

Evaluation of Selection Criteria for the Level of Liquid Nitrogen in HTS Magnet System

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Background

- HTS magnet system is immersed in LN₂ and continuously refrigerated by a cryogenic cooling system.
- Especially, in case of the side-wall cooling type, HTS magnet system is located well below the level of LN₂ for thermal and electrical safety and the CGN₂ is filled above LN₂.
- However, the method of determining selection criteria for the optimum level of LN₂ in HTS magnet system has not been yet deeply investigated.
- Therefore, in this work, the process of determining the selection criteria for the level of LN₂ in HTS magnet system is proposed.

Objectives

- A sphere-to-plane electrode system made with stainless steel is used under AC and DC.
- The electric field intensity according to the level of LN₂ is calculated by the finite element method (FEM) and the experimental results are analyzed using the weibull distribution.
- The utilization factor (ξ) is adopted to analyze the uniformity of the electric field of the electrode system, and to derive the selection criteria.
- Moreover, a method of selecting the level of LN₂ on the 3D model of HTS magnet is proposed through the calculated selection criteria.

Calculation of selection criteria for the level of LN₂

- $V_{BD, 7\%}$ increases as the level of LN₂ and the diameter of the sphere electrode increase as shown Fig. 5.
- Also, the DC voltage do not differ according to the polarity, and the $V_{BD, 7\%}$ of the DC voltage is larger than that of the AC voltage.
- ξ is adopted to analyze the uniformity of the electric field of the electrode system, and to derive the selection criteria as shown equation (1). $\xi = \frac{E_{MAX, 1kV}}{E_{MEAN, 1kV}}$ (1)
- The variation of $E_{BD, CGN2, MAX, 7\%}$ and $E_{BD, LN2, MEAN, 7\%}$ according to ξ considering the level of LN₂ is plotted in Fig. 6, and the equations for calculating $E_{BD, CGN2, MAX, 7\%}$ and $E_{BD, LN2, MEAN, 7\%}$ are deduced in Table 2.
- It is found that the selection criteria according to the level of LN₂ can be derived.

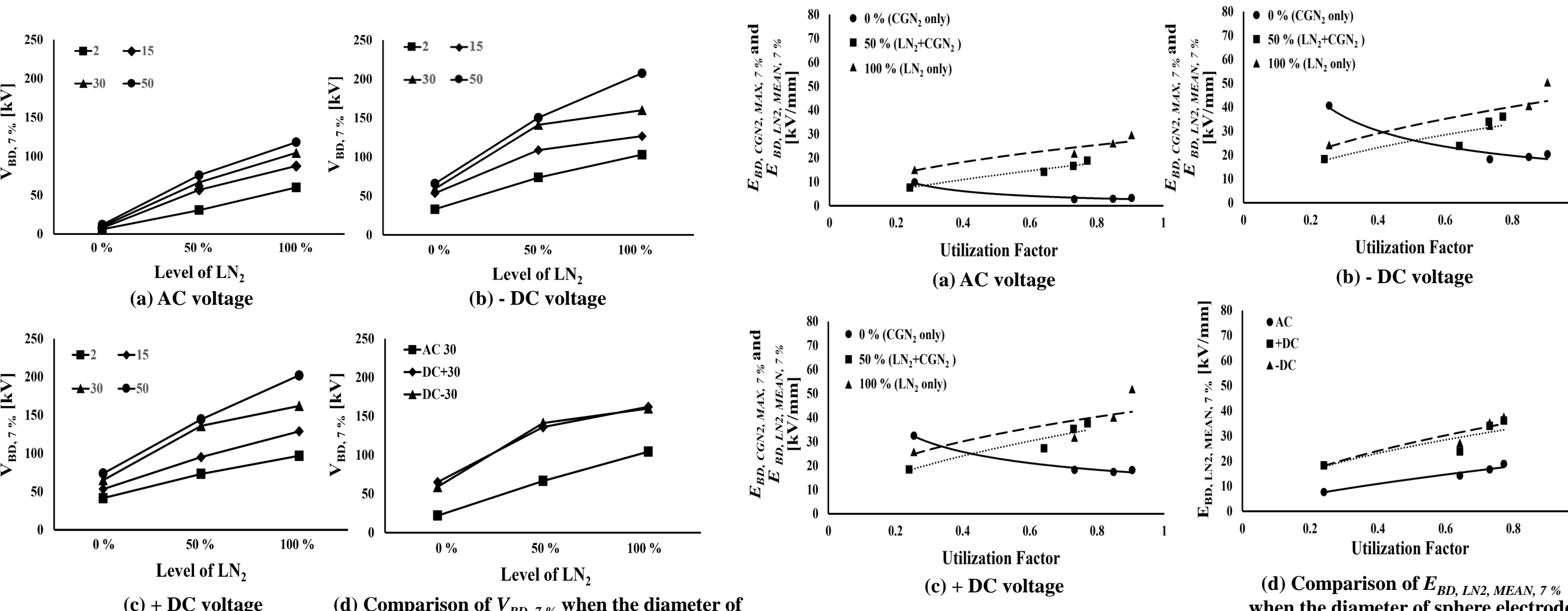


Fig. 5 $V_{BD, 7\%}$ according to each voltage

Fig. 6 Comparison of $E_{BD, CGN2, MAX, 7\%}$ and $E_{BD, LN2, MEAN, 7\%}$ and ξ according to each voltage

Table 2. $E_{BD, 7\%}$ according to the level of LN₂ and each voltage

	AC	+DC	-DC
0 %	$y = 2.30x^{-0.53}$	$y = 16.95x^{-0.60}$	$y = 16.38x^{-0.50}$
50 %	$y = 20.81x^{0.71}$	$y = 37.05x^{0.52}$	$y = 40.30x^{0.56}$
100 %	$y = 23.60x^{0.522}$	$y = 44.67x^{0.47}$	$y = 44.29x^{0.42}$

Experimental set-up & analysis method

- Fig. 1 shows the schematic drawing of experimental set-up, and the electrode system is immersed in LN₂.
- After degassing the remaining air with a rotary pump, the experiment is performed after waiting for CGN₂ to vaporize for 30 min.
- The ramping up rate of voltages is about 1 kV/s., and the time interval is set to 60 sec under AC voltage and 10 min under DC voltage to minimize the influences of space charges.
- Fig. 2 shows the measuring the level of LN₂ between the sphere-to-plane electrodes, and the specifications of experimental conditions are shown in Table 1.
- Each experiment is repeated 7 times on every condition and five values except for maximum and minimum values are used to calculate the mean value of experimental results.
- The experimental results are analyzed by the weibull distribution to calculate 7 % probability for electrical breakdown ($V_{BD, 7\%}$) in accordance with IEC 62271-1 as shown Fig. 3.
- The maximum and mean values of electric field intensity ($E_{MAX, 1kV}$ and $E_{MEAN, 1kV}$) are calculated through the path of electric field as shown Fig. 4.
- Also, $E_{MAX, 1kV}$ and $E_{MEAN, 1kV}$ at $V_{BD, 7\%}$ ($E_{BD, CGN2, MAX, 7\%}$ and $E_{BD, LN2, MEAN, 7\%}$) are calculated because gas insulation is affected by maximum electric field intensity and liquid insulation are affected by the mean electric field.

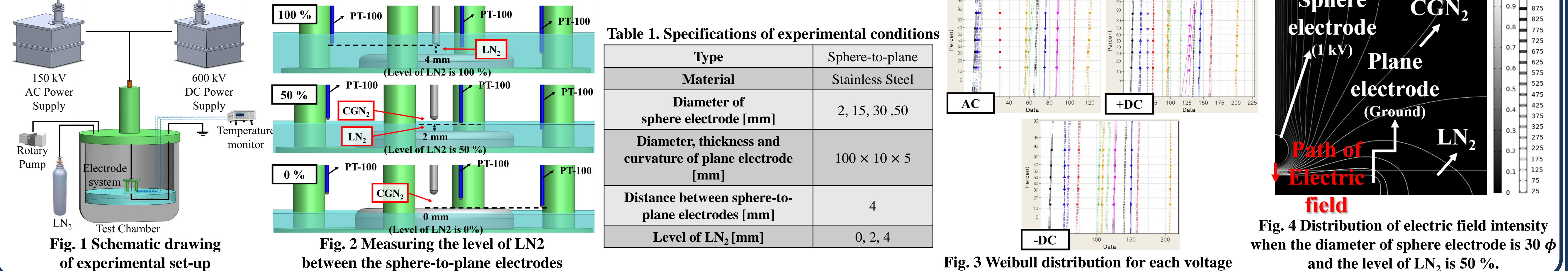
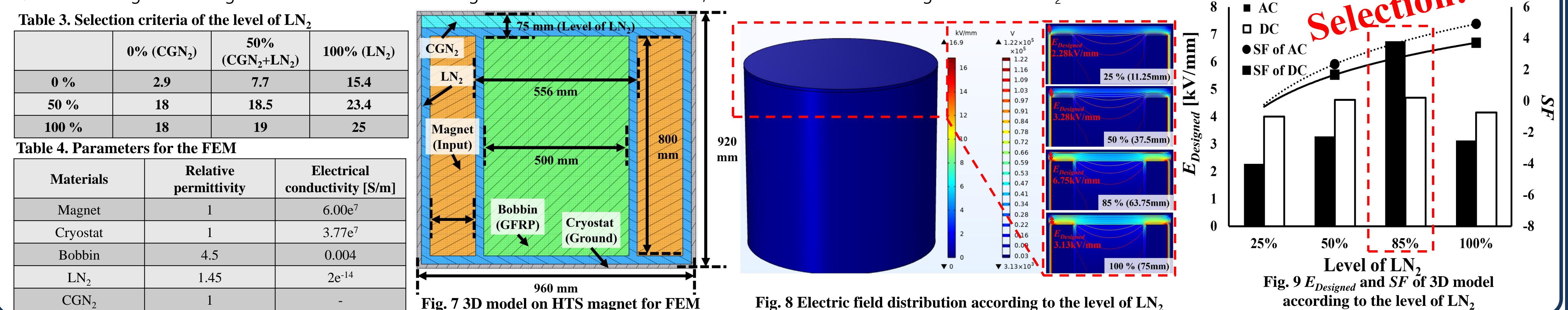


Table 1. Specifications of experimental conditions

Type	Sphere-to-plane
Material	Stainless Steel
Diameter of sphere electrode [mm]	2, 15, 30, 50
Diameter, thickness and curvature of plane electrode [mm]	100 x 10 x 5
Distance between sphere-to-plane electrodes [mm]	4
Level of LN ₂ [mm]	0, 2, 4

Evaluation method of the level of LN₂ through selection criteria

- Table 3 shows the selection criteria of the level of LN₂ derived through formulas, and as the level of LN₂ increased, it is increased.
- Fig. 7 shows the 3D model on HTS magnet for FEM, and Table 4 shows the parameters for the FEM.
- 100 kV is applied in magnet, and cryostat is grounded, and Fig. 8 shows the electric field distribution of 3D model according to the level of LN₂.
- The Safety Factor (SF) is adopted to select the level of LN₂ as shown equation (2), and SF is based on 1, where lower means unsafe, and high means safe. $SF = \frac{E_{Selection Criteria}}{E_{Designed}}$ (2)
- Fig. 9 shows the $E_{Designed}$ and SF of 3D model according to the level of LN₂, and $E_{Designed}$ according to the level of LN₂ increased to 85 %, and then decreased when it reached 100 %.
- Considering the cooling characteristics of the HTS magnet and the selection criteria, 85% is selected with the highest level of LN₂ and SF of 1 or more.



Conclusion

- In this work, the process of determining the selection criteria for the level of LN₂ in HTS magnet system is proposed.
- Through the proposed selection criteria and evaluation method, it is confirmed that the level of LN₂ of the HTS magnet is 85 % most efficient.
- It is found that It is helpful in selecting the level of LN₂ of HTS magnet through the calculated selection criteria and evaluation method.