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## Introduction

In the framework of JT-60SA tokamak commissioning (Japan, 2021), 20 **Toroidal Field Coils (TFC)** were tested at the **Cold Test Facility (CTF)**, at CEA-Saclay (France, 2018).

- quench acceptance test (quench temperature up to 7.5 K at nominal current)
- complementary tests on spare coil TFC02 with different quench conditions:
  - reduced current (at 75% and 50% of nominal current)
  - delayed quench detection (increased holding time  $\tau_h = 0.5$  s, instead of  $\tau_{h,nominal} = 0.1$  s)

Numerical simulations of these tests were performed using SuperMagnet code coupling:

- THEA (Thermohydraulic and electrical 1-D physics of Cable In Conduit Conductor, CICC)
- Flower (Hydraulic model of external cryogenic network)

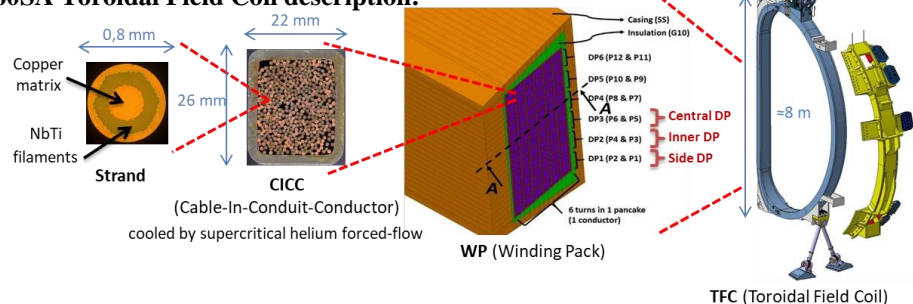


TFC installed in Cold Test Facility

TABLE I  
TFC02 COMPLEMENTARY QUENCH TESTS MAIN INITIAL PARAMETERS

| TFC02 Tests           | I (kA) | B <sub>max</sub> (T) | T <sub>cs,min</sub> (K) | τ <sub>h</sub> (s) |
|-----------------------|--------|----------------------|-------------------------|--------------------|
| Acceptance            | 25.7   | 3.05                 | 7.42                    | 0.1                |
| Delayed detection     | 25.7   | 3.05                 | 7.42                    | 0.5                |
| 75 % I <sub>nom</sub> | 19.5   | 2.29                 | 7.83                    | 0.1                |
| 50 % I <sub>nom</sub> | 12.9   | 1.52                 | 8.24                    | 0.1                |

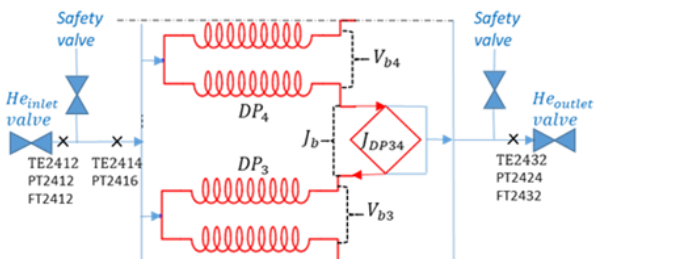
## JT-60SA Toroidal Field Coil description:



## 1. Estimation of experimental normal length propagation

CTF instrumentation, namely double-pancake voltage and helium flow measurements, allow:

- Determination of resistance and normal length evolution in each CICC
- Analysis of the helium flow (P, T, ṁ) at winding pack inlet and outlet



Fast Safty Discharge (FSD) induces voltages

$$V_{b,DP}(t) = L_{DP} \frac{dI(t)}{dt} + M_{DP} \frac{dI_p(t)}{dt} + R_{DP}(t) I(t)$$

$$V_{DP}(t) = \left( \frac{V_{b,DP}(t)}{V_{pickup}(t)} \right) = \left( \frac{V_{DP,inductive}(t)}{V_{pickup}(t)} \right)_{\text{quench}} = \left( \frac{V_{DP,resistive}(t)}{V_{pickup}(t)} \right)_{\text{quench}}$$

*Pure discharge*

CICC quench propagation heuristic model

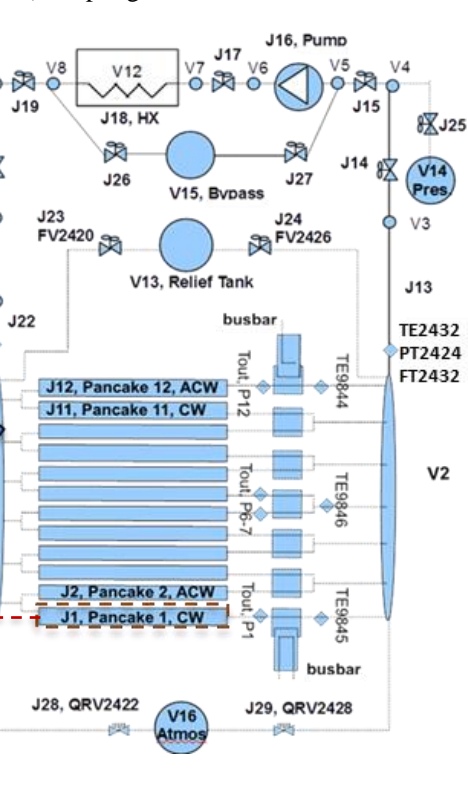
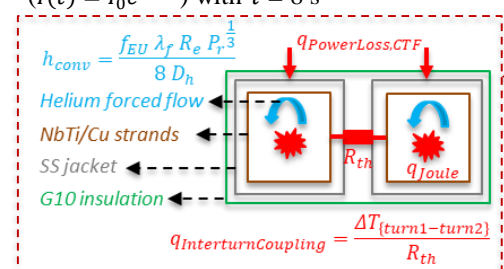
$$\int_0^{NL_p(t)} \frac{\eta_{Cu}(B(t,x), T(t,x), RRR)}{A_{Cu}} dx \geq R_p(t)$$

$$NL_p(t) = \frac{R_{DP}(t)}{A_{Cu}}$$

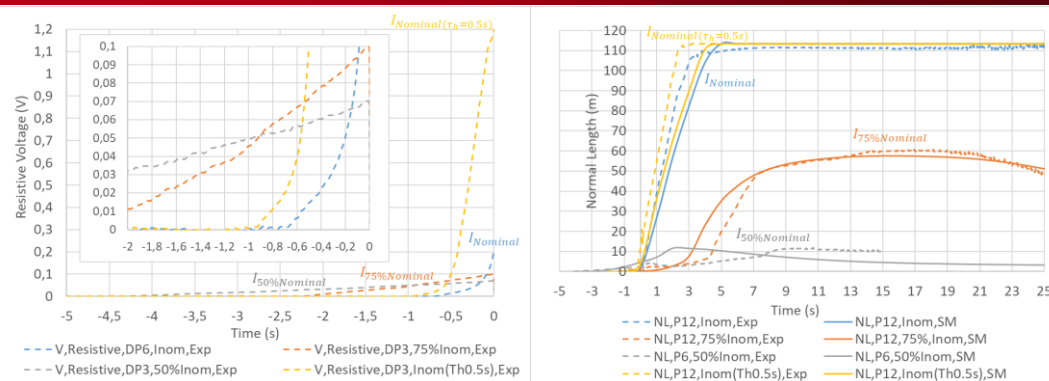
## 2. Numerical quench model

Model developed with SuperMagnet (L. Bottura, CERN) coupling THEA and Flower codes:

- Flower models the cryodistribution
- THEA models the 12 CICC (helium, conductor, jacket)
- Magnetic field profiles calculated with TRAPS code
- Friction factor correlations from experimental measurements
- Primary quench detection features: voltage threshold  $V_{detect} = 0.1$  V and holding time  $\tau_h = 0.1$  s or 0.5 s
- FSD: current exponential decay ( $I(t) = I_0 e^{-t/\tau}$ ) with  $\tau = 8$  s



## 3. TFC02 complementary quench tests results



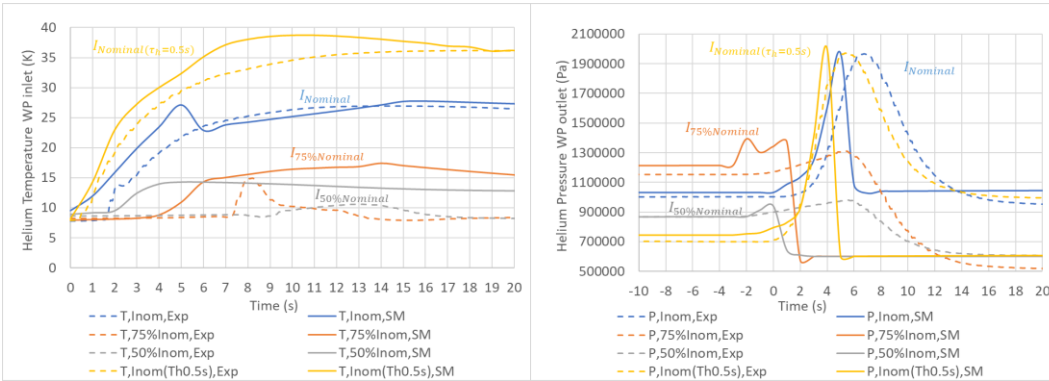
Early quench development: Quench initiation of the whole coil and quench detection ( $t = 0$  s taken at FSD start) for each quench test are analyzed with experimental DP resistive voltages:

$$V_{Resistive,DP6,Inom}(0) = 0.24 \text{ V} \quad V_{Resistive,DP3,75\%Inom}(0) = 0.11 \text{ V}$$

$$V_{Resistive,DP3,Inom(\tau_h=0.5s)}(0) = 1.19 \text{ V} \quad V_{Resistive,DP3,50\%Inom}(0) = 0.07 \text{ V}$$

Propagation during current fast discharge: Both experimental and calculated maximal normal lengths reached for each test show that **reduced current induces slow quench propagation with conductors not fully quenched:**

$$NL_{max,Inom} = 113.2 \text{ m} \quad NL_{max,75\%Inom} = 60.7 \text{ m} \quad NL_{max,50\%Inom} = 11.7 \text{ m}$$



- Helium temperature: Delayed quench detection (at nominal current) increases Joule energy dissipated before FSD, increasing CICC temperature by 10 K compared to acceptance test
- Helium pressure: Quench tests at reduced current induce low pressure rise and do not open quench relief valves, whereas at nominal current the pressure threshold of 20 bars is reached

## 4. Discussion on smooth quench criticality

Experimental results comparison with SuperMagnet and analytical approach:

Quench velocity  $v_q$  provided by A. Shajii analytical scaling laws:  $v_q(t) = \frac{dNL(t)}{dt}$

$$\frac{dT_{cond}(t)}{dt} = \frac{\eta_{Cu}(t) NL(t)}{L (A_{Cu} \rho_{Cu} C_{Cu}(t) + A_{NbTi} \rho_{NbTi} C_{NbTi}(t))} I(t)^2 - h_{conv} P_{w,cond} L (T_{cond}(t) - T_{He}(t))$$

$$v_q(t) = 0.766 \left( \frac{2 D_h}{f} \right)^{\frac{1}{5}} \left( \frac{r NL_{ini} \alpha_0 J_0^2}{c_0} \right)^{\frac{2}{5}} \frac{1}{t^{\frac{1}{5}}}$$

Nominal current: Long coil-High pressure rise Regime

$$v_q(t) = \frac{r \rho_0 NL_{ini} \alpha_0 J_0^2}{2 p_0}$$

Reduced current: Long coil-Low pressure rise Regime

TABLE II  
SUMMARY OF CALCULATED AND EXPERIMENTAL QUENCH VELOCITIES, TEMPERATURES AND EARLY QUENCH PROPAGATION TIMES

| TFC02 Tests                   | Acceptance | Delayed detection | 75 % I <sub>nom</sub> | 50 % I <sub>nom</sub> | "smooth" quench occurs at reduced current  |
|-------------------------------|------------|-------------------|-----------------------|-----------------------|--|
| $v_q, NL_{max,Exp}$           | 25.6 m/s   | 32.1 m/s          | 3.9 m/s               | 0.7 m/s               | Low quench propagation velocities  |
| $v_q, NL_{max,SM}$            | 22.7 m/s   | 22.1 m/s          | 3.2 m/s               | 1.6 m/s               |  |
| $v_q, analytical$             | 16.1 m/s   | 12.8 m/s          | 3.6 m/s               | 0.6 m/s               |  |
| $\tau_{da} = \tau_h + \tau_p$ | 0.61 s     | 0.92 s            | 2.12 s                | 4.18 s                | Quench propagation time $\tau_p$ for reaching $V_{detect}$ increases   |
| $T_{He,max,Exp}$              | 26.3 K     | 36.9 K            | 14.9 K                | 10.5 K                | CICC $T_{cond,max}$ are:<br>- mainly affected by $\tau_h$ at $I_{nom}$<br>- lower at reduced currents even if $\tau_p$ is larger |
| $T_{He,max,SM}$               | 27.7 K     | 38.7 K            | 17.4 K                | 14.3 K                |  |
| $T_{cond,max,SM}$             | 32.6 K     | 38.9 K            | 17.5 K                | 16.6 K                |  |
| $T_{cond,max,analytical}$     | 44.25 K    | 40.8 K            | 19.1 K                | 12.4 K                |  |

## Conclusion

Numerical model validation:

- Large scale model of one JT-60SA TFC with its cryodistribution in CTF allowed simulating the quench transient phenomenon.
- Simulation results were compared to experimental measurements of TFC02 complementary quench tests and were found in rather good agreement.

Main results:

- Delayed detection at nominal current significantly increases the Joule energy dissipated before the fast current discharge and thus induces large CICC temperature rise.
- Smooth quench at reduced current are characterized by slower quench propagation velocities, inducing not fully quenched coil, lower temperature and pressure rises.