

# CEPC Superconducting Quadrupole in Interaction Region

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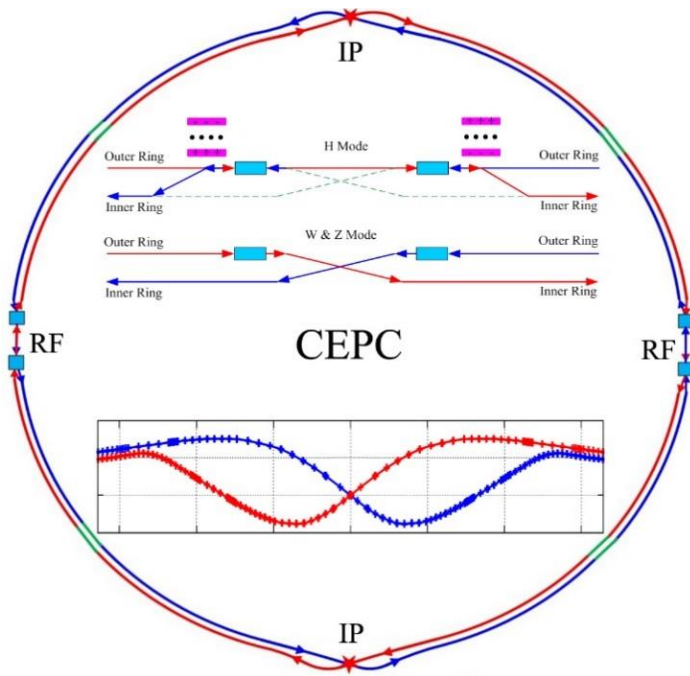
# Outline

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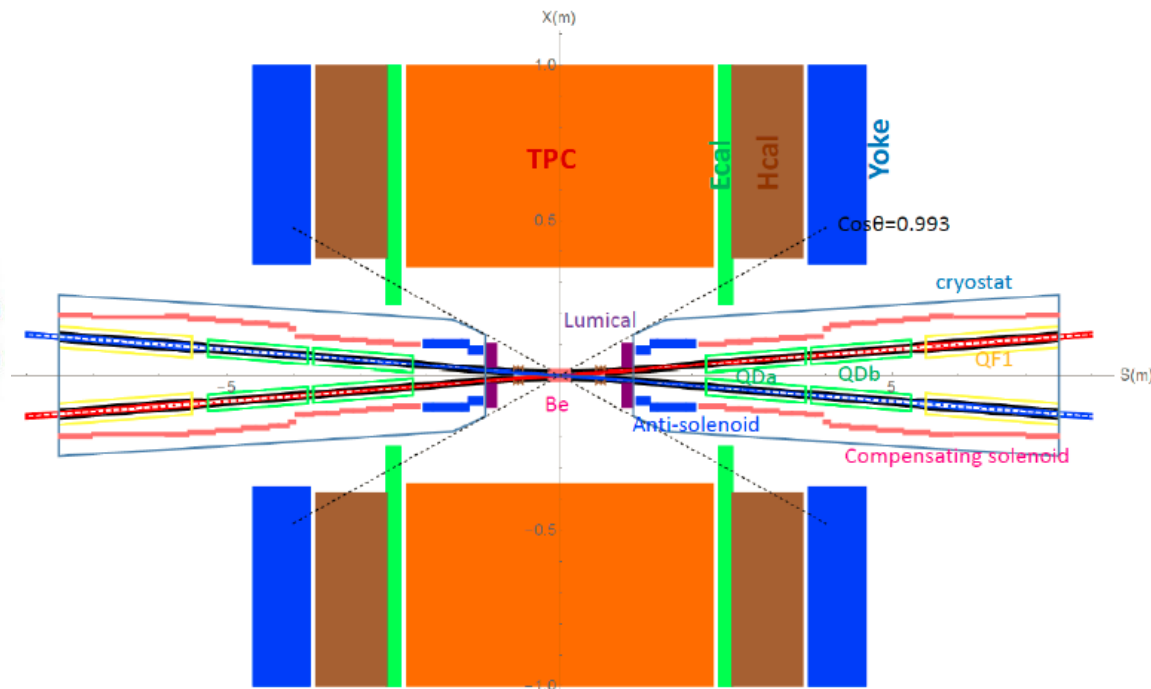
- **Introduction**
- **Overall design of CEPC Interaction Region Superconducting Quadrupole**
- **Conceptual design of HTS final focus quadrupole**
  - 1)  $\text{Cos}2\theta$  coil
  - 2) CCT coil
  - 3) Racetrack coil
- **Summary**

# Introduction

- ◆ CEPC is a Circular Electron Positron Collider with a circumference about 100 km, beam energy up to 120 GeV proposed by IHEP.
- ◆ Most magnets in CEPC Accelerator are conventional magnets.
- To greatly squeeze the beam for high luminosity, compact **high gradient final focus quadrupole magnets** are required on both sides of the IP points in CEPC collider ring.



Sketch of CEPC Collider ring



CEPC MDI layout

# Introduction

- ◆ The **CDR requirements** of the Final Focus quadrupoles (QD0 and QF1) are based on  $L^*$  of 2.2 m, beam crossing angle of 33 mrad.

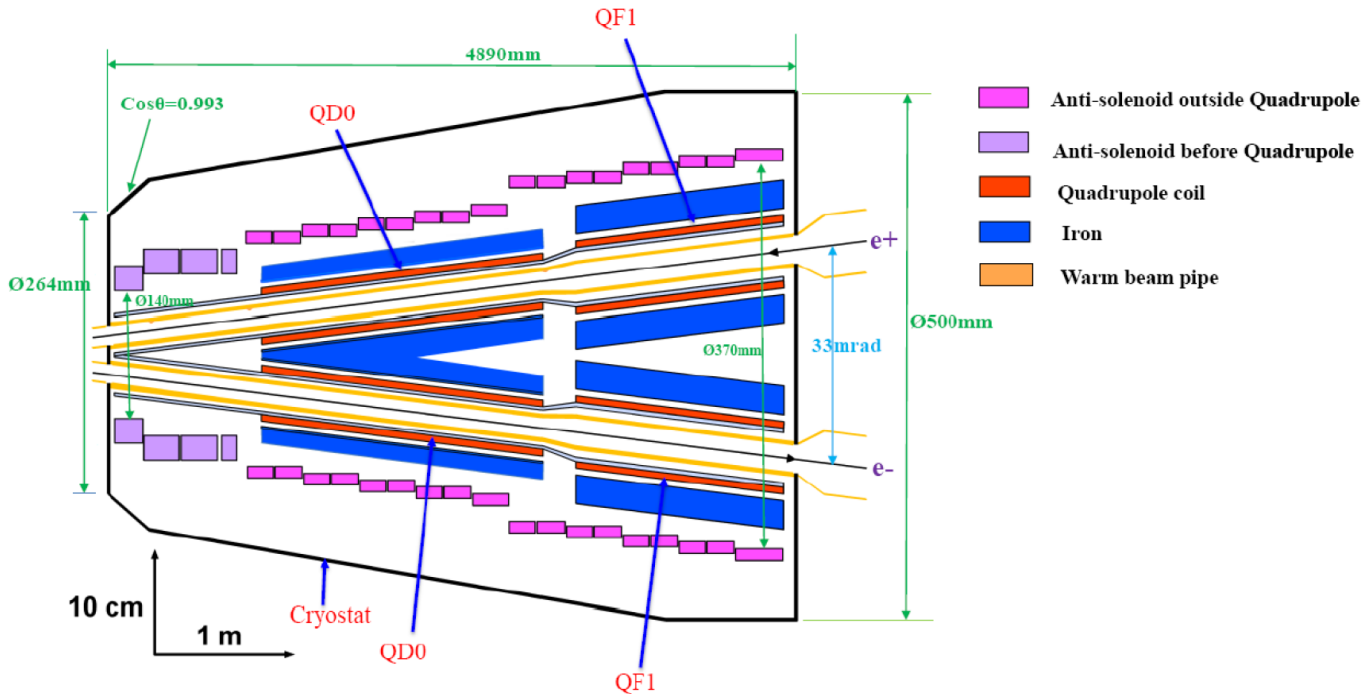
Table 1: CDR requirements of Interaction Region quadrupole magnets for Higgs

Magnet	Central field gradient (T/m)	Magnetic length (m)	Width of GFR (mm)	Minimal distance between two aperture beam lines (mm)
QD0	136	2.0	19.6	72.6
QF1	110	1.48	27.0	146.20

- ◆ QD0 and QF1 magnets are operated inside the field of **Detector solenoid magnet with a central field of 3.0 T**.
- To cancel the effect of the longitudinal detector solenoid field on the accelerator beam, **anti-solenoids before QD0, outside QD0 and QF1 are needed**.
- The total integral longitudinal field generated by the detector solenoid and accelerator anti-solenoid is zero; Local net solenoid field in the region of quadrupole is close to zero.

# Introduction

- ◆ CEPC MDI SC Magnets start at  $z=1.12\text{m}$ , including: superconducting QD0, QF1, anti-solenoid on each side of the IP point.
- ◆ Inner radius of beam pipe is 10 mm in CDR; Checked by HOM heating load calculation.
- QD0, QF1, and anti-solenoid coils are in the same cryostat.



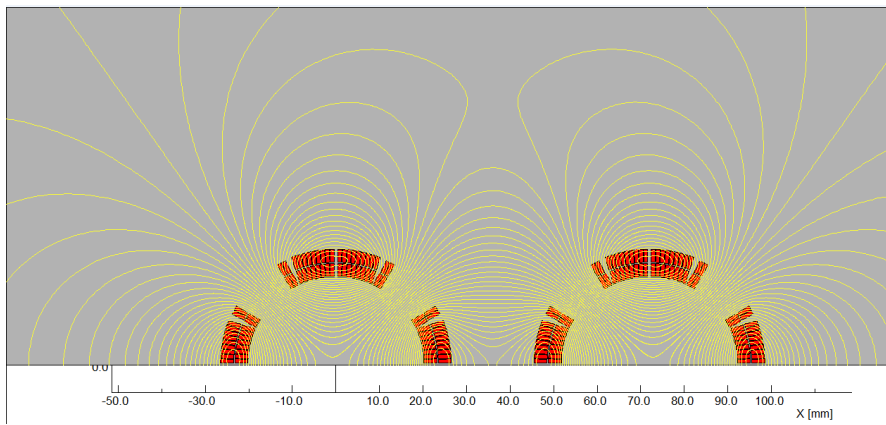
Schematic layout of QD0, QF1, and anti-solenoid

# Overall design of CEPC Interaction Region Superconducting Quadrupole

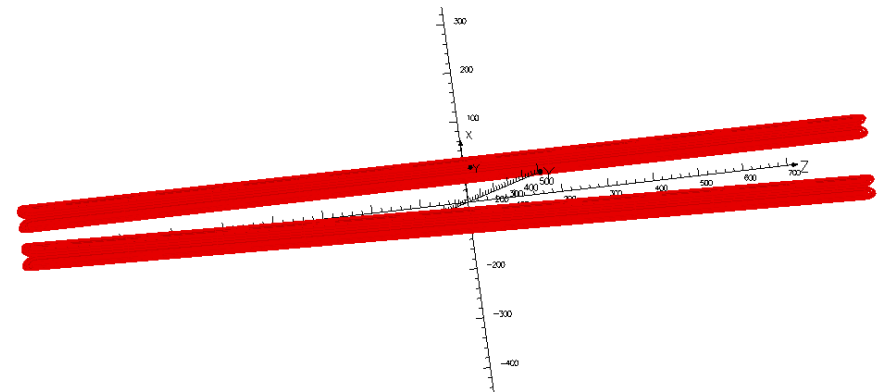
## Overall design of QD0

### Option1: Iron-free design of QD0 (CDR)

- ◆ Minimum distance between QD0 two aperture centerlines: 72.61 mm.
- ◆ The Iron-free design of QD0 is based on **two layers  $\cos 2\theta$  quadrupole coil using NbTi Rutherford cable without iron yoke.**
- The QD0 single aperture coil cross section is optimized with four coil blocks in two layers separated by wedges, and there are 21 turns in each pole.
- The excitation current is 2600A. the field crosstalk between the two apertures is **very large.** Integrated multipoles in 3D : **b3 19 unit** ( $1 \times 10^{-4}$ ), **b4 3.6 unit.**



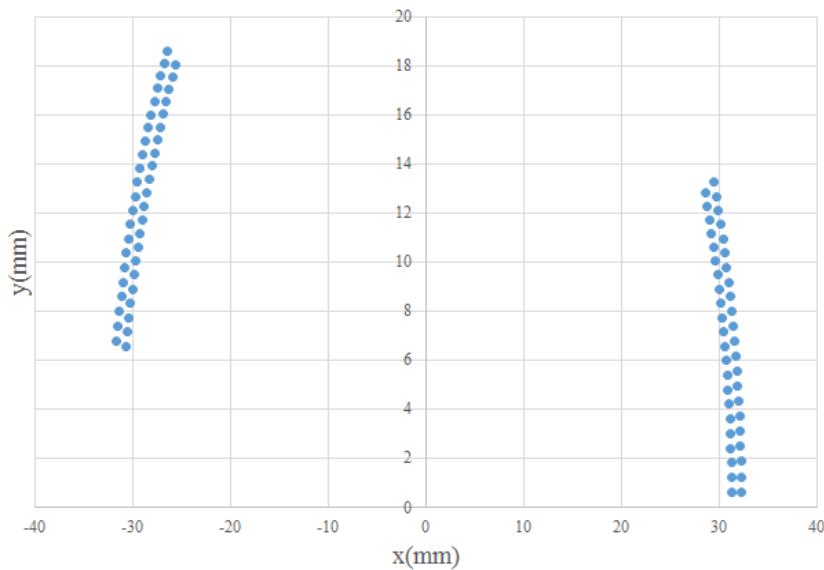
2D flux lines



3D model

# Overall design of QD0

- ◆ Two layers of shield coil is introduced outside the quadrupole coil to **improve the field quality**. The shield coil is not symmetric within each aperture, but the shield coils for two apertures are symmetric.
- ◆ The conductor for the shield coil is round NbTi wire with 0.5 mm diameter. The calculated **integrated** field quality and multipole fields **at different longitudinal positions** are all smaller than  $3 \times 10^{-4}$ .



Shield coil layout (half)

Table 2: Integrated field harmonics with shield coil  
( $1 \times 10^{-4}$ )

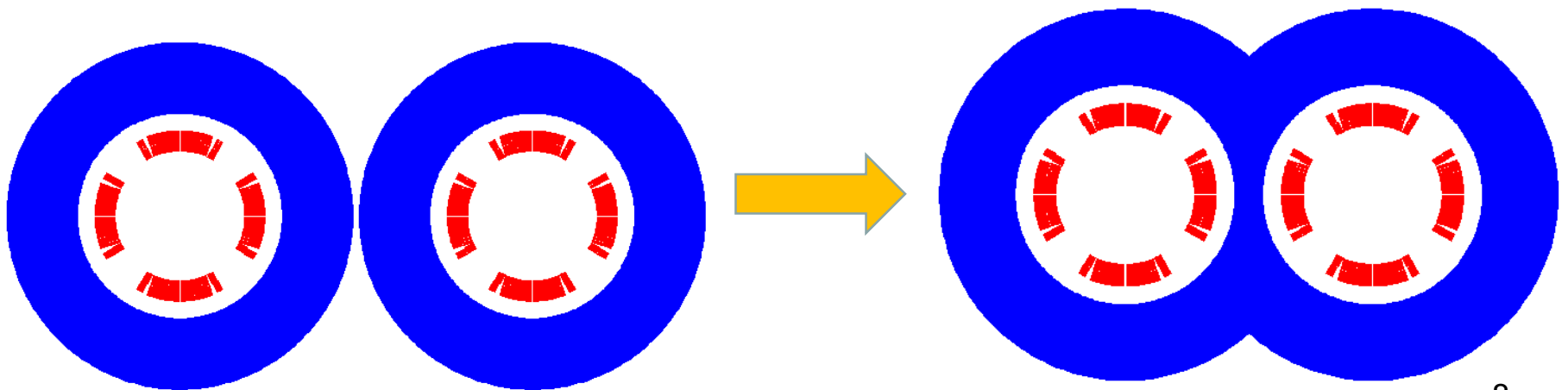
n	$B_n/B_2@R=9.8 \text{ mm}$
2	10000.0
3	-0.57
4	1.53
5	0.38
6	-0.14
7	0.015
8	-0.031
9	-0.02
10	-0.058

## Option2: QD0 design with iron

- QD0 CDR: 136T/m, **inner diameter 40mm**, length 2m.

### QD0 design of iron option

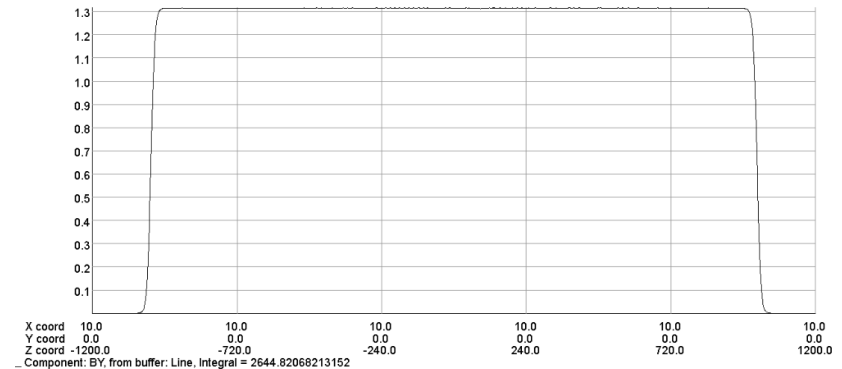
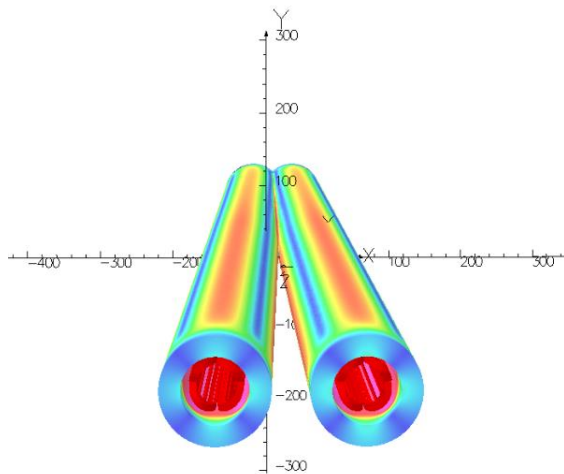
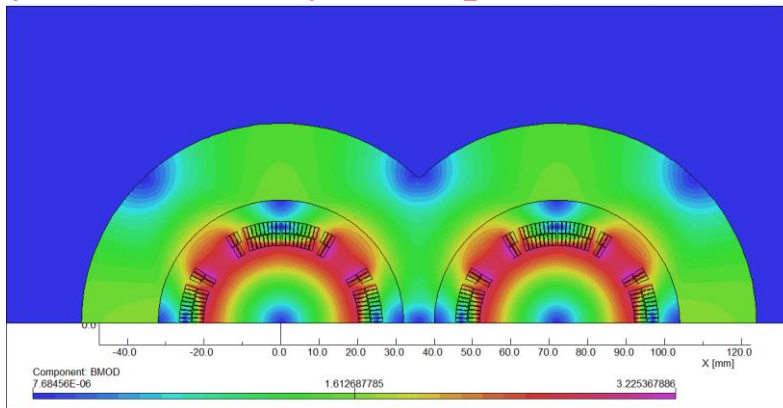
- Iron yoke is added outside the collar to enhance the field gradient, reduce the coil excitation current, and shield the field crosstalk.
- Not enough space to place two single apertures side by side, so a compact design is adopted.
- $\cos 2\theta$  quadrupole coil using NbTi Rutherford: highest magnetic efficiency and cooling capacity, good stability, elimination of field crosstalk.
- ✓ **Iron core in the middle part is shared by the two apertures.**





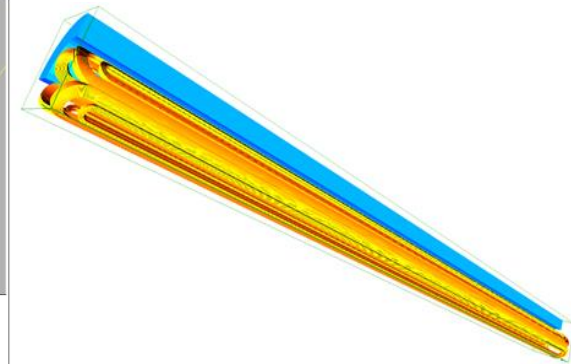
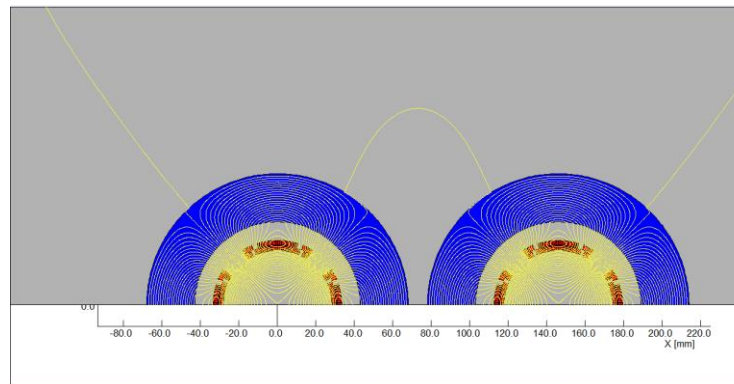
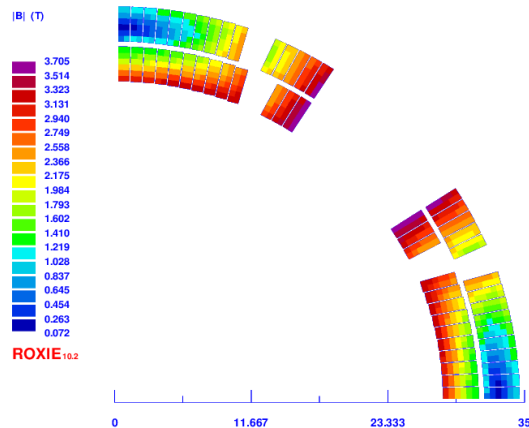
# Option2: QD0 design with iron

- The excitation current is **2080A @4.2K**.
- The field harmonics as a result of field crosstalk is smaller than  $0.5 \times 10^{-4}$ .  
Compared with the iron-free design, **the excitation current can be reduced.**
- **Novel design:** Double aperture quadrupole magnet using  $\cos 2\theta$  coil with **iron yoke shared by two apertures**, with crossing angle between two apertures.



# Overall design of superconducting quadrupole magnet QF1

- Since the distance between the two apertures is much larger, the field cross talk between the two apertures of QF1 is not a problem using iron yoke.
- After optimization, the QF1 coil consists of four coil blocks in two layers separated by wedges, and there are 28 turns in each pole.
- Each systematic field harmonics is smaller than 1 unit ( $1 \times 10^{-4}$ ).
- Current: 2280A. The non-systematic field harmonics as a result of field cross talk can be neglected.

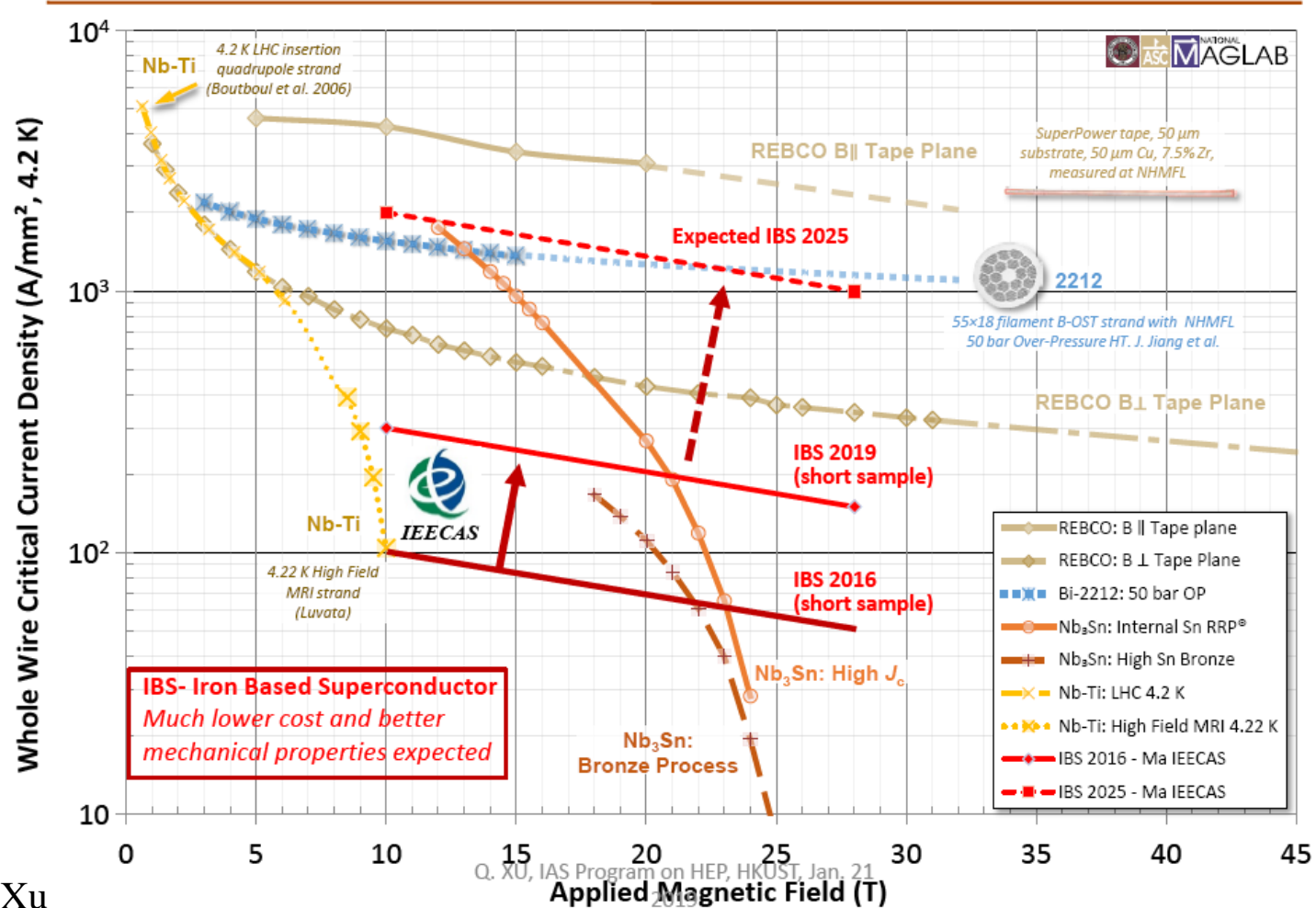


Field simulation of QF1

# Conceptual design of HTS final focus quadrupole coils in CEPC IR

◆ HTS conductor: Bi-2212 (Tc 80K), Bi-2223, YBCO (Tc 92K), MgB2, IBS...

## $J_c$ of IBS: 2016-2025



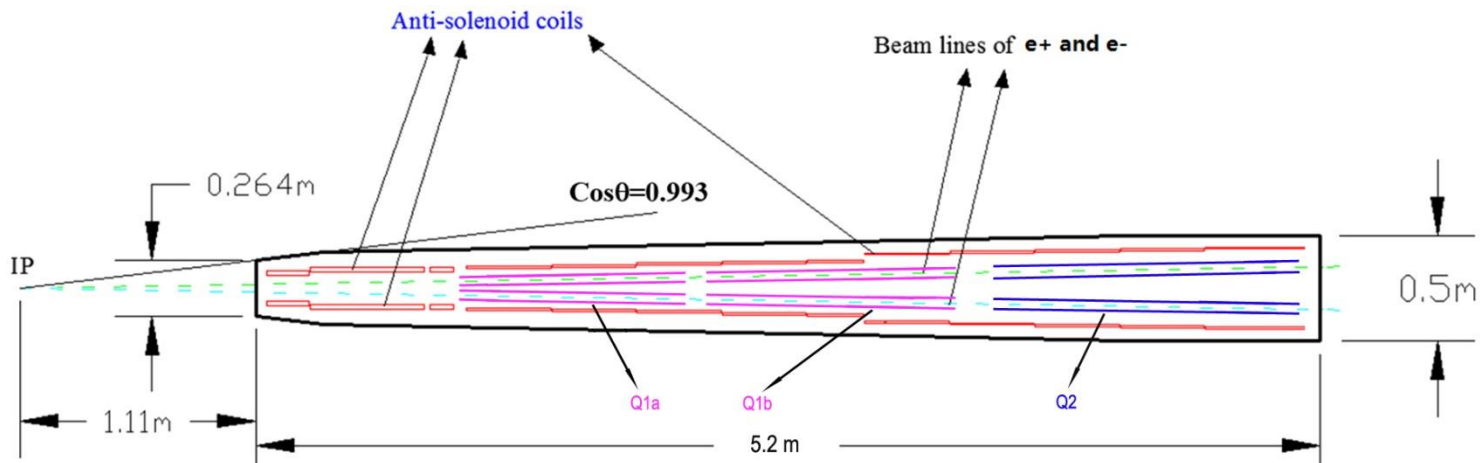
From Q.J.Xu

# Conceptual design of HTS final focus quadrupole coils in CEPC IR

- The requirement of the CEPC double aperture Final Focus quadrupoles is recently updated for **high luminosity** with  $L^*=1.9\text{m}$ .

Table 3: Updated Requirements of final focus quadrupole magnets for Higgs

Magnet	Central field gradient (T/m)	Magnetic length (m)	Width of GFR (mm)	Minimal distance between two aperture beam lines (mm)
Q1a	<b>141</b>	1.21	15.21	<b>62.71</b>
Q1b	84.7	1.21	17.92	105.28
Q2	94.8	1.5	24.14	155.11



# Conceptual design of HTS final focus quadrupole coils in CEPC IR

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## Design considerations

- The field gradient of quadrupoles is **stronger** compared to that in CDR, and the available **bore space for the coil is smaller**.
- The development of Q1a is the most challenging.
- Design of quadrupoles and anti-solenoid is similar to that in CDR.
- Corrector coils will be inside the bore of Q1b and Q2 quadrupole coil.
- Iron yoke is used to eliminate the field crosstalk between the two apertures.
- Inside quadrupole, beam pipe diameter is around 17mm or 18 mm.

# Conceptual design of HTS final focus quadrupole coils in CEPC IR

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- Feasibility of HTS superconducting magnet technology is being considered for CEPC IR superconducting magnets.
- Both HTS round wire and tape are considered.

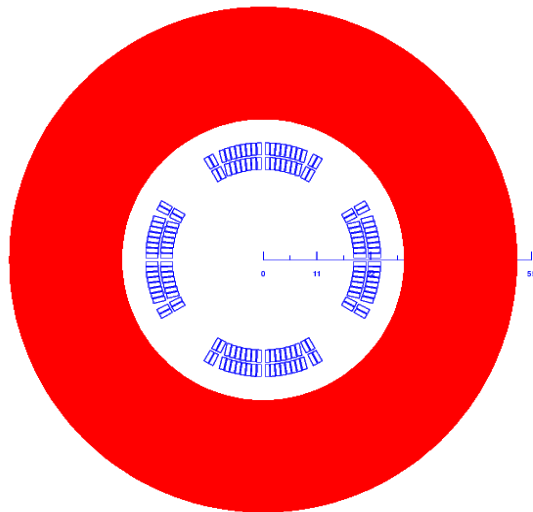
**Advantage:** Large critical current (expected), light weight of magnet  
heat load resistant  
Higher operating temperature.

**Disadvantage:** HTS conductor not mature now, expensive  
Poor mechanical properties  
HTS coil manufacture needs heat treatment  
Large diameter of superconductor filament or layer.

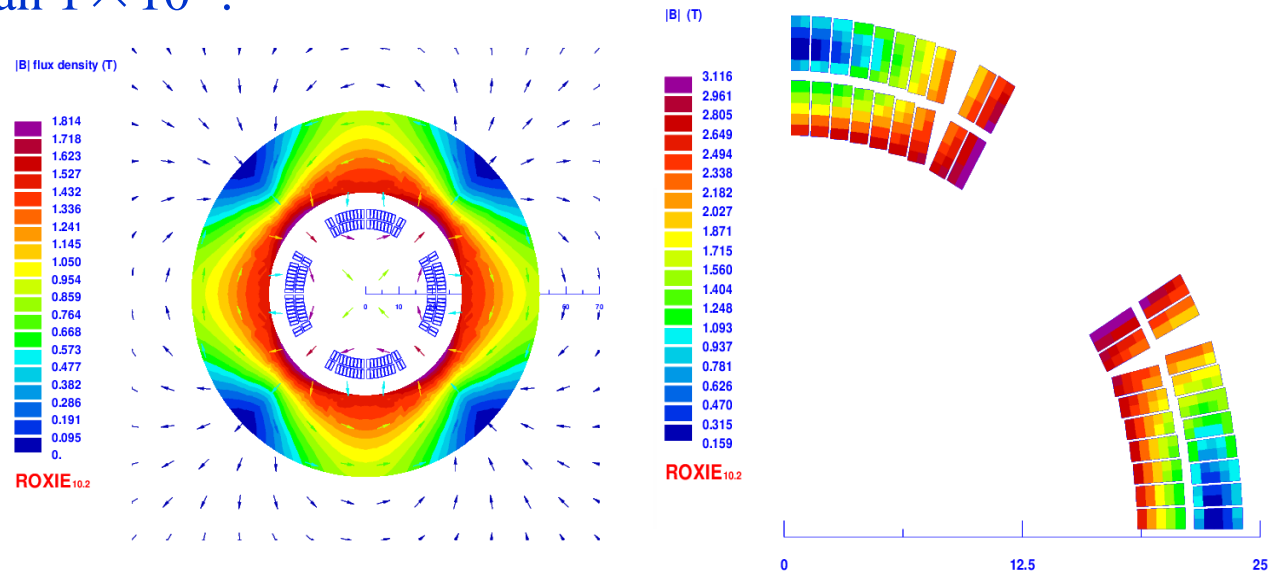
# Conceptual design of Q1a for high luminosity with $L^*=1.9\text{m}$

## 1) Cos $2\theta$ option of Q1a

- HTS Bi-2212 0.5mm wire or other conductor.
- The design of Q1a is based on two layers cos $2\theta$  quadrupole coil using Rutherford cable with iron yoke. The inner diameter of the coil is 37mm.
- Single aperture cross section is optimized with four coil blocks in two layers separated by wedges, using ROXIE.
- The width of the cable is 2.5mm, and there are 19 turns in each pole.
- The excitation current of Q1a is 1970A, and each multipole field in single aperture is smaller than  $1 \times 10^{-4}$ .



2D model (single aperture)

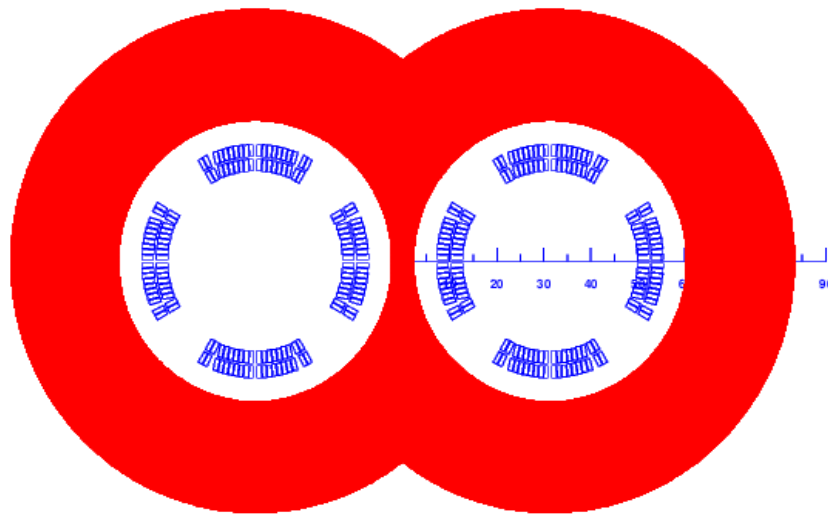


Magnetic flux density distribution

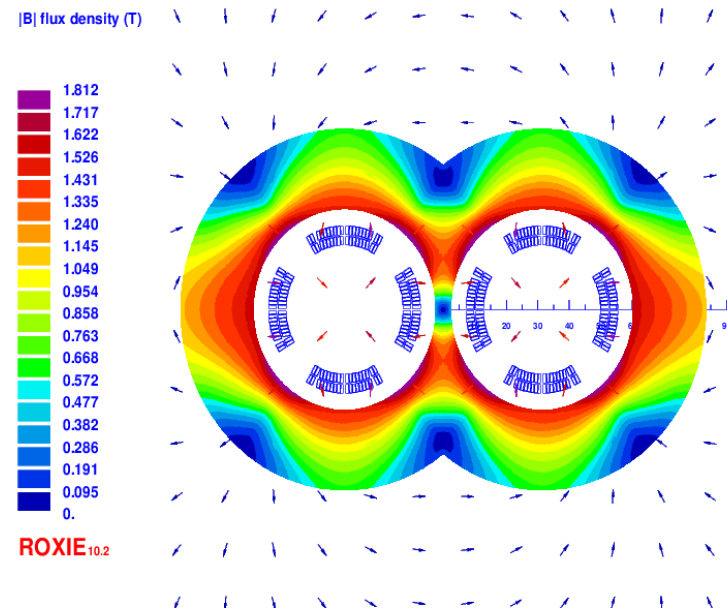
## Cos2θ option of Q1a

### Field cross talk of the two apertures

- 2D field cross talk of Q1a two apertures near the IP side, where the distance between two aperture centerlines is minimum.
- ◆ Iron yoke width in the middle is very limited; the field harmonics as a result of field crosstalk is smaller than  $0.5 \times 10^{-4}$ .
- ◆ The dipole field in each single aperture as a result of field crosstalk is smaller than 5 Gs. Magnetic field cross talk between two apertures is negligible.



Double aperture model



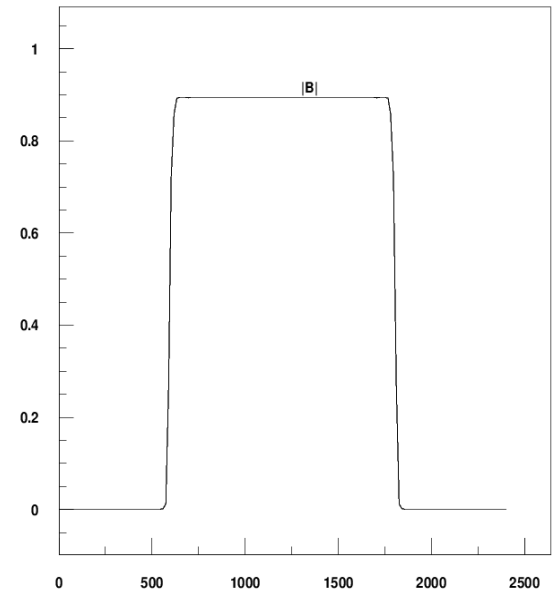
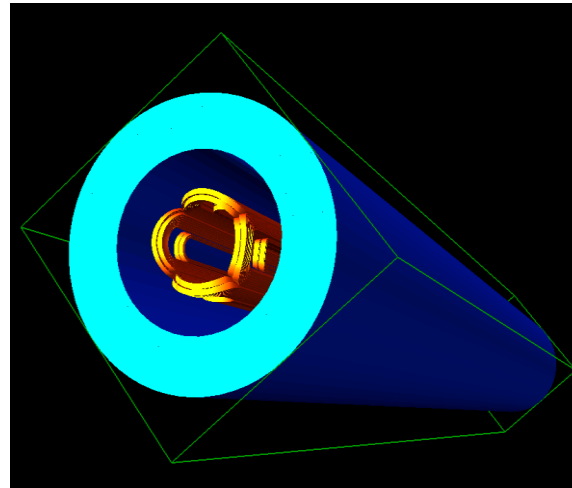
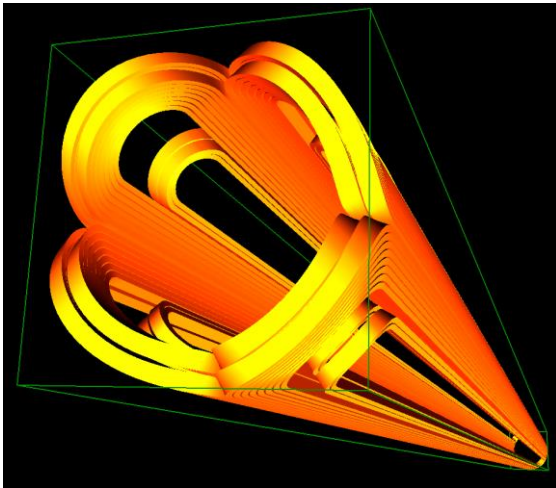
2D Flux lines



## Cos2 $\theta$ option of Q1a

### 3D design of Q1a

- 3D magnetic field is modeled and analysed using ROXIE.
- Coil end detailed shaped is optimized and determined.
- Field gradient 142T/m, each integrated field harmonics is smaller than  $1 \times 10^{-4}$ .
- ◆ The 3D magnetic field performance meets requirement.



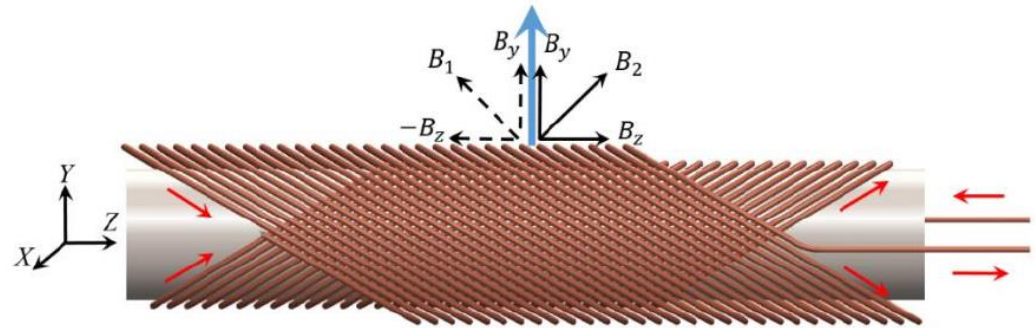
Single aperture model in 3D

# Conceptual design of Q1a for high luminosity with $L^*=1.9\text{m}$

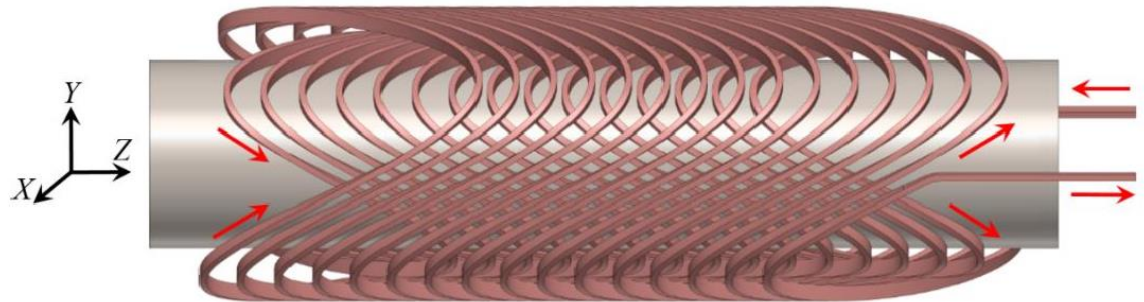
## 2) CCT option of Q1a

- CCT : Canted cosine theta
- The CCT design is based on a pair of conductors wound and powered such that their **transverse field components sum up** and their **solenoid fields cancel**.
- In practice, the conductor is wound on a pre-cut groove in a supporting hollow cylinder or mandrel.

CCT dipole



CCT quadrupole



$$\vec{P}(\theta) = \begin{cases} r \cos \theta \\ r \sin \theta \\ A_n \sin(2\theta) + \frac{w\theta}{2\pi} \end{cases} \quad -\pi N \leq \theta \leq \pi N$$

## CCT option of Q1a

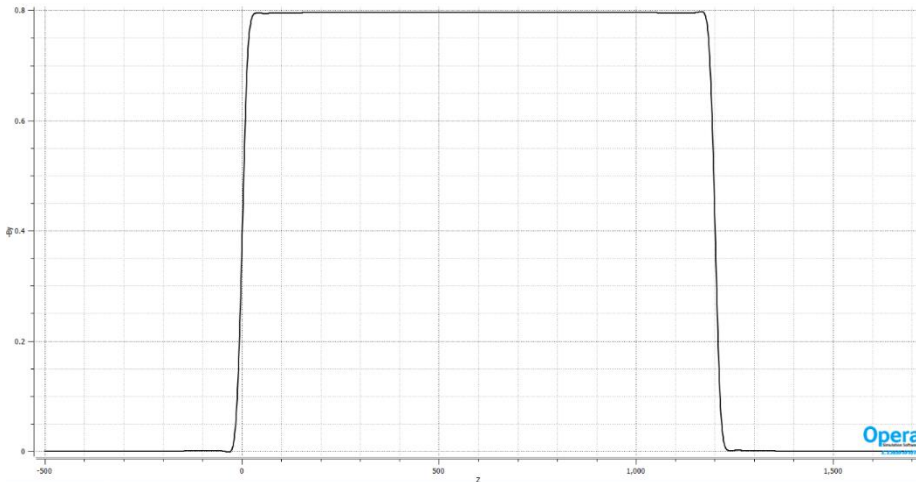
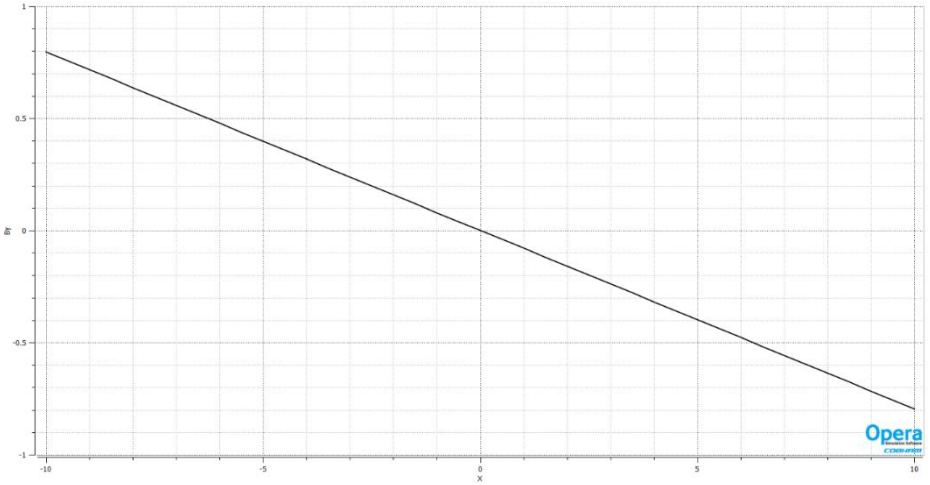
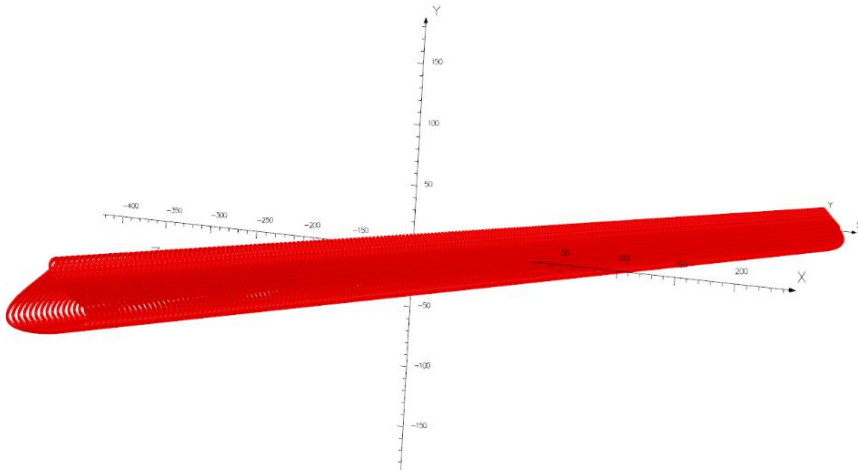
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### CCT option of Q1a, conceptual design

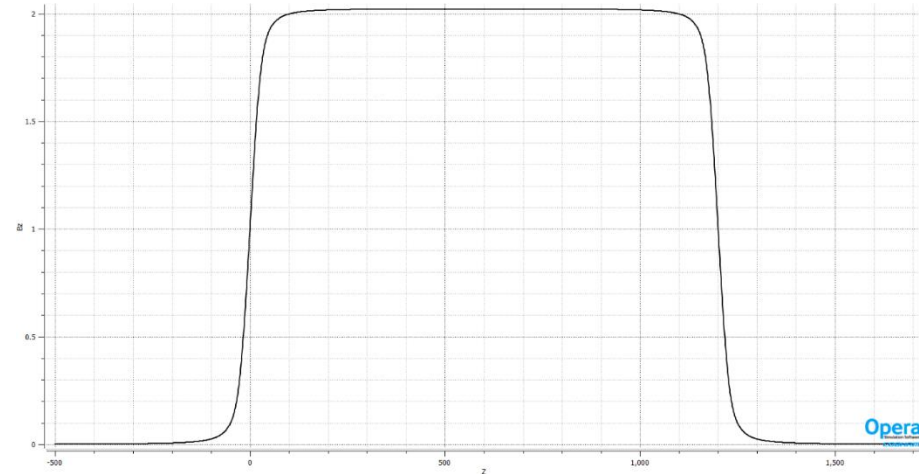
- HTS Bi-2212 0.8mm round wire or other conductor.
- The design of Q1a is based on two layers CCT quadrupole coil. The inner radius of the spar is 18.5mm.
- Outer radius of single aperture coil: 29mm.
- Groove on the spar:  $2 \times 3$ mm; 6 wires in a groove.
- Conductor canted angle: 30 deg
- The excitation current of Q1a is 1342A,
- ✓ Each integrated multipole field in single aperture is smaller than  $1 \times 10^{-4}$ .

# CCT option of Q1a

**1st layer CCT coil of Q1a:** consists of many small conductors



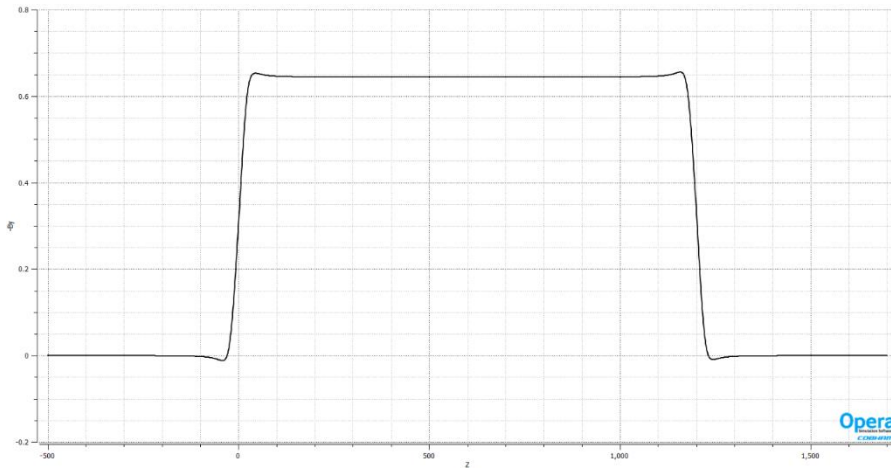
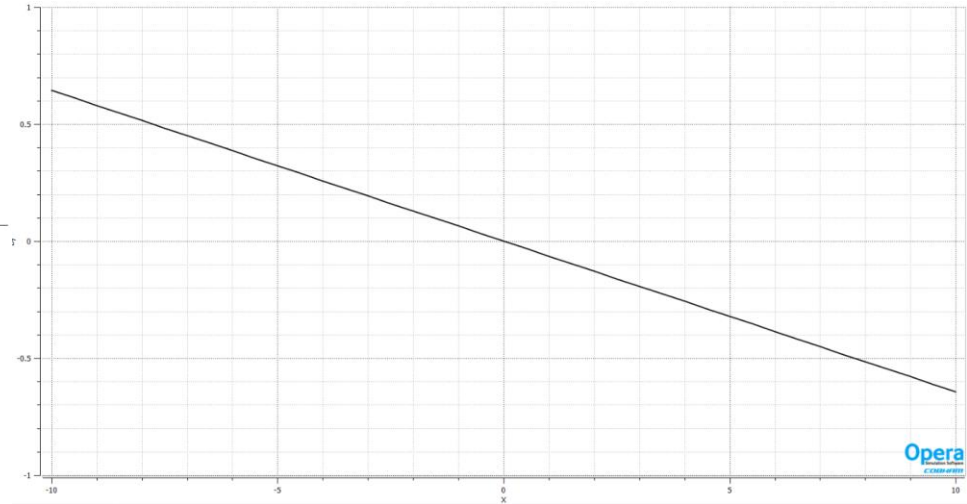
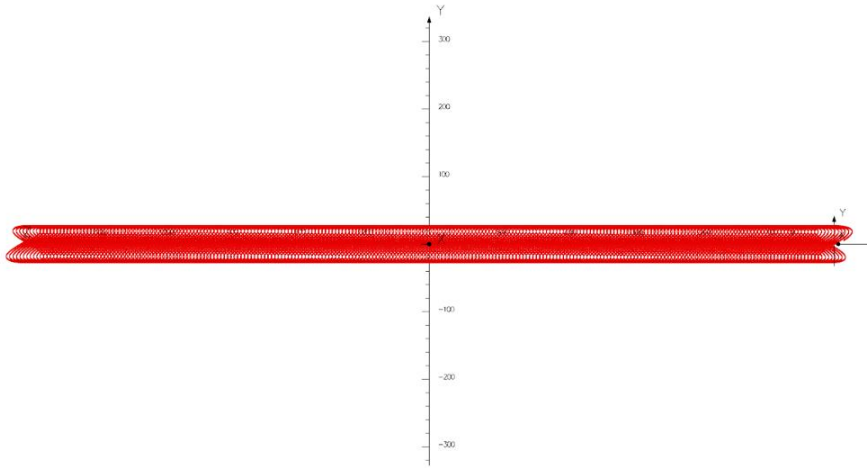
By along  $z$



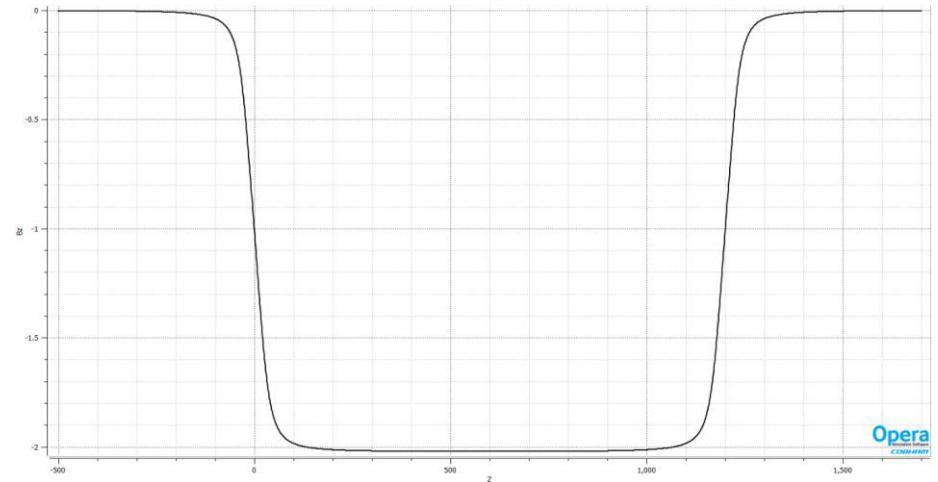
Solenoid field along  $z$

# CCT option of Q1a

## 2nd layer CCT coil of Q1a



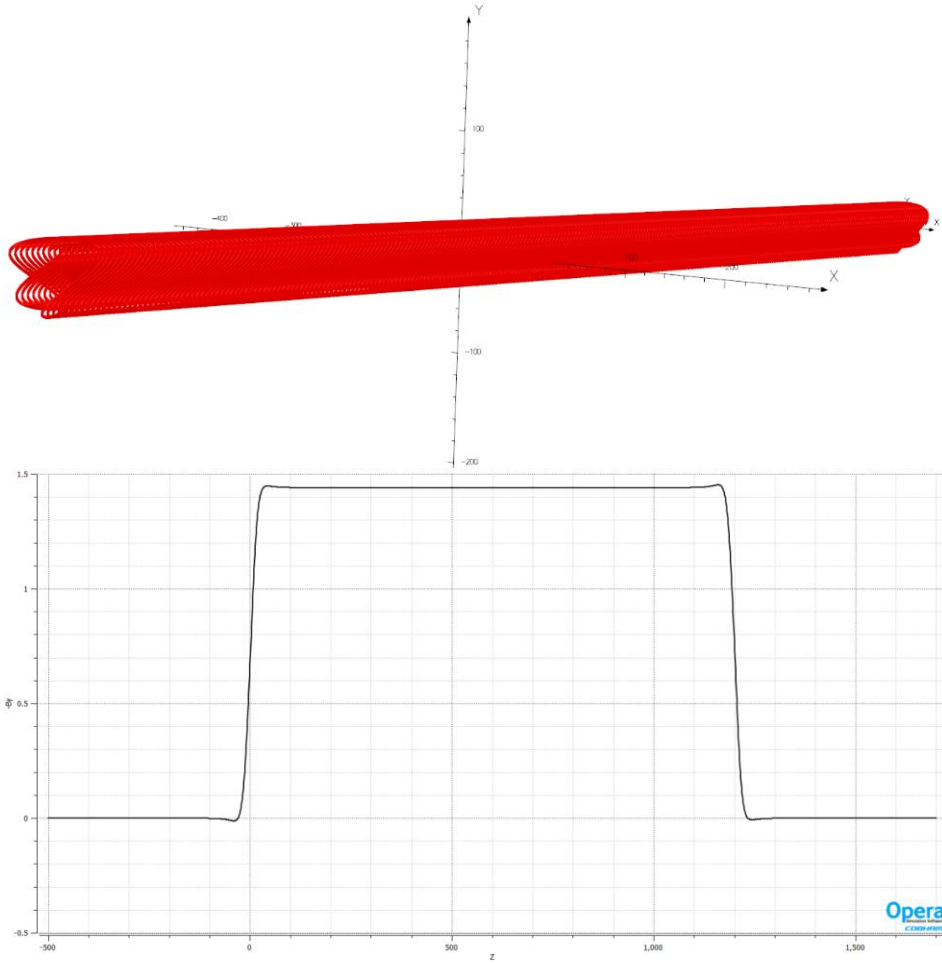
By along z



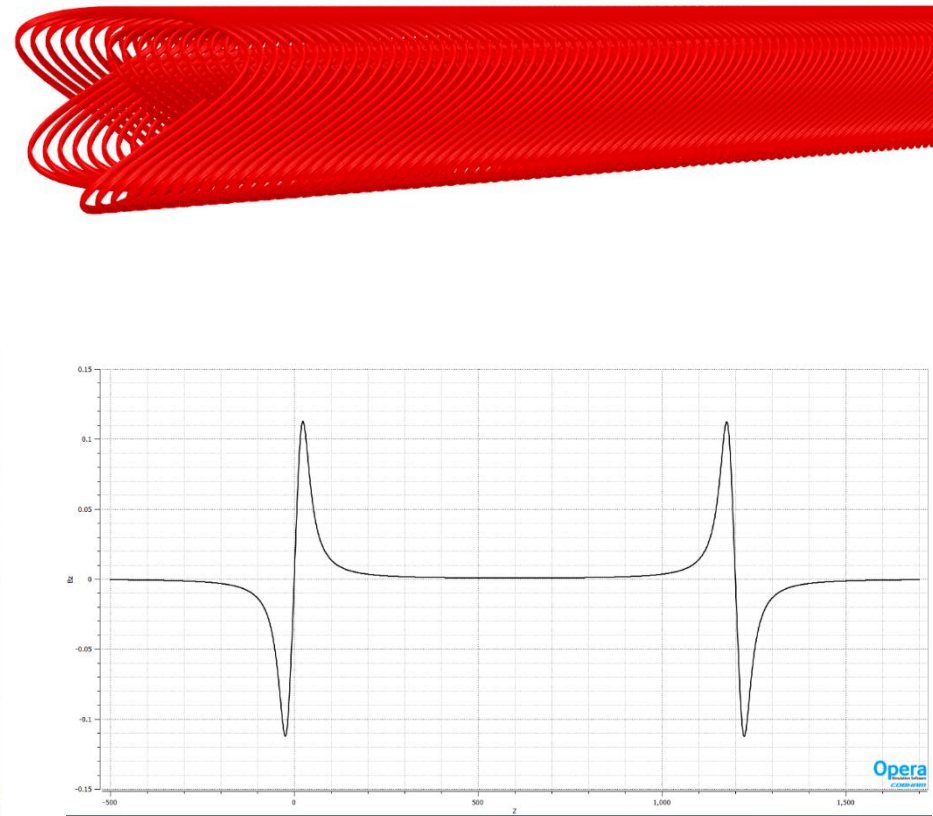
Solenoid field along z

## CCT option of Q1a

**Double layer CCT coil of Q1a:** Most of the solenoid fields of two layers cancel out. Field gradient and field harmonics meets the requirement.



By along  $z$

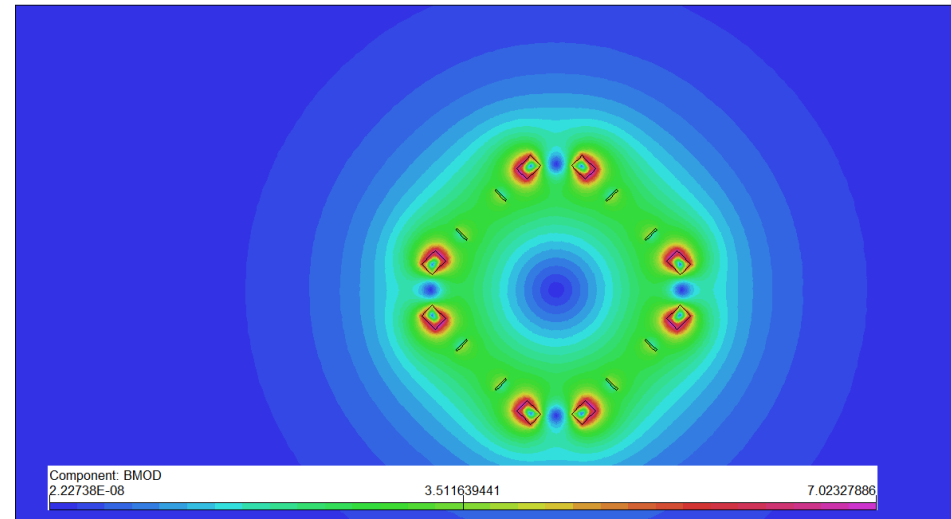
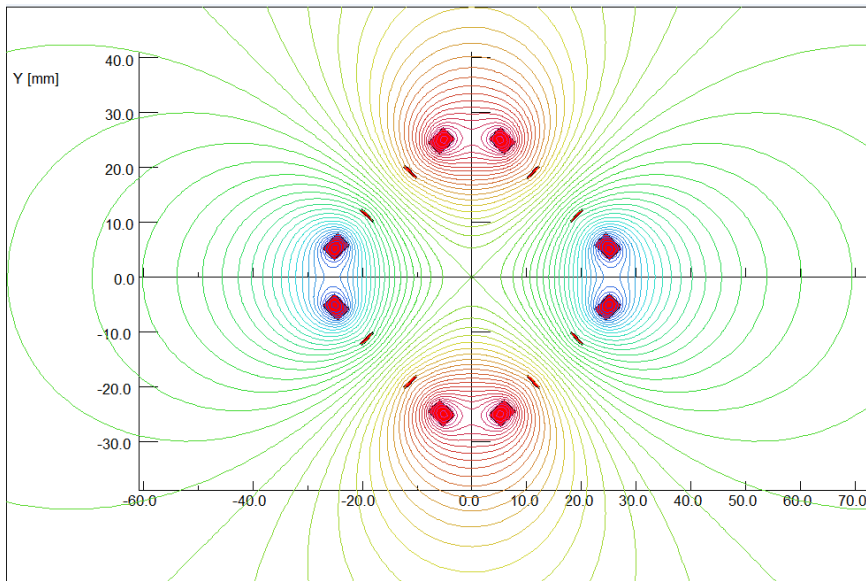


Solenoid field along  $z$

# Conceptual design of Q1a for high luminosity with $L^*=1.9\text{m}$

## 3) Racetrack coil option of Q1a

- Iron-dominated HTS quadrupole magnet using racetrack coils has been studied and fabricated in the world.
- *Can coil-dominated HTS quadrupole magnet using racetrack coils work?* ( field harmonics around  $1 \times 10^{-4}$  ).
- ✓ Quadrupole coil using racetrack coils for Q1a is optimized. Each multipole field is smaller than  $1 \times 10^{-4}$  (b6:  $-0.5 \times 10^{-4}$ ; b10:  $-0.2 \times 10^{-4}$ ,  $R_{\text{ref}}=7.6\text{mm}$ ).

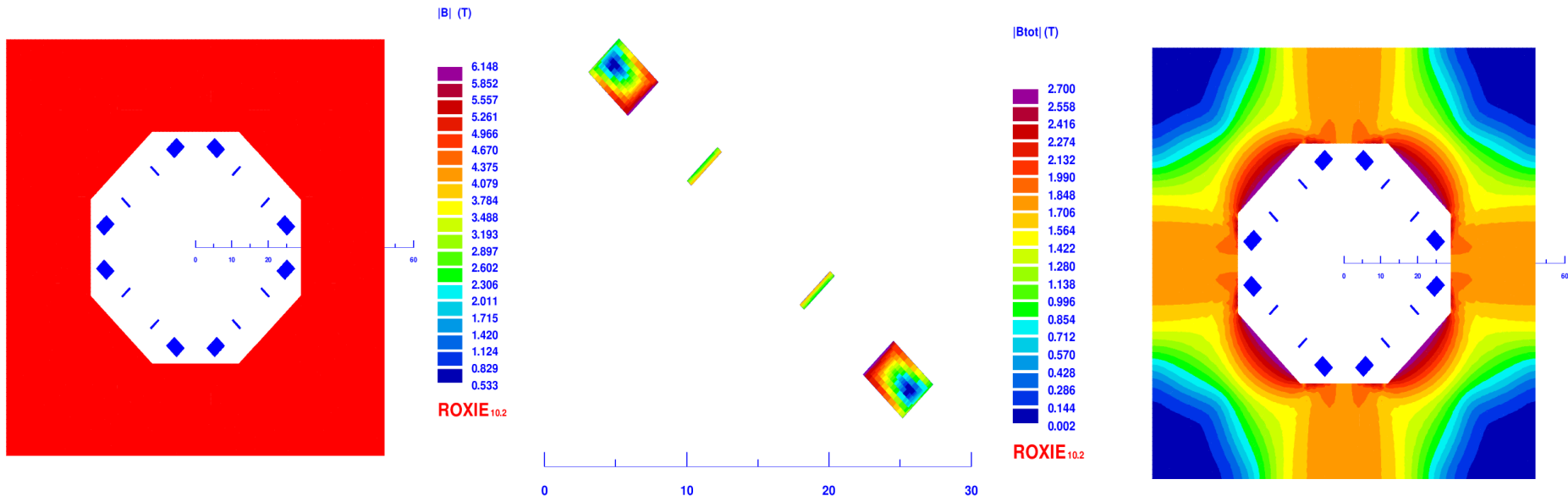


Quadrupole racetrack coils

# Racetrack coil option of Q1a

## Racetrack coil option of Q1a, conceptual design

- HTS YBCO tape (width 3 mm, thickness 0.1 mm) or other conductor.
- Single aperture field calculation of Racetrack coils with iron
- The excitation current of Q1a is 1020A; 43 turns for each pole
- Each multipole field in single aperture is smaller than  $1 \times 10^{-4}$  (Rref=7.6mm).



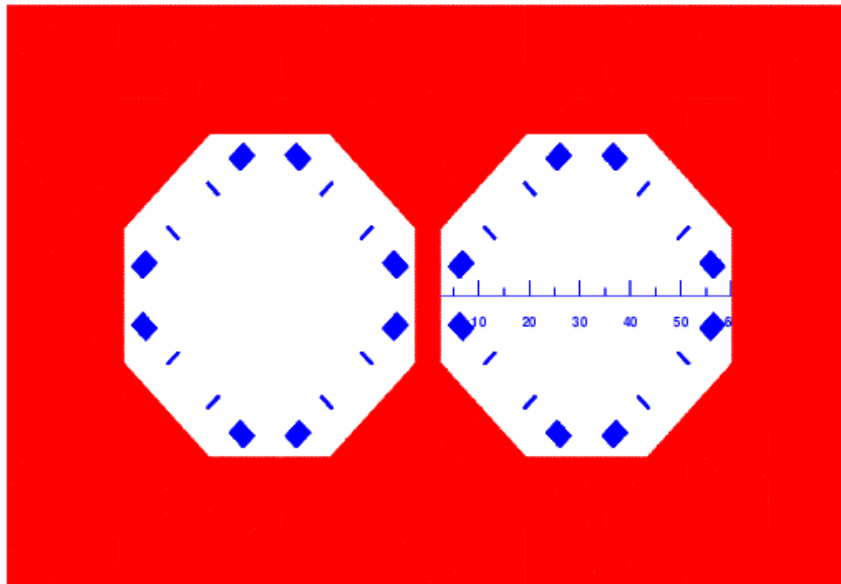
Quadrupole racetrack coils 2D field calculation



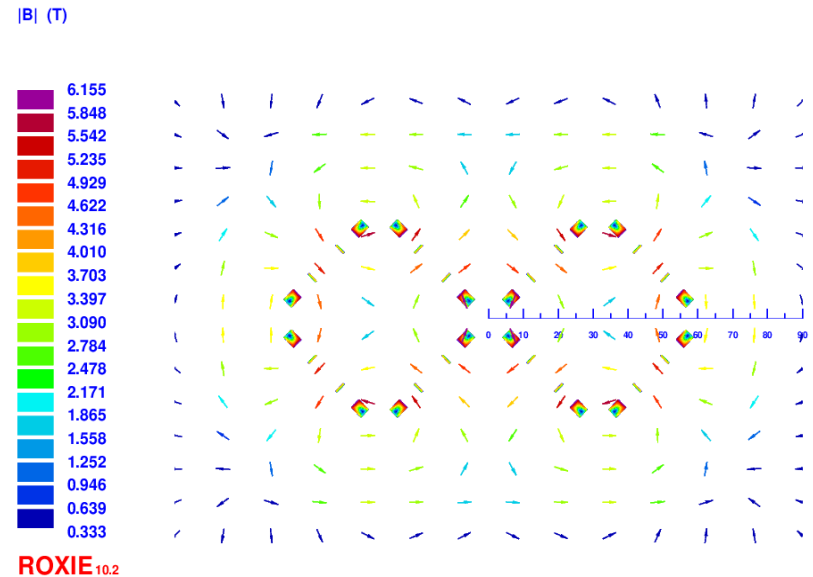
# Racetrack coil option of Q1a

## Field cross talk of the two apertures

- 2D field cross talk of Q1a two apertures near the IP side, where the distance between two aperture centerlines is minimum.
- The field gradient in each aperture reaches 141 T/m.
- ◆ Iron yoke width in the middle is very limited; **the field harmonics as a result of field crosstalk is smaller than  $2.0 \times 10^{-4}$ .**
- ◆ Magnetic field cross talk between two apertures is small.



Double aperture model

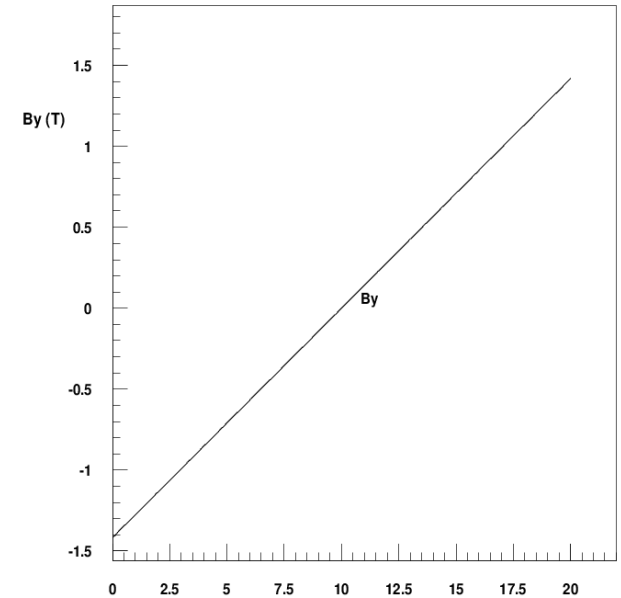
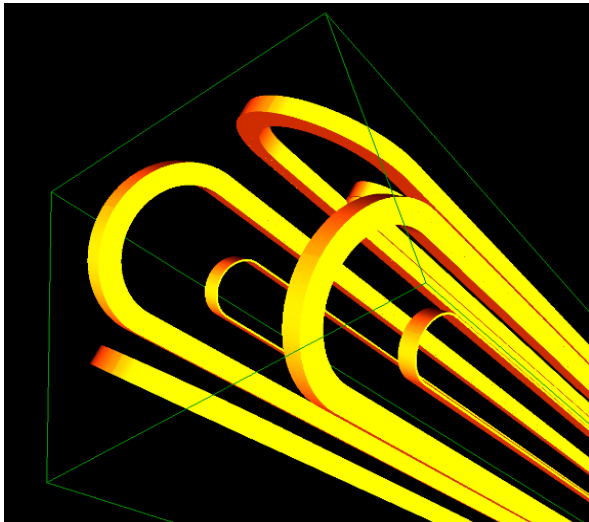


2D BMOD

## Racetrack coil option of Q1a

### 3D design of Q1a with Racetrack coils

- 3D magnetic field is modeled and analysed using ROXIE.
- Coil end detailed shaped is optimized and determined.
- Field gradient 141T/m, each integrated field harmonics is smaller than  $1 \times 10^{-4}$ .
- ◆ The 3D magnetic field performance meets requirement.



Single aperture model in 3D

# Conceptual design of Q1a for high luminosity with $L^*=1.9\text{m}$

## Comparison of three design HTS options of Q1a (141T/m)

Option	Excitation current (A)	Needed Engineering current density $J_E$ on wire (A/mm <sup>2</sup> )	Bmax on coil (T)	Possible Conductor
Cos2 $\theta$	1970	1004	3.2	Bi-2212
CCT	1342 (940 with iron)	2670 (1870 with iron)	3.8	Bi-2212
Racetrack coil	1020	3400	6.2	YBCO

- From the comparison, Cos2 $\theta$  coil has the highest magnetic efficiency, lowest needed Engineering current density; the current carrying capacity of Bi-2212 conductor is close to it.

# Summary

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- Superconducting quadrupole magnets are key devices for CEPC. The design of quadrupole magnets with the CDR parameter meets the requirement.
- Despite limited space, field cross talk effect between two apertures in QD0 is negligible using iron yoke.
- **Coil-dominated HTS quadrupole magnet using racetrack coils** has been studied in the CEPC IR. Field quality of the coil layout  $< 1 \times 10^{-4}$ .
- Three HTS options have been studied for the Q1a magnet using high luminosity parameters with  $L^*=1.9\text{m}$ : *Cos2 $\theta$  coil*, *CCT coil*, *Racetrack coil*.
- **Cos2 $\theta$  coil has the highest magnetic efficiency**, and the current carrying capacity of Bi-2212 conductor is close to the requirements.



**Thanks for your attention!**

