

# DC characterization of a Low-Field Nb<sub>3</sub>Sn prototype conductor for a DEMO TF coil

Abstract ID: 307

November 18<sup>th</sup>, MT27

session THU-OR5-601 A15-type Superconducting Wires and Cables

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## - ENEA conceptual design studies for the DEMO TF coils:

DEMO ENEA Low Field layer wound Wind&React Conductor (LF-WR4 CICC):  
designed with a small number of sc Nb<sub>3</sub>Sn strands (#120) and a high number of  
stabilization copper wires (#690) → lowest field grade

## - LF-WR4 DC characterization (Sultan facility at SPC)

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could not reach operating conditions (5.4T – 70.8kA) due to early quenches → but  
achieved  $T_{cs}$  is stable with cycling

Investigation/explanation of DC results:

- Measurements analysis
- tomographic analysis



Susceptibility analysis of strain distribution

ENE A layer wound winding pack layout for the DEMO TF coils → **advantage:**  
optimized distribution of steel and superconductor in winding pack

**CICC design: rectangular, with:**

- **thick** steel jacket (const. thickness)
  - **distributed** pressure relief channels
  - Low Void Fraction (**25-28%**)
  - **Long Twist Pitch** cable configuration
- HF-WR1 conductor (#1080 Nb<sub>3</sub>Sn strands) prototype feasibility has already been demonstrated in 2015 and performances measured at SPC
  - LF-WR4 is the **lowest field grade**: #120 Nb<sub>3</sub>Sn strands and #690 copper wires → prototype feasibility has been demonstrated and test performed at SPC in February 2021



# Low Field layer wound WR4

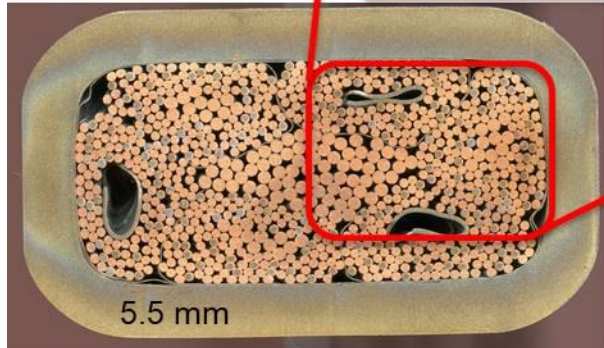


27<sup>th</sup> International Conference on  
Magnet Technology (MT27)  
Fukuoka, Japan / 2021

DEMO LF-WR4 is an  
extreme case: huge  
amount of Cu to limit  
 $T_{hs} \rightarrow 15\% \text{ sc}$

few  $\text{Nb}_3\text{Sn}$   
strands in the  
cross section

$J_{op} = 1500 \text{ A/mm}^2$



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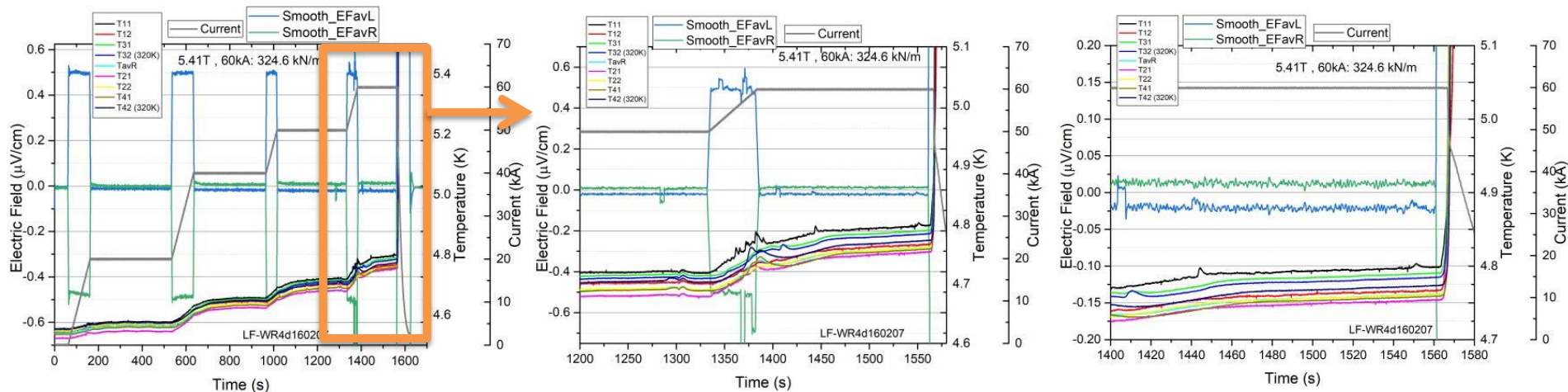
Sultan sample:  
assembly  
procedure at  
SPC  $\rightarrow$  application  
of Cu sleeves at  
conductor  
termination, steel  
transition pieces,  
Copper termination,  
instrumentation,  
insulations,  
mechanical  
structure etc.



# LF-WR4: investigation on DC transition

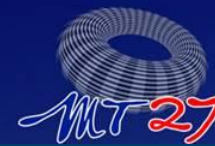


First DC measurements: quench at 60kA flattop (5.41T x 60kA → 324.6kN/m) → could not reach operative conditions (5.4T – 70.8kA)



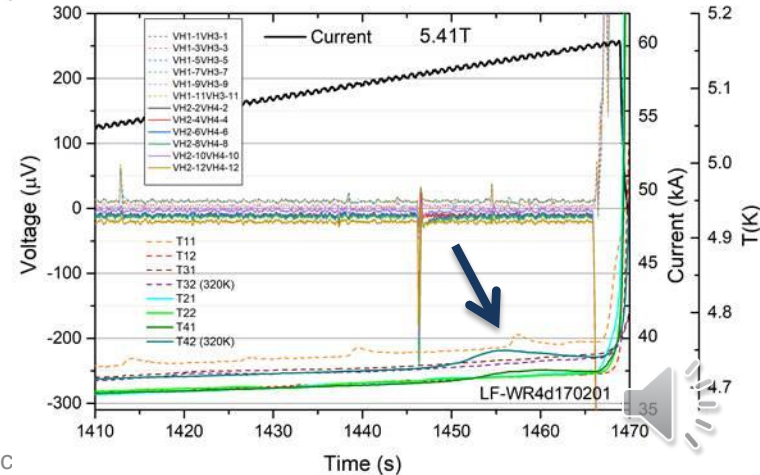
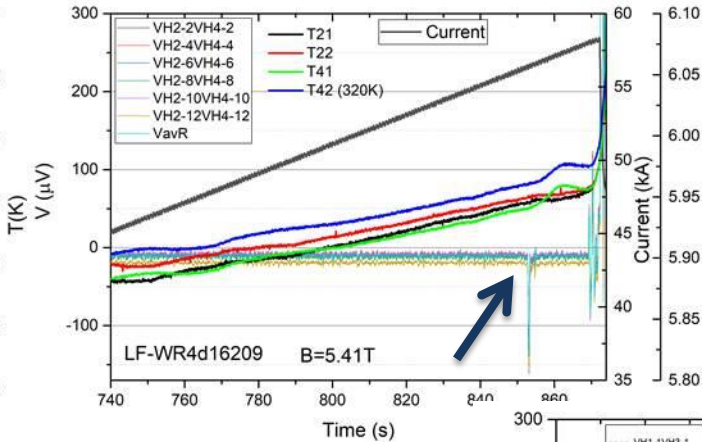
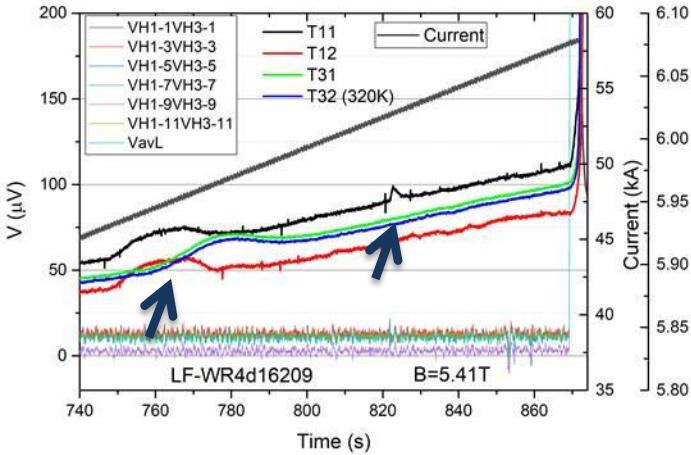
- At flattop a current re-distribution is likely: from an «inductance-dominated» configuration to a «contact resistance-dominated» configuration
- redistribution could be not effective as there are few Nb<sub>3</sub>Sn strands in the cable section

# LF-WR4: investigation on DC transition



## Quenches during current ramps

Voltage spikes during the ramps, accompanied by temperature oscillations



Possible explanations for early quenches:

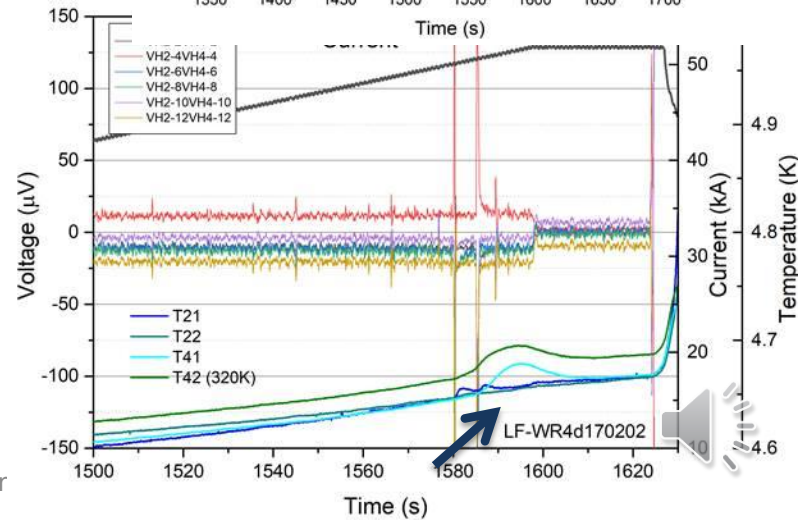
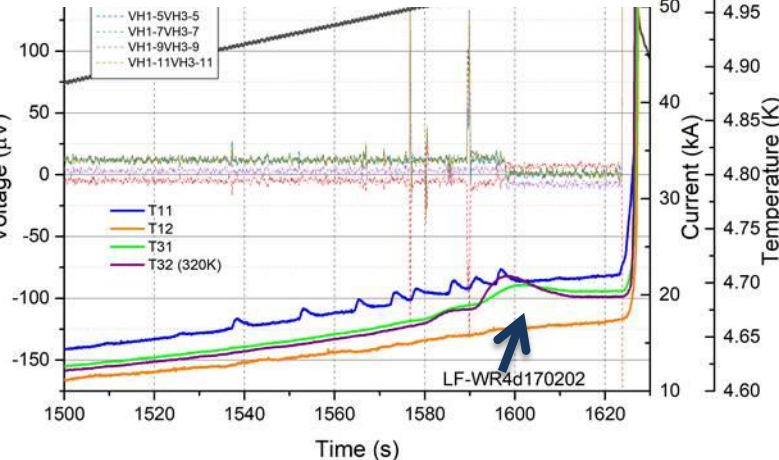
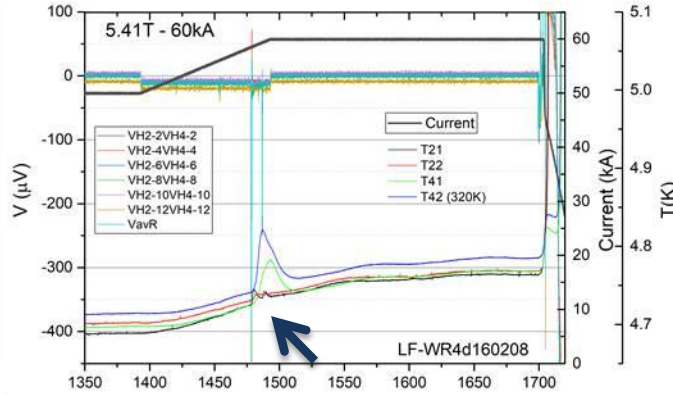
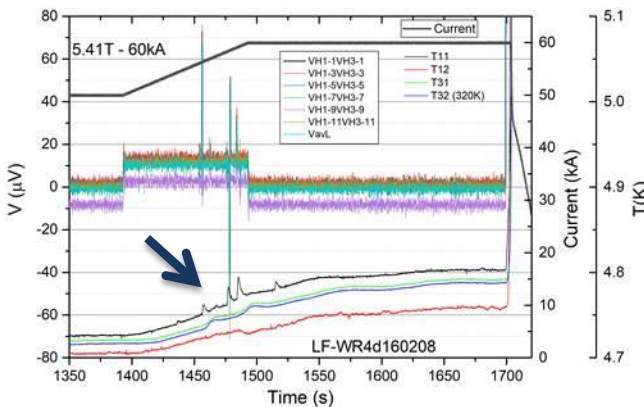
- Strands movements due to E-M. load
- Uneffective current redistribution among the few sc strands in the cross section

# LF-WR4: investigation on DC transition



In some runs voltages spikes and temperature oscillations are even more evident

5.41T x 60kA → 324.6 kN/m  
7T x 52kA → 364 kN/m



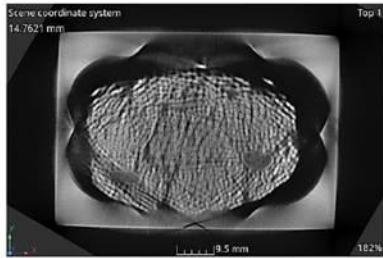
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of a low-field prototype cor

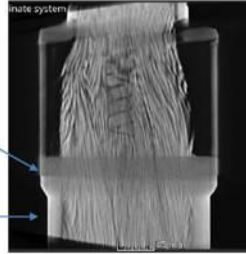
# LF-WR4: X-ray microtomography analysis



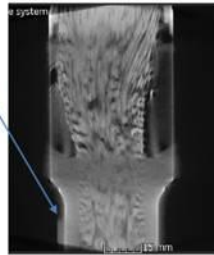
- “Box” with CICC interface



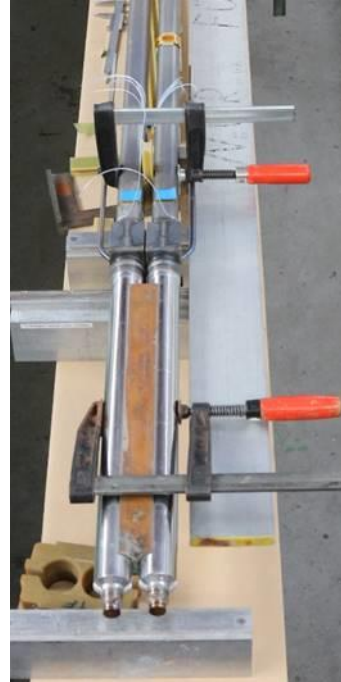
Box-CICC interface



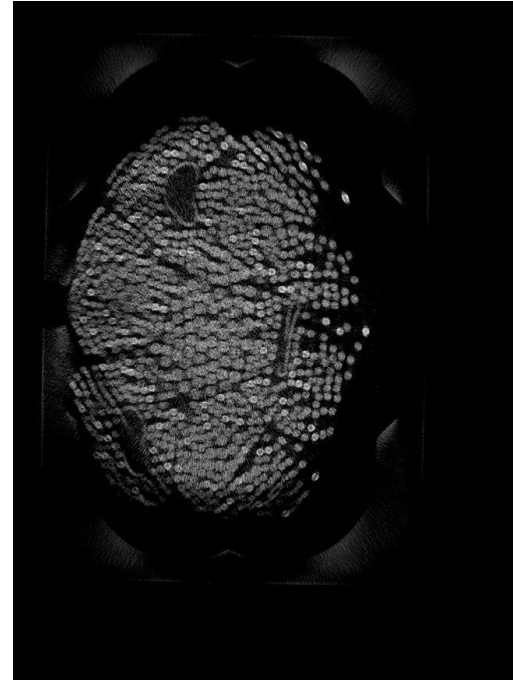
CICC



Sample length ~ 400 mm  
320 mm were XCT scanned

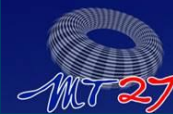


*Microtomography group of National Institute for Laser, Plasma and Radiation Physics, Bucharest (Romania)*





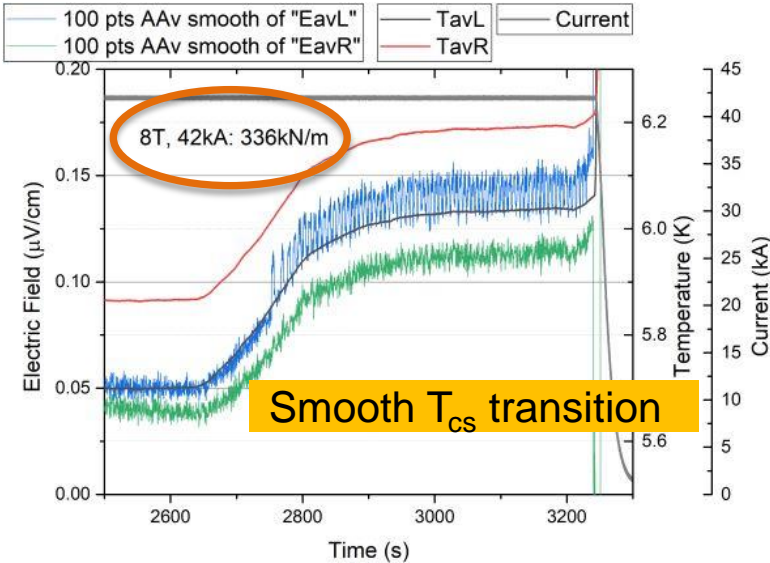
# LF-WR4: comparison among similar E.M. loads



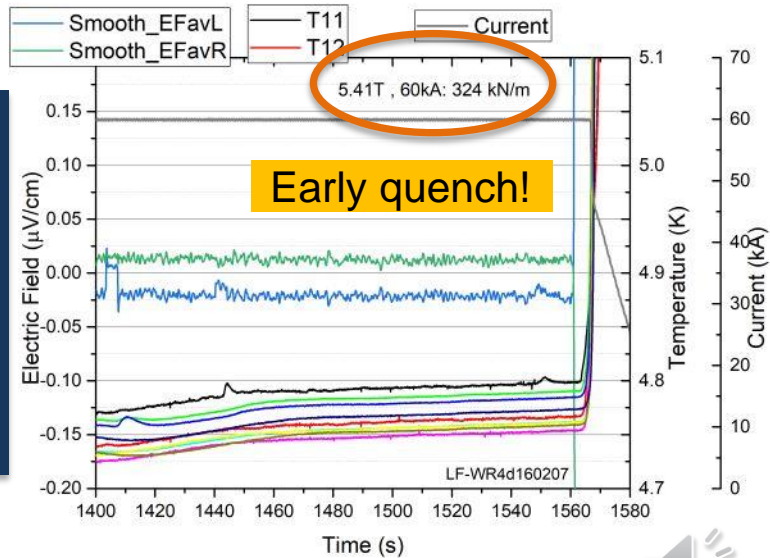
At the same E.M. load the measurements at higher current → quench



→ The issue seems not (only) the e.m. load, but especially the current:



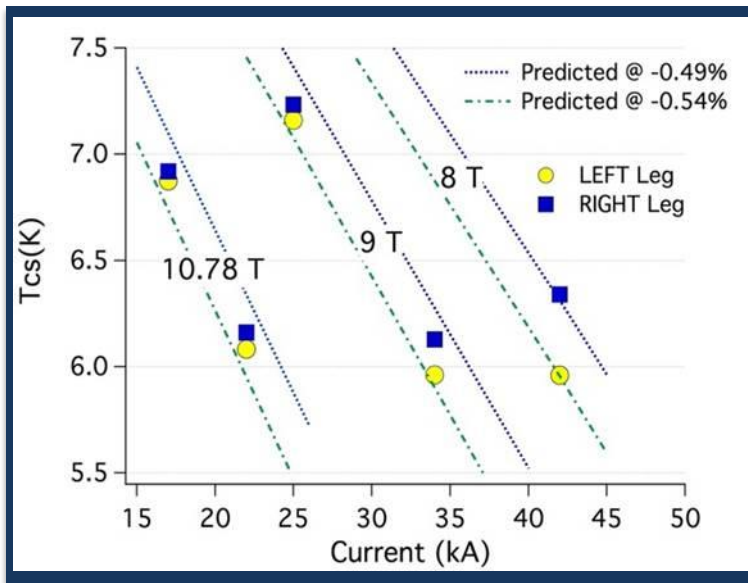
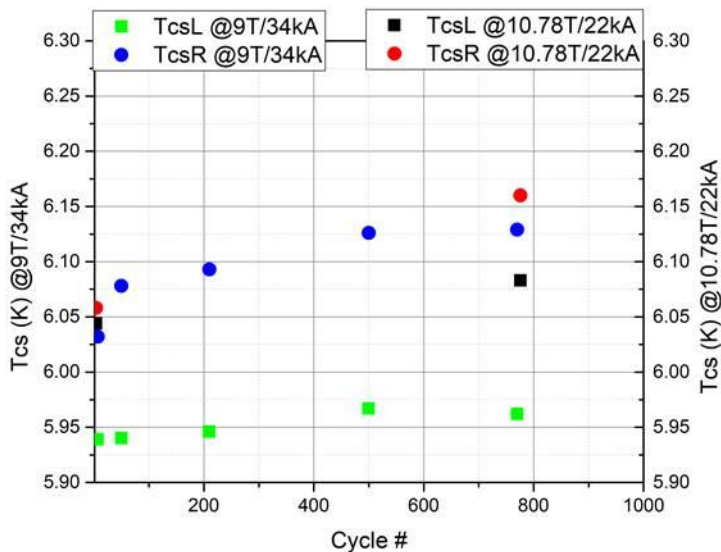
#783 cycles of electromagnetic loads @ 9T X 40kA=360kN/m were applied to the sample



# LF-WR4 DC results



Measurements could not reach operating conditions but → at lower currents (34kA and 22kA) → no degradation with cycling



After cycling:

$T_{cs}$  data described by  $\epsilon_{eff} = -0.54\% \text{ to } -0.49\%$

# Inductive $T_{cs}$ test before and after E.M. cycles



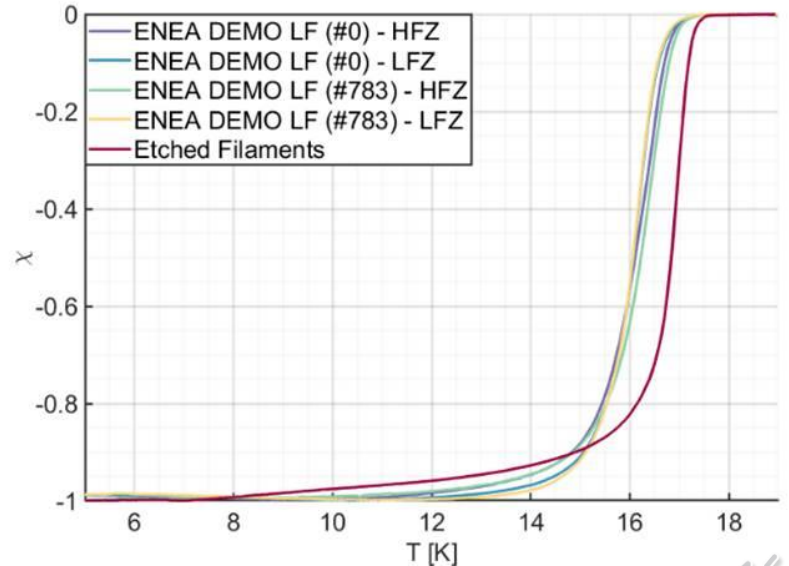
Pick up and excitation coils installed on the right leg: HFZ and LFZ → detect a signal proportional to the magnetic susceptibility of the conductor



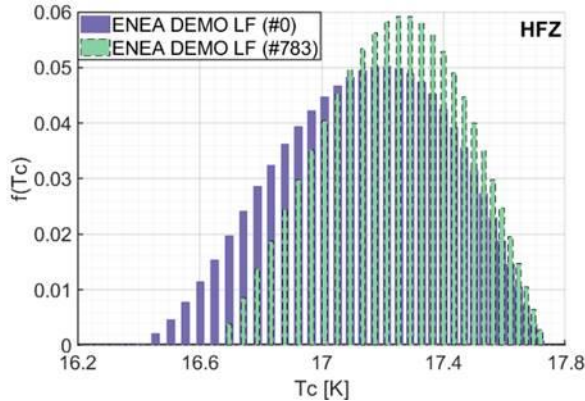
$I_{exc}=250 \text{ mA}_{RMS}$  @11hz

inductive response of the conductor: recorded while slowly increasing the sample temperature from 4.2 K to  $\approx 25$  K and then decreasing it back to 4.2 K

Comparison between susceptibilities of the etched filaments and of the ENEA DEMO LF conductor at the beginning and at the end of the test campaign

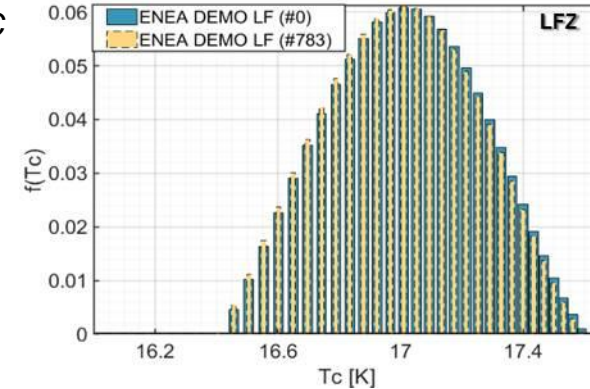


# T<sub>c</sub> and strain distribution inside LF-WR4



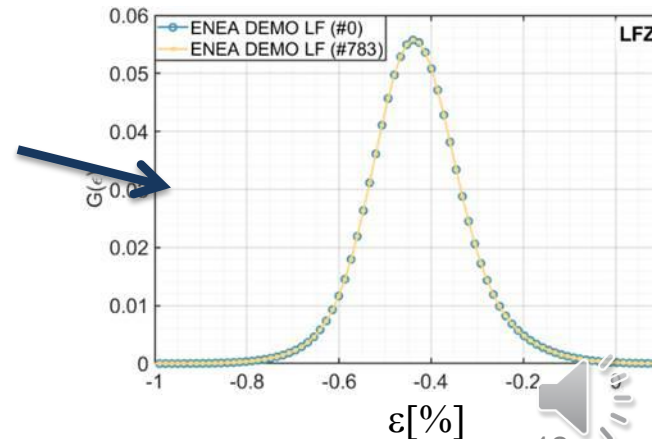
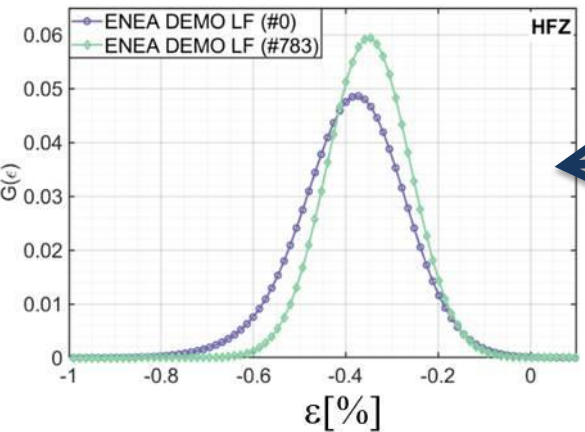
inductive measurements elaboration are by SPC

## T<sub>c</sub> distribution



## strain distribution

narrow  $\epsilon_{th}$  distribution  
around the mean value  $\rightarrow$   
it does not broaden after  
cyclic loading  $\rightarrow$  true both  
for HFZ and LFZ



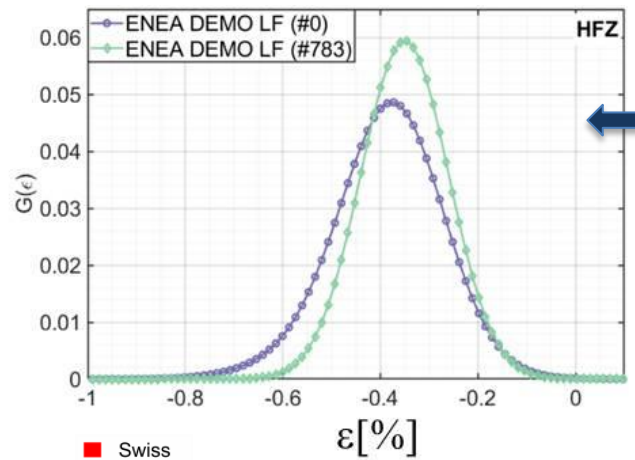
C. Calzolaio, "Irreversible Degradation in Nb3Sn Cable in Conduit Conductors," PhD Thesis, 2013.

Arend Nijhuis, "TF conductor samples strand thermo mechanical critical performances tests", Final Report, MAG-MCD-4.3-T004-FD, EFDA\_D\_2M5SMM, Dec 2015, <https://idm.euro-fusion.org/?uid=2M5SMM>.

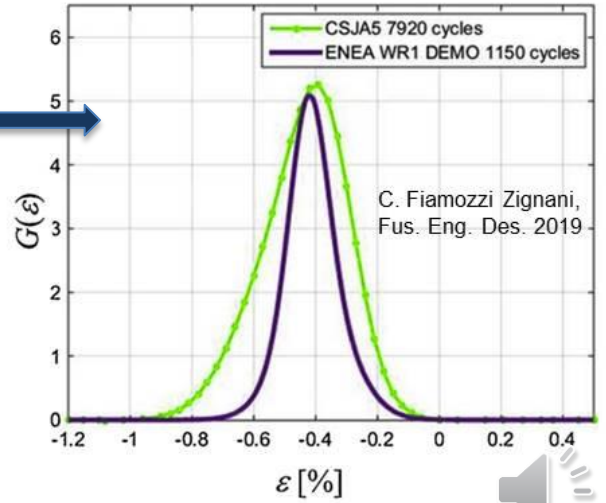
# LF-WR4: mean value width of the strain distribution

| cycle | HFZ       |              | LFZ       |              |
|-------|-----------|--------------|-----------|--------------|
|       | $\mu$ [%] | $\sigma$ [%] | $\mu$ [%] | $\sigma$ [%] |
| #0    | -0.38     | 0.10         | -0.43     | 0.09         |
| #783  | -0.35     | 0.09         | -0.43     | 0.09         |

relatively low mean absolute value of  $\epsilon_{th}$  in compression compared to other types of conductors (e.g. the W&R ITER conductors)



*Congruent with HF-WR1 results  $\rightarrow$  same design approach: rectangular CICC with long twist pitch and low void fraction)*



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- LF-WR4 prototype conductor tested at Sultan facility: both DC and AC characterization → here only DC characterization is presented

- After microtomography and measurements analysis:

No strands damage, small movements in the collar are possible, but **at the same E.M. load and lower currents the transition appears smooth → the quench is likely due to current sharing issue among strands**

**DC characterization gave important feedbacks on LF CICC design →**

Possible solutions: sc strands closer together or «overdesign» i.e. maintaining a minimum fraction of sc in cross-section

**CICC design with rectangular geometry, low V.F. and long twist pitch →**

$T_{CS}$  with relatively narrow strain distribution and stable vs cycling

# Thank you

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This work has been carried out within the framework of the EUROfusion Consortium and has received funding from the Euratom research and training programme 2014-2018 and 2019-2020 under grant agreement No 633053. The views and opinions expressed herein do not necessarily reflect those of the European Commission.



C. Fiamozzi Zignani - DC characterization of a low-field prototype conductor for a DEMO TF coil - MT27 – Nov, 18th 2021