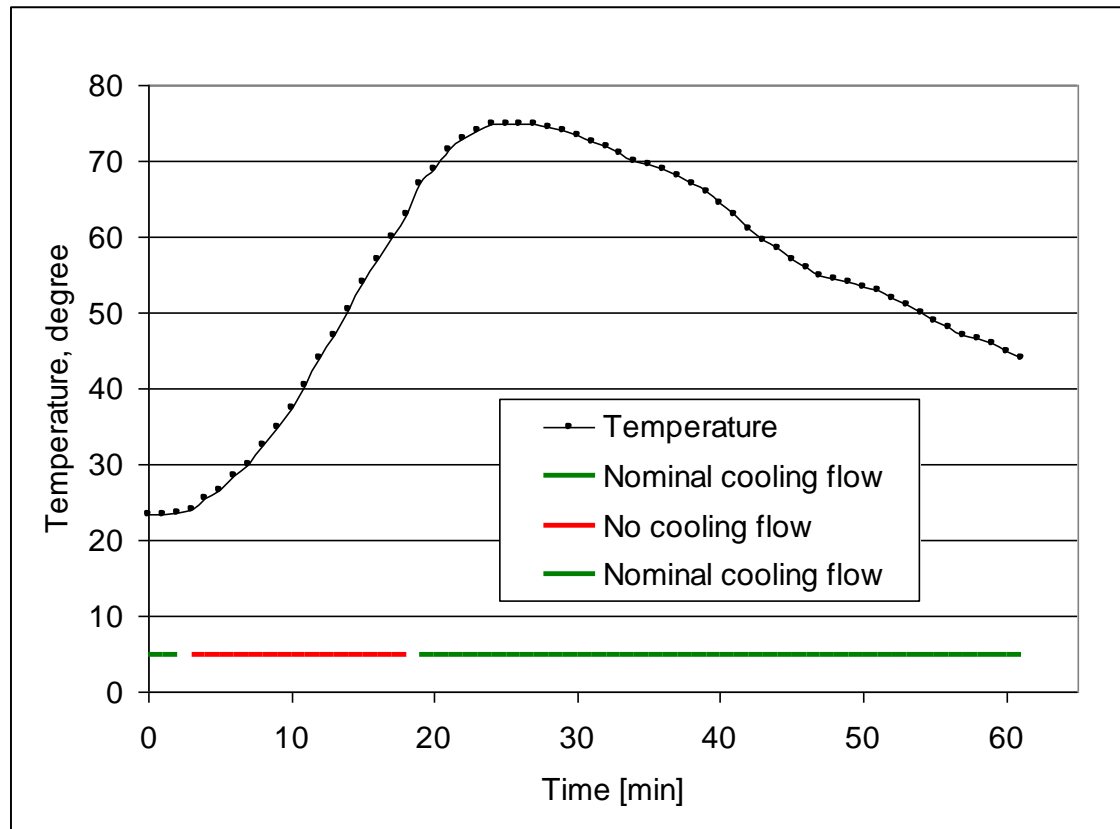
$$\Rightarrow \Delta R / R \approx 4\%$$



Thermal protection

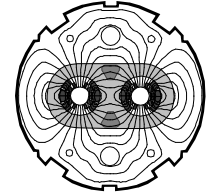


- ◆ Each layer: thermoswitch
- ◆ Test of thermoswitches by stopping cooling water:

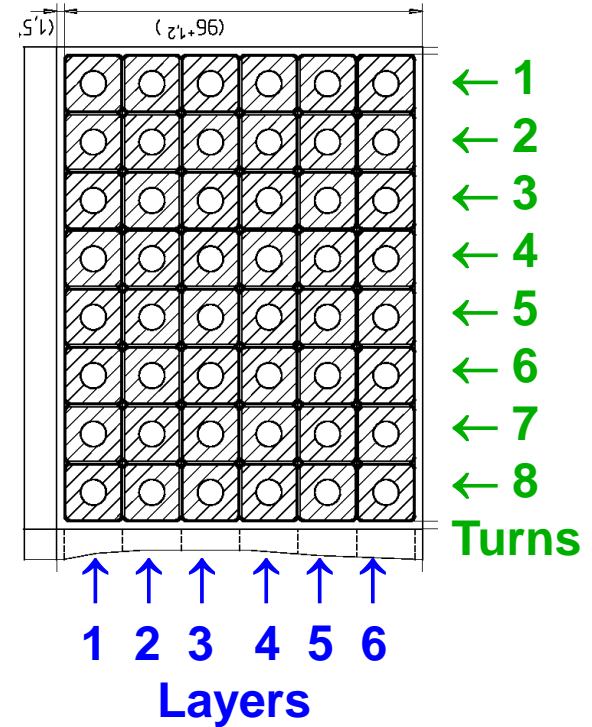
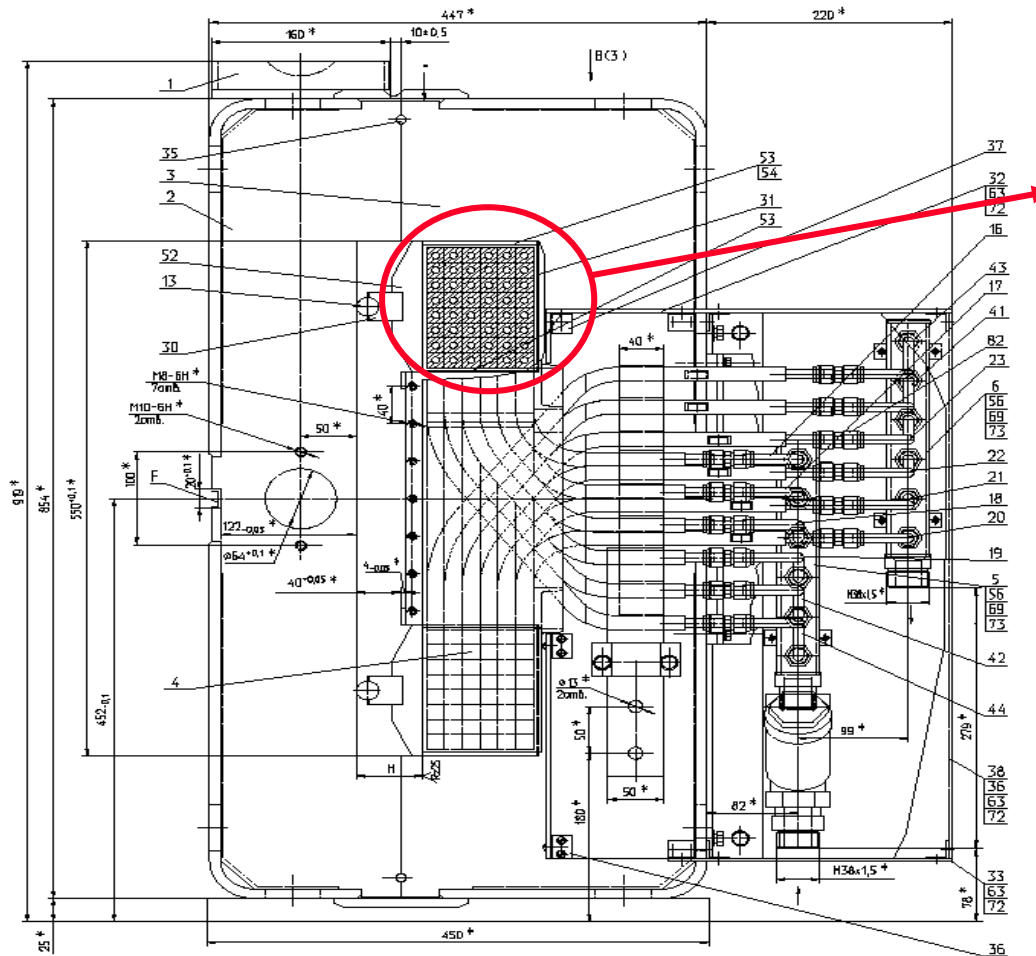




Coil design (1)



MSDC front view:

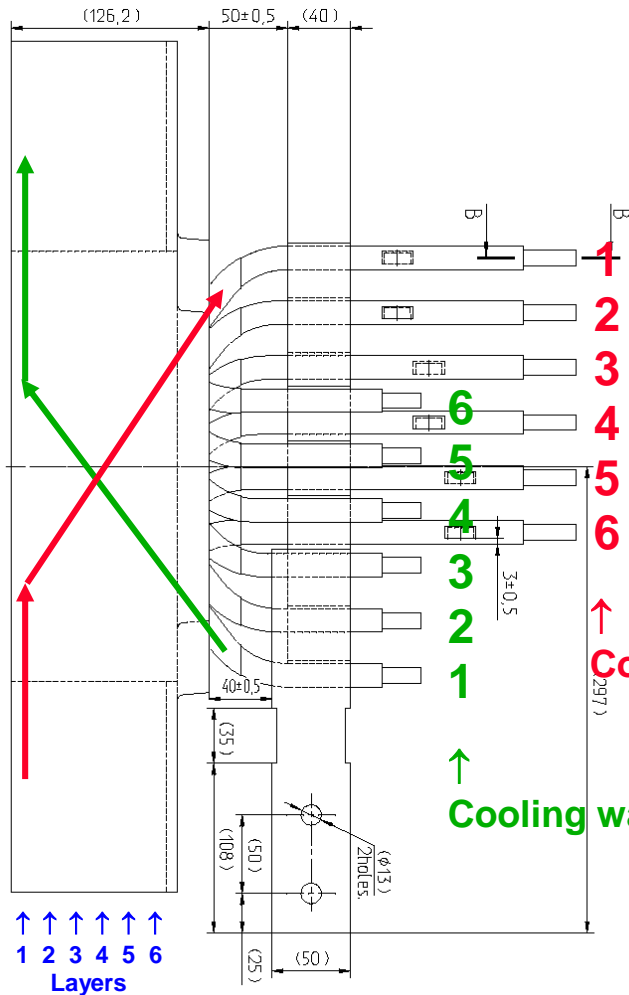
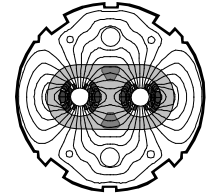


Electrically: in series
Hydraulically: in parallel

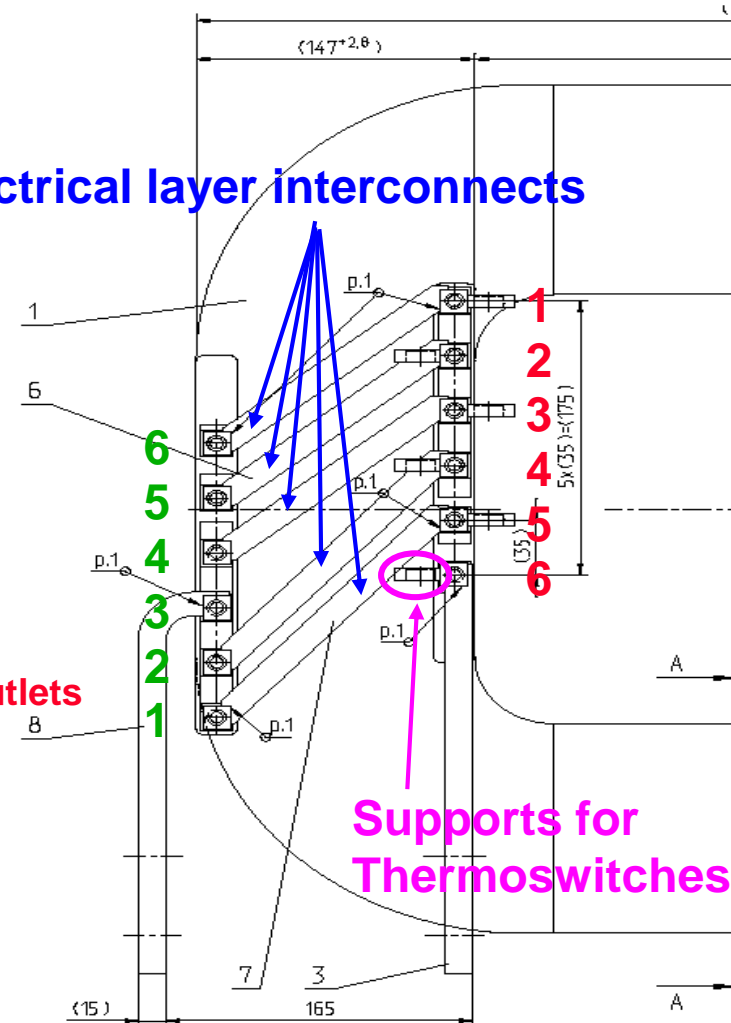
MSDB: 5 layers
MSDA: 4 layers



Coil design (2)

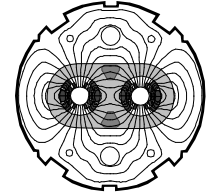


Electrical layer interconnects

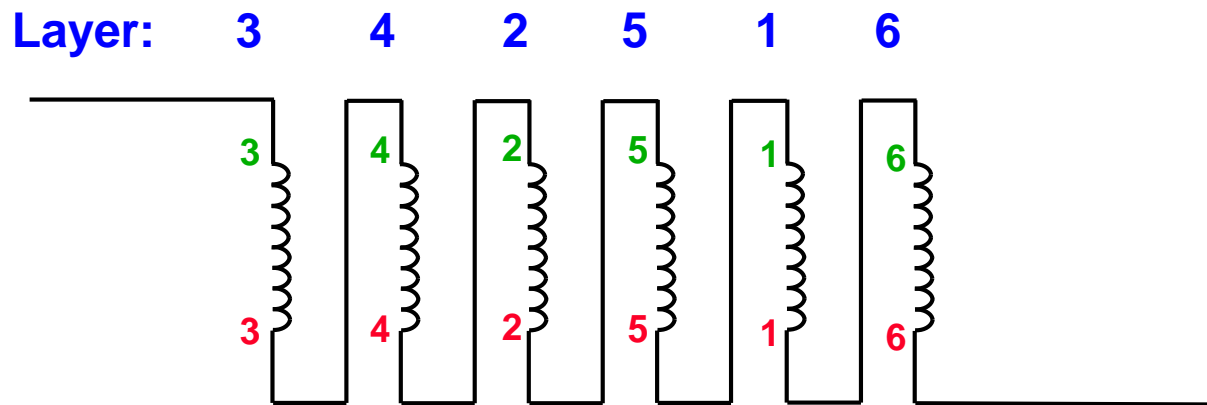




Coil design (3)



Electrical series connection of layers:



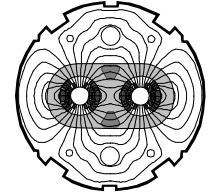
$$I_{nom} = 880 \text{ A} \quad (\text{at top energy})$$

$$R_{layer} = 6.76 \text{ m}\Omega \quad (\text{at } T=20^\circ\text{C})$$

$$U_{layer} = 5.95 \text{ V} \quad (\text{at } T=20^\circ\text{C})$$



Interturn short-circuits (1)



- ◆ **Integrated field of a dipole magnet:**

$$\int Bdl = \frac{\mu_0 nI}{g + \frac{d}{\mu}} (l + k \cdot g)$$

$nI =$ **Ampere-turns**

$g =$ **Gap height**

$d =$ **Path length in return yoke**

$\mu =$ **Steel permeability**

$l =$ **Yoke length**

- ◆ **Interturn short-circuit**

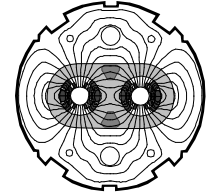
=> reduction of nI

=> reduction of $\int Bdl$

=> wrong deflection angle θ



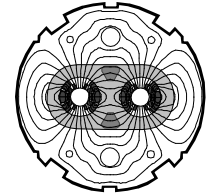
Interturn short-circuits (2)



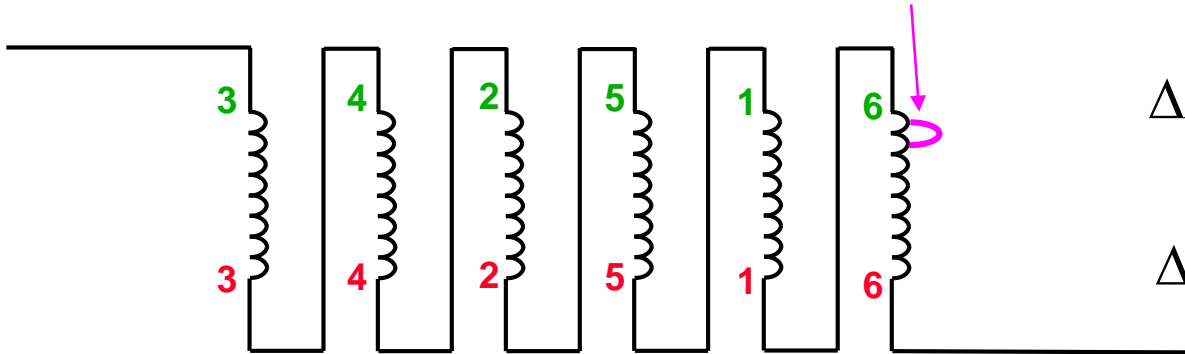
- ◆ **For one beam:**
 - 5 MSDA
 - 5 MSDB
 - 5 MSDC
- ◆ **Total number of turns:** $n_{tot} = 5 \cdot (4 \cdot 8 + 5 \cdot 8 + 6 \cdot 8)$
 $= 600$
- ◆ **Worst case for one interturn short-circuit:**
 $\Delta n = 2 \cdot 8 = 16$
 $\frac{\Delta n}{n} = \frac{\Delta \int B dl}{\int B dl} = \frac{\Delta \theta}{\theta} = 2.7\%$



Interturn short-circuits (3)



◆ **Between two turns within one layer:**

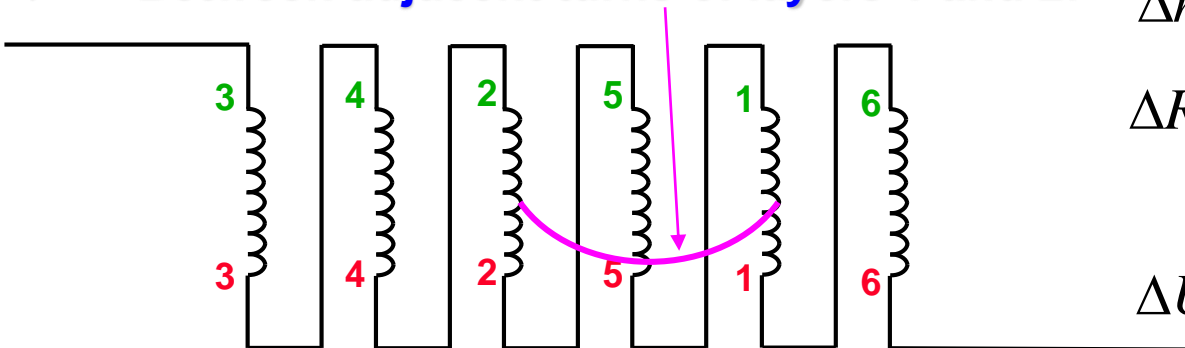


$$\Delta n = 1$$

$$\Delta R = -\frac{1}{8} R_{layer}$$

$$\Delta U_i = \begin{cases} \Delta R \cdot I & i = 6 \\ 0 & i = 1 \dots 5 \end{cases}$$

◆ **Between adjacent turns of layers 1 and 2:**



$$\Delta n = 16$$

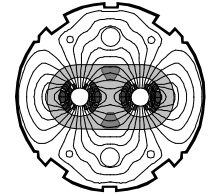
$$\Delta R = 2 \cdot R_{layer}$$

$$\Delta U_i = \begin{cases} -R_{layer} \cdot I & i = 5 \\ \neq 0 & i = 1, 2 \\ = 0 & \textit{else} \end{cases}$$

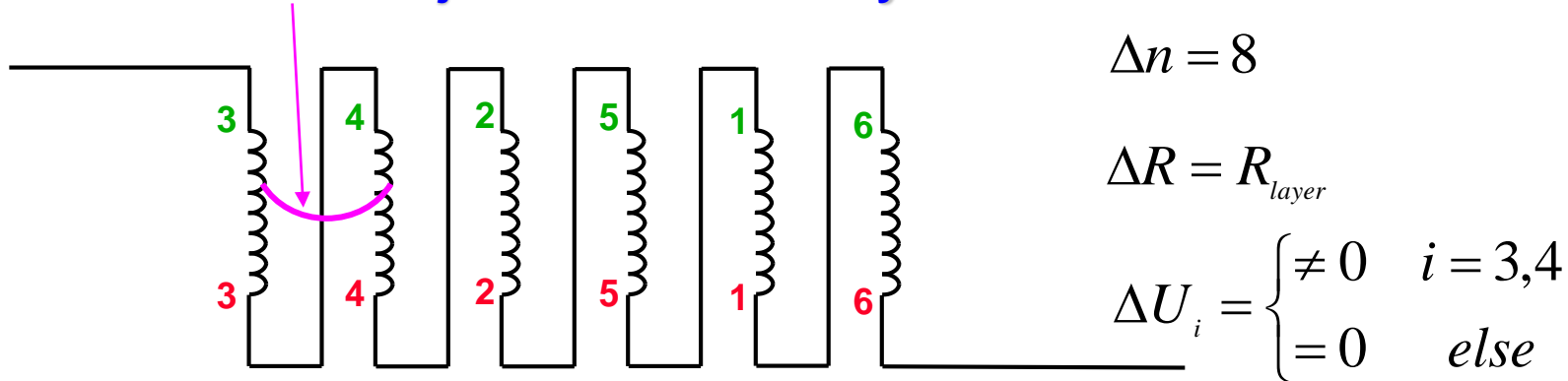
(similar: 2-3, 4-5, 5-6)



Interturn short-circuits (4)



- ◆ **Between adjacent turns from layers 3 and 4:**



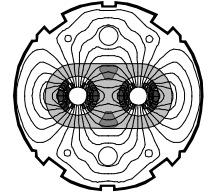
- ◆ **etc. for MSDB coil (5 layers) and MSDA coil (4 layers)**

- ◆ **Worst case: $\Delta n = 16$**

- ◆ **To detect interturn short circuits:
Absolute value of layer voltage is not useful
(depends on coil temperature and current)
=> Compare the voltage of the different layers**



Summary



- ◆ **Non-linearity of $\int B dl$ vs. I**
- ◆ **Thermoswitches as protection against overheating**
- ◆ **To detect interturn short circuits:
Compare the voltage of the different layers**

To be studied in detail:

- **“Matrix” for comparison of layer voltages**
- **Threshold values**
- **Residual temperature dependence**
- **Systematic differences from layer to layer**
- **Long term stability**
- **Calibration**
- **....**