

# *Test and Analysis of Stacked-Tape-Wound Laboratory-Scale NI HTS TF Single Pancake Coil*

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MT27 (hybrid), Fukuoka, Japan

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and also by R&D program of “code No. CN2101” through the Korea institute of Fusion Energy(KFE) funded by the Government funds

# Background: Active Use of the HTS for Fusion

- Various research and developments are being conducted from HTS cables and conductors to stacked tape wound magnets



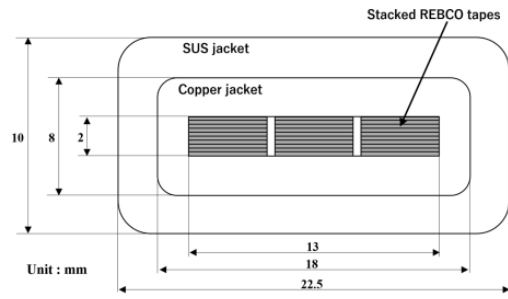
STARS  
conductor



Z. Melhem, et al., *IEEE Trans. Appl. Supercond.*, vol. 25, no. 3, June 2015.

A. Down, Oral Presentation at Applied Superconductivity Conference, Wk1L0r2B-05, 2020.

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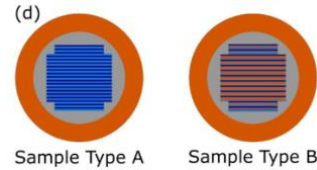
T. Obana and N. Yanagi, *Cryogenics* 115 (2021) 103278



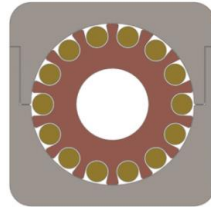
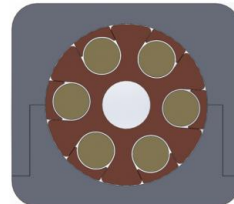
CroCo  
conductor



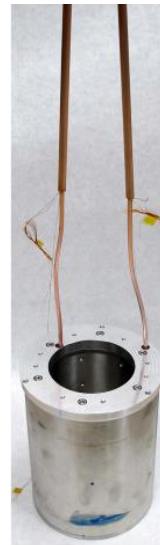
Advanced Conductor Technologies LLC  
[www.advancedconductor.com](http://www.advancedconductor.com)



M. J. Wolf, et al., *Fusion Eng. Des.* 172 (2021): 112739.

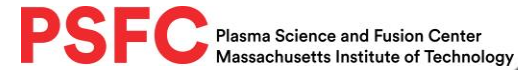


CORC<sup>®</sup> cable  
insert solenoid



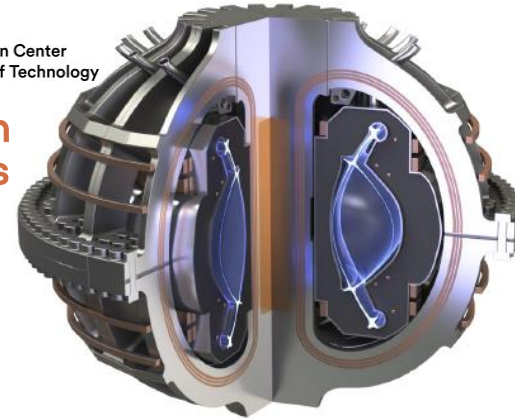
D. C Van Der Laan, et al., *Supercond. Sci. Technol.* 33 (2020) 05LT03 (10pp)

Lab-scale NI TF Single Pancake Coil, 11/17/2021  
MT27 (hybrid), Fukuoka, Japan, WED-OR3-201-07

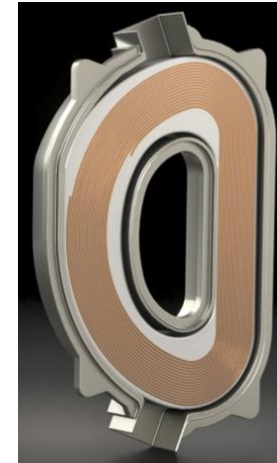


SPARC

Z. Hartwig, Oral presentation at Applied Superconductivity Conference, Wk1L0r2B-01, 2020; <https://cfs.energy/technology>



ARC



<https://cfs.energy/technology/#hts-magnets-enabling-technology>  
<https://www.cnbc.com/2021/09/08/fusion-gets-closer-with-successful-test-of-new-kind-of-magnet.html>

# Previous Works: No-insulation and Co-winding Methods in Solenoid Shape

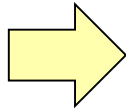
## Development of No-insulation (NI) HTS Coil

The first NI HTS coil

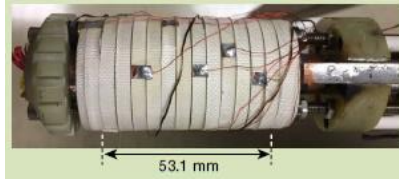


S. Hahn, et al., *IEEE Trans. Appl. Supercond.* 21.3 (2010): 1592-1595.

NHMFL 32 T



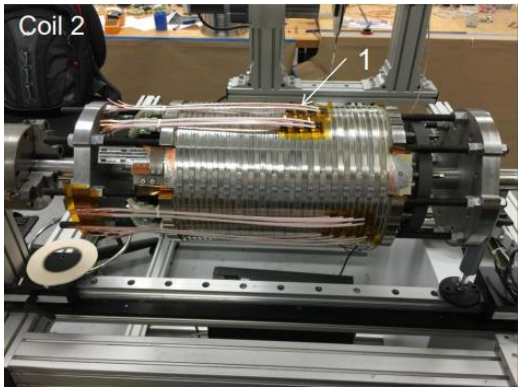
The highest magnetic field (45.5 T) achieved by NI HTS coil, LBC III



S. Hahn, et al., *Nature* 570, 7762 (2019): 496-499.

CAS 32 T

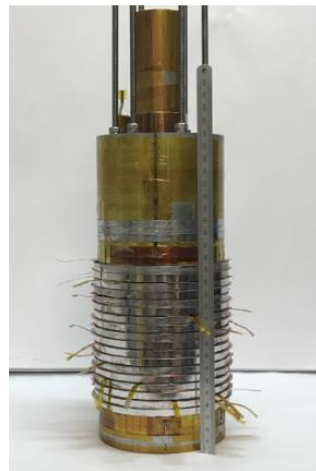
Grenoble 32 T



H. W. Weijers, et al., "The NHMFL 32 T superconducting magnet," *EUCAS 2017*.



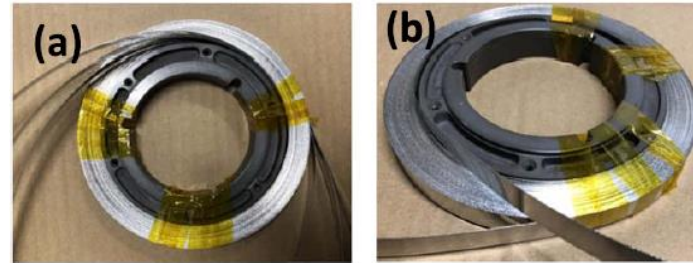
J. Liu, et al., *Supercond. Sci. Technol.* 33.3 (2020): 03LT01.



P. Fazilleau, et al., *Cryogenics* 106 (2020): 103053.

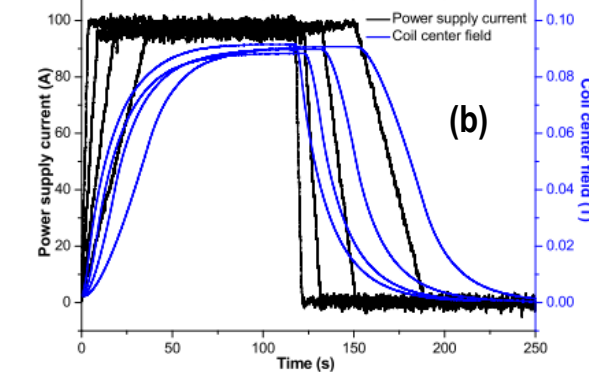
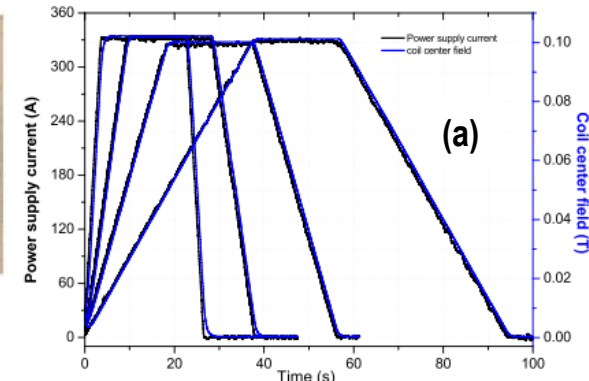
## Features of Co-winding Coil

- Reduced charging delay compared to NI HTS coil
- Reduced coil voltage and charging loss
- Increased engineering current density



3 HTS tapes co-wound NI coil    Single tape NI coil  
J. Geng and M. Zhang. *Supercond. Sci. Technol.* 32.8 (2019): 084002.

Co-winding method introduced by Tokamak Energy



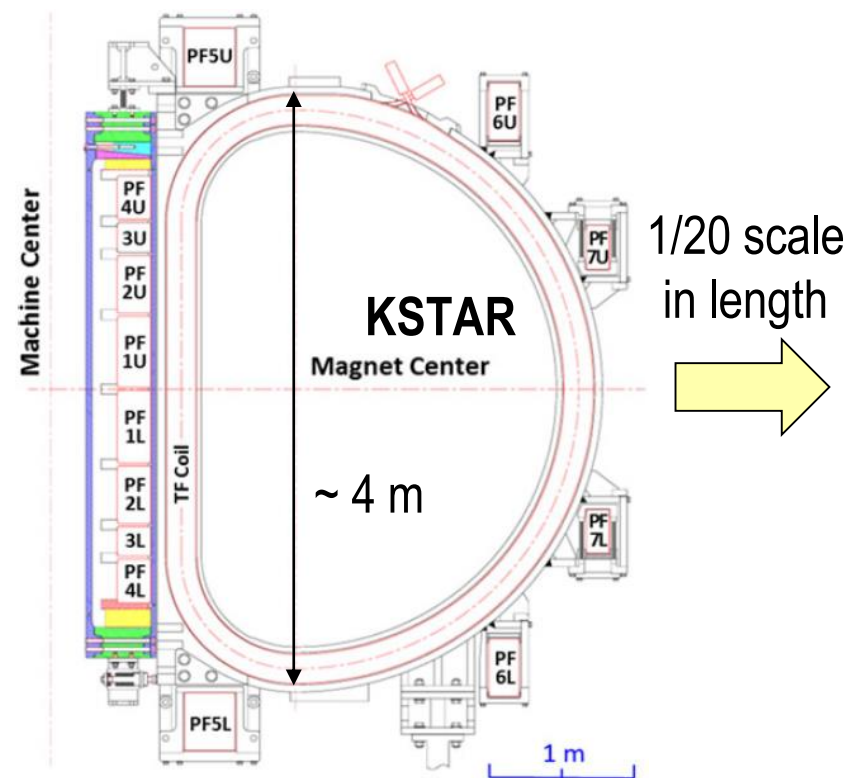
Tokamak Energy, <https://youtu.be/43TI39CYhNM?t=33>



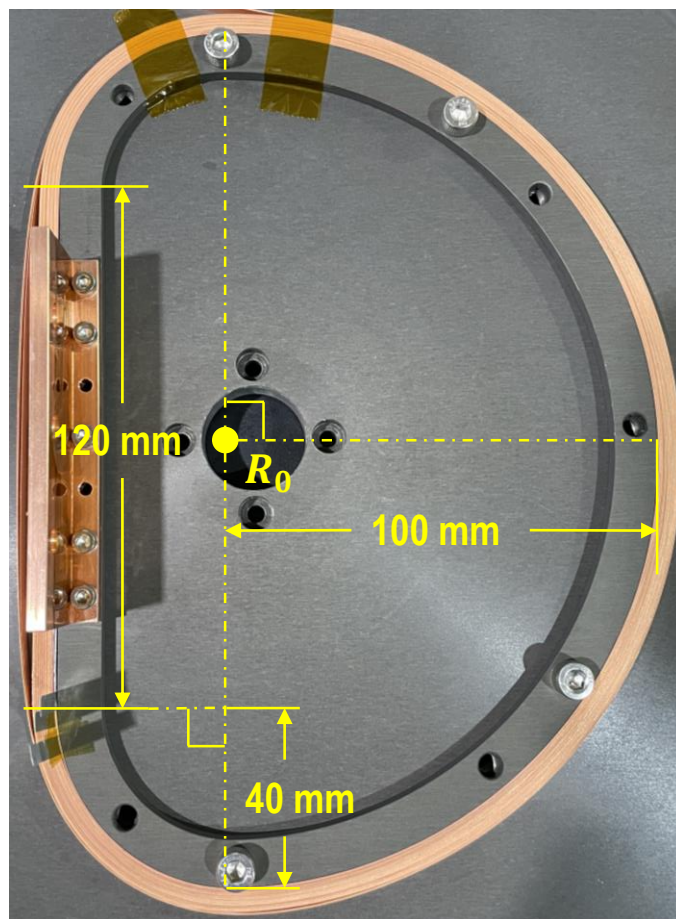
# Laboratory-scale NI HTS TF Single Pancake Coil

## :The First D-shaped NI HTS Coil in Korea for High-field Fusion

- Design and winding practice, initial investigation on the D-shaped coil characteristics
- The KSTAR was chosen as a reference in size and shape to make 1/20 in length



\*Ref: H. J. Ahn et al., *IEEE Trans. Appl. Supercond.*, Vol., 28, No. 3, 2018. (4204105)



Lab-scale NI TF Single Pancake Coil, 11/17/2021  
MT27 (hybrid), Fukuoka, Japan, WED-OR3-201-07

Parameters	Unit	Values
<b>Conductor</b>		
Manufacturer		SuNAM
Average width	[mm]	4.1
Average thickness	[mm]	0.14
Critical current at 77 K, self-field	[A]	> 150
<b>Coil</b>		
Length of straight section	[mm]	120
Radius of quarter circular section	[mm]	40
Radius of half circular section	[mm]	100
Bobbin width; height	[mm]	140; 200
Number of HTS tapes per turn, $N_{tape}$		1; 2; 3
Number of turns, $N_{turn}$		36; 18; 12
Conductor length	[m]	20.72
Inductance	[ $\mu$ H]	565.3; 141.3; 62.8

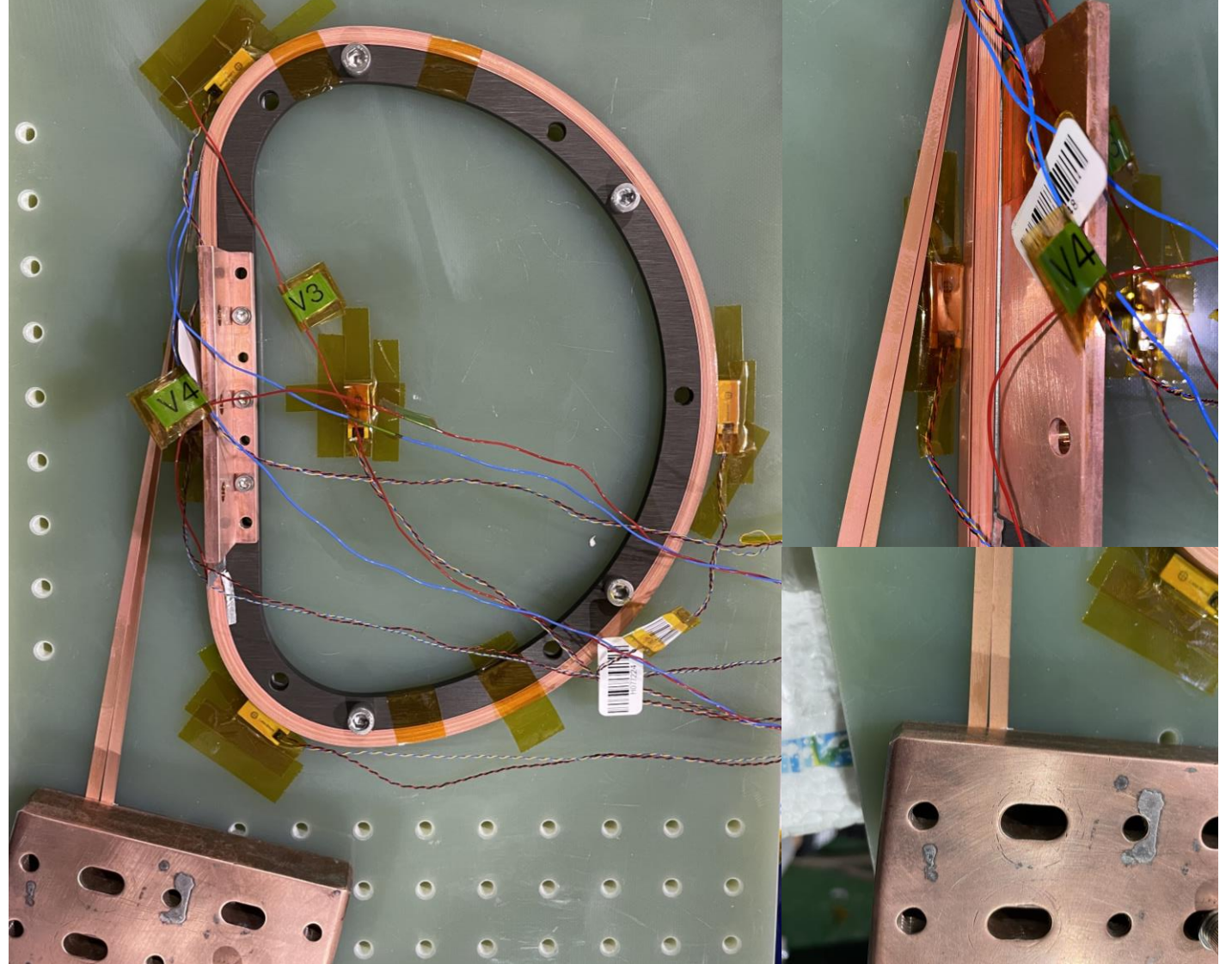


# Fabrication of the Co-wound NI HTS TF Module Coil

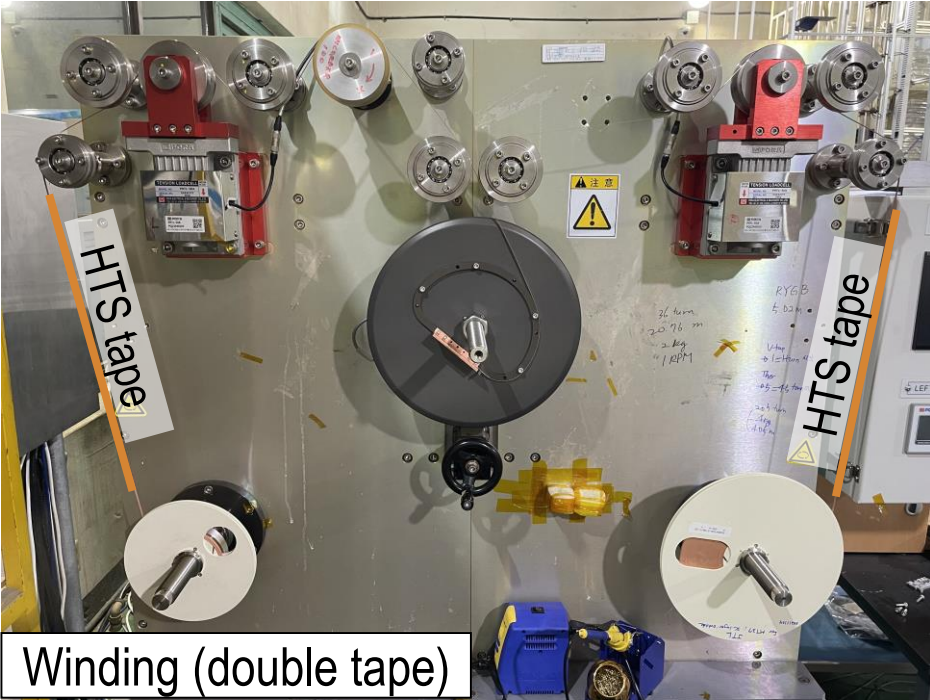
Input current lead and inner voltage tap



Instrumentation setup

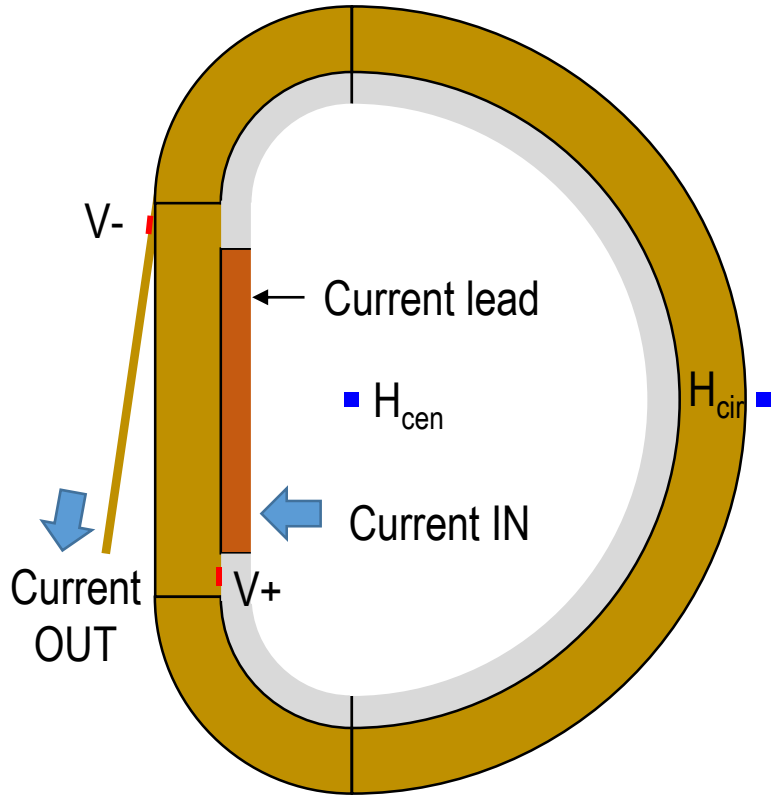


Winding (double tape)

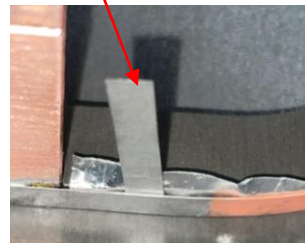
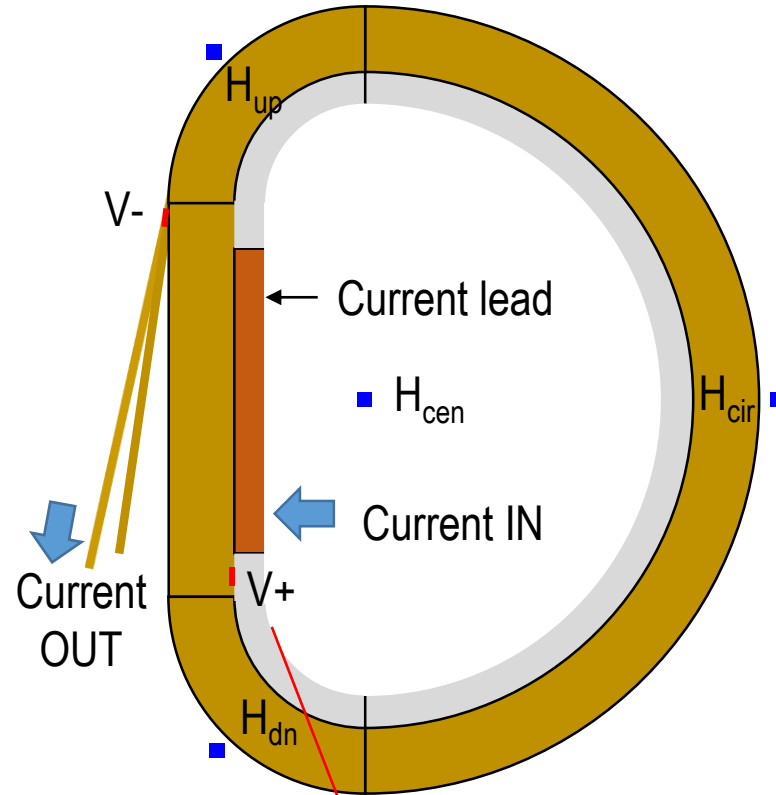


# Voltage Taps and Hall Sensors Configuration

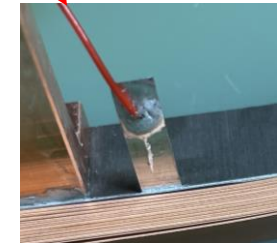
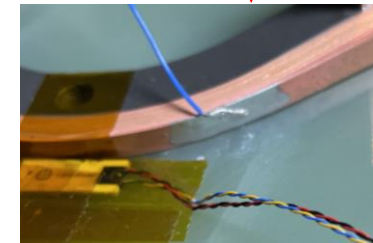
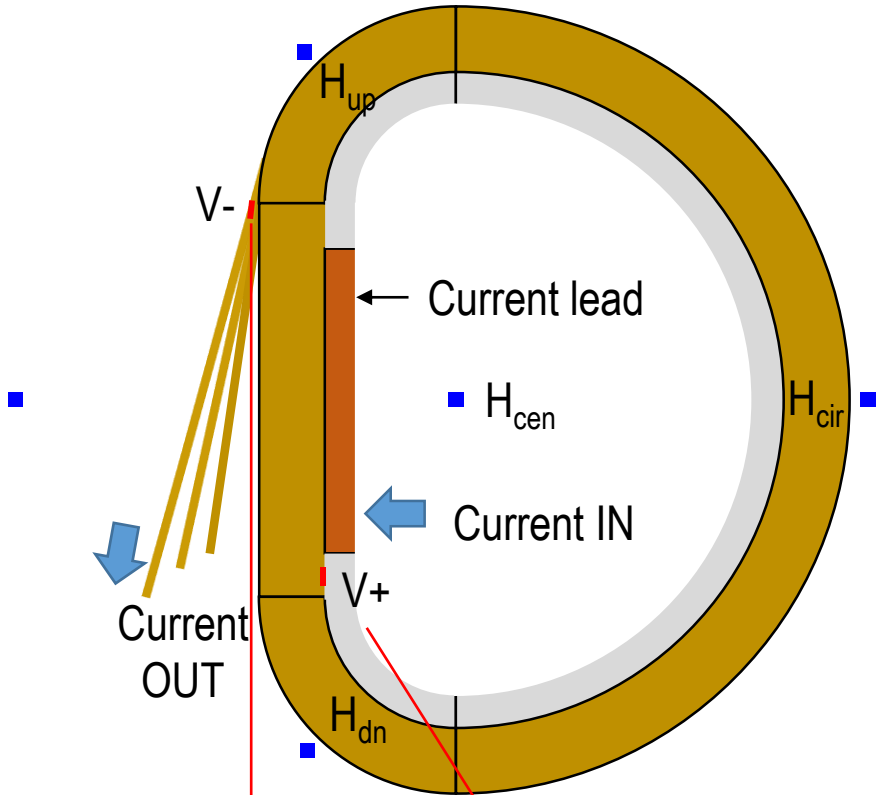
Single Tape Wound NI Coil (NI-1)



Double Tape Co-wound Coil (NI-2)



Triple Tape Co-wound Coil (NI-3)

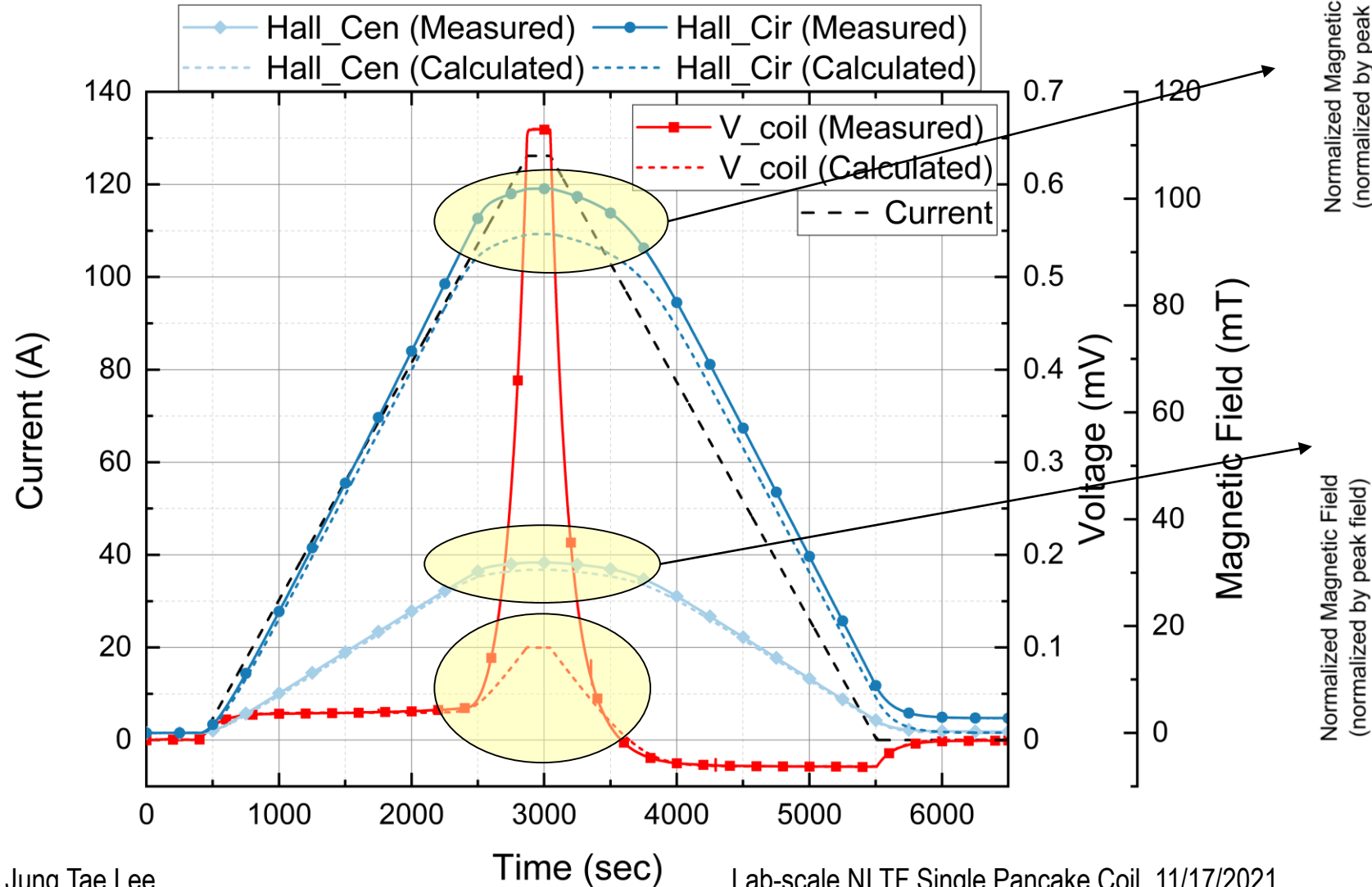


- Voltage taps
- Hall sensors

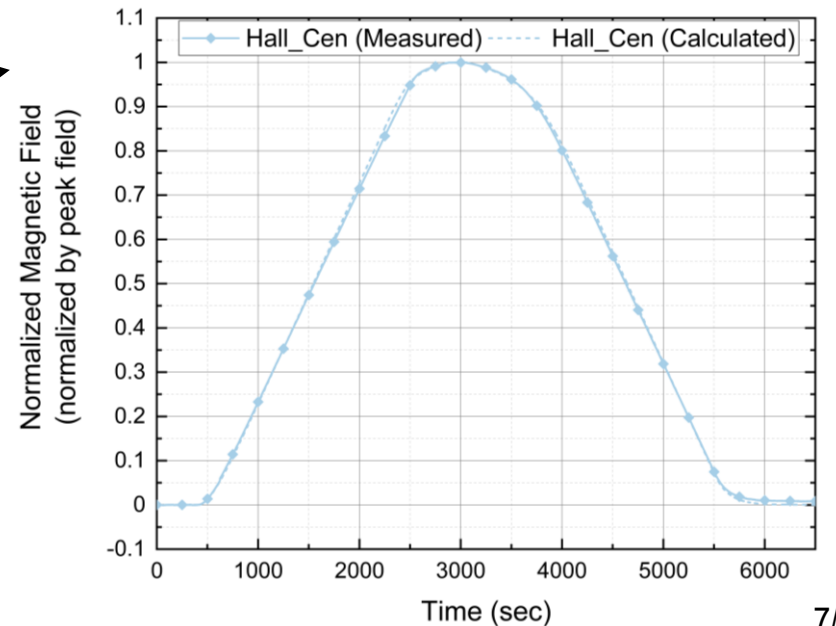
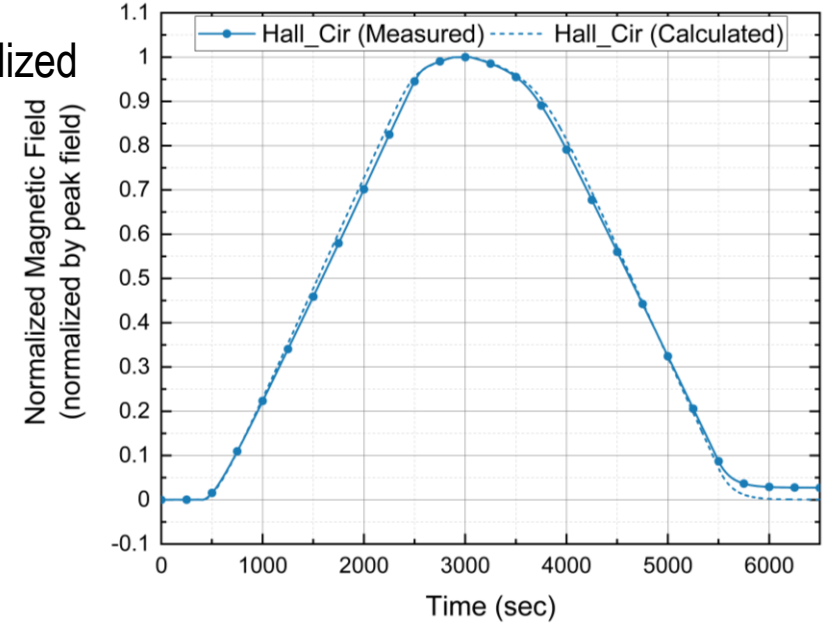


# Test Results: Single Tape NI HTS TF Pancake Coil

- Charging/discharging test in LN2 bath
- Simulation by lumped circuit model

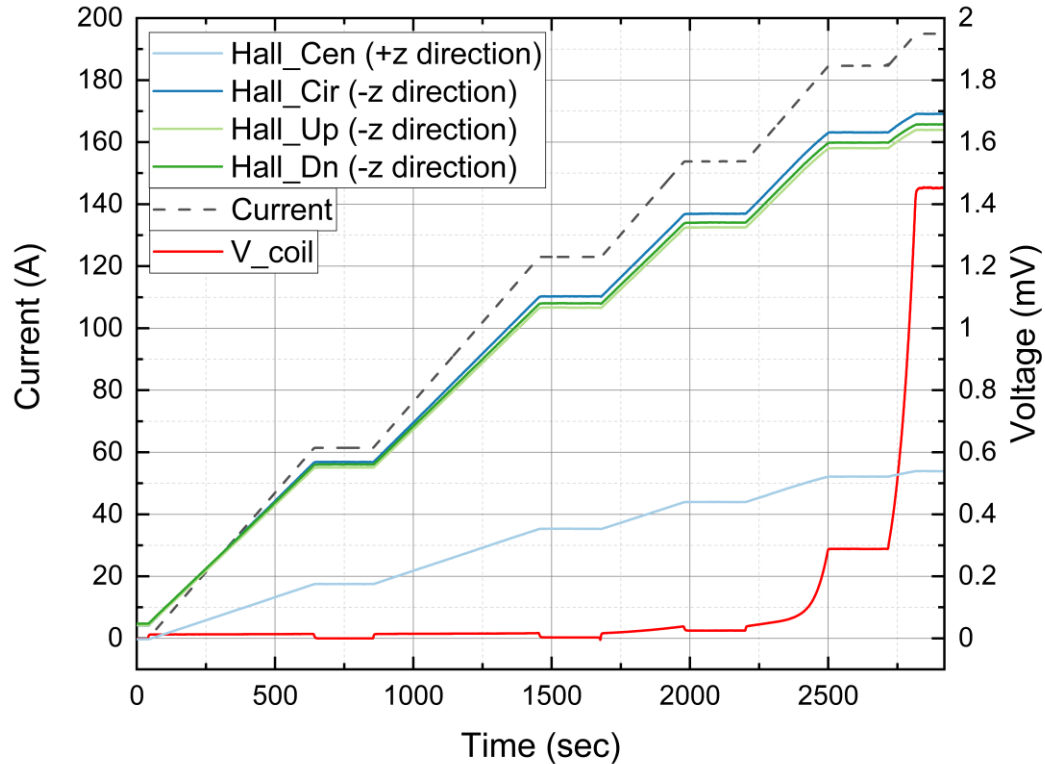


Magnetic field normalized by its peak value

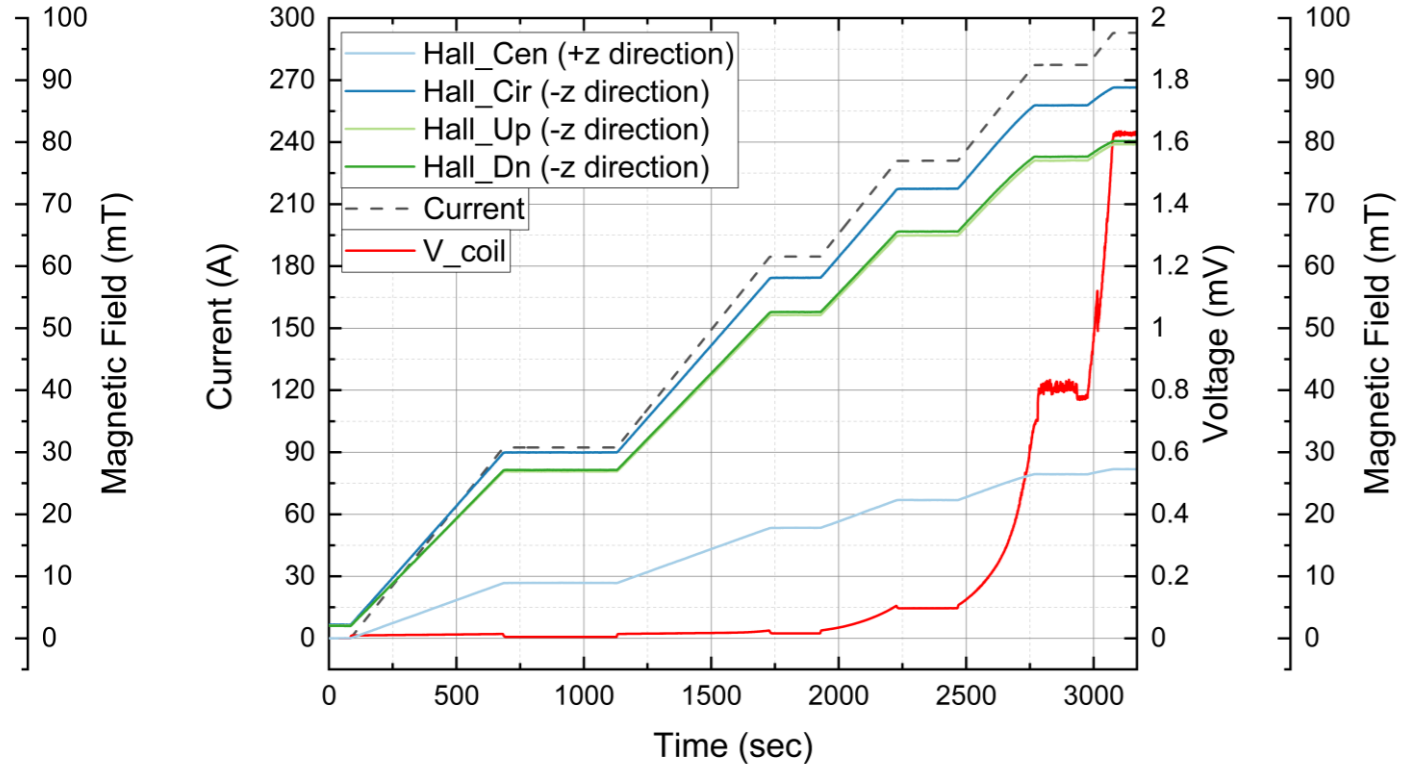


# Test Results: Co-wound NI HTS TF Pancake Coils

## Double Tape Co-wound Coil (NI-2)



## Triple Tape Co-wound Coil (NI-3)



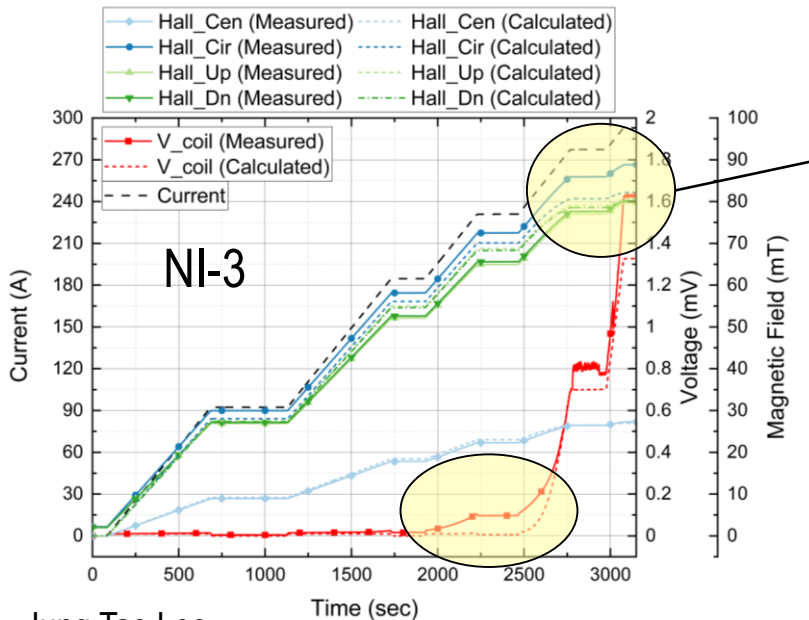
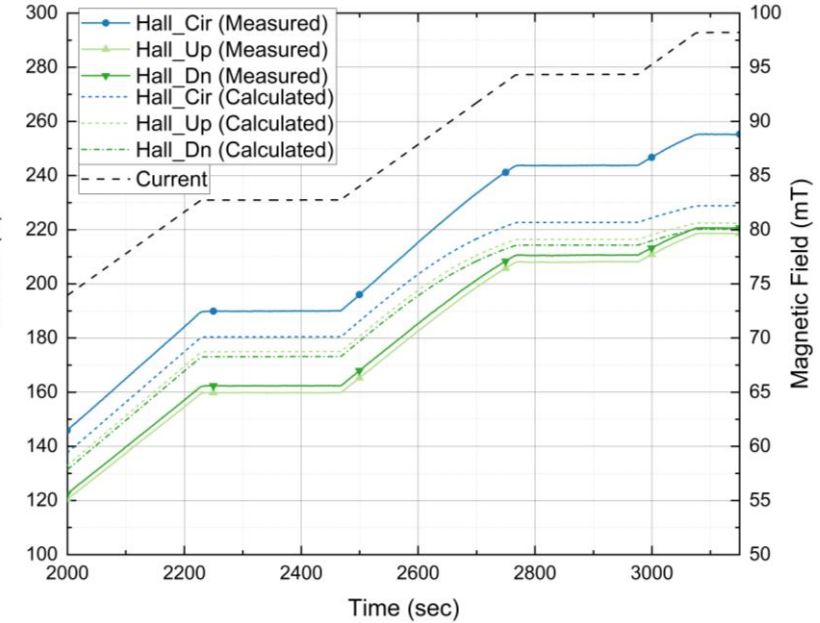
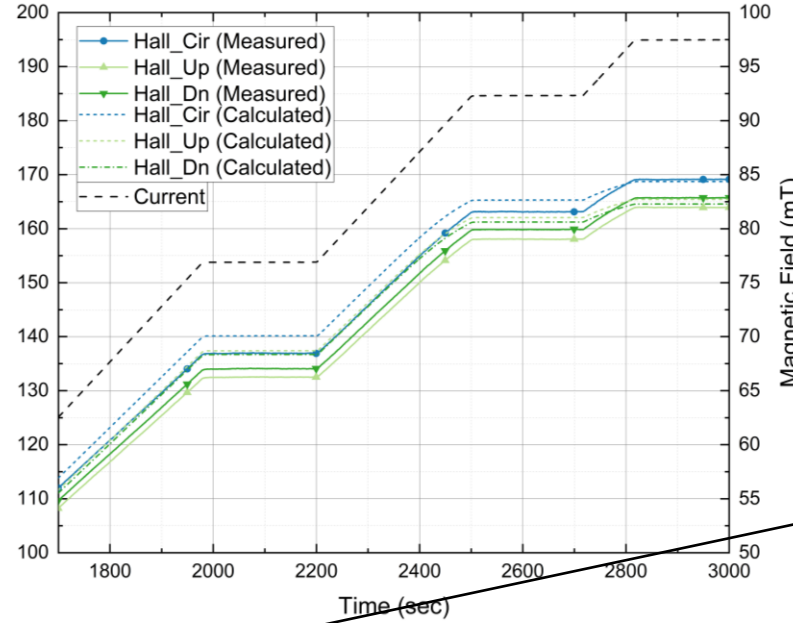
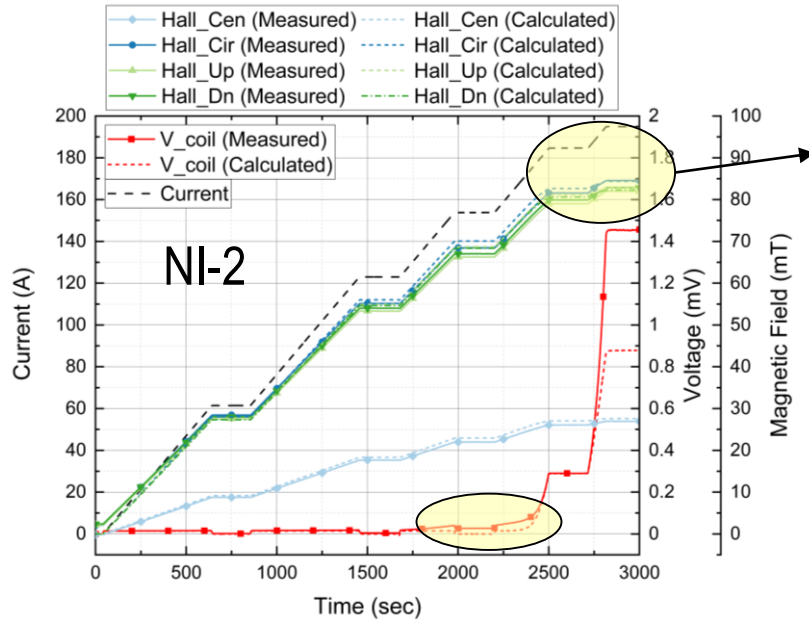
- Step-hold charging test in LN2 bath
- Ramping rate set to match the Ampere-turns for both coils
  - NI-2:  $0.1 \text{ A/s} \times 18 \text{ Turns} = 1.8 \text{ A-turns/s}$
  - NI-3:  $0.15 \text{ A/s} \times 12 \text{ Turns} = 1.8 \text{ A-turns/s}$

Fitted coil parameters	NI-2	NI-3
Critical current, $I_c$ [A]	193.9	280.3
Index number, $n$	27	12
Contact resistance, $R_c$ [ $\mu\Omega$ ]	59.4	41.2

←  $1 \mu\text{V/cm}$  criterion



# Test Results: Co-wound NI HTS TF Pancake Coils



Coil parameters	NI-2		NI-3	
	Fitting	Simulation	Fitting	Simulation
Critical current, $I_c$ [A]	193.9	178.1	280.3	248.2
Index number, $n$	27	54	12	34
Contact resistance, $R_c$ [ $\mu\Omega$ ]	59.4	90.0	41.2	60.0

Decrease in  $I_c$ , increase in  $n$  and  $R_c$

# Time Constant Comparison between the Test Coils

Assuming ideally same winding tension and contact surface conditions between each coil (i.e. same contact resistance),

$$\tau_{NI-1} = \frac{L_{NI-1}}{R_{cNI-1}},$$

$$\tau_{NI-2} = \frac{L_{NI-2}}{R_{cNI-2}} \approx \frac{1}{N_{turns}^2} \frac{L_{NI-1}}{R_{cNI-1}}$$



Time constant is inversely proportional to the square of the number of turns

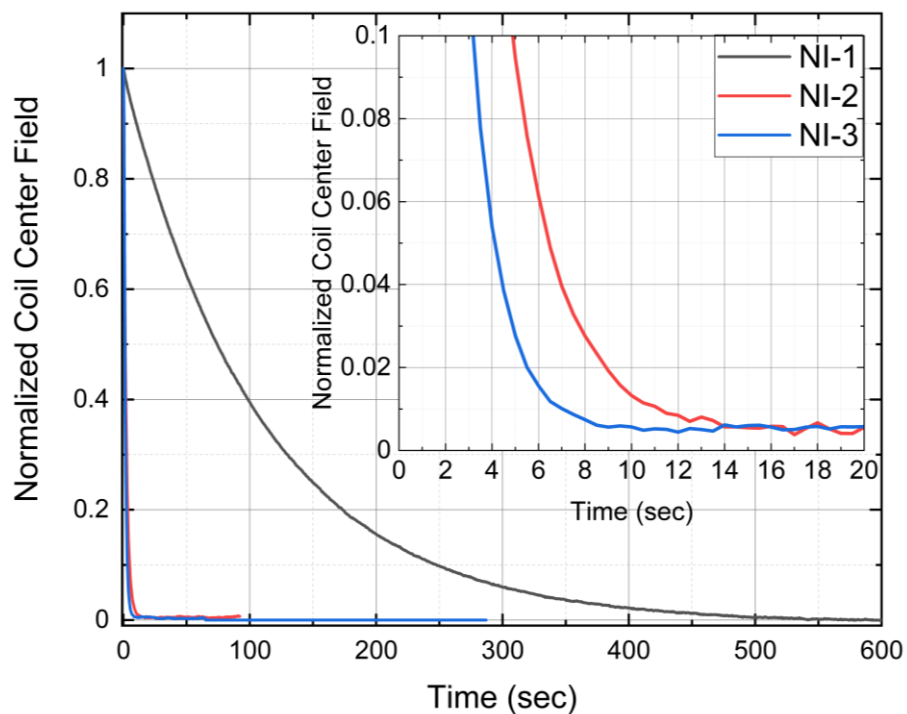
- NI-1: Single Tape Wound NI Coil
- NI-2: Double Tape Co-wound Coil
- NI-3: Triple Tape Co-wound Coil
- $N_{turns}$ : number of co-wound turns

Before test

After test



BUT, surface contact condition is never the same



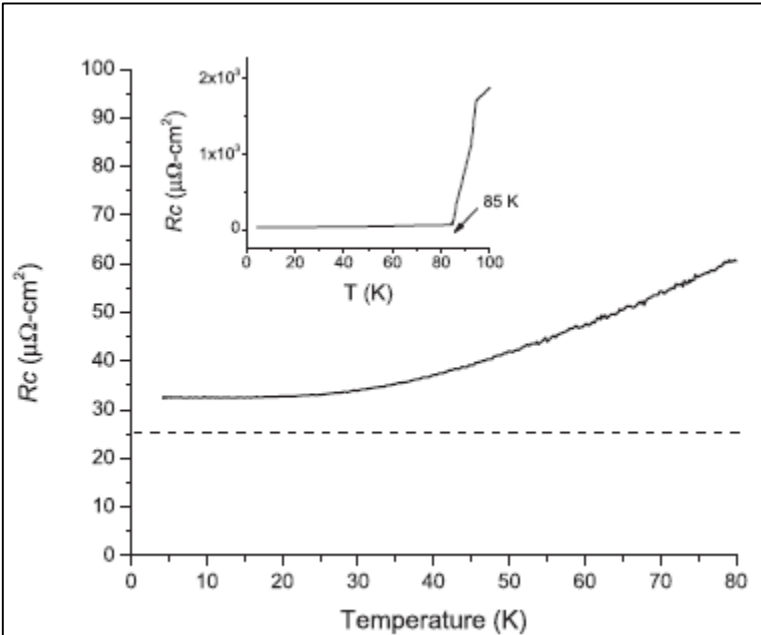
	NI-1	NI-2	NI-3
Inductance, $L$ [ $\mu\text{H}$ ]	565	141	62.8
Time constant, $\tau$ [s]	109	2.38	1.53
Contact resistance, $R_c$ [ $\mu\Omega$ ]	5.17	59.4	41.2

$1/46$

$1/71$

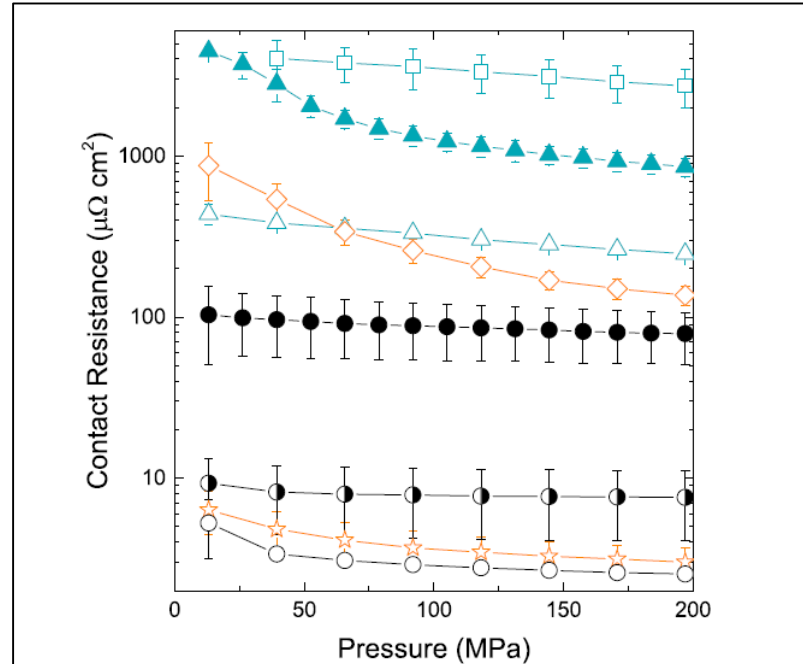
# Discussions on Contact Resistance

- Reports on contact resistance under various load and load cycles
  - implication for TF coil would be “to take extra care on the straight section of the coil” as well as other parts of the coil where contact resistance may differ



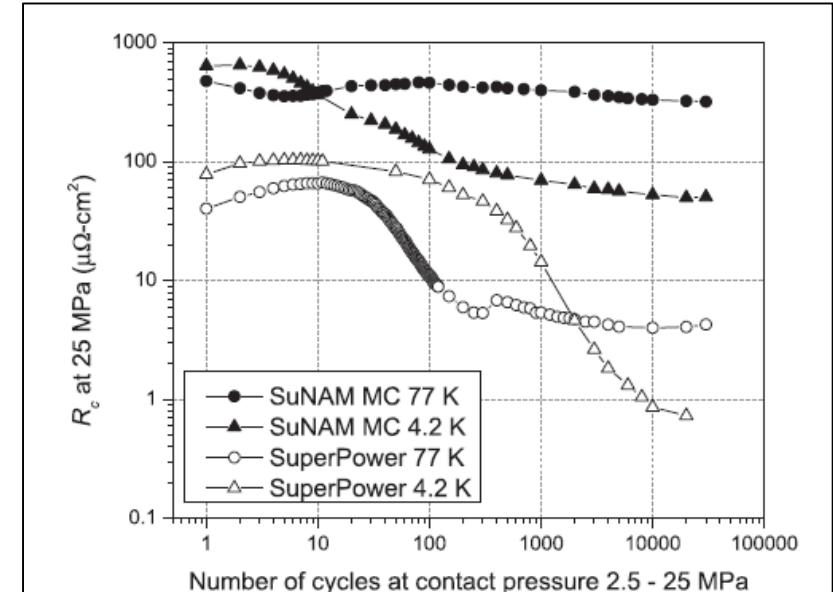
J. Lu, et al., *Supercond. Sci. Technol.* **30**:035020, 2017.

→  $R_c$  decreases dramatically to ~ 50 % of the initial value from 80 K to 20 K and becomes subtle afterwards



- Co-winding with SS (43  $\mu\text{m}$ ), CCs' oxide removed by etching
- ▲ CC (no oxide removal) + stainless-steel-sputtered (2  $\mu\text{m}$ ) CC
- △ CC (oxide removed by etching) + stainless-steel-sputtered (2  $\mu\text{m}$ ) CC
- ◇ Co-winding with CuZn37 (100  $\mu\text{m}$ ), CCs' oxide removed by etching
- CC + CC (no oxide removal)
- CC + CC (oxide partially removed by sanding)
- ★ CC (oxide removed by etching) + CuZn37-sputtered (3  $\mu\text{m}$ ) CC
- CC + CC (oxide removed by etching)

M. Bonura, et al., *IEEE Trans. Appl. Supercond.*, vol. 29, no. 5, August 2019



J. Lu, et al., *Supercond. Sci. Technol.* **31** (2018) 085006 (8pp)

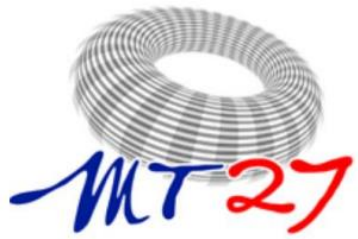
→  $R_c$  changes even under the same load when the coil experiences load cycles

→ Wide range of  $R_c$  with different surface conditions and different load levels



# Conclusion: Focus need to be taken on the relation between the unique “D” shape properties and coil performance in further research.

- Double and Triple tape co-wound coils were tested showing some noticeable points to discuss
  - Relatively gradual transition to the index region compared to single tape coil (sharp transition)  
→ small index number in coil level
  - Different magnitude of the magnetic field in the same location for double and triple tape co-wound coil  
→ possibly due to different current distribution between co-wound tapes? Or by the difference in the contact resistance due to asymmetric shape of the coil?
  - Largely reduced time constant from single tape coil for both co-wound coils → possibly due to the failure in tension control in the straight section leading to high contact resistance
- Two main takeaways
  - The straight section of the TF single pancake coil holds large variability which needs to be controlled to analyze the coil more systematically
  - Current distribution between co-wound tapes needs to be investigated relating the effects of the “D” shape contribution to difference in contact resistance in different sections of the coil



# Thank you for your attention

## Q&A

This work was supported by the National Research Foundation of Korea (NRF) grant funded by the Korea government (MSIT) (No. 2018R1A2B3009249) and also by R&D program of “code No. CN2101” through the Korea institute of Fusion Energy(KFE) funded by the Government funds