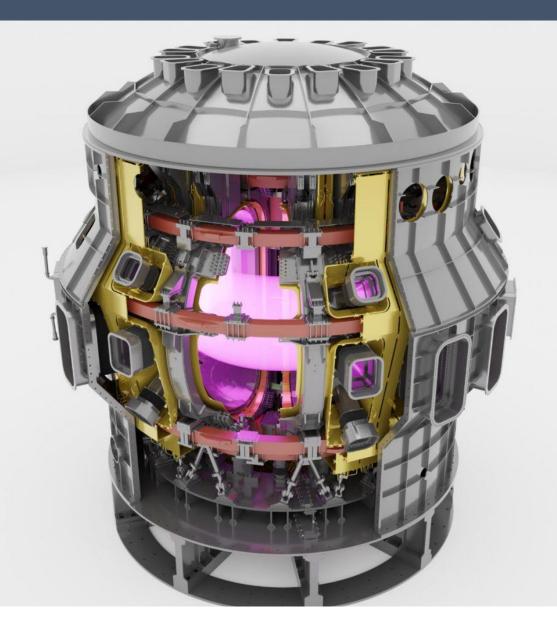
AC losses in JT-60SA TF magnet during commissioning: experimental analysis and modeling A. Louzguiti¹, S. Davis², K. Fukui³, K. Hamada³, C. Hoa⁴, B. Lacroix¹, Q. Le Coz⁵, F. Michel⁴, H. Murakami³, S. Nicollet¹, G. Sannazzaro², V. Tomarchio², A. Torre¹, L. Zani¹ ¹CEA IRFM, Cadarache, France / ²F4E Garching, Germany / ³QST, Naka, Japan / ⁴ CEA IRIG, Grenoble, France / ⁵Assystem, Pertuis, France

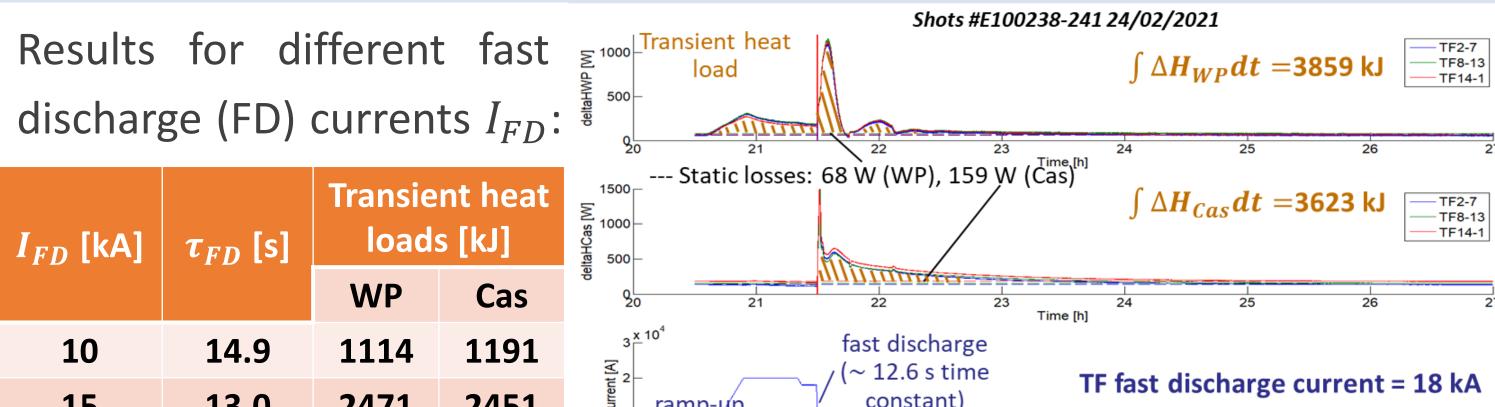
alexandre.louzguiti@cea.fr

THU-PO3-206-01

ABSTRACT

tokamak •JT-60SA Integrated commissioning started in 2020, April superconducting magnets from tests January to March 2021 •Toroidal Field (TF) magnet successfully achieved 25.7 kA nominal current •TF current tests create AC losses in TF winding pack (WP) and casing





•Losses estimated from enthalpy balances using TF He inlet/outlet sensors •Theoretical calculation of hysteresis and coupling losses in the WP and eddy currents losses in the casing

•Comparison between experimental and theoretical energy values

EUROfusion JT-60SA

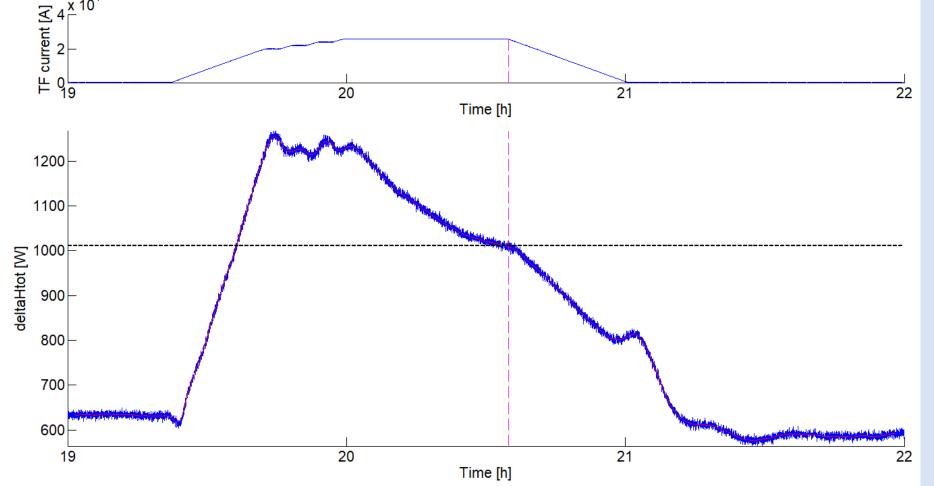
AC LOSSES MODELING

•Hysteresis losses computed as in [1] (Traps field map [2], B. Turck analytical formulae [3], deff=18 μ m [4] and Jc(B,T) measured in [5]. •Coupling losses computed with $P = n\tau \dot{B_a}^2/\mu_0$ (TF discharge time constant > 10 s >> $n\tau$). We assume $n\tau(B) = cst/\rho_{Cu}(B) = 1/(aB + b)$; a and b deduced from $n\tau$ (5.65 T)=279 ms (Sultan [5]) and $n\tau$ (0.5 T)=604 ms (CEA [6]). To account for field orientaton, we use $P = n\tau(B_a)(\alpha \dot{B}_{a,x}^2 +$ JT-60SA

2471 2451 13.0 15 ਤ੍ਹਿ ramp-up 18 3859 3623 12.6

TF fast discharge time constants τ_{FD} are decreasing with increasing I_{FD} because $\tau_{FD} = L_{TF}/R_d$ and the higher I_{FD} the higher the energy dissipated in the dump resistance R_d , so the higher its effective temperature and resistance.

• Joints Joule losses participate in transient heat loads during TF currents their total tests SO resistance $R_{TF joints}$ needs to be determined



At the end of the plateau at nominal current, from an enthalpy balance we determine $R_{TF joints} = 573$ n Ω . This value is conservative since the stationary regime is not completely reached (see plot above).

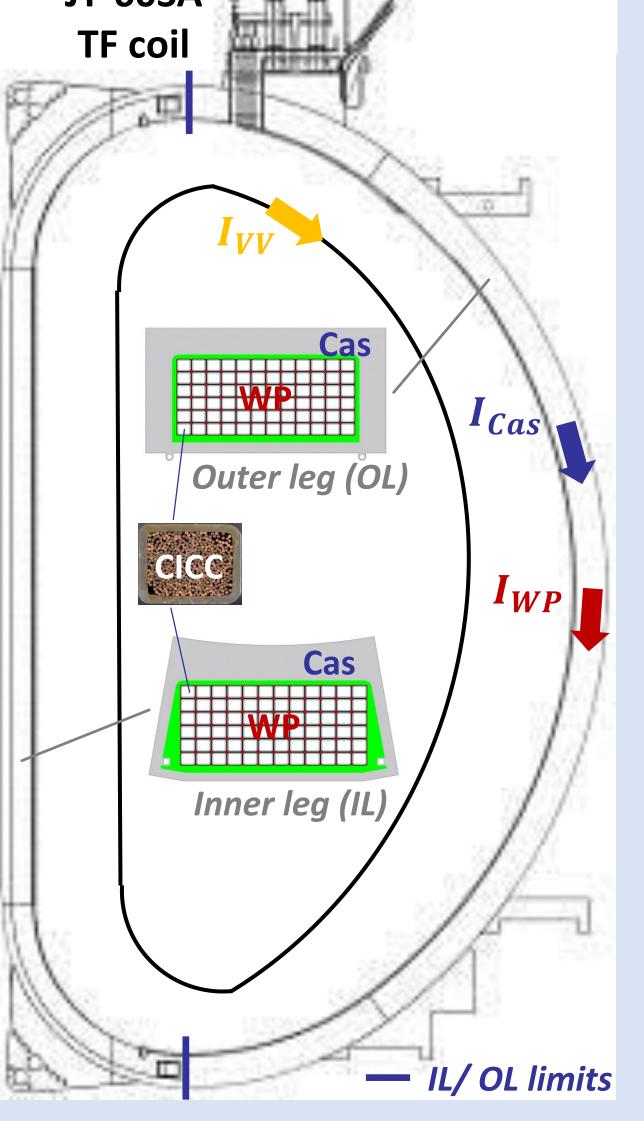
SYNTHESIS AND COMPARISON EXPERIMENT VS MODELING

•Eddy currents losses in TF casing are computed through solving of R,L circuits equations with data from [8]

$$\begin{bmatrix} R_{Cas}I_{Cas} + L_{Cas}\frac{dI_{Cas}}{dt} + M_{Cas/VV}\frac{dI_{VV}}{dt} = -M_{Cas/WP}\frac{dI_{WP}}{dt} \\ R_{VV}I_{VV} + L_{VV}\frac{dI_{VV}}{dt} + M_{Cas/VV}\frac{dI_{Cas}}{dt} = -M_{VV/WP}\frac{dI_{WP}}{dt} \\ E_{Cas}[J] = \int P_{Cas}dt = \int R_{Cas}I_{Cas}^{2}dt$$

Inner leg (IL) of casing is shorter and thinner than its outer leg (OL)

- \rightarrow 43% of total power is generated in IL and 57% in OL
- \rightarrow average power per unit volume is 1.55 times higher in IL than in OL.



 $T_{in,WP}, P_{in,WP}$

T_{in,Cas}, P_{in,Cas}

TF coils

(WP)

TF + CS

structures

(TF Cas)

 m_{Cas_k}

lout,Cask

Pout,Cask

Supercritical He at

~4.4 K, 5.3 Bar

 \dot{m}_{WP_k}

T_{out,WP}

 P_{out,WP_k}

•Theoretical transient heat loads computed with AC losses modeling and joints Joule losses	100 % 0f load % 0 T	3 4 90 91 -7 5 10 15 F Fast discharge cur	7 Hyst+Coup 88 EC 5 Joints 18 rrent [kA]
estimate from $R_{TF joints}$.	I _{FD} [kA]	Total exp [kJ]	Total th [kJ]
About 90% of the load is	10	2305	2703 (+17 %)
due to eddy currents	15	4922	5409 (+10 %)
losses in TF casings	18	7482	7975 (+7 %)

•Comparison between total experimental and theoretical transient heat load show a fair agreement in the 5-15% range even with a conservative estimate of the joints contribution

•WP absorbs about 50 % of the				
load while 90 % of it is generated				
in casing → casing heats WP				
 Lorentz forces increase this effect 				

	I _{FD} [kA]	Exp transient heat loads [kJ]		
5		WP	Cas	
c	10	1114 (48.3 %)	1191	
	15	2471 (50.2 %)	2451	
t	18	3859 (51.6 %)	3623	

EXPERIMENTAL DATA ANALYSIS

CONCLUSION

•Enthalpy balances of Helium flow in TF WP and casing during fast discharge tests allow AC losses determination (transient heat loads)

Simplified scheme of Helium massstruct. temperature tlow, and pressure sensors is shown on the right.

$$\Delta H_{WP}[W] = \dot{m}_{WP}[h(T_{out,WP}, P_{out,WP}) - h(T_{in,WP}, P_{in,WP})]$$

$$\Delta H_{Cas}[W] = \dot{m}_{Cas}[h(T_{out,Cas}, P_{out,Cas}) - h(T_{in,Cas}, P_{in,Cas})]$$

•AC losses modeling in fair agreement with JT-60SA experimental results Major contribution of casing eddy currents and large redistribution to WP •Consistency of observation with AC losses study in CTF [1]

ACKNOWLEDGEMENTS / REFERENCES

This work has been carried out within the framework of the EUROfusion Consortium and has received funding from the Euratom research and training programme 2014-2018 and 2019-2020 under grant agreement No 633053. The views and opinions expressed herein do not necessarily reflect those of the European Commission. The authors gratefully acknowledge members of the JT-60SA Integrated Project Team for data exchange and fruitful discussions. **References:** [1] A. Louzguiti et al., IEEE Trans. Appl. Supercond., 2021 / [2] P. Hertout et al., IEEE Trans. Appl. Supercond., 2002 / [3] B. Turck, CEA Technical note, 1985 / [4] M. Chiletti et al., IEEE Trans. Appl. Supercond., 2020 / [5] L. Zani et al., IEEE Trans. Appl. Supercond., 2013 / [6] M. Chiletti, PhD Dissertation, 2021 / [7] Amikam Aharoni, J. Appl. Phys., 1998/ [8] JT-60SA PID