

OBJECTIVES

- Conceptual design for a **20 T dipole**
- Hybrid magnet = **HTS Bi2212 + Nb₃Sn**
- Feasibility of a **block-coil design**?
- Take the **stress into account**
 → See “Towards 20 T hybrid accelerator dipole magnets”, FRI-OR6-101-04

| D [mm] | Nstr | Th [mm] | W [mm] | Cu:nCu | J0/JE | J0/Jc |
|------------|-----------|-------------|-------------|------------|--------------|--------------|
| 1.2 | 54 | 2.46 | 34.3 | 1.1 | 0.724 | 0.345 |
| 1.2 | 27 | 2.46 | 17.3 | 1.1 | 0.717 | 0.342 |
| 1.0 | 32 | 2.10 | 17.1 | 1.1 | 0.700 | 0.333 |
| 0.85 | 38 | 1.83 | 17.3 | 1.1 | 0.683 | 0.325 |
| 0.7 | 46 | 1.56 | 17.2 | 1.1 | 0.660 | 0.314 |

Considered Cables (bare reacted)

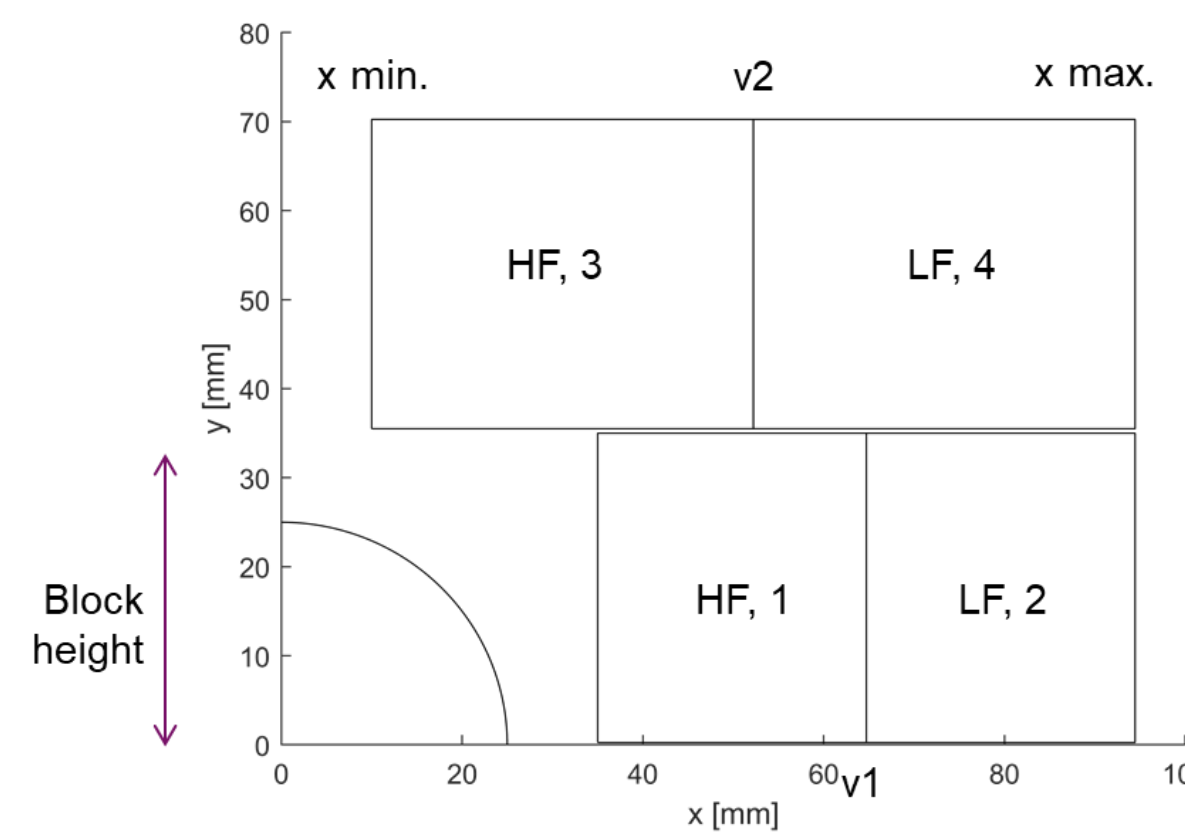
SUMMARY

- parametric analysis to identify the “ideal” X-section
- **Compact design**
- **Stress limitation**

- Exploration of stress-managed layouts
- « hybrid magnet » vs « hybrid coils »
- Hybrid coils → **internal rib**
- **Acceptable stress at nominal**
- **Compact and efficient**
- **Coil fabrication R&D required**

PRELIMINARY PARAMETRIC ANALYSIS

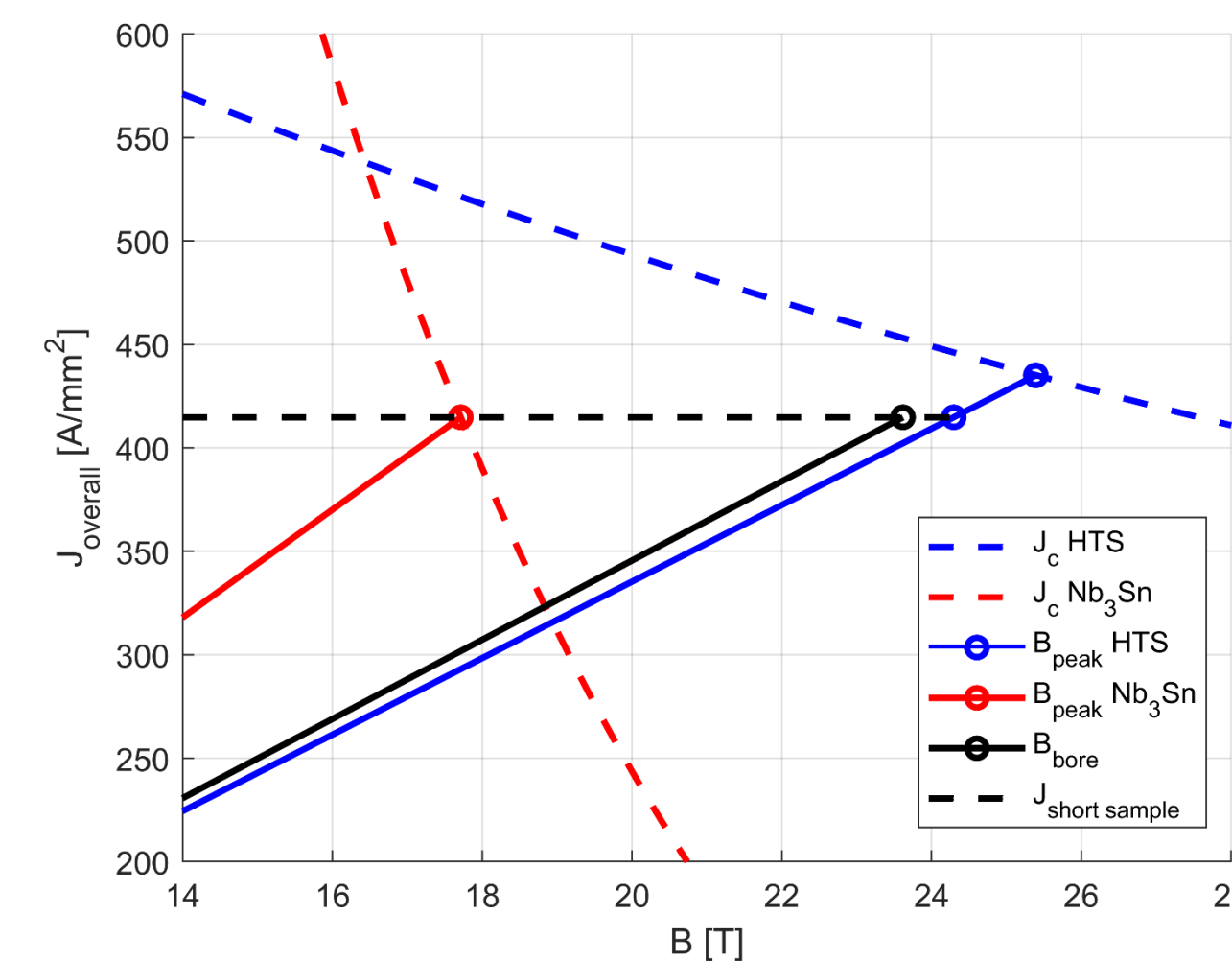
- **Blocks with homogeneous J**
- **Analytical formulas for B and S**
- **Parametric analysis without iron**



- **Determination of the minimum amount of conductor:**

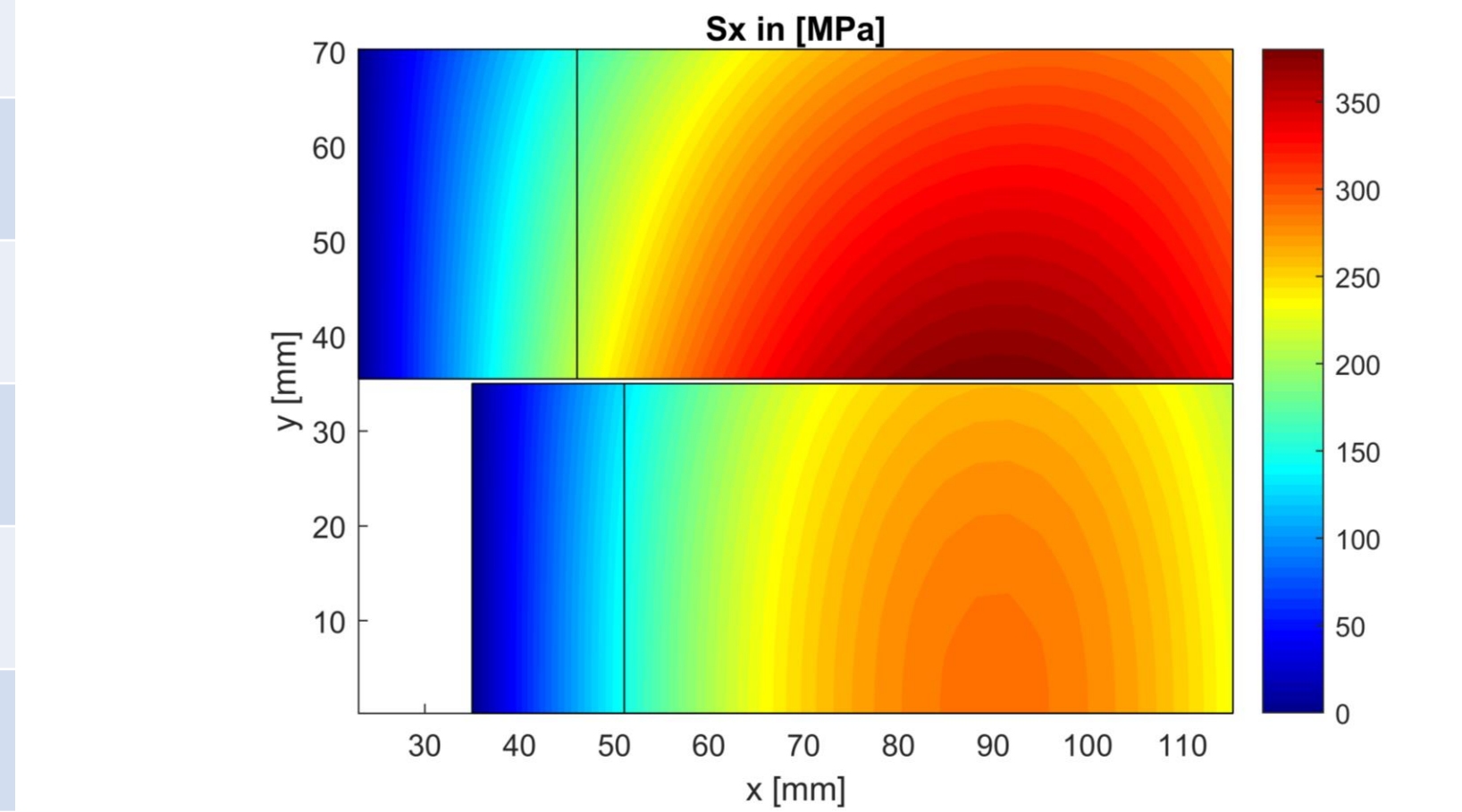
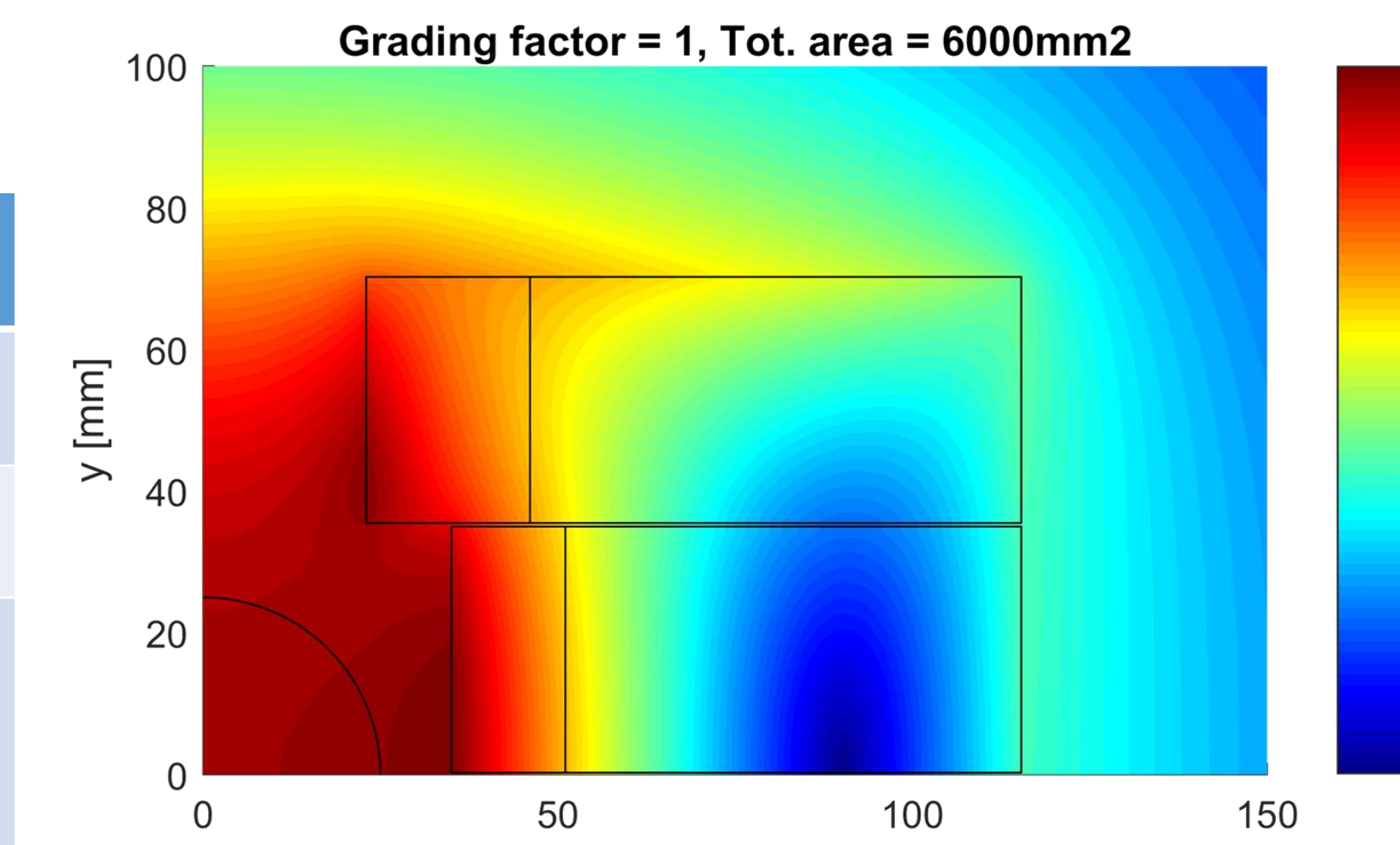
1. given conductor area and minimum radius xmin
2. boundaries v1 and v2 are varied.
3. Max. bore field at short sample is selected.
4. The solution with the min. area of Bi2212 is selected.
5. 1. to 3. repeated, changing area or xmin.
6. A final solution is chosen based on the criteria.

| Max. Stress | SS | 85% SS |
|-------------|-----|------------|
| Sx Nb3Sn | 380 | 275 |
| Sy Nb3Sn | 151 | 109 |
| Sx Bi2212 | 215 | 155 |
| Sy Bi2212 | 139 | 100 |



- **Final solution computed with iron using FEM**

| Parameter | Unit | Hybrid | | | HTS only | LTS only |
|------------------|-------------------|------------------|------------------|------------------|----------|----------|
| | | SS no iron | 83%SS | SS | SS | SS |
| Area | A/mm ² | 6000 | 6000 | 6000 | 1360 | 4740 |
| B0 total HTS+LTS | T | 23.3 6.5+16.8 | 20.0 6.5+13.5 | 23.7 7.6-16.1 | 10.4 | 16.6 |
| Bp HTS | T | 24.16 | 20.6 | 24.3 | 12.4 | |
| Bp LTS | T | 17.15 | 15.1 | 17.2 | | 18.2 |
| J HTS | A/mm ² | 447.5 | 346.1 | 416.9 | 593.7 | 0 |
| J LTS | A/mm ² | 447.5 | 346.1 | 416.9 | 0 | 387.9 |
| Margin HTS | % | 0 | 20.5 | 4.2 | 0 | - |
| Margin LTS | % | 0.93 | 17.0 | 0 | - | 0 |



OUTLOOK FOR STRESS-MANAGED HYBRID DESIGNS

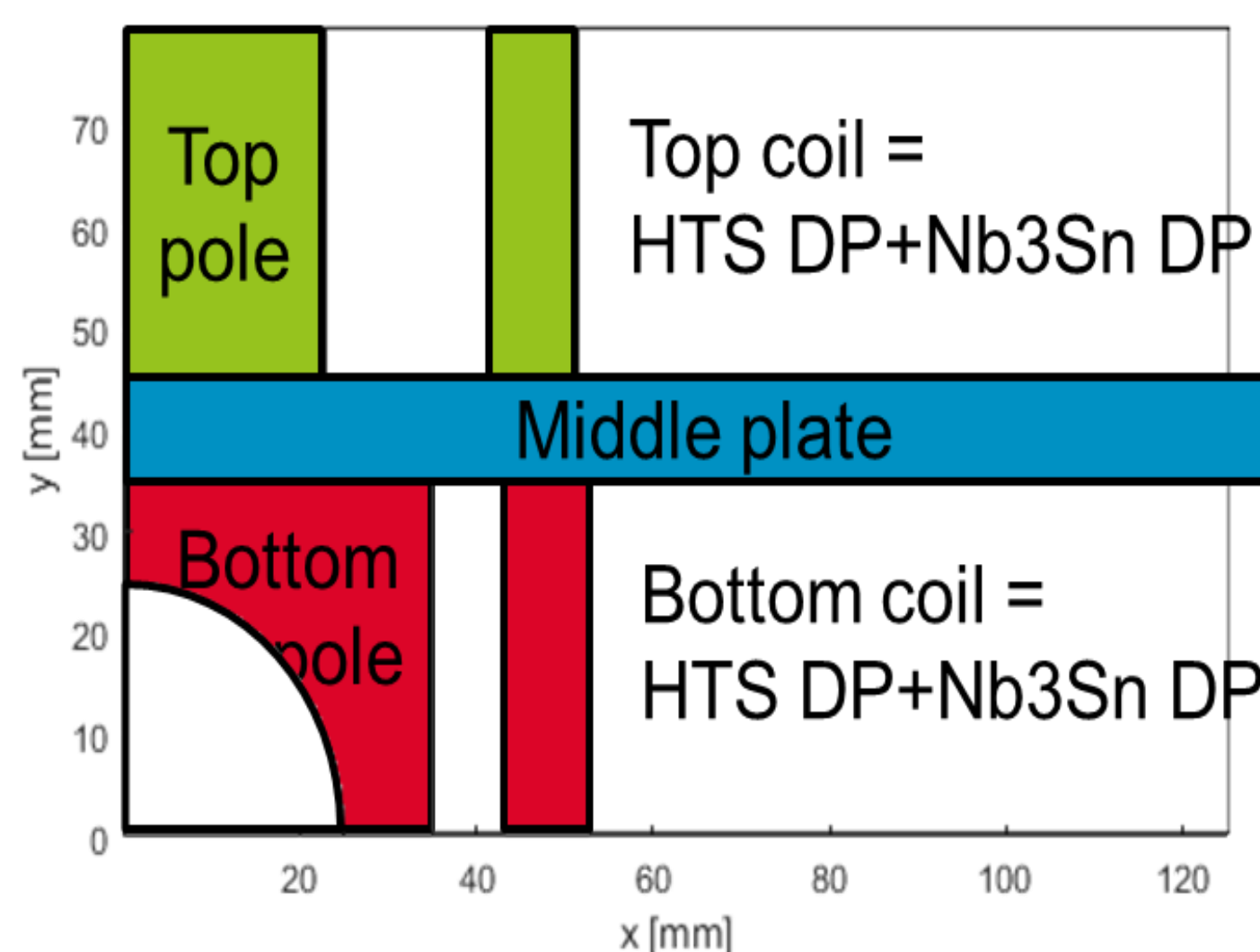
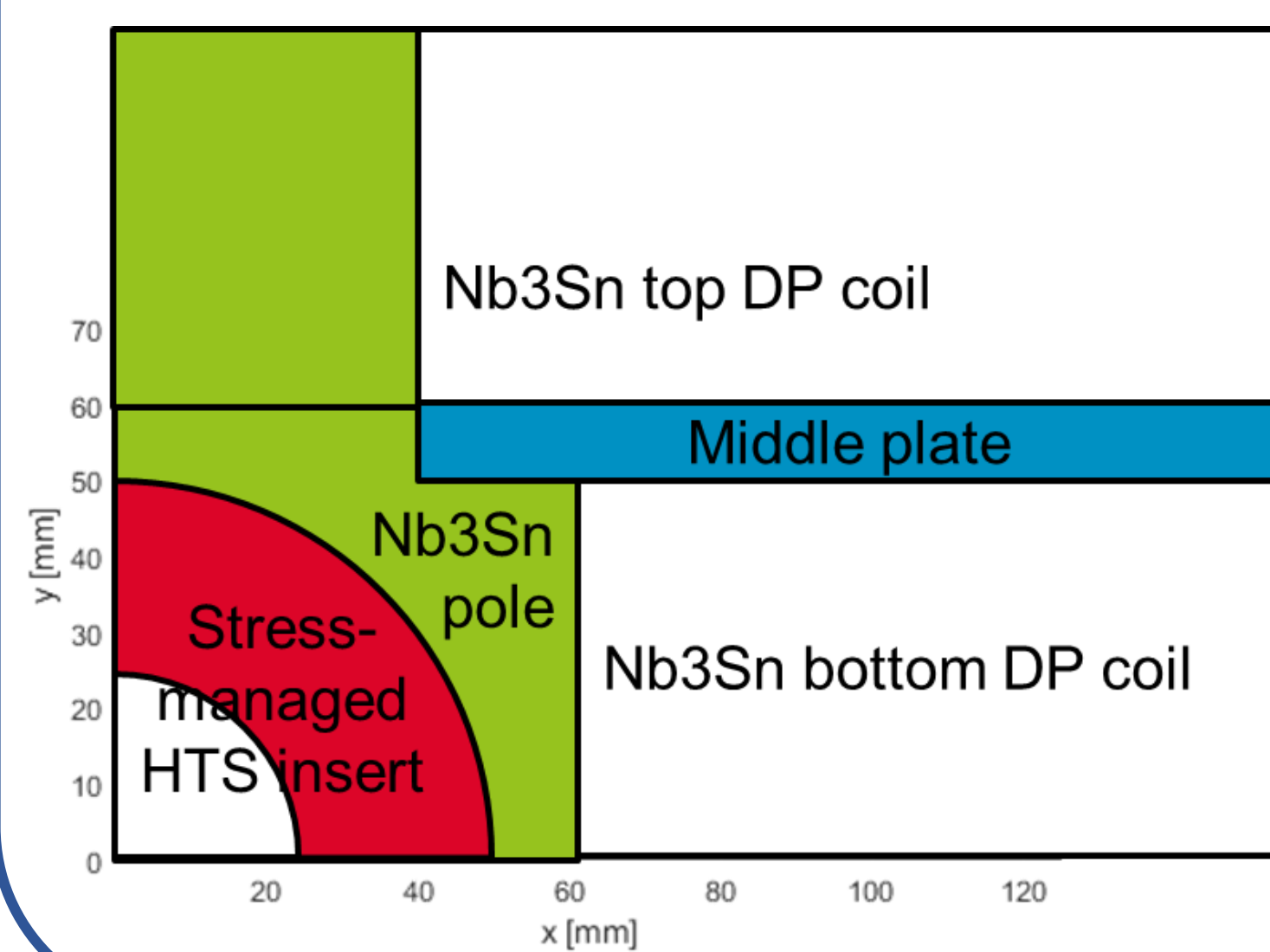
“Hybrid magnet” assembly

VS

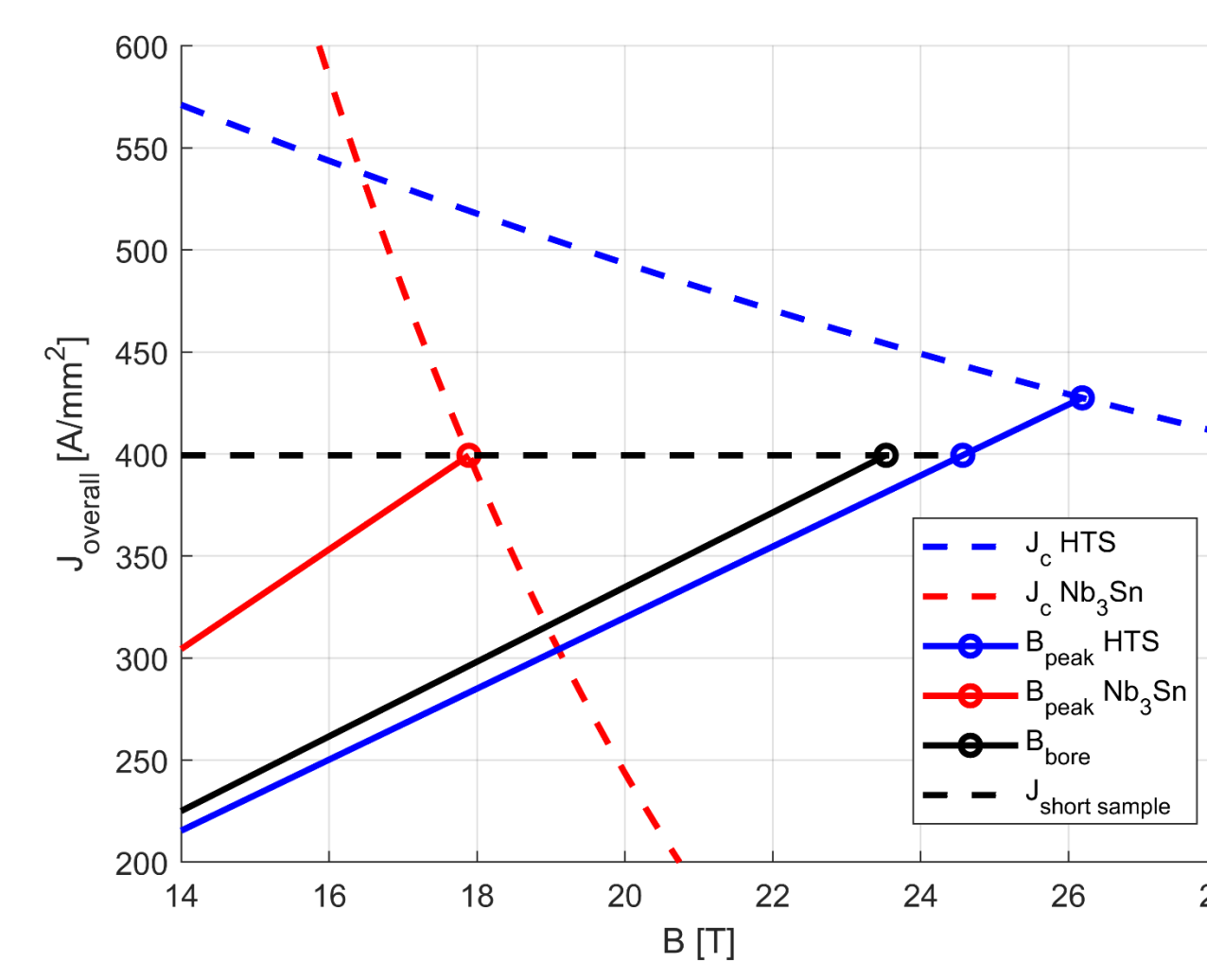
“Hybrid coils”

- ✓ **Mechanically decoupled**
- ✓ **Independent R&D Nb₃Sn / Bi2212**
- ✗ **Less degrees of freedom**
- ✗ **Nb₃Sn outsert less compact**

- ✗ **Separate coil fabrication**
- ✗ **External/internal joints**
- ✓ **Ribs to intercept Sx**
- ✓ **More compact**



| Max. Stress | SS | 85% SS |
|-------------|-----|------------|
| Sx Nb3Sn | 222 | 160 |
| Sy Nb3Sn | 136 | 98 |
| Sx Bi2212 | 193 | 139 |
| Sy Bi2212 | 84 | 61 |



- **Final solution computed with iron using FEM**

| Parameter | Unit | Hybrid | | | HTS only | LTS only |
|------------------|-------------------|------------------|------------------|------------------|----------|----------|
| | | SS no iron | 83.5%SS | SS | SS | SS |
| Area | A/mm ² | 7500 | 7500 | 7500 | 1500 | 6000 |
| B0 total HTS+LTS | T | 23.4 6.5+16.9 | 20.0 6.3+13.7 | 23.6 7.4+16.2 | 10.6 | 16.2 |
| Bp HTS | T | 24.58 | 20.9 | 24.7 | 12.1 | |
| Bp LTS | T | 17.57 | 15.2 | 18.0 | | 18.5 |
| J HTS | A/mm ² | 427.9 | 334.8 | 401.0 | 598.2 | 0 |
| J LTS | A/mm ² | 427.9 | 334.8 | 401.0 | 0 | 367.3 |
| Margin HTS | % | 2.2 | 21.7 | 6.2 | 0 | - |
| Margin LTS | % | 0 | 16.5 | 0 | - | 0 |

