



All credit to the exceptional team that delivered the TFMC Project

- Chief Engineer: Rui Vieira
- Group leaders: Brian LaBombard (E&M), Chris Lammi (Analysis), Joy Dunn (Manufacturing),

Ted Golfinopoulos and Phil Michael (Test)

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Bill Byford
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Pete Stahle Ken Stevens Joe Stiebler Deepthi Tammana Tom Toland Dave Tracey Ronnie Turcotte Kiran Uppalapati Matt Vernacchia Chris Vidal Alex Warner Amy Watterson Dennis Whyte Sidney Wilcox Michael Wolf ** **Bruce Wood** Lihua Zhou Alex Zhukovsky

Context: High-field fusion energy and early HTS R&D (2 min)

The SPARC Toroidal Field Model Coil (12 min)

- Program: Requirements and objectives
- Magnet: Specifications, design, and assembly
- Facility: Capabilities and key enabling technologies
- Test: Results of the first full performance 20 T ramp

Summary (1 min)

This talk is intended as a high-level overview and status of an extensive on-going project. More in-depth presentation of the project will be in upcoming publications and conferences.

HTS magnets enable the high-field path to fusion energy



High-field fusion science

Phase 1: Technology R&D



Phase 2: Demonstration



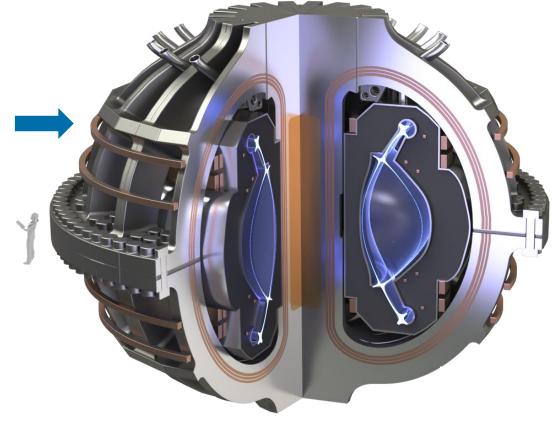




Alcator C-Mod



SPARC



HTS CICC-like concepts





No-insulation HTS concepts

Q>2

ARC

2016

2021

2025

2030s

HTS magnets enable the high-field path to fusion energy





Phase 1: **Technology** R&D

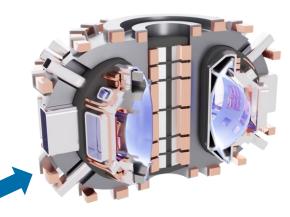






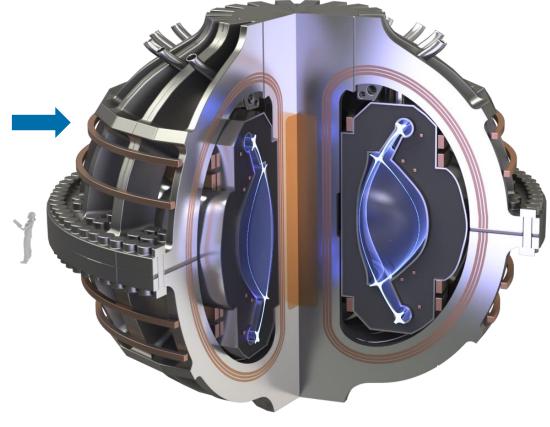
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ARC



11/17/2021

No-insulation HTS concepts

SPARC

(2017-2019)

2016

2021

(2019-2021)

magnet R&D HTS model coil

2025

2030s

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Early R&D resulted in two viable high-field HTS technologies

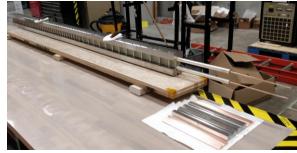


Starting in 2017, both technologies were built on HTS magnet work pioneered at MIT

VIPER HTS cables

- Based on traditional SC CICC cables using the TSTC architecture for REBCO tapes [1]
- Demonstrated high IxB robustness, fiber optic quench detection, $\sim n\Omega$ joints [2,3]
- Developed for multiple SPARC applications:
 - High current feeder cables
 - AC magnets: SPARC CS, PF (w/ modifications)
 - DC magnets: back-up for SPARC TF





VIPER SULTAN assembly (2018)

- [1] M. Takayasu et al., IEEE Trans. Appl. Sup., 21 (2011) 2340
- [2] Z. S. Hartwig et al., SuST, 33 (2020) 11LT01
- [3] E. E. Salazar et al., SuST, 34 (2021) 035027

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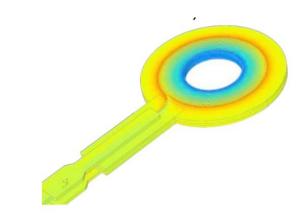
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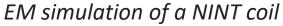
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No Insulation No Twist (NINT) Coils

- HTS cable-based adaptation of single tape NI coils [4] with innovations to enable large-scale fusion magnets
- Demonstrated passive quench handling, advanced EM modeling capabilities, low voltage operation
- Developed for a *specific* SPARC application:
 - DC magnet: SPARC TF magnet -> The TFMC







^[1] M. Takayasu et al., IEEE Trans. Appl. Sup., 21 (2011) 2340

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The TFMC Project seeks to eliminate risk in the production and operation of large-scale HTS DC magnets



RISK

High field

Operation

Quench

Design Achieve SPARC requirements (B_{peak}, J_{wp}, P_{cooling}, etc); EM modeling tools; ...

Supply Chain HTS supply and characterization; Structural materials; large-scale vendors; ...

Fabrication Tooling; Manufacturing process and equipment; Process control, Scalability, ...

Structural loading; IxB and strain on HTS; I_c limits on HTS; ...

Current leads; Feeder cables; Instrumentation; Cooling system; ...

Stored magnetic energy; high pressure coolant; induced eddy forces; ...

Objective: Design, build, and test (1) a representative SPARC TF model coil and (2) a fully capable test facility in 2 years to maximize risk retirement for SPARC

Time Frame: July 2019 – Sep 2021

Team Size: 80+ people at 3 sites

The TFMC is the first NI large-scale high-field fusion magnet



Targeting peak fields >20 T with simple manufacturing, novel cooling, passive quench handling



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Parameters of the SPARC Toroidal Field Model Coil





JACO 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1



Nominal Operating Parameter	Value
Number of pancakes	16
Total turns	256
Total REBCO tape	270 km
Operating temperature	20 K
Coolant type	Supercrit. He
Operating coolant pressure	20 bar
Operating terminal current	40 kA
Peak magnetic field	20 T
Peak IxB force on REBCO	800 kN/m
Inductance	0.14 H
Magnetic stored energy	110 MJ
WP mass	5,113 kg
WP current density	153 A/mm ²
WP + case mass	10,058 kg
WP + case linear size	2.9 x 1.9 m

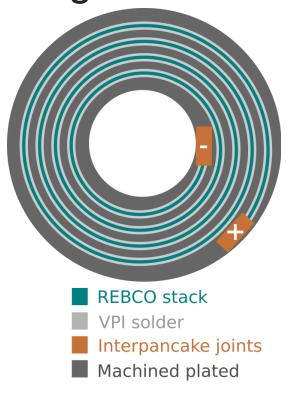
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TFMC uses an HTS stack-in-plate channel design



Pancakes

- A machined steel radial plate with channels for HTS and cooling
- The HTS is stack wound into the grooves
- The HTS stack is terminated at internal pancake-to-pancake joints
- VPI solder process bonds mechanically, electrically, and thermally



TFMC is based on NI HTS stack-in-plate channel design



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Winding pack

- The core of the winding pack comprises 16 stacked, internally jointed pancakes
- Winding pack has 2 top and bottom termination plates for current leads

Magnet

- The winding pack is contained within a steel structural and pressure vessel case
- High pressure plena on the case enable current, cooling, and instrumentation



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Propose Design Features	Advantage(s) to be proven in the TFMC Project
Modular, simple construction	Rapid assembly; Maintenance options; scalable for commercial production
Intrinsically low voltage (<1 V)	Minimal insulation; simple fabrication, low voltage leads and feeds, safety
High thermal stability	Robust to damage, defects, and off-normal events
Pressure vessel cooling approach	Enhanced heat removal; Local cooling optimization; simplified manifolding
High winding pack current density	Compact magnet; expanded design space
Passively safe to quench	No quench detection systems

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A new magnet test facility has been established at MIT



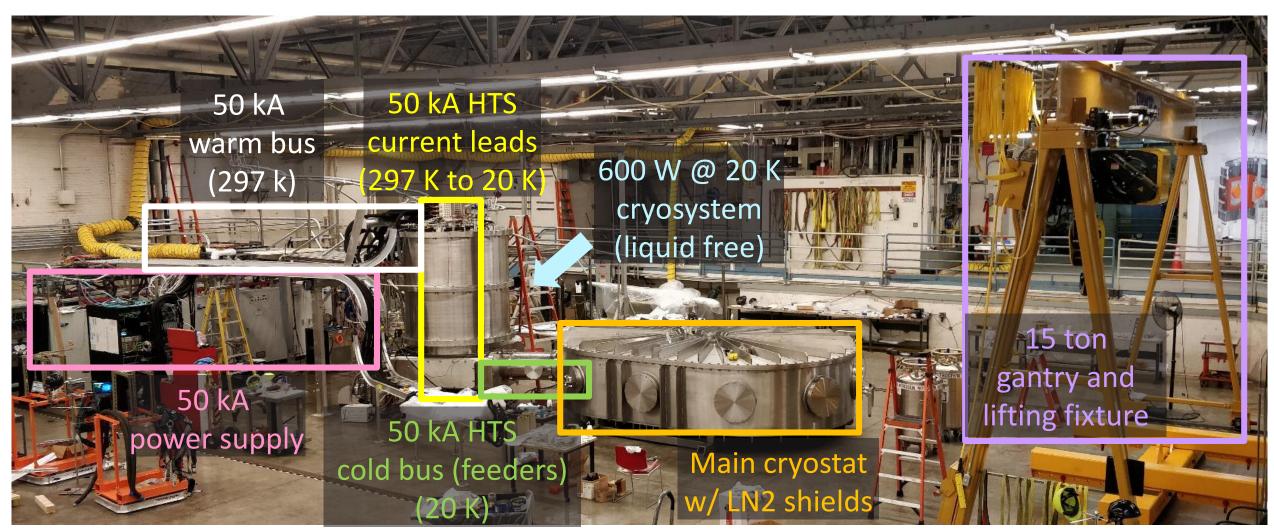
Facility provides substantial test capabilities for the TFMC and future magnet R&D



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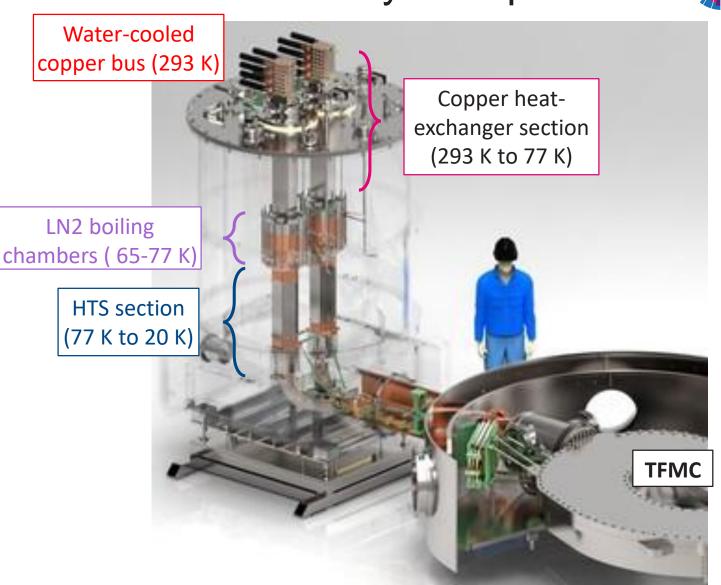


Not shown: SHe and LN2 distribution systems; Vacuum systems; I&C system; Safety systems; Control Room

Binary 50 kA HTS current leads and feeder system proven



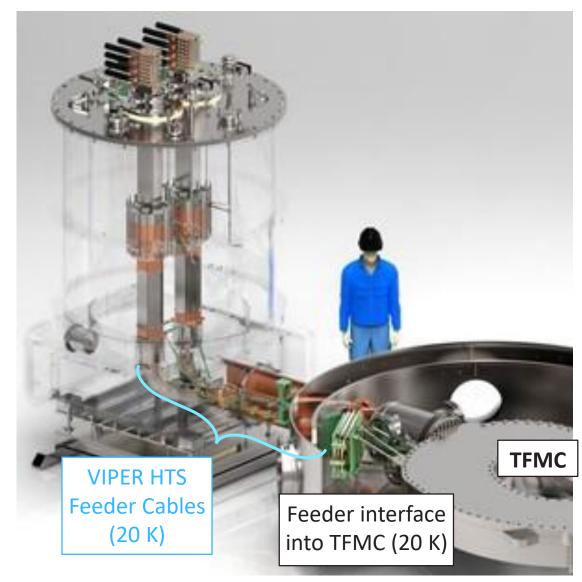
- Binary HTS current leads were designed, fabricated, and commissioned in-house
 - Designed to supply up to 50 kA for low voltage DC magnets
 - LN2 section can be sub-cooled to enable high current performance
 - In-house development required to meet performance and schedule requirements



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 - In-house development required to meet performance and schedule requirements
- Feeder system to magnet composed of 3 sets of VIPER HTS cables
 - Complex shape to mitigate thermally induced differential strain due to cooldown
 - 3 sets of joints to simplify assembly
 - Unique high-pressure feedthrough to enable connection to TFMC magnet
- Leads and feeder system commissioned in advance of TFMC installation
 - Tested to 41 kA (max required current)
 - All joints with 1.5 2.0 nOhm performance



1st Test: Assess DC operation of the TFMC at full performance

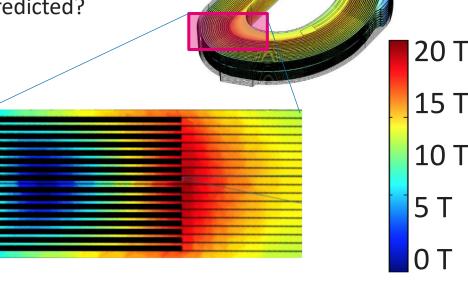


• First full-performance test asked 3 primary questions of the coil operating in DC:

Does the TFMC precisely match design B-field and withstand static loading?

Does the coil distribute current during charging and flat-top as predicted?

Does the TFMC distribute voltage (heating) as predicted?



EM simulations of B-field at $I_{terminal}$ =40 kA (top) and the test plan for the approach to 20 T (bottom)

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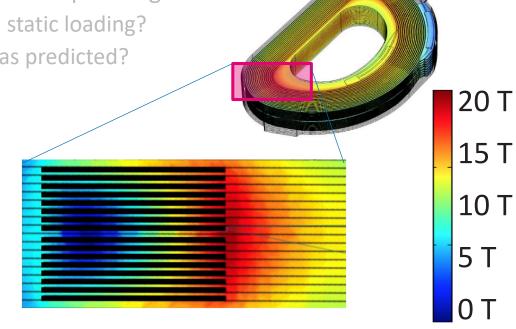
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• Does the TFMC distribute voltage (heating) as predicted?

 The winding pack contained an extensive array of internal embedded instrumentation to provide complete characterization of the coil electrically and thermally

- >180 voltage taps (internal)
- >30 Cernoxes RTDs (internal)
- 4 embedded hall probes (internal)
- Helium flow and pressure sensors (internal)
- Strain gauges (external)
- Two external 3D hall probes were used to produce robust confirmation of magnetic field metrology
 - Calibrated against fiber optic current sensors (FOCS) measuring azimuthal current in the coil



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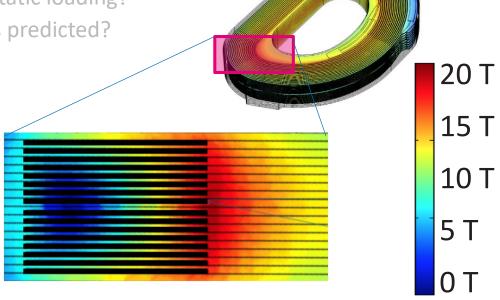
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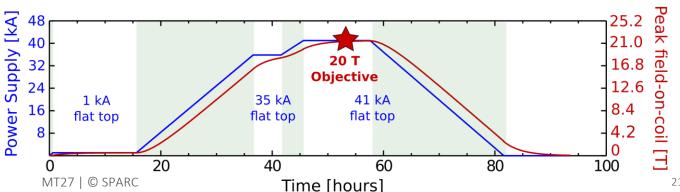
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1st Test: Key performance objectives met for the TFMC at 20 T SPARCE

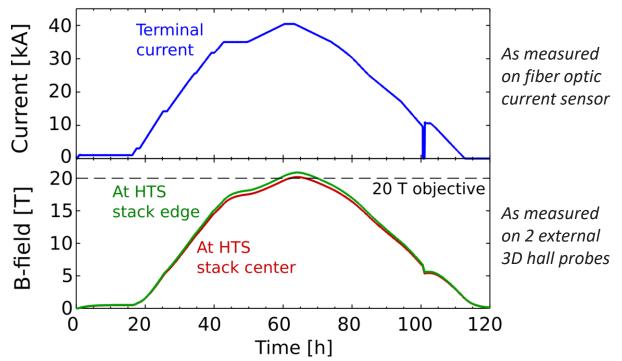


First full performance test largely followed the plan predicted by experience and modeling:

Vacuum: 2 day pump down to 10⁻⁶ torr vacuum Cooldown: 7 day cooldown from 293 to 18 K

Charging: 5 day test campaign to ramp to 20 T back to 0 T





1st Test: Key performance objectives met for the TFMC at 20 T SPARCE

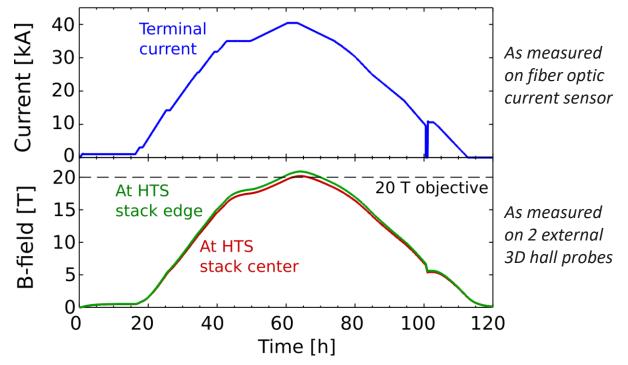


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Experimental measurements of 20 T ramp



High-field performance confirmed

- B~20.3 T average on inner radius HTS stacks
- IxB>800 kN/M radial loading on HTS stacks

Low-resistance internal pancake-to-pancake joints

- R of 1.0-1.5 nΩ at maximum current of ~40 kA
- Structural robust within 5 T (outer) and 12 T (inner)

Excellent cryogenic performance, stability, control

- WP temperature control between 18 32 K
- WP temperature uniformity of 1 − 2 K

Significant structural loading handled as designed

- Winding pack stress >800 MPa, case >900 MPa
- Smooth stress-strain; strain gauges matched prediction

Excellent matches to simulated predictions

- Global B-field magnitude and 3D metrology
- Magnet charging/settling times
- Voltage distribution within pancakes
- Cryogenic cooling and temperature distributions

The TFMC has established a solid foundation to design and operate large-scale, large-bore HTS magnets exceeding 20 tesla



The TFMC has begun a new generation of superconducting magnets at unprecedented performance and compact size

- Established manufacturing knowledge base to begin commercial-scale production
- Created enabling innovations (e.g. 50 kA HTS current leads, advanced EM modeling, etc.)
- Resulted in establishment of a new, highly capable magnet test facility at MIT

The TFMC and other MIT-CFS R&D will continue to retire critical risk for SPARC and large-scale NI HTS magnets

- Exploring passive quench handling and assessment of operation limits
- Robustness to mechanical and thermal cycling
- EM model validation and extrapolation to the SPARC TF design

TFMC-like performance (> 20 T peak field-on-coil) would enable SPARC to achieve a $Q_{physics}$ =11 (burning plasma regime)

- 40x smaller net-energy fusion tokamaks than traditional LTS magnets
- Increased future economic prospects (= P_{fusion} with much less mass/volume and cost)

